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RAILROAD ENGINEERING

By WILLIAM G. RAYMOND

Railroad Field Geometry (Without Tables)

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Railroad Field Manual for Civil Engineers

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Railroad Field Manual

for

Civil Engineers

BY

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FIRST THOUSAND

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PREFACE

This book is for field use rather than for office use, though it is adapted to a large percentage of office work. It is made on a new plan which is not expected to gain immediate favor but which it is hoped will eventually appeal to railroad engineers as sensible and worthy of adoption, because its use will save time and lessen the liability of error. The degree is divided decimally instead of sexagesimally.

When the author was a young man engaged on railroad location he knew one or two engineers who had one vernier of their transits graduated to read hundredths of degrees for greater convenience in setting out curves. They would have done all their work in decimals if tables had been available.

When the author was planning this book he gave much thought to the question of the division of the degree and the forms of the tables that would be most convenient and time saving for the field men who might use the book. He remembered that in practically every curve problem it is necessary at some stage of the solution to transpose from minutes and seconds to decimals of a degree or vice versa. membered that to lay out subchords would require much less mental effort if the transit were divided to read decimals of degrees rather than minutes. He wrote to a half dozen of the leading instrument makers to learn what would be the cost of changing the verniers on an old transit to read decimals of a degree and to know whether there would be any difference in price between two instruments ordered new, one to be divided in the usual way and the other divided to read decimals of a degree. All but one of the makers gave a price in the neighborhood of \$20 for changing the verniers on an old instrument, and no difference in cost for new instruments. The author then wrote to about fifty engineers, chief engineers of railroads, independent practicing engineers, and professors of railroad engineering in colleges and asked their opinions as to the desirability of a change in practice from sexagesimal to decimal division of the degree, and whether or not a table book based on the decimal division would help to bring about the change, if desirable. All but one of these engineers replied that the change is desirable. The one was a professor of railroad engineering. Of the others all but two thought it doubtful if the change could be brought about, owing to the conservatism of the craft. Two chief engineers of prominent eastern roads discussed the matter with their assistants and were so favorably impressed with the plan as to say that they would adopt it if they had the tables to make it possible. Those who thought it unlikely that the change could be brought about cited the difficulty with the introduction of the metric system as an argument. To this the author replies that the adoption of the metric system involves a change of unit. The adoption of the decimal division of the degree involves no change of unit and merely does for angle work what American engineers long since did for their linear work. The book still retains the 90° quadrant. To be sure, minutes and even seconds have become a sort of unit, but so were inches, chains, and links. These are practically done away with for surveyor's use and there would seem to be as good reason for doing away with minutes and seconds. Practically every computation involving trigonometric logarithms requires less work by the decimal system than it does by the sexagesimal system. Instruments will be graduated to read to hundredths of degrees directly or 0.6 of a minute.

Although the author believes that the "degree" of a curve should be the angle subtended by an arc of one hundred feet instead of a chord he has not adopted that definition, but has adhered to the definition approved by the American Railway Engineering Association.

Five-place tables have been adopted as representing as high a degree of precision as is warranted by the field work. Computations of tables and some few other calculations require more extended tables but these practically always arise in connection with office work where it is assumed that there are, or may be if necessary, six-place, seven-place, and even ten-place tables. The author has used seven-place tables, and occasionally ten-place tables, for the computation of the tables of this book. Persons do not always realize it, but considerable additional time is required to use six-place tables over that required for five-place tables. In his "Plane Surveying for Classroom and Field," the author discusses this question at some length and works examples to show the relative precision of four-place and five-place tables. The conclusions of the discussion are as follows:

"I. It is useless to make linear measurements with a precision of more than I in 3500 if angles are to be read to the nearest minute only.

"2. It is useless to use tables of more than four places for angles read to the nearest minute only.

"It is difficult for many persons to bring themselves to use the smaller tables because they seem to see a greater precision in the use of tables giving results that are true to five and six significant figures, and fail to realize that the field work on which the computations depend does not warrant any such degree of precision, which is therefore only a seeming precision that is misleading and does not exist in fact. It is true that linear measurements can in general be made with greater precision than the angle work gives and, hence, it is the angle work that fixes the precision and the tables to be used. The following rules may be formulated:

- " For angles read to the nearest minute use four-place tables.
- "For angles read to less than 0° 00' 30" use five-place tables.
- "For work in general requiring certainty in the third significant figure use four-place tables, in the fourth significant figure five-place tables, and in the fifth significant figure six-place tables.
- "But it must be remembered that no ordinary surveying work is precisely enough done to warrant results certain to more than four significant figures, and that five-place tables are as extensive as are warranted by any land, topographic, railroad, or other surveys except the most refined city, bridge, and geodetic surveys.

"Computation labor is increased about 50 per cent by using five-place tables instead of four-place tables, and about one-third by using sixplace tables instead of five-place tables."

Before using the logarithmic tables even persons somewhat familiar with the use of logarithms should read the explanatory text preceding the tables.

The text concerning spirals and the spiral tables are based on the American Railway Engineering Association's ten-chord spiral. The author is indebted to Mr. Jenks B. Jenkins, Valuation Engineer for the Baltimore and Ohio Railroad and Chairman of the Track Committee of the A.R.E.A., and who devised the ten-chord spiral, for assistance with this part of the work.

The author has endeavored to include beside bare tables — many of which have been computed for this book and are not found in other books — just so much of explanation of common field problems as would seem necessary to refresh the memory of young engineers who have not had these drilled into them by long experience.

A few tables have been taken from other books. Acknowledgment is due Mr. Shelby S. Roberts for courteous permission to use tables from his "Track Formulæ and Tables" and to the American Book Company for permission to use plates from the author's "Plane Surveying for Classroom and Field" for Tables I, XXIV, and LXXXIII, and to use the matter of Tables LXX, LXXI, and LXXVII.

Great care has been taken with the computations and the proofreading but it is incredible that so many new computations should have been made and the results printed without error. The author will esteem it a favor if persons will report any errors that may be discovered to him or to the publishers.

This book may be used about as conveniently as other books based on the sexagesimal division of the degree by those who do not care to have their instruments changed or to adopt the decimal division for their final records, and it has some features not found in existing field books that may commend it to field men. Therefore, it is put forth under the hope that it may find immediate approval in a few places; that it may be tried in some other places; and that familiarity and experience with it will convince users that the author is not a mere faddist but has contributed something of real use to the fraternity.

WILLIAM G. RAYMOND

STATE UNIVERSITY OF IOWA, IOWA CITY, IOWA, 1915.

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RAILROAD FIELD MANUAL

CHAPTER I

SIMPLE, COMPOUND, AND VERTICAL CURVES

SIMPLE CURVES

Fundamental notations and equations. — The curve running from A to B in Fig. 1,

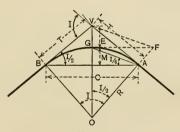


FIG. I.

A = T. C. (tangent-curve).

B = C. T. (curve-tangent).

V = P.I. (point of intersection of tangents).

I = central angle or deflection angle of tangents.

 $T = \text{tangent distance} = R \tan \frac{1}{2} I$.

C = long chord = $2 R \sin \frac{1}{2} I$.

 $M = \text{middle ordinate} = R \text{ vers } \frac{1}{2}I.$

 $E = \text{external distance} = R \operatorname{exsec} \frac{1}{2} I$.

 $E = T \tan \frac{1}{4} I.$

 $C = 2 M \cot \frac{1}{4} I.$

 $C = 2 T \cos \frac{1}{2} I.$

 $GA = \frac{C}{2} \sec \frac{1}{4} I.$

Definition. — The "degree" of a curve in American practice is the angle subtended at the center of a circular arc by a chord of 100 feet. In Latin American states where the metric system is used the "degree"

is the angle subtended by a chord of 20 meters. If R be the radius and D the degree of a curve, then, in American practice,

$$R = \frac{50}{\sin\frac{1}{2}D}.$$

Fig. 2. Table I gives R and its logarithm for various degree curves.

Tangent offset t = R vers $I = \frac{C^2}{2R}$. The tangent offset for one station is tabulated in Table I. For a subchord c the tangent offset is

$$t_c = t_{100} \frac{c^2}{10,000}.$$

Approximate Fundamental Relations. — Approximately, radii are inversely as the degrees or

 $\frac{R}{R'} = \frac{D'}{D}$ (approx.).

Radius of a 1° curve is 5729.65 = 5730 (approx.).

$$R_D = \frac{5730}{D}$$
 (approx.).

Tangent distance for a D° curve of central angle I is

$$T_D = \frac{T_1 \circ}{D}$$
 (approx.).

Table II gives tangent distances for a 1° curve and various values of I, and Table III gives corrections to $T_D = \frac{T_{10}}{D}$ for more precise re-

sults. Values of C, M, and E, for D° curves are also found approximately by dividing the values for a 1° curve for a given I by D. Table IV gives values of E for a 1° curve.

A curve departs from a tangent approximately thus: $O = \frac{7}{8} n^2 D$, n being the number of stations from the tangent point and D the degree of curve. Two curves of degrees D

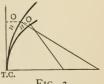


Fig. 3.

and D_1 depart from each other by the same approximate law, substituting the difference of degrees $D - D_1$ or $D_1 - D$ of the D of the foregoing formula.

The deflection angle Δ , for a chord of 100 feet is $\frac{1}{2}D$; for a subchord, c, it is given by

$$\sin\delta = \frac{c}{2R},$$

or, with sufficient exactness for all curves under about 8°,

$$\delta = \frac{c}{100} \times \frac{D}{2} = 0.5 \, cD$$
, in hundredths of degrees,
 $\delta = 0.3 \, cD$, in minutes.

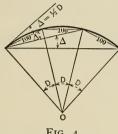






FIG. 5.

The ordinate from a chord at any point given by its distance from the center is

$$K = \sqrt{(R+a)(R-a)} - \sqrt{\left(R + \frac{c}{2}\right)\left(R - \frac{c}{2}\right)}$$

or, approximately,

or

$$K = M\left(1 - 4\frac{a^2}{c^2}\right).$$

Whence, for

$$a = \frac{1}{8}c, K = \frac{15}{16}M;$$

$$a = \frac{1}{4}c, K = \frac{3}{4}M;$$
 (approx.).
$$a = \frac{3}{8}c, K = \frac{7}{16}M.$$

If the point is given by the distance from one extremity,

$$K = \frac{Q \times S}{2 R} \text{ (approx.)}$$
$$= \frac{872 Q \times S \times D}{10,000,000} \text{ (approx.)}.$$

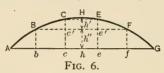
Approximately

$$M=\frac{C^2}{8R}, \qquad m=\frac{M}{4}.$$

Location by Offsets from Long Chord. -

$$AG = 2R\sin\frac{n}{2}D$$
, $n = \text{number stations } A \text{ to } G$, $BF = 2R\sin\frac{n-2}{2}D$, $Ab = fG = \frac{AG - BF}{2}$; $CE = \text{100 or } 2R\sin\frac{n-4}{2}D$, $bc = ef = Bc' = e'F = \frac{BF - CE}{2}$, etc.

 $Bb = Ff = Hh - Hh'' = R \text{ (vers } \frac{1}{2} nD - \text{vers } \frac{1}{2} (n-2) D), \text{ etc.},$



or

$$Ab = fG = 100 \cos \frac{n-1}{2} D.$$

$$Bc' = e'F = 100 \cos \frac{n-3}{2} D, \text{ etc.}$$

$$Bb = Ff = 100 \sin \frac{n-1}{2} D.$$

$$Cc' = Ee' = 100 \sin \frac{n-3}{2} D.$$
Use natural functions and move decimal.

In the particular figure $Hh' = 50 \tan \frac{1}{4}D$ because n is odd.

If the number of chords is not more than 8 or the degree more than 20 and of an even number of tenths, the long chords and middle ordinates may be taken from Tables V and VI, thus:

AG = long chord of n stations.

$$Ab = fG = \frac{\text{long chord of } n \text{ stations} - \text{long chord of } (n-2) \text{ stations}}{2}$$
, etc.

Bb = Ff =middle ordinate for n stations middle ordinate for (n-2) stations, etc.

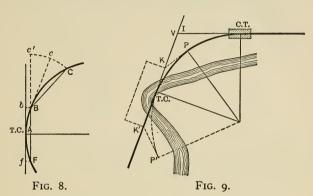
Location from Chord Produced. -

Bb = R vers D, or 100 sin $\frac{1}{2}$ D for natural functions.

Bb = tangent offset of Table I.A V or XA gives line of tangent.

Stretch the tape from A to B so that Bbshall measure as above. Produce AB to c',

one tape length, and swing about B until c'C = 2Bb. Produce BC to e' and swing about C until e'E = 2Bb, etc. If the curve begins with a subchord, l, swing l feet above A to B (Fig. 8) until $Bb = l \sin \frac{l}{100} \frac{D}{2}$. Swing 100 -l about A to F until $Ff = (100 - l) \sin \frac{100 - l}{100} \frac{D}{2}$. Produce FB to c', 100 feet, and swing about B until $c'C = 2 \times 100$ sin $\frac{1}{2}$ D, or twice the tangent offset of Table I. Produce BC, etc., as



before. For ending use the same method reversed. Supposing the curve to be running from C to B to A, locate F by producing CB, measure over Ff and Bb, and establish A between f and b at b feet from B.

Problems. — Suggestions for passing obstacles. If TC only is inaccessible:

- (a) Run to V to CT and run curve backwards.
- (b) Assume a point on the curve beyond the obstacle; compute the

tangent distance for the point, as TC - K; run to K; deflect angle at K and run to P and run the curve backward and forward. If CT is inaccessible the same methods with obvious modifications may be used.

To pass an obstacle on a curve one of the methods suggested by the figure may be used. The line AbC is run as ABC would be run only with the center on the opposite side.

To change TC or CT. First method: Assume or know the necessary change in

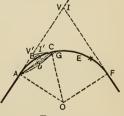


Fig. 10.

tangent distance and compute a new degree of curve. Second method: Assume a new D a round number, probably such as to accomplish the

desired result; change in CT or TC = change in tangent distances, or $m = T_2 - T_1 = (R_2 - R_1) \tan \frac{1}{2} I$.

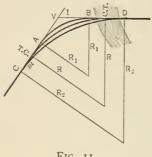


Fig. 11.

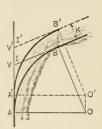
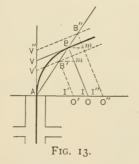


FIG. 12.

A curve ends in VB or V'B'; required to end in V'B' or VB. Degree does not change. It is necessary to find change in A.

$$AA' = VV' = BB' = OO' = \frac{K}{\sin I}.$$



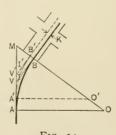


FIG. 14.

A curve ends in VB; required to end in V'B' or V"B" without changing A. Degree changes.

$$R' = R \mp \frac{K}{\text{vers } I}$$
, that is, change in $R = \frac{K}{\text{vers } I}$.

A curve ends in VB; required to end in V'B'. A and D change. $R' = R \pm \frac{K}{\text{exsec } I}$, according as B' is inward or outward from B. AA' = (R - R') tan I, or K cot $\frac{1}{2}I$, A being moved ahead or back according as R' is less or greater than R.

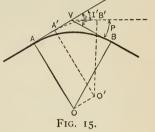
A curve ends in VB; required to end in VB'. Without changing degree AA' = R (tan $\frac{1}{2}I - \tan \frac{1}{2}I'$),

and A is moved forward or back according as I' is less or greater than I. Changing degree and keeping A fixed,

$$T$$
 is unchanged. $\therefore R' = \frac{T}{\tan \frac{1}{2} I'}$ or $T \cot \frac{1}{2} I'$.

A curve ends in VB; required to end in V'B. Fig. 16. D and A change.

$$R' = R \frac{\text{vers } I}{\text{vers } I'}$$



 $AA = (R \sin I - R' \sin I')$ and A is moved forward or back according as I' is greater or less than I.

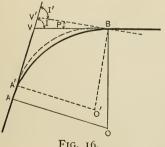
A curve ends in VB; required to end in V'B'. Fig. 17.

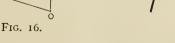
1. Assume new $R' \leq R$ according as B' is inside or outside VB. Then

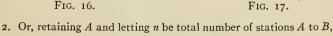
$$\cos \alpha = I - \frac{K}{R - R'}$$
 or $I - \frac{K}{R' - R}$,

 $n \text{ stations} = \frac{\alpha}{D}$.

Begin at *n* stations from *B* and run in curve of *D'* for *n'* stations = $\frac{\alpha}{D'}$.







$$D' = D \pm \frac{K}{\frac{7}{2}n^2}$$
, approx.

D' will be greater or less than D according as V'B' lies inside or outside of VB. Take D' nearest round number that will be sufficiently exact and run the curve D' for n' stations $=\frac{I}{D'}$.

3. Or, assuming a new degree less or greater than the original according as the tangent is to be thrown out or in, find n of Method 1 by

$$n = \sqrt{\frac{8K}{7(D - D')}}, \text{ approx.}$$

(D-D') is to be taken as the difference of degrees, subtracting the smaller from the larger. $\alpha=nD,\ n'=\frac{\alpha}{D'}$ to make the tangents parallel. Run curve of degree D' from C.C.

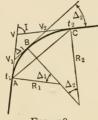


Fig. 18.

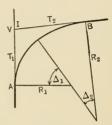


Fig. 19.

COMPOUND CURVES

Given R_1 , R_2 , Δ_1 , and Δ_2 ; required T_1 and T_2 . Fig. 18.

$$V_1 V_2 = t_1 + t_2.$$

Solve triangle VV_1V_2 for V_1V and V_2V .

$$T_1 = VV_1 + t_1$$
: $T_2 = VV_2 + t_2$.

Given I, T_1 , T_2 , and R_1 ; required R_2 , Δ_1 , and Δ_2 . Fig. 19.

$$\cot \frac{1}{2} \Delta_2 = \frac{T_2 + T_1 \cos I - R_1 \sin I}{T_1 \sin I - R_1 \text{ vers } I},$$

$$\Delta_1 = I - \Delta_2,$$

$$R_2 = R_1 + \frac{T_1 \sin I - R_2 \text{ vers } I}{\text{vers } \Delta_2}.$$
(a)

Given I, T_1 , T_2 , and R_2 ; required R_1 , Δ_1 , and Δ_2 .

$$\cot \frac{1}{2} \Delta_{1} = \frac{R_{2} \sin I - T_{1} - T_{2} \cos I}{R_{2} \text{ vers } I - T_{2} \sin I},$$

$$\Delta_{2} = I - \Delta_{1},$$

$$R_{1} = R_{2} - \frac{R_{2} \text{ vers } I - T_{2} \sin I}{\text{ vers } \Delta_{1}}.$$
(b)

Given I, T_1 , R_1 , and Δ_1 ; required Δ_2 , R_2 , and T_2 .

$$\Delta_2 = I - \Delta_1$$

 R_2 is given by equation (a) above.

$$T_2 = (R_2 - R_1) \sin \Delta_2 + R_1 \sin I - T_1 \cos I$$
.

Given I_1 , T_2 , R_2 , and Δ_2 ; required Δ_1 , R_1 , and T_1 .

$$\Delta_1 = I - \Delta_2$$

R is given by equation (b) above.

$$T_1 = R_2 \sin I - T_2 \cos I - (R_2 - R_1) \sin \Delta_1$$

To end a compound curve in a new tangent, parallel to that first located.

(a) Move the curve parallel to itself along

the first tangent, a distance $AA' = \frac{K}{\sin I}$

(b) Retaining the first branch, changing only the degree of the second,

$$R_2' = R_2 \pm \frac{K}{\text{vers } \Delta_2},$$

 $R_1' = R_1 \pm \frac{K}{\text{vers } \Delta_1},$

according as the curve ends with the larger or shorter radius.

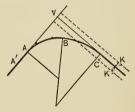


FIG. 20.

(c) Retaining both degrees, changing the Δ 's and the station of CC. If the new tangent is *inside* and the longer radius ends the curve the CC is advanced; if the new tangent is outside the CC is moved back; if the shorter radius ends the curve the movement of the CC is reversed. The new values for the *final* Δs are had from

vers
$$\Delta_2' = \text{vers } \Delta_2 \pm \frac{K}{R_2 - R_1}$$
,
vers $\Delta_1' = \text{vers } \Delta_1 \pm \frac{K}{R_2 - R_1}$.

To change the direction of the final tangent by a given amount. Solve the triangle VV'C for the new final tangent and the change in the initial tangent. The new I being known, retain the first radius and

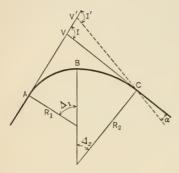


FIG. 21.

solve for the new final radius and the two central angles, by preceding equations.

VERTICAL CURVES

The rate of change of grade in passing sags and summits in the grade line, as recommended by the American Railway Engineering Association, is: For first-class railways change not more than 0.1 foot per station on summits and not more than 0.05 foot per station in sags; for second-class roads not more than double these rates.

How to determine the elevation of the several stations on the vertical curve will be shown by two examples. The first step is to determine the length of the curve; it will be convenient to adopt a rate of change that will give an even number of stations for the length.

Example 1. Two grades, -0.8 and +0.6, meet at station 462 where the elevation is 723. Required a vertical curve to connect with a change of 0.1 per station. The total change in rate is 0.8 + 0.6 = 1.4, giving 14 stations = 1.4 ÷ 0.1, of curve, or 7 stations each side of the vertex. The beginning of the curve is therefore at sta. 462 - 7 = 455 and the end is at 455 + 14 = 469. The elevation of 455 is $723.0 + 7 \times 0.8 = 728.6$; the elevation of sta. 469 is $723.0 + 7 \times 0.6 = 727.2$.

The rate of change for the first station is taken at half the station rate of change or 0.05. Therefore the elevation of

sta.
$$456 = 728.6 - (0.8 - 0.05) = 728.6 - 0.75 = 727.85$$

 $457 = \text{elev.} \ 456 - (0.8 - 0.15) = 727.85 - 0.65 = 727.20$
 $458 = \text{elev.} \ 457 - (0.8 - 0.25) = 727.20 - 0.55 = 726.65$
 $459 = \text{elev.} \ 458 - (0.8 - 0.35) = 726.65 - 0.45 = 726.20$
 $460 = \text{elev.} \ 459 - (0.8 - 0.45) = 726.20 - 0.35 = 725.85$
 $461 = \text{elev.} \ 460 - (0.8 - 0.55) = 725.85 - 0.25 = 725.60$
 $462 = \text{elev.} \ 461 - (0.8 - 0.65) = 725.60 - 0.15 = 725.45$
 $463 = \text{elev.} \ 462 - (0.8 - 0.75) = 725.45 - 0.05 = 725.40$
 $464 = \text{elev.} \ 463 - (0.8 - 0.85) = 725.40 + 0.05 = 725.45$

```
465 = \text{elev.} \ 464 - (0.8 - 0.95) = 725.45 + 0.15 = 725.60
466 = \text{elev.} \ 465 - (0.8 - 1.05) = 725.60 + 0.25 = 725.85
467 = \text{elev.} \ 466 - (0.8 - 1.15) = 725.85 + 0.35 = 726.20
468 = \text{elev.} \ 467 - (0.8 - 1.25) = 726.20 + 0.45 = 726.65
469 = \text{elev.} \ 468 - (0.8 - 1.35) = 726.65 + 0.55 = 727.20
```

It will be noticed that the final elevation agrees with that computed above; this proves the work. It will also be noticed that after the bottom of the sag is passed the elevations repeat themselves in reverse order. The bottom of the sag is not always the same station as the apex. This depends on the relative rates of the grades.

Example 2. — Two grades, -0.2 and -1.0, meet at station 867.0, where the elevation is 466.0. To connect the grades with a vertical curve changing at the rate of 0.1 per station. Total change in rate 0.8. Length of curve 8 stations. Beginning of curve sta. 867 - 4 = 863; end = sta. 871.

```
Elev. sta. 863 = 466 + 4 \times 0.2 = 466.8

Elev. sta. 871 = 466 - 4 \times 1.0 = 462.0

Elev. sta. 864 = elev. 863 - (0.2 + 0.05) = 466.8 - 0.25 = 466.55

Elev. sta. 865 = elev. 864 - (0.2 + 0.15) = 466.55 - 0.35 = 466.20

Elev. sta. 866 = elev. 865 - (0.2 + 0.25) = 466.20 - 0.45 = 465.75

Elev. sta. 867 = elev. 866 - (0.2 + 0.35) = 465.75 - 0.55 = 465.20

Elev. sta. 868 = elev. 867 - (0.2 + 0.45) = 465.20 - 0.65 = 464.55

Elev. sta. 869 = elev. 868 - (0.2 + 0.55) = 464.55 - 0.75 = 463.80

Elev. sta. 870 = elev. 869 - (0.2 + 0.65) = 463.80 - 0.85 = 462.95

Elev. sta. 871 = elev. 870 - (0.2 + 0.75) = 462.95 - 0.95 = 462.00
```

The work is proved since 462.0 is the elevation first found for station 871. There is no summit or bottom in this case as both grades are of the same sign.

TABLE I

Radii and their logarithms, and tangent offsets, and middle ordinates, for 100 feet chords of curves of degrees given. The degrees are given in degrees and decimals of a degree.

	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
0.00	∞0	∞	.000	.000	1.00	5729.65	3.75813	.873	.218
.02	286478.90	5.45709	.017	.004	.02	5617.31	·74953	.890	.223
.04	143239.45	.15606	.035	.009	.04	5509.29	.74110	.908	.227
.06	95492.97	4.97997	.052	.013	.06	5405.34	.73283	.925	·23I
	71619.73	.85503 4.75812	.070	.017	.08	5305.24	.72471	.942	.236
.10	57295.79 47746.49	.67804	.105	.022	.IO	5115.78	3.71674 .70801	.960	.240
.12	40925.57	.61100	.105	.031	.12	5026.03	.70091	·977	.244
.16	35809.87	.55400	.140	.035	.16	4939.38	.60367	1.012	.253
.18	31831.00	.50285	.157	.030	.18	4855.66	.68625	.030	.257
.20	28647.90	4.45700	.175	.044	.20	4774.74	3.67805	1.047	.262
.22	26043.55	.41570	.192	.048	.22	4606.46	.67177	.065	.266
.24	23873.26	.37791	.200	.052	.24	4620.72	.66471	.082	.271
.26	22036.86	.34315	.227	.057	.26	4547.38	.65776	.100	.275
.28	20462.80	.31007	.244	.061	.28	4476.33	.65092	.117	.279
-30	19098.61	4.28100	.262	.065	.30	4407.46	3.64419	1.134	.284
.32	17904.95	.25297	.279	.070	.32	4340.69	.63756	.152	.288
-34	16851.73	.22664	.297	.074	-34	4275.90	.63103	.169	.292
.36	15915.52	.20182	.314	.079	.36	4213.02	.62459	.187	.297
.38	15077.86	.17834	.332	.083	.38	4151.97	.61825	.204	.301
.40	14323.97	4.15606	-349	.087	.40	4092.66	3.61201	1.222	.305
.42	13641.88	.13487	.367	.092	.42	4035.02	.60585	.239	.310
-44	13021.80	.11467	.384	.0 96	-44	3978.98	-59977	-257	.314
.46	12455.64	.09537	.401	.100	.46	3924.47	-59378	-274	.319
.48	11936.66	.07688	.419	.105	.48	3871.44	.58787	-292	.323
.50	11459.19	4.05915	.436	.109	.50	3819.83	3.58204	1.309	-327
-52	11018.46	.04212	·454	.113	.52	3769.57	.57629	.326	-332
-54	10610.37	.02573	.471	.118	.54	3720.62	.57061	-344	.336
.56	10231.43	.00994	.489	.122	.56	3672.92	.56501	.361	-340
.58 .60	9878.62	3.99470	.506	.127	.58 .60	3626.43	-55948	·379	-345
.62	9549-34	3.97997	.524	.131	.62	3581.10	3.55402	1.396	-349
.64	9241.30 8952.51	.96573	.541	.135	.64	3493.76	.54329	.431	·353
.66	8681.26	.95194	·559	.140	.66	3493.70	.53803	.449	.362
.68	8425.90	.93030	.593	.148	.68	3410.50	.53283	.466	.367
.70	8185.16	3.91303	.611	.153	.70	3370.46	3.52769	1.483	.371
.72	7957.80	.90079	.628	.157	.72	3331.28	.52261	.501	-375
.74	7742.73	.88889	.646	.161	.74	3292.99	.51759	.518	.380
.76	7539-97	.87731	.663	.166	.76	3255.57	.51263	.536	.384
.78	7345.67	.86603	.681	.170	.78	3218.99	.50772	.553	.388
.80	7162.03	3.85504	.698	.175	.80	3183.23	3.50287	1.571	-393
.82	6987.35	.84431	.716	.179	.82	3148.25	.49807	.588	-397
.84	6820.99	.83385	-733	.183	.84	3114.03	.49332	.606	.401
.86	6662.36	.82363	.750	.188	.86	3080.55	.48863	.623	.406
.88	6510.95	.81364	.768	.192	.88	3047.78	.48398	.641	.410
.90	6366.26	3.80388	.785	.196	.90	3015.71	3.47939	1.658	.415
.92	6227.87	·79434	.803	.201	.92	2984.29	.47484	.675	.419
.94	6095.36	.78500	.820	.205	.94	2953.53	.47034	.693	.423
.96	5968.38	.77586	.838	.209	.96	2923.40	.46589	.710	.428
.98	5846.58	.76690	.855	.214	.98	2893.87	.46148	.728	.432
1.00	5729.65	3.75813	.873	.218	2.00	2864.93	3.45711	1.745	.436

Deg.	Radius	Logarithm	Tan.	Mid.	Deg.	Radius	Logarithm	Tan.	Mid.
Deg.	R	Log R	Off.	Ord.	Dog.	R	Log R	Off.	Ord.
U	n	Lug II	t	m	"		Log n	t	m
0					0				
2.00	2864.93	3.45711	1.745	.436	3.00	1910.08	3.28105	2.618	.655
.02	2836.57	.45279	.763	.441	.02	1897.43	.27817	.635	.659
.04	2808.76	.44852	.780	-445	.04	1884.95	.27530	.653	.663
.06	2781.50	.44428	.798	•449	.06	1872.63	.27245	.670	.668
.08	2754.76	.44008	.815	-454	.08	1860.48 1848.48	.26962 3.26681	.687	.672
.10	2728.52	3.43593 .43181	.850	.458	.10	1836.63	.26402	2.705	.676 .681
.12	2677.53	.42773	.867	.467	.12	1824.93	.26125	.740	.685
.16	2652.74	.42369	.885	.471	.16	1813.30	.25849	.757	.680
.18	2628.40	.41969	.902	.476	.18	1801.99	.25575	.775	.694
.20	2604.51	3.41573	1.920	.480	.20	1790.73	3.25303	2.792	.698
.22	2581.05	.41180	.937	.484	.22	1779.63	.25032	.810	.702
.24	2558.01	.40790	-955	.489	.24	1768.62	.24764	.827	.707
.26	2535.38	.40404	.972	·493	.26	1757.78	.24496	.845	.711
.28	2513.14	.40022	.990	·497	.28	1747.06	.24231	.862	.716
.30	2491.29	3.39642	2.007	.502	.30	1736.48	3.23967	2.879	.720
.32	2469.81	.39266	.024	.506	.32	1726.02	.23705	.897	.724
-34	2448.71 2427.96	.38894	.042	.511	-34	1715.69	.23444	.914	.729
.36 .38	2427.90	.38158	.059	.515	.36 .38	1695.39	.22027	.932	·733
.40	2387.50	3.37794	2.004	.524	.40	1685.42	3.22671	2.967	.742
.42	2367.77	.37434	.112	.528	.42	1675.56	.22416	.984	.746
.44	2348.36	.37077	.120	-532	-44	1665.83	.22163	3.002	.751
.46	2329.28	.36722	.147	.537	.46	1656.19	.21911	.019	.755
.48	2310.49	.36370	.164	.541	.48	1646.68	.21661	.036	.759
.50	2292.01	3.36022	2.181	-545	.50	1637.28	3.21412	3.054	.764
.52	2273.83	.35676	.199	.550	.52	1627.98	.21165	.071	.768
-54	2255.92	·35332	.216	-554	-54	1618.78	.20019	.089	.772
.56	2238.30	-34992	.234	-559	.56	1609.69	.20674	.106	.777
.58 .60	2220.95	.34654	.251 2.260	.563	.58 .60	1600.70	3.20180	3.141	.781
.62	2203.87	3.34319 .33986	,286	.567 -572	.62	1583.02	.10040	.150	.790
.64	2170.40	.33656	.304	.576	.64	1574.32	.19709	.176	-794
.66	2154.17	.33328	.321	.580	.66	1565.72	.19472	.103	.799
.68	2138.10	.33003	-339	.585	.68	1557.22	.19235	.211	.803
.70	2122.26	3.32681	2.356	.589	.70	1548.80	3.19000	3.228	.807
.72	2106.66	.32359	·373	.593	.72	1540.48	.18766	.246	.812
.74	2001.20	.32041	.391	.598	.74	1532.24	.18533	.263	.816
.76	2076.13	.31726	.408	.602	.76	1524.10	.18301	.281	.820
.78	2061.20	.31412	.426	.607	.78	1516.14	.18071	.298	.825
.80	2046.48	3.31101	2.443	.611	.80 .82	1508.06	3.17842	3.316	.829
.8 ₂	2031.97	.30792	.460	.620	.82	1500.17	.17014	.333	.838
.86	2003.56	.30405	.496	.624	.86	1484.63	.17367	.368	.842
.88	1989.65	.20878	.513	.628	.88	1476.98	.16037	.385	.847
.00	1975.93	3.29577	2.530	.633	.90	1469.41	3.16714	3.403	.851
.92	1962.40	.29279	.548	.637	.92	1461.91	.16492	.420	.855
.94	1949.05	.28982	.565	.641	.94	1454.49	.16271	.438	.860
.96	1935.88	,28688	.583	.646	.96	1447.15	.16051	-455	.864
.98	1922.89	.28396	,600	.650	.98	1439.88	.15833	.473	.868
3.00	1910.08	3.28105	2.618	.655	4.00	1432.69	3.15615	3.490	.873
L	i	1	1	·	•	1		I	1

Deg.	Radius	Logarithm	Tan.	Mid.	Deg.	Radius	Logarithm	Tan.	Mid.	
D D	R	Log R	Off.	Ord.	D	R	Log R	Off.	Ord.	
١ "	••	208	t	m			s	t	m	
0					0					
4.00	1432.69	3.15615	3.490	.873	5.00	1146.28	3.05929	4.362	1.091	
.02	1425.56	.15399	.507	.877	.02	1141.72	.05756	-379	.095	
.04	1418.51	.15183	-525	.881	.04	1137.19	.05583	-397	.100	
.06	1411.52	.14969	-542	.886	.06	1132.70	.05411	.414	.104	
.08	1404.60	.14755	.560	.890	.08	1128.24	.05240	.432	.108	
.IO	1397.76	3.14543	3.577	.895	.10	1123.82	3.05070	4.449	1.113	
.12	1390.98	.14332	•595	.899	.12	1119.43	.04900	.467	.117	
.14	1384.26	.14122	.612	.903	.14	1115.08	.04731	.484	.122	
.16	1377.61	.13912	.629	.908	.16	1111.00	.04571	.501	.126	
.18	1371.02	.13704	.647	.912	.18	1106.47	.04394	.519	.130	
.20	1364.49	3.13497	3.664	.916	.20	1102.22	3.04227	4.536	1.135	
.22	1358.03	.13291	.682	.921	.22	1003.81	.04060	-554	.139	
.24	1351.31	.13076	.699	.925	.24		.03894	-571	.143	
.26	1345.28	.12881	.717	.929	.26	1089.66	.03729	.589	.148	
.28	1339.00	.12678	.734	.934	.28	1085.53	.03564	.606	.152	
.30	1332.77	3.12476	3.752	.938	.30	1081.44	3.03400	4.623	1.156	
.32	1326.61	.12274	.769	.943	-32	1077.38	.03237	.641	.161	
-34	1320.49	.12074	.786	.947	-34	1073.34	.03074	.658	.165	
.36	1314.44	.11874	.804 .821	.951	.36	1069.34	.02912	.676	.170	
.38	1308.44	.11675		.956	.38	1065.37	.02750	.693	.174	
.40	1302.50	3.11478	3.839	.960	.40	1061.43	3.02589	4.711	1.178	
-42	1296.61			.964	.42	1057.51	.02429	.728	.183	
-44	1290.77	.11085	.874	.969	-44	1053.63	.02269	.746	.187	
.46		.10696	.891	.973 .978	.46	1049.77	.01951	.763	.191	
.48	1279.25	3.10502	.909 3.926	.982	.48 .50	1045.94	3.01793	.780 4.798	1.200	
.50	1267.93	.10310		.986		1038.37	.01635	.815		
-52	1262.35	.10310	.943 .961	.900	-52 -54	1034.62	.01478	.833	.205	
·54 ·56	1256.82	.00027	.978	.995	.56	1034.02	.01322	.850	.213	
.58	1251.33	.09737	.996	.993	.58	1030.90	.01166	.868	.218	
.60	1245.80	3.09548	4.013	1.004	.60	1023.55	3.01011	4.885	1.222	
.62	1245.50	.09340	.031	.008	.62	1019.91	.00856	.902	.226	
.64	1235.16	.09300	.048	.012	.64	1016.20	.00702	.902	.231	
.66	1229.86	.08986	.065	.017	.66	1012.70	.00548	-937	.235	
.68	1224.61	.08800	.083	.021	.68	1000.14	.00305	-955	.239	
.70	1210.40	3.08615	4.100	1.026	.70	1005.60	3.00243	4.972	1.244	
.70	1214.24	.08430	.118	.030	.72	1002.00	.00001	.990	.248	
.74	1200.12	.08247	.135	.034	-74	998.60	2.00030	5.007	.253	
.76	1204.04	.08064	.I53	.039	.76	995.14	.99788	.024	-257	
.78	1100.00	.07882	.170	.043	.78	991.68	.99638	.042	.261	
.80	1194.01	3.07701	4.188	1.047	.80	988.28	2.99488	5.059	1.266	
.82	1189.06	.07520	.205	.052	.82	984.89	.99339	.077	.270	
.84	1184.15	.07341	.222	.056	.84	981.52	.99190	.094	.274	
.86	1179.28	.07162	.240	.060	.86	978.17	.99041	.112	.279	
.88	1174.45	.06983	.257	.065	.88	974.66	.98885	.129	.283	
.90	1169.66	3.06806	4.275	1.069	.90	971.54	2.98746	5.146	1.287	
.92	1164.91	.06629	.292	.074	.92	968.26	.98599	.164	.292	
.94	1160.19	.06453	.310	.078	.94	965.01	.98453	.181	.296	
.96	1155.52	.06278	.327	.082	.96	961.77	.98307	.199	.301	
.98	1150.88	.06103	-345	.087	.98	958.56	.98162	.216	.305	
5.00	1146.28	3.05929	4.362	1.001	6.00	955-37	2.98017	5.234	1.309	

Deg.	Radius . R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg.	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
6.00	955-37	2.98017	5.234	1.309	7.00	819.02	2.91329	6.105	1.528
.02	952.20	.97873	.251	.314	.02	816.69	.91206	.122	.532
.04	949.05	.97729	.268	.318	.04	814.37	.91082	.140	.536
.06 .08	945.92	.97585 .97442	.303	.322	.o6 .o8	809.78	.90959	.157	.541
.00	939.72	2.97300	5.321	1.331	.00	807.50	2.90714	6.102	·545 1.550
.12	939.72	.97158	.338	+335	.12	805.23	.90592	.200	.554
.14	933.60	.07016	.356	.340	.14	802.08	.90471	.227	.558
.16	930.57	.96875	-373	-344	.16	800.74	.90349	.244	.563
.18	927.58	.96734	.390	-349	.18	798.51	.90228	.262	.567
.20	924.58	2.96594	5.408	1.353	,20	796.30	2.90108	6.279	1.572
.22	921.61	.96455	.425	-357	.22	794.10	.89987	.296	.576
.24	918.66	.96315	-443	.362	.24	791.90	.89867	.314	.580
.26	915.72	.96176	.460	.366	.26	789.73	.89748	·33I	.584
.28	912.81	.96038	.478	.370	.28	787.56	.89628	.349	.589
.30	909.92	2.95900	5.495	1.375	.30	785.40	2.89509	6.366	1.593
.32	906.48	.95736	.512	-379	.32	783.26	.89391	.384	.598
-34	904.18	.95625	.530	.384	-34	781.13	.89272	.401	.602
.36	901.34 898.52	.95489	.547	.389	.36	779.01 776.00	.89154	.418	.606
.38	895.71	-95353	.565 5.582	.392 1.397	.38	774.81	.89037	.436	.611
.40	892.92	.95081	.600	.401	.40 .42	772.72	.88802	6.453	.61g
.44	890.15	.94947	.617	.405	.44	770.65	.88685	.488	.624
.46	887.40	.94947	.634	.410	.46	768.58	.88569	.505	.628
.48	884.67	.94678	.652	.414	.48	766.53	.88453	.523	.632
.50	881.95	2.94544	5.660	1.418	.50	764.49	2.88337	6.540	1.637
.52	879.24	.94411	.687	-423	.52	762.46	.88222	-558	.641
-54	876.56	.94278	.704	.427	-54	760.44	.88106	•575	.646
.56	873.89	.94146	.722	.432	.56	758.45	.87993	•593	.650
.58	871.24	.94014	.739	.436	.58	756.43	.87877	.610	.654
.60	868.60	2.93882	5.756	1.440	.60	754-44	2.87763	6.627	1.659
.62	865.98	.93751	-774	·445	.62	752.47	.87649	.645	.663
.64	863.37	.93620	.791	·449	.64	750.50	.87535	.662	.667
.66	860.78	.93489	.809	-453	.66	748.54	.87422	.680	.672
.68	858.21	-93359	.826	.458	.68	746.60	.87309	.697	.676
.70	855.65	2.93230	5.844 .861	1.462	.70	744.66	2.87196	6.714	1.680
.72 .74	853.10 850.58	.93100	.878	.466	.72 .74	742.74	.87083 .86071	.732	.685
.74 .76	848.06	.92971	.896	.471	.74 .76	738.01	.86850	·749	.694
.78	845.56	.92043	.913	.480	.78	737.02	.86748	.784	.698
.80	843.08	2.92587	5.931	1.484	.80	735.13	2.86636	6.802	1.702
.82	840.61	.92459	.948	.488	.82	733.25	.86525	.810	.707
.84	838.16	.92332	.965	•493	.84	731.38	.86415	.836	.711
.86	835.71	.92206	.983	•497	.86	729.53	.86304	.854	.715
.88	833.29	.92080	6.000	1.501	.88	727.68	.86194	.871	.720
.90	830.88	2.91954	6.018	1.505	.90	725.85	2.86084	6.889	1.724
.92	828.48	.91828	.035	.510	.92	724.01	.85974	.906	.729
.94	826.09	.91703	.053	.515	.94	722.19	.85865	.923	-733
.96	823.72	.91578	.070	.519	.96	720.38	.85756	.941	.737
.98	821.36	.91454	.087	.523	.98	718.57	.85647	.958	.742
7.00	819.02	2.91329	6.105	1.528	8.00	716.78	2.85539	6.976	1.746

Deg.	Radius	Logarithm	Tan. Off.	Mid. Ord.	Deg.	Radius	Logarithm	Tan. Off.	Mid. Ord.
D	R	Log R	t	m	D	R	Log R	t	m
0	()				0				
8.00	716.78	2.85539	6.976	1.746	9.00	637.27	2.80433	7.846	1.965
.02	714.99	.85430 .85322	.993 7.010	.750 .755	.02	634.46	.80336	.863 .881	.969
.06	711.45	.85215	.028	·759	.06	633.06	.80145	.898	.973 .978
.08	709.69	.85107	.045	.764	.08	631.67	.80040	.916	.982
.10	707.94	2.85000	7.063	1.768	.10	630.29	2.79954	7.933	1.987
.12	706.20	.84893	.080	.772	.12	628.91	.79859	.950	.991
.14	704.47	.84786	.098	-777	.14	627.53	.79764	.968	.995
.16	702.75	.84680	.115	.781 .785	.16 .18	626.17	.79669	.985	-999
.10	699.33	.84574 2.84468	.132 7.150	1.700	.10	623.45	.79574 2.79480	8.002	2.004
.20	697.63	.84362	.167	•794	.20	622.10	.79386	.037	.013
.24	695.94	.84257	.185	.798	.24	620.76	.79292	.055	.017
.26	694.25	.84152	.202	.803	.26	619.42	.79198	.072	.021
.28	692.58	.84047	.219	.807	.28	618.09	.79105	.090	.026
.30	690.91	2.83942	7.237	1.811	.30	616.76	2.79012	8.107	2.030
.32	689.26	.83838	-254	.816	.32	615.44	.78919	.124	.034
•34	687.61	.83734	.272	.820	-34	614.12	.78826	.142	.039
.36	685.96	.83630	.289	.825 .820	.36	612.82	.78733 .78640	.159	.043
.38	684.33 682.70	.83527 2.83423	.306 7.324	1.833	.38	610.21	2.78548	.176	2.052
.40	681.00	.83320	.341	.838	.42	608.92	.78456	.211	.056
-44	679.47	.83217	-359	.842	.44	607.63	.78364	.220	.061
.46	677.87	.83115	.376	.847	.46	606.35	.78272	.246	.065
.48	676.27	.83012	-393	.851	.48	605.08	.78181	.263	.069
.50	674.69	2.82910	7.411	1.855	.50	603.80	2.78090	8.281	2.074
.52	673.11	.82808	.428	.86o	.52	602.54	-77999	.298	.078
-54	671.53	.82707	.446	.864	-54	601.28	.77908	.316	.083
.56	669.9 7 668.41	.82605	.463	.868	.56	600.02	.77817	∙333	.087
.58 .60	666.86	.82504 2.82403	.480 7.498	.873 1.877	.58 .60	598.77 597.53	2.77636	.350 8.368	2.096
.62	665.33	.82303	.515	.881	.62	596.20	.77546	.385	.100
.64	663.77	.82202	.533	.886	.64	595.06	.77456	.403	.104
.66	662.24	.82102	.550	.800	.66	593.83	.77366	.420	.100
.68	660.72	.82002	.567	.895	.68	592.60	.77276	-437	.113
.70	659.21	2.81902	7.585	1.899	.70	591.38	2.77187	8.455	2.117
.72	657.70	.81803	.602	.903	.72	590.17	.77098	-472	.121
.74	656.19	.81703	.620	.908	.74	588.96	.77009	.490	.126
.76 .78	654.70 653.21	.81604 .81505	.637	.912	.76 .78	587.76 586.56	.76920	.507 -524	.131
.70 .80	651.73	2.81407	7.672	1.021	.80	585.36	2.76743	8.542	2.139
.82	650.25	.81308	.689	.925	.82	584.17	.76654	-559	.144
.84	648.79	.81210	.707	.930	.84	582.99	.76566	.576	.148
.86	647.32	.81112	.724	-934	.86	581.81	.76478	-594	.152
.88	645.87	.81014	.742	.938	.88	580.64	.76390	.611	.157
.90	644.42	2.80917	7.759	1.943	.90	579.46	2.76303	8.629	2.161
.92	642.98	.80820	.776	-947	.92	578.30	.76215	.646	.166
.94 .96	641.54	.80723	.794 .811	.951	.94 .96	577·14 575·99	.70128	.681	.170
.90 .98	638.69	.80520	.820	.950	.90 .98	575.99	.75954	.698	.174
9.00	637.27	2.80433	7.846	1.965	10.00	573.69	2.75867	8.716	2.183
J	107.27	10-400	,	11923		3,09	,,,,,,		

Deg.	Radius	Logarithm	Tan. Off.	Mid.	Deg.	Radius	Logarithm	Tan. Off.	Mid.
D	R	Log R	t t	Ord.	Ď	R	Log R	υπ. t	Ord.
	1		<u> </u>	m				- 1	m
0	60	06-	06	0-	0	-06	0		
10.0	573.69 568.02	2.75867 .75436	8.716 .803	2.183	15.0	383.06	2.58327	13.053	3.277
.2	562.47	.75010	.889	.205	.1	378.05	-57755	.139	.299
-3	557.02	.74587	.976	.234	.3	375.60	.57472	.312	-343
.4	551.68	.74169	9.063	.270	.4	373.17	.57191	-399	.365
.5	546.44	2.73754	9.150	2.203	-5	370.78	2.56012	13.485	3.387
.6	541.30	.73344	.237	.314	.6	368.42	.56634	.572	.400
.7	536.25	.72937	.324	.336	.7	366.09	.56358	.658	.431
.8	531.30	.72534	.411	.358	.8	363.78	.56084	-744	-452
.9	526.44	.72135	.498	.38o	.9	361.51	.55812	.831	-474
11.0	521.67	2.71740	9.585	2.402	16.0	359.26	2.55541	13.917	3.496
I.	516.99	.71348	.671	.423	.I	357.05	·55273	14.004	.518
.2	512.38	.70960	.758	•445	.2	354.86	.55006	.090	.540
-3	507.86	.70575	.845	.467	-3	352.70	-54740	.177	.562
-4	503.42 400.06	.70193	.932	.489	-4	350.56	.54476	.263	.584
.5 .6	494.77	2.69815 .69441	.106	2.511	.5 .6	348.45	2.54214	14.349	3.606
.7	494.77	.69669	.100	•533	.7	346.37 344.31	-53953 -53694	.436	.650
.8	486.42	.68701	.279	•555 •577	.8	344.31	.53094	.522 .608	.672
.0	482.34	.68336	.366	.598	.0	342.27	.53181	.605	.694
12.0	478.34	2.67074	10.453	2.620	17.0	338.27	2.52027	14.781	3.716
1.	474.40	.67614	.540	.642	.1	336.31	.52674	.867	.738
.2	470.53	.67258	.626	.664	.2	334.37	.52423	.954	.760
-3	466.72	.66905	.713	.686	.3	332.45	.52173	15.040	.781
.4	462.96	.66555	.800	.708	.4	330.56	.51924	.126	.803
-5	459.28	2.66207	10.887	2.730	-5	328.69	2.51677	15.212	3.825
.6	455.65	.65863	•973	.752	.6	326.83	.51432	.299	.847
.7	452.07	.65521	11.060	.774	7	325.00	.51188	.385	.869
.8	448.56	.65182	.147	.795	.8	323.18	.50945	.471	.891
.9	445.00	.64845	.234	.817	.9	321.39	.50704	-557	.913
13.0	441.68	2.64511	11.320	2.839	18.0	319.62	2.50464	15.643	3.935
ı.	438.33	.64180	.407	.861	.I	317.87	.50225	.730	957
.2	435.02 431.76	.63851	•494 •580	.883	.2	316.14	.49988	.816	-979
•3	431.70	.63201	.667	.905	-3	314.43	·49752	.902	4.00I .023
.5	425.40	2.62879	11.754	2.949	•4 •5	311.06	.49517 2.49284	16.074	4.045
.6	422.28	.62560	.840	.949	.6	300.40	.49052	.160	.067
.7	410.22	.62244	.927	.992	.7	307.76	.48821	.246	.080
.8	416.10	.61929	12.014	3.014	.8	306.14	.48501	•333	.111
.9	413.21	.61617	.100	.036	.9	304.53	.48363	.419	.133
14.0	410.28	2.61308	12.187	3.058	19.0	302.94	2.48136	16.505	4.155
ı.	407.38	.61000	.274	.080	.ı	301.37	.47910	.591	.177
.2	404.53	.60695	.360	.102	.2	299.82	.47686	.677	.199
-3	401.71	.60391	-447	.124	•3	298.28	.47462	.763	.221
-4	398.94	.60090	•533	.146	-4	296.75	.47240	.849	•243
5	396.20	2.59791	12.620	3.168	.5	295.25	2.47019	16.935	4.265
.6	393.50	•59495	.706	.190	.6	293.76	.46799	17.021	.287
.7 .8	390.84	.59200	.793 .880	.211	.7 .8	292.28	.46580	.107	.308
.0	385.62	.58616	.066	.233		289.37	.46362 .46145	.193	.330
15.0	383.06	2.58327	13.053	.255 3.277	.9 20.0	287.94	2.45930	17.365	-35 ² 4-374
- 5.5	000.00	3-3-7	-333	3.277	20.0	207194	-143930	7.503	4.074

Deg.	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
20.0	287.94	2.45930	17.365	4.374	25.0	231.01	2.36363	21.644	5.476
ı.	286.52	.45716	.451	.396	.I	230.11	.36193	.729	.498
.2	285.12	.45502	-537	.418	.2	229.21	.36023	.814	.520
-3	283.73	.45290	.623	.440	-3	228.32	-35854	.899	-542
-4	282.35 28 0 .00	.45079	.708	.462	-4	227.43	.35685	.985	.564
·5 .6	270.64	2.44869 .44660	17.794 .880	4.484 .506	·5 .6	225.68	2.35517 .35350	.155	5.586
.7	278.30	.44452	.966	.528	.7	224.82	.35184	.240	.630
.8	276.98	.44432	18.052	.550	.8	223.96	.35018	.325	.653
.9	275.67	.44039	.138	.572	.9	223.11	.34853	.410	.675
21.0	274.37	2.43834	18.224	4.594	26.0	222.27	2.34688	22.495	5.697
ı.	273.08	.43630	.300	.616	.1	221.43	-34524	.58c	.719
.2	271.81	.43427	-395	.638	.2	220.60	.34361	.665	.741
-3	270.55	.43225	.481	.660	-3	219.78	.34199	.750	.763
-4	269.30	.43024	.567	.682	-4	218.96	.34037	.835	.785
-5	268.56	2.42824	18.652	4.704	-5	218.15	2.33875	22.920	5.807
.6	266.34	.42624	.738	.726	.6	217.34	.33715	23.005	.829
.7	265.62	.42426	.824	.748	.7	216.54	-33555	.000	.852
.8	264.42	.42229	.910	.770	.8	215.75	-33395	.175	.874
.9	263.22	.42033	-995	.792	.9	214.96	·33237	.260	.896
22.0	262.04	2.41837	19.081	4.814	27.0	214.18	2.33078	23.345	5.918
.I	260.87	.41643	.167	.836	.I	213.41	.32921	-429	.940
.2	259.71	.41449	.252	.858	.2	212.64	.32764	.514	.962
-3	258.56	.41256	.338	.881	-3	211.87	.32608	.599	.984
-4	257.42	.41064	.423	.903	-4	211.11	.32452	.684	6.006
.5 .6	256.29 255.17	2.40873 .40683	19.509	4.925	.5 .6	210.36	2.32297	23.769	6.029 .051
	255.17	.40404	.595 .680	.947 .969	.7	208.87	.31988	.938	.031
.7 .8	252.06	.40394	.766	.909	.8	208.14	.31835	24.023	.005
.9	251.87	.40118	.851	5.013	.0	207.40	.31682	.108	.117
23.0	250.70	2.39931	19.937	5.035	28.0	206.68	2.31520	24.192	6.130
.I	249.72	.39746	20.022	.057	.1	205.96	.31378	.277	.161
.2	248.66	.39561	.108	.079	.2	205.24	.31227	.362	.184
-3	247.61	.39376	.193	.IOI	-3	204.53	.31076	.446	.206
.4	246.56	.39193	.279	.123	-4	203.83	.30926	.531	.228
-5	245.53	2.39010	20.364	5.145	-5	203.13	2.30776	24.615	6.250
.6	244.50	.38829	.450	.167	.6	202.43	.30627	.700	.272
-7	243.49	.38647	·535	.189	.7	201.74	.30479	.784	.294
.8	242.48	.38467	.620	.211	.8	201.05	.30331	.869	.316
.9	241.48	.38288	.706	.233	.9	200.37	.30184	.954	.339
24.0	240.49	2.38100	20.791	5.255	29.0	199.70	2.30037	25.038	6.361
ı.	239.50	.37931	.877	.278	.I .2	199.02	.29891	.207	.405
.2	230.53	·37754 ·37578	21.047	.299	.2	195.30	.29745	.207	.405
·3 ·4	237.50	.37570	.132	-343	.4	197.70	.29455	.376	.450
·4 ·5	235.65	2.37227	21.218	5.366	.5	196.38	2.29311	25.460	6.472
.6	234.71	.37053	.303	.388	.6	195.74	.20167	-545	-494
.7	233.77	.36879	.388	.410	.7	195.09	.29024	.629	.516
.8	232.84	.36707	.474	-432	.8	194.45	.28881	.713	.538
.9	231.92	.36535	-559	-454	.9	193.82	.28739	.798	.560
25.0	231.01	2.36363	21.644	5.476	30.0	193.19	2.28597	25.882	6.583
	1	1						1	

Deg.	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg.	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
30.0	193.19	2.28597	25.882	6.583	35.0	166.28	2.22083	30.071	7.696
.r	192.56	.28456	.966	.605	.I	165.82	.21963	.154	.718
.2	191.94	.28315	26.050	.627	.2	165.36	.21843	.237	.740
-3	191.32	.28175	.135	.649	-3	164.91	.21724	.320	.763
-4	190.70	2.27896	26.303	.671 6.694	-4	164.46	.21605 2.21486	.403	.785
·5 .6	189.49	.27757	.387	.716	.5 .6	163.56	.21368	30.486	7.807
.7	188.88	.27619	.471	.738	.7	163.12	.21300	.570	.852
.8	188.28	.27481	.556	.760	.8	162.68	.21133	.736	.874
.9	187.60	.27344	.640	.782	.0	162.24	.21016	.819	.897
31.0	187.10	2.27207	26.724	6.805	36.0	161.80	2.20800	30.002	7.010
I.	186.51	.27071	.808	.827	.1	161,37	.20782	.985	.942
.2	185.93	.26935	.802	.849	.2	160.94	.20666	31.068	.964
-3	185.35	.26799	.976	.871	-3	160.51	.20550	.151	.986
-4	184.77	.26664	27.060	.894	-4	160.08	.20435	.233	8.000
-5	184.20	2.26530	27.144	6.916	∙5	159.66	2.20320	31.316	8.031
.6	183.63	.26395	.228	.938	.6	159.24	.20205	-399	.053
.7	183.07	.26262	.312	.960	.7	158.82	.20091	.482	.076
.8	182.51	.26128	.396	.983	.8	158.40	.19977	.565	.098
.9	181.95	.25996	.480	7.005	.9	157.99	.19863	.648	.121
32.0	181.40	2.25863	27.564	7.027	37.0	157.58	2.19749	31.730	8.143
.I	180.85	.25731	.648	.049	.I	157.17	.19636	.813	.165
.2	180.30	.25600	.731	.072	.2	156.76	.19523	.896	.188
-3	179.76	.25469	.815	.094	-3	156.35	.19411	.979 32.061	.210
•4	178.68	2.25208	27.083	7.138	-4	155.55	2.19187	32.144	.233 8.255
·5 .6	178.15	.25078	28.067	.161	.5 .6	155.15	.19076	.227	.277
.7	177.62	.24949	.150	.183	.7	154.75	.18064	.300	.300
.8	177.00	.24820	.234	.205	.8	154.36	.18854	-392	.322
.9	176.57	.24601	.318	.227	.9	153.97	.18743	•474	-345
33.0	176.05	2.24563	28.402	7.250	38.0	153.58	2.18633	32.557	8.367
ı.	175-53	.24435	.485	.272	ı.	153.19	.18523	.639	.390
.2	175.02	.24308	.569	.294	.2	152.80	.18413	.722	.412
-3	174.51	.24181	.652	.316	-3	152.42	.18304	.804	-434
-4	174.00	.24054	.736	-339	-4	152.04	.18195	.887	.457
-5	173.49	2.23928	28.820	7.361	-5	151.66	2.18086	32.969	8.479
.6	172.99	.23802	.903	.383	.6	151.28	.17978	33.051	.502
.7	172.49	.23677	.987	.406	.7	150.90	.17870	.134	-524
.8	172.00	.23552	29.070	.428	.8	150.53	.17762	.216	·547
.9 34.0	171.50	2.23303	154 29.237	7.473	.9 39.0	149.79	2.17547	33.381	8.592
34.0 .I	170.53	.23180	.321	•495	39.0 .I	149.79	.17441	.463	.614
.2	170.04	.23056	.404	.517	.2	149.42	.17334	.545	.636
-3	160.56	.22933	.487	-539	.3	148.60	.17228	.627	.659
.4	169.09	.22811	.571	.562	-4	148.33	.17122	.710	.681
-5	168.61	2.22688	29.654	7.584	-5	147.97	2.17016	33.792	8.704
.6	168.14	.22567	-737	.606	.6	147.61	.16911	.874	.726
-7	167.67	.22445	.821	.629	.7	147.25	.16805	.956	.749
.8	167.20	.22324	.904	.651	.8	146.89	.16701	34.038	.771
.9	166.74	.22203	.987	.673	.9	146.54	.16596	.120	.794
35.0	166.28	2.22083	30.071	7.696	40.0	146.19	2.16492	34.202	8.816
		-	l	1			1	1	

TABLE II. — Tangent Distances for a 1° Curve for Varying I's $T_D = T_{1^{\circ}}/D + C$ of Table III

100	.00
0.4 2.00 52.00 102.01 152.04 202.09 252.17 302.28 352.6 0.6 3.00 53.00 103.01 153.04 203.09 253.17 303.29 353.6 0.8 4.00 54.00 104.01 154.04 204.09 254.17 304.29 354.6 10 5.00 55.00 105.01 155.04 205.09 255.17 305.29 355.6 12 6.00 56.00 106.01 155.04 206.09 256.17 306.39 356.6 14 7.00 57.00 107.01 157.04 207.09 257.18 307.30 357.6 16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358.6 18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359.6 20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360.6 22 11.00 61.00 111.02 161.04 211.10 261.18 311.31 361.6 24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362.6 362.00 330.00 330.00 330.00 330.00 362.00 312.31 362.6 330.31 330.00 362.00 312.31 362.6 330.31 330.00 362.00 312.31 362.6 330.31 330.00 362.00 312.31 362.00 312.31 362.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 363.00 36	
0.6	
.08 4.00 54.00 104.01 154.04 204.09 254.17 304.29 354.2 .10 5.00 55.00 105.01 155.04 205.09 255.17 305.29 355.2 .12 6.00 56.00 106.01 156.04 206.09 256.17 306.30 356.3 .14 7.00 57.00 107.01 157.04 207.09 257.18 307.30 357. .16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358.3 .18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359.3 .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360. .24 12.00 62.00 112.02 161.04 211.10 262.19 312.31 362.	.04
.10 5.00 55.00 105.01 155.04 205.09 255.17 305.29 355.2 .12 6.00 56.00 106.01 156.04 206.09 256.17 306.30 356.3 .14 7.00 57.00 107.01 157.04 207.09 257.18 307.30 357.4 .16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358. .18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359. .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360. .24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362.	.06
.12 0.00 56.00 106.01 156.04 206.09 256.17 306.30 356.30 .14 7.00 57.00 107.01 157.04 207.09 257.18 307.30 357.4 .16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358. .18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359.3 .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360 .22 11.00 61.00 112.02 162.05 212.10 262.19 312.31 362 .24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362	.08
.14 7.00 57.00 107.01 157.04 207.09 257.18 307.30 357.3 .16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358.0 .18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359 .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360 .22 11.00 61.00 111.02 161.04 211.10 261.18 311.31 361 .24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362	.IO
.16 8.00 58.00 108.01 158.04 208.09 258.18 308.30 358.3 .18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359.3 .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360. .22 11.00 61.00 111.02 161.04 211.10 261.18 311.31 361. .24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362.	.12
.18 9.00 59.00 109.01 159.04 209.10 259.18 309.30 359.30 .20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360 .22 11.00 61.00 111.02 161.04 211.10 261.18 311.31 361 .24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362	.14
20 10.00 60.00 110.01 160.04 210.10 260.18 310.31 360 22 11.00 61.00 111.02 161.04 211.10 261.18 311.31 361 24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362	.16
.22 II. 00 61.00 III. 02 I61.04 2II. 10 261. 18 3II. 3I 361 .24 I2. 00 62. 00 II2. 02 I62. 05 2I2. 10 262. 19 3I2. 3I 362	.18
.24 12.00 62.00 112.02 162.05 212.10 262.19 312.31 362	.20
	.22
26 13.00 63.00 113.02 163.05 213.10 263.19 313.32 363.05 313.05	.24
	.26
.28 14.00 64.00 114.02 164.05 214.10 264.19 314.32 364.	.28
.30 15.00 65.00 115.02 165.05 215.10 265.19 315.32 365.	.30
.32 16.00 66.00 116.02 166.05 216.11 266.19 316.32 366.	.32
.34 17.00 67.00 117.02 167.05 217.11 267.20 317.33 367.	
.36 18.00 68.00 I18.02 I68.05 218.11 268.20 318.33 368.	
.38 19.∞ 69.∞ 119.02 169.05 219.11 269.20 319.33 369.	
.40 20.00 70.00 120.02 170.05 220.11 270.20 320.34 370.	.40
.42 21.00 71.00 121.02 171.05 221.11 271.21 321.34 371.	.42
.44 22.00 72.00 122.02 172.05 222.11 272.21 322.34 372.	
.46 23.00 73.00 123.02 173.05 223.12 273.21 323.35 373	
.48 24.00 74.01 124.02 174.06 224.12 274.21 324.35 374.	.48
.50 25.00 75.01 125.02 175.06 225.12 275.21 325.35 375.	50
.52 26.00 76.01 126.02 176.06 226.12 276.22 326.36 376.	.52
.54 27.00 77.01 127.02 177.06 227.12 277.22 327.36 377.	
.56 28.00 78.01 128.02 178.06 228.12 278.22 328.36 378.	
.58 29.00 79.01 129.02 179.06 229.12 279.22 329.37 379.	- 1
.60 30.00 80.01 130.02 180.06 230.13 280.23 330.37 380.	-
.62 31.00 81.01 131.02 181.06 231.13 281.23 331.37 381.	
.64 32.00 82.01 132.03 182.06 232.13 282.23 332.38 382.	
.66 33.00 83.01 133.03 183.06 233.13 283.23 333.38 383.	
.68 34.00 84.01 134.03 184.07 234.13 284.24 334.38 384.	
.70 35.00 85.01 135.03 185.07 235.13 285.24 335.39 385.	
.72 36.00 86.01 136.03 186.07 236.14 286.24 336.39 386.	
.74 37.00 87.01 137.03 187.07 237.14 287.24 337.39 387.	
76 38.00 88.01 138.03 188.07 238.14 288.25 338.40 388. 78 39.00 89.01 139.03 189.07 239.14 289.25 339.40 389.	
	-
	-1
.82 41.00 91.01 141.03 191.07 241.15 291.25 341.41 391. .84 42.00 92.01 142.03 192.07 242.15 292.26 342.41 392.	
.84 42.00 92.01 142.03 192.07 242.15 292.26 342.41 392. .86 43.00 93.01 143.03 193.07 243.15 293.26 343.42 393.	
.88 44.00 94.01 144.03 194.08 244.15 294.26 344.42 394.	
.90 45.00 95.01 145.03 195.08 244.15 295.26 345.42 394.	
.92 46.00 96.01 146.03 196.08 246.15 296.27 346.43 396.	
.94 47.00 97.01 147.03 197.08 247.16 297.27 347.43 397.	
.96 48.00 98.01 148.03 198.08 248.16 298.27 348.43 398.	
.98 49.00 99.01 149.04 199.08 249.16 299.28 349.44 399.	
1.00 50.00 100.01 150.04 200.08 250.16 300.28 350.44 400.	_

TABLE II. — (Continued) .

$^{\circ}I$	8°	9°	10°	11°	12°	13°	14°	15°	I
.00	400.66	450.93	501.28	551.70	602.21	652.81	703.51	754.32	.00
.02	401.66	451.94	502.29	552.71	603.22	653.82	704.53	755.34	.02
.04	402.67	452.95	503.29	553.72	604.23	654.84	705.54	756.36	.04
.06	403.67	453.95	504.30	554.73	605.24	655.85	706.56	757.38	.06
.08	404.68	454.96	505.31	555.74	606.26	656.86	707.57	758.39	.08
.10	405.68	455.96	506.32	556.75	607.27	657.88	708.59	759.41	.10
.12	406.69	456.97	507.33	557.76	608.28	658.89	709.60	760.43	.12
.14	407.69	457.98	508.33	558.77	609.29	659.90	710.62	761.45	.14
.16	408.70	458.98	509.34	559.78	610.30	660.92	711.63	762.46	.16
.18	409.70	459.99	510.35	560.79	611.31	661.93	712.65	763.48	.18
.20	410.71	461.00	511.36	561.80	612.32	662.94	713.67	764.50	.20
.22	411.71	462.00	512.37	562.81	613.33	663.96	714.68	765.52	.22
.24	412.72	463.01	513.37	563.82	614.35	664.97	715.70	766.53	.24
.26	413.72	464.02	514.38	564.83	615.36	665.98	716.71	767.55	.26
.28	414.73	465.02	515.39	565.84	616.37	667.00	717.73	768.57	.28
.30	415.73	466.03	516.40	566.85	617.38	668.01	718.74	769.59	.30
.32	416.74	467.04	517.41	567.86	618.39	669.02	719.76	770.61	.32
-34	417.74	468.04	518.41	568.87	619.40	670.04	720.78	771.62	-34
.36	418.75	469.05	519.42	569.88	620.42	671.05	721.79	772.64	.36
.38	419.75	470.06	520.43	570.89	621.43	672.07	722.81	773.66	.38
.40	420.76	471.06	521.44	571.90	622.44	673.08	723.82	774.68	.40
.42	421.76	472.07	522.45	572.91	623.45	674.09	724.84	775.70	.42
-44	422.77	473.08	523.46	573.92	624.46	675.11	725.86	776.72	-44
.46	423.78	474.08	524.46	574.93	625.47	676.12	726.87	777.73	.46
.48	424.78	475.09	525.47	575.94	626.49	677.13	727.89	778.75	.48
.50	425.79	476.10	526.48	576.95	627.50	678.15	728.90	779.77	.50
.52	426.79	477.10	527.49	577.96	628.51	679.16	729.92	780.79	.52
-54	427.80	478.11	528.50	578.97	629.52	680.18	730.94	781.81	-54
.56	428.80	479.12	529.51	579.98	630.54	681.19	731.95	782.83	.56
.58	429.81	480.13	530.51	580.99	631.55	682.21	732.97	783.85	.58
.60	430.81	481.13	531.52	582.00	632.56	683.22	733.99	784.86	.60
.62	431.82	482.14	532.53	583.01	633.57	684.23	735.00	785.88	.62
.64	432.83	483.15	533.54	584.02	634.58	685.25	736.02	786.90	.64
.66	433.83	484.15	534.55	585.03	635.60	686.26	737.03	787.92	.66
.68	434.84	485.16	535.56	586.04	636.61	687.28	738.05	788.94	.68
.70	435.84	486.17	536.57	587.05	637.62	688.29	739.07	789.96	.70
.72	436.85	487.18	537.57	588.06	638.63	689.31	740.08	790.98	.72
.74	437.85	488.18	538.58	589.07	639.65	690.32	741.10	792.00	-74
.76 .78	438.86	489.19	539.59	590.08	640.66	691.33	742.12	793.02	.76
80	439.87	490.20	540.60	591.09		692.35	743.13	794.04	
	440.87	491.20	541.61	592.10	642.68	693.36	744.15	795.05	.80
.82	441.88	492.21	542.62	593.11	643.70	694.38	745.17	796.07	.82
.84	442.88	493.22	543.63	594.12	644.71	695.39	746.19	797.09	.84
	443.89	494.23	544.64	595.13	645.72	696.41	747.20	798.11	
.88	444.90	495.23	545.65	596.14	646.73	697.42	748.22	799.13	.88
.90	445.90 446.91	496.24	546.66	597.16	647.75	698.44	749.24	800.15	.90
			547.67			699.45	750.25	801.17	.92
.94	447.91	498.26	548.67	599.18	649.77	700.47	751.27	802.19	.94
.96	448.92	499.26	549.68	600.19	650.79	701.48	752.29	803.21	.96
1.00	449.93					702.50	753.31	804.23	1.00
1.00	450.93	501.28	551.70	602.21	652.81	703.51	754.32	805.25	1.00

I	16°	17°	18°	19°	20°	21°	22°	23°	I
.00	805.25	856.30	907.49	958.81	1010.29	1061.93	1113.73	1165.71	.00
.02	806.27	857.32	908.51	959.84	1011.32	1062.96	1114.77	1166.75	.02
.04	807.29	858.35	909.54	960.87	1012.35	1064.00	1115.81	1167.79	.04
.06	808.31	859.37	910.56	961.90	1013.39	1065.03	1116.85	1168.83	.06
.08	809.33	860.39	911.59	962.93	1014.42	1066.07	1117.88	1169.88	.08
.10	810.35	861.41	912.61	963.96	1015.45	1067.10	1118.92	1170.92	.10
.12	811.37	862.44	913.64	964.98	1016.48	1068.14	1119.96	1171.96	.12
.14	812.39	863.46	914.66	966.or	1017.51	1069.17	1121.00	1173.00	.14
.16	813.41	864.48	915.69	967.04	1018.54	1070.21	1122.04	1174.04	.16
.18	814.43	865.51	916.72	968.07	1019.58	1071.24	1123.07	1175.09	.18
.20	815.45	866.53	917.74	969.10	1020.61	1072.27	1124.11	1176.13	.20
.22	816.47	867.55	918.77	970.13	1021.64	1073.31	1125.15	1177.17	.22
.24	817.49	868.57	919.79	971.16	1022.67	1074.35	1126.19	1178.21	.24
.26	818.51	869.60	920.82	972.19	1023.70	1075.38	1127.23	1179.25	.26
.28	819.53	870.62	921.84	973.21	1024.73	1076.42	1128.27	1180.30	.28
.30	820.55	871.64	922.87	974.24	1025.77	1077.45	1129.31	1181.34	.30
.32	821.57	872.67	923.90	975.27	1026.80	1078.49	1130.35	1182.38	.32
-34	822.59	873.69	924.92	976.30	1027.83	1079.52	1131.38	1183.43	-34
.36	823.61	874.71	925.95	977.33	1028.86	1080.56	1132.42	1184.47	.36
.38	824.63	875.74	926.97	978.36	1029.89	1081.59	1133.46	1185.51	.38
.40	825.66	876.76	928.00	979.39	1030.93	1082.63	1134.50	1186.55	.40
.42	826.68	877.78	929.03	980.42	1031.96	1083.66	1135.54	1187.60	.42
-44	827.70	878.81	930.05	981.45	1032.99	1084.70	1136.58	1188.64	-44
.46	828.72	879.83	931.08	982.48	1034.02	1085.74	1137.62	1189.68	.46
.48	829.74	880.85	932.11	983.50	1035.06	1086.77	1138.66	1190.73	.48
.50	830.76	881.88	933.13	984.53	1036.09	1087.81	1139.70	1191.77	.50
.52	831.78	882.90	934.16	985.56	1037.12	1088.84	1140.74	1192.81	.52
-54	832.80	883.92	935.19	986.59	1038.16	1089.88	1141.78	1193.86	-54
.56	833.82	884.95	936.21	987.62	1039.19	1090.92	1142.82	1194.90	.56
.58	834.84	885.97	937.24	988.65	1040.22	1091.95	1143.86	1195.94	.60
.60	835.87	887.00	938.27	989.68	1041.25	1092.99	1144.90	1196.99	
.62	836.89	888.02	939.29	990.71	1042.29	1094.03	1145.94	1198.03	.62
.64 .66	837.91 838.93	889.04	940.32	991.74	1043.32	1095.06	1146.98	1199.07	.66
		890.07	941.35	992.77	1044.35				
.68	839.95	891.09	942.37	993.80	1045.39	1097.14	1149.06	1201.16	.68
.70	840.97	892.12	943.40	994.83 995.86	1046.42	1098.17	1151.14	1202.21	.72
.72	841.99	893.14	944-43						
-74	843.02	894.17	945.46	996.89	1048.49	1100.25	1152.18	1204.29	.74
.76 .78	844.04 845.06	895.19	946.48 947.51	997.92 998.95	1049.52	1101.28	1153.22	1205.34	.78
.80	846.08	897.24	947.51	999.98	1051.59	1103.36	1155.30	1207.43	.80
					1052.62	1104.39	1156.34	1208.47	.82
.82 .84	847.10 848.12	898.26 899.29	949.57	1001.01	1052.02	1104.39	1157.38	1209.52	.84
.86	849.15	900.31	950.59 951.62	1002.04	1054.69	1106.47	1158.42	1210.56	.86
.88	850.17	901.34	952.65	1004.11	1055.72	1107.51	1159.46	1211.60	.88
.90	851.19	901.34	952.05	1004.11	1056.76	1107.31	1160.50	1212.65	.90
.92	852.21	903.39	954.70	1006.17	1057.79	1109.58	1161.55	1213.69	.92
.94	853.24	904.41	955.73	1007.20	1058.83	1110.62	1162.59	1214.74	.94
.96	854.26	905.44	956.76	1007.20	1059.86	1111.66	1163.63	1215.78	.96
.98	855.28	906.46	957.79	1009.26	1060.89	1112.69	1164.67	1216.83	.98
1.00	856.30	907.49	958.81	1010.29	1061.93	1113.73	1165.71	1217.87	1.00
	307					-			_

TABLE II. — (Continued)

I	24°	25°	26°	27°	28°	29°	30°	31*	I
.00	1217.87	1270.23	1322.79	1375.57	1428.56	1481.79	1535.25	1588.97	.00
.0:	1218.92	1271.28	1323.85	1376.62	1429.62	1482.86	1536.33	1590.05	.02
.0.		1272.33	1324.90	1377.68	1430.69	1483.92	1537.40	1591.13	.04
.00	1221.01	1273.38	1325.95	1378.74	1431.75	1484.99	1538.47	1592.20	.06
.0	1222.06	1274.43	1327.01	1379.80	1432.81	1486.06	1539.54	1593.28	.08
.10	1	1275.48	1328.06	1380.86	1433.87	1487.12	1540.62	1594.36	.10
.1:	-	1276.53	1329.12	1381.91	1434.94	1488.19	1541.69	1595.44	.12
.1.	1225.19	1277.58	1330.17	1382.97	1436.00	1489.26	1542.76	1596.51	.14
.10		1278.63	1331.22	1384.03	1437.06	1490.33	1543.83	1597.59	.16
.1		1279.68	1332.28	1385.09	1438.13	1491.39	1544.91	1598.67	.18
.20		1280.73	1333.33	1386.15	1439.19	1492.46	1545.98	1599.75	.20
.23		1281.78	1334.39	1387.21	1440.25	1493.53	1547.05	1600.82	.22
.24		1282.83	1335.44	1388.27	1441.32	1494.60	1548.12	1601.90	.24
.20		1283.88	1336.50	1389.32	1442.38	1495.67	1549.20	1602.98	.26
.28	1	1284.93	1337.55	1390.38	1443.44	1496.73	1550.27	1604.06	.28
.30		1285.98	1338.60	1391.44	1444.51	1497.80	1551.34	1605.14	.30
.3:		1287.03	1339.66	1392.50	1445.57	1498.87	1552.42	1606.22	.32
.3		1288.08	1340.71	1393.56	1446.63	1499.94	1553.49	1607.30	.34
.3		1289.13	1341.77	1394.62	1447.70	1501.01	1554.56	1608.37	.36
.3		1290.18	1342.82	1395.68	1448.76	1502.08	1555.64	1609.45	.38
.40		1291.23	1343.88	1396.74	1449.82	1503.15	1556.71	1610.53	.40
.4:		1292.28	1344.93	1397.80	1450.89	1504.21	1557.79	1611.61	.42
.4		1293.33	1345.99	1398.86	1451.95	1505.28	1558.86	1612.69	.44
.40		1294.39	1347.04	1399.92	1453.02	1506.35	1559.93	1613.77	.46
.4	1242.98	1295.44	1348.10	1400.98	1454.08	1507.42	1561.01	1614.85	.48
-5		1296.49	1349.15	1402.04	1455.15	1508.49	1562.08	1615.93	.50
.5	1245.08	1297.54	1350.21	1403.10	1456.21	1509.56	1563.16	1617.01	.52
-54	1246.12	1298.59	1351.26	1404.16	1457.27	1510.63	1564.23	1618.09	.54
.5	1247.17	1299.64	1352.32	1405.22	1458.34	1511.70	1565.31	1619.17	.56
.5	1248.22	1300.69	1353.38	1406.28	1459.40	1512.77	1566.38	1620.25	.58
.6	1249.27	1301.74	1354.43	1407.34	1460.47	1513.84	1567.46	1621.33	.60
.6:	1250.31	1302.80	1355.49	1408.40	1461.53	1514.91	1568.53	1622.41	.62
.6.	1251.36	1303.85	1356.54	1409.46	1462.60	1515.98	1569.60	1623.49	.64
.6	1252.41	1304.90	1357.60	1410.52	1463.66	1517.05	1570.68	1624.57	.66
.6	1253.46	1305.95	1358.66	1411.58	1464.73	1518.12	1571.76	1625.65	.68
.79	1254.50	1307.00	1359.71	1412.64	1465.80	1519.19	1572.83	1626.73	.70
.73	1255.55	1308.06	1360.77	1413.70	1466.86	1520.26	1573.91	1627.81	.72
.74	1256.60	1309.11	1361.83	1414.76	1467.93	1521.33	1574.98	1628.89	.74
.7		1310.16	1362.88	1415.82	1468.99	1522.40	1576.06	1629.97	.76
.78		1311.21	1363.94	1416.88	1470.06	1523.47	1577.13	1631.05	.78
.80	1259.75	1312.27	1365.00	1417.94	1471.12	1524.54	1578.21	1632.14	.80
.8:		1313.32	1366.05	1418.01	1472.19	1525.61	1579.28	1633.21	.82
.8.		1314.37	1367.11	1420.07	1473.26	1526.68	1580.36	1634.30	.84 .86
.80		1315.42	1368.17	1421.13	1474.32	1527.76	1581.44	1635.38	
.88		1316.48	1369.22	1422.19	1475.39	1528.83	1582.51	1636.46	.88
.90		1317.53	1370.28	1423.25	1476.45	1529.90	1583.59	1637.54 1638.62	.90
.9:		1318.58	1371.34	1424.31	1477.52	1530.97	1584.67	•	.92
.9.		1319.63	1372.39	1425.38	1478.59	1532.04	1585.74	1639.70	.94
.9		1320.69	1373.45	1426.44	1479.66	1533.11	1586.82	1640.79 1641.87	.96 .98
.9		1321.74	1374.51	1427.50					1.00
1.0	1270.23	1322.79	1375.57	1428.56	1481.79	1535.25	1588.97	1642.95	1.00

TABLE II. — (Continued)

I	32°	33°	34°	35°	36°	37°	38°	39°	I
.00		1697.20	1751.73	1806.55	1861.68	1917.11	1972.88	2028.98	.00
.02	1644.04	1698.29	1752.82	1807.65	1862.78	1918.23	1974.00	2030.10	.02
.04		1699.37	1753.92	1808.75	1863.89	1919.34	1975.11	2031.23	.04
.06		1700.46	1755.01	1809.85	1864.99	1920.45	1976.23	2032.35	.06
.08	1647.28	1701.55	1756.10	1810.95	1866.10	1921.56	1977.35	2033.48	.08
.10		1702.64	1757.20	1812.05	1867.21	1922.68	1978.47	2034.60	.10
.12	1649.45	1703.73	1758.29	1813.15	1868.31	1923.79	1979.59	2035.73	.12
.14		1704.82	1759.39	1814.25	1869.42	1924.90	1980.71	2036.86	.14
.16		1705.91	1760.48	1815.35	1870.53	1926.01	1981.83	2037.98	.16
.18	1652.70	1706.99	1761.58	1816.45	1871.63	1927.13	1982.95	2039.11	18
.20	1653.78	1708.08	1762.67	1817.55	1872.74	1928.24	1984.07	2040.24	.20
.22	1654.86	1709.17	1763.77	1818.65	1873.85	1929.35	1985.19	2041.36	.22
.24	1655.95	1710.26	1764.86	1819.75	1874.95	1930.47	1986.31	2042.49	.24
.26	1657.03	1711.35	1765.95	1820.85	1876.06	1931.58	1987.43	2043.62	.26
.28	1658.11	1712.44	1767.05	1821.96	1877.17	1932.69	1988.55	2044.74	.28
.30	1659.20 1660.28	1713.53	1768.14	1823.06	1878.27	1933.81	1989.67	2045.87	.30
.32		1714.62	1769.24	1824.16	1879.38	1934.92	1990.79	2047.00	.32
-34	1661.36	1715.71	1770.34	1825.26	1880.49	1936.04	1991.91	2048.13	-34
.36 .38	1662.45 1663.53	1716.80	1771.43 1772.53	1826.36 1827.46	1881.60	1937.15	1993.03	2049.26	.36
.40	1664.62						1994.15	2050.38	.38
		1718.98	1773.62	1828.56	1883.81	1939.38	1995.28	2051.51	.40
.42	1665.70 1666.79	1720.07	1774.72	1829.67	1884.92	1940.49	1996.40	2052.64	.42
.44 .46	1667.87	1721.10	1775.81	1830.77 1831.87	1886.03	1941.61	1997.52	2053.77	.44 .46
.48	1668.96		-		1888.25			-	
.50	1670.04	1723.34 1724.43	1778.00	1832.97 1834.08	1889.36	1943.84	1999.76	2056.03	.48
.52	1671.13	1725.52	1780.20	1835.18	1890.46	1946.07	2002.01	2058.38	.52
.54	1672.21	1726.61	1781.30	1836.28	1891.57	1947.18	2003.13	2059.41	
.56	1673.30	1727.70	1782.39	1837.38	1892.68	1947.10	2004.25	2060.54	.54 .56
.58	1674.38	1728.79	1783.49	1838.49	1893.79	1949.42	2005.37	2061.67	.58
.60	1675.47	1729.88	1784.59	1839.59	1894.90	1950.53	2006.49	2062.80	.60
.62	1676.55	1730.97	1785.68	1840.69	1896.01	1951.65	2007.62	2063.93	.62
.64	1677.64	1732.07	1786.78	1841.80	1897.12	1952.76	2008.74	2065.06	.64
.66	1678.72	1733.16	1787.88	1842.90	1898.23	1953.88	2009.86	2066.19	.66
.68	1679.81	1734.25	1788.98	1844.00	1899.34	1955.00	2010.99	2067.32	.68
.70	1680.90	1735.34	1790.07	1845.11	1900.45	1956.12	2012.11	2068.45	.70
.72	1681.98	1736.43	1791.17	1846.21	1901.56	1957.23	2013.23	2069.58	.72
.74	1683.07	1737.52	1792.27	1847.31	1902.67	1958.35	2014.36	2070.71	.74
.76	1684.15	1738.62	1793.37	1848.42	1903.78	1959.47	2015.48	2071.84	.76
.78	1685.24	1739.71	1794.46	1849.52	1904.89	1960.58	2016.60	2072.97	.78
.80	1686.33	1740.80	1795.56	1850.63	1906.00	1961.70	2017.73	2074.10	.80
.82	1687.41	1741.89	1796.66	1851.73	1907.11	1962.82	2018.85	2075.24	.82
.84 .86	1688.50	1742.99	1797.76	1852.84 1853.94	1908.22	1963.93	2019.98	2076.37	.84 .86
.88	1690.67	1745.17	1799.96	1855.04		1966.17			.88
.00	1691.76	1745.17	1801.06	1856.15	1910.44	1967.28	2022.22	2078.63	.90
.92	1692.85	1747.36	1802.15	1857.25	1911.30	1968.40	2023.35	2080.89	.90
.94	1693.94	1748.45	1803.25	1858.36	1913.78	1969.52	2025.60	2082.03	.94
.96	1695.02	1749.54	1804.35	1859.46	1913.70	1909.52	2025.00	2082.03	.96
.98	1696.11	1750.64	1805.45	1860.57	1916.00	1971.76	2027.85	2084.29	.98
1.00	1697.20	1751.73	1806.55	1861.68	1917.11	1972.88	2028.98	2085.42	1.00

TABLE II. — (Continued)

I	40°	41°	42°	43°	44°	45°	46°	47°	I
_		-							-1
.00			2199.41	2256.97	2314.93	2373.30	2432.09		
.02	1	2143.37	2200.55	2258.12	2316.09	2374.47	2433.27	2492.5I 2493.70	
.06		2145.65	2202.85	2260.44	2318.42	2376.81	2435.63	2494.89	
.08	1	2146.79	2204.00	2261.59	2319.58	2377.99	2436.71	2496.08	
.10		2147.93	2205.15	2262.75	2320.75	2379.16	2438.00	2497.27	
.12		2149.07	2206.29	2263.90	2321.91	2380.33	2439.18	2498.46	
.14	2093.35	2150.21	2207.44	2265.06	2323.08	2381.50	2440.36	2499.65	.14
.16	2094.49	2151.35	2208.59	2266.22	2324.24	2382.68	2441.54	2500.84	.16
.18	2095.62	2152.49	2209.74	2267.37	2325.40	2383.85	2442.72	2502.03	.18
.20	2096.75	2153.63	2210.89	2268.53	2326.57	2385.02	2443.90	2503.22	.20
.22		2154.78	2212.04	2269.69	2327.73	2386.20	2445.08	2504.41	.22
.24	2099.02	2155.92	2213.19	2270.84	2328.90	2387.37	2446.27	2505.60	.24
.26		2157.06	2214.33	2272.00	2330.06	2388.54	2447.45	2506.80	.26
.28		2158.20	2215.48	2273.16	2331.23	2389.72	2448.63	2507.99	.28
.30	2102.43 2103.56	2159.34	2216.63	2274.3I 2275.47	2332.40 2333.56	2390.89	2449.82 2451.00	2509.18 2510.37	.30
								1	.32
.34	2104.70	2161.63	2218.93	2276.63	2334.73 2335.89	2393.24 2394.4I	2452.18 2453.36	2511.56 2512.75	-34
.38	2106.97	2163.91	2221.23	2278.95	2337.06	2395.59	2454.55	2513.95	.36
.40	2108.10	2165.05	2222.38	2280.10	2338.23	2396.76	2455.73	2515.14	.40
.42	2109.24	2166,20	2223.53	2281.26	2339.39	2397.94	2456.91	2516.33	.42
.44	2110.37	2167.34	2224.68	2282.42	2340.56	2399.11	2458.10	2517.53	.44
.46	2111.51	2168.48	2225.84	2283.58	2341.73	2400.29	2459.28	2518.72	.46
.48	2112.64	2169.63	2226.99	2284.74	2342.89	2401.47	2460.47	2519.91	.48
.50	2113.78	2170.77	2228.14	2285.90	2344.06	2402.64	2461.65	2521.11	.50
.52	2114.92	2171.91	2229.29	2287.06	2345.23	2403.82	2462.84	2522.30	.52
.54	2116.05	2173.06	2230.44	2288.22	2346.40	2404.99	2464.02	2523.49	-54
.56	2117.19	2174.20	2231.59	2289.38	2347.56	2406.17	2465.21	2524.69	.56
.58	2118.32	2175.34	2232.74	2290.54	2348.73	2407.35	2466.39	2525.88	.58
60	2119.46	2176.49	2233.90	2291.70	2349.90	2408.52	2467.58	2527.08	.60
.62	2120.60	2177.63	2235.05	2292.86	2351.07	2409.70	2468.76	2528.27	.62
.64 .66	2121.74	2178.78 2179.92	2236.20 2237.35	2294.02 2295.18	2352.24	2410.88 2412.05	2469.95	2529.47	.64
.68					2353.41		2471.13	2530.66	.66
.70	2124.01 2125.15	2181.07	2238.5I 2239.66	2296.34 2297.50	2354.58 2355.74	2413.23 2414.41	2472.32 2473.5I	2531.86 2533.05	.68
.72	2126.29	2183.36	2240.81	2298.66	2356.91	2415.59	2474.69	2534.25	.70 .72
.74	2127.42	2184.50	2241.97	2299.82	2358.08	2416.76	2475.88	2535.44	
.76	2128.56	2185.65	2243.12	2300.98	2359.25	2417.94	2477.07	2536.64	.74 .76
.78	2129.70	2186.79	2244.27	2302.14	2360.42	2419.12	2478.25	2537.83	.78
.80	2130.84	2187.94	2245.43	2303.30	2361.59	2420.30	2479.44	2539.03	.80
.82	2131.98	2189.09	2246.58	2304.47	2362.76	2421.48	2480.63	2540.23	.82
.84	2133.11	2190.23	2247.73	2305.63	2363.93	2422.66	2481.82	2541.43	.84
.86	2134.25	2191.38	2248.89	2306.79	2365.10	2423.84	2483.00	2542.62	.86
.88	2135.39	2192.52	2250.04	2307.95	2366.27	2425.01	2484.19	2543.82	.88
.90	2136.53	2193.67	2251.20	2309.12	2367.44	2426.19	2485.38	2545.02	.90
.92	2137.67	2194.82	2252.35	2310.28	2368.61	2427.37	2486.57	2546.21	.92
.94	2138.81	2195.97	2253.50	2311.44	2369.78	2428.55	2487.76	2547.41	.94
.96 .98	2139.95	2197.11	2254.66	2312.60 23 ¹ 3.77	2370.96	2429.73	2488.95	2548.61	.96
1.00	2142.23				2372.13	2430.91	2490.13	2549.81	.98
2.00	2142.23	2199.41	2256.97	2314.93	2373.30	2432.09	2491.32	2551.00	1.00

TABLE II. — (Continued)

I	48°	49°	50°	51°	52°	53°	54°	55°	I
.00	2551.00	2611.15	2671.78	2732.90	2794.54	2856.70	2919.40	2982.67	.00
.02	2552.20	2612.36	2672.99	2734.13	2795.77	2857.95	2920.66	2983.94	.02
.04	2553.40	2613.57	2674.21	2735.36	2797.01	2859.20	2921.92	2985.21	.04
.06	2554.60	2614.78	2675.43	2736.59	2798.25	2860.44	2923.18	2986.48	.06
.08	2555.80	2615.98	2676.65	2737.81	2799.49	2861.69	2924.44	2987.75	.08
.10	2557.00	2617.19	2677.86	2739.04	2800.73	2862.94	2925.70	2989.02	.10
.12	2558.20	2618.40	2679.09	2740.27	2801.97	2864.19	2926.96	2990.30	.12
.14	2559.40	2619.61	2680.31	2741.50	2803.21	2865.44	2928.23	2991.57	.14
.16	2560.60	2620.82	2681.53	2742.73	2804.45	2866.69	2929.49	2992.84	.16
.18	2561.80	2622.03	2682.74	2743.96	2805.69	2867.94	2930.75	2994.12	.18
.20	2563.00	2623.24	2683.96	2745.19	2806.93	2869.20	2932.01	2995.39	.20
.22	2564.20	2624.45	2685.18	2746.42	2808.17	2870.45	2933.27	2996.66	.22
.24	2565.40	2625.66	2686.40	2747.65	2809.41	2871.70	2934.53	2997.94	.24
.26	2566.60	2626.87	2687.62	2748.88	2810.65	2872.95	2935.80	2999.21	.26
.28	2567.80	2628.08	2688.84	2750.11	2811.89	2874.20	2937.06	3000.48	.28
.30	2569.00	2629.29	2690.06	2751.34	2813.13	2875.45	2938.32	3001.76	.30
.32	2570.20	2630.50	2691.28	2752.57	2814.37	2876.70	2939.59	3003.03	.32
.34	2571.40	2631.71	2692.50	2753.80	2815.61	2877.96	2940.85	3004.31	.34
.36	2572.60	2632.92	2693.73	2755.03	2816.85	2879.21	2942.11	3005.58	.36
.38	2573.80	2634.13	2694.95	2756.26	2818.10	2880.46	2943.38	3006.86	.38
.40	2575.01	2635.34	2696.17	2757.49	2819.34	2881.71	2944.64	3008.13	.40
.42	2576.21	2636.56	2697.39	2758.73	2820.58	2882.97	2945.90	3009.41	.42
-44	2577.41	2637.77	2698.61	2759.96	2821.82	2884.22	2947.17	3010.63	-44
.46	2578.61	2638.99	2699.83	2761.19	2823.06	2885.47	2948.43	3011.96	.46
.48	2579.82	2640.19	2701.06	2762.42	2824.3I	2886.73	2949.70	3013.24	.48
.50	2581.02	2641.40	2702.28	2763:65	2825.55	2887.98	2950.96	3014.51	.50
.52	2582.22	2642.62	2703.50	2764.89	2826.79	2889.24	2952.23	3015.79	.52
-54	2583.43	2643.83	2704.72	2766.12	2828.04	2890.49	2953.49	3017.07	.54
.56	2584.63	2645.04	2705.95	2767.35	2829.29	2891.74	2954.76	3018.35	.56
.58	2585.83	2646.26	2707.17	2768.59	2830.52	2893.00	2956.03	3019.62	.58
.60	2587.04	2647.47	2708.39	2769.82	2831.77	2894.26	2957.29	3020.90	.60
.62	2588.24	2648.68	2709.62	2771.05	2833.01	2895.51	2958.56	3022.18	.62
.64	2589.44	2649.90	2710.84	2772.29	2834.26	2896.77	2959.83	3023.46	.64
.66	2590.65	2651.11	2712.06	2773.52	2835.50	2898.02	2961.09	3024.74	.66
.68	2591.85	2652.33	2713.29	2774.76	2836.75	2899.28	2962.36	3026.02	.68
.70	2593.06	2653.54	2714.51	2775.99	2837.99	2900.53	2963.63	3027.29	.70
.72	2594.26	2654.76	2715.74	2777.23	2839.24	2901.79	2964.90	3028.57	.72
.74	2595 . 47	2655.97	2716.96	2778.46	2840.48	2903.05	2966.16	3029.85	.74
.76	2596.67	2657.18	2718.19	2779.70	2841.73	2904.30	2967.43	3031.13	.76
.78	2597.88	2658.40	2719.41	2780.93	2842.98	2905.56	2968.70	3032.41	.78
.80	2599.08	2659.62	2720.64	2782.17	2844.22	2906.82	2969.97	3033.69	.80
.82	2600.29	2660.83	2721.86	2783.41	2845.47	2908.07	2971.24	3034.97	.82
.86	2601.50 2602.70	2662.05 2663.26	2723.09 2724.32	2784.64 2785.88	2846.72 2847.96	2909.33 2910.59	2972.5I 2973.78	3036.25 3037.54	.86
.88	2603.91	2664.48	2725.54	2787.11	2849.21 2850.46	2911.85	2975.05	3038.82	.88
.90	2605.12 2606.32	2665.69 2666.91	2726.77 2727.99	2788.35 2789.59	2851.71	2913.11 2914.37	2976.31 2977.58	3040.10	.90
	-								_
.94	2607.53	2668.13	2729.22	2790.82	2852.95	2915.63	2978.86	3042.66	.94 .96
.96 .98	2608.74 2609.94	2669.34 2670.56	2730.45 2731.68	2792.06 2793.30	2854.20 2855.45	2916.88 2918.14	2980.13 2981.48	3043.94 3045.23	.98
1.00	2611.15	2671.78						3045.23	1.00
1.00	2011.15	20/1.78	2732.90	2794.54	2856.70	2919.40	2982.67	3040.51	1.00

TABLE II. — (Continued)

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L	I	56°	57°	58°	59°	60°	61°	62°	63°	I
	.00	3046.51	3110.95	3176.00	3241.68	3308.01	3375.02	3442.72	3511.14	.00
н	.02	3047.79	3112.24	3177.30	3243.00	3309.35	3376.37	3444.08	3512.51	.02
	.04	3049.07	3113.54	3178.61	3244.32	3310.38	3377.72	3445.44	3513.88	.04
	.06	3050.36	3114.83	3179.92	3245.64	3312.02	3379.06	3446.81	3415.26	.06
	.08	3051.64	3116.13	3181.23	3246.96	3313.35	3380.41	3448.17	3516.64	.08
	10	3052.92	3117.42	3182.54	3248.28	3314.69	3381.76	3449.53	3518.02	.10
1	12	3054.21	3118.72	3183.85	3249.61	3316.02	3383.11	3450.89	3519.39	.12
	14	3055.49	3120.02	3185.15	3250.93	3317.36	3384.46	3452.26	3520.77	.14
	16	3056.78 3058.06	3121.31 3122.61	3186.46 3187.77	3252.25 3253.57	3318.69 3320.03	3385.81 3387.16	3453.62 3454.98	3522.15	.16 .18
	20			3189.08	3254.89	3321.36	3388.51		3523.53	.20
		3059.35	3123.91					3456.35	3524.90	
	22	3060.63	3125.20 3126.50	3190.39 3191.70	3256.22 3257.54	3322.70 3324.03	3389.85 3391.21	3457.71 3459.07	3526.28 3527.66	.22
	24	3061.92 3063.20	3127.80	3193.01	3258.86	3325.37	3392.56	3460.44	3529.04	.24
	28		3129.10	3194.32	3260.19	3326.71	3393.91	3461.80	3530.42	.28
	30	3064.49 3065.78	3129.10	3194.32	3261.51	3328.05	3395.26	3463.17	3530.42	.30
	32	3067.06	3131.69	3196.95	3262.83	3329.38	3396.61	3464.53	3533.18	.32
	34	3068.35	3132.99	3198.26	3264.16	3330.72	3397.97	3465.90	3534.56	.34
	36	3069.64	3134.29	3199.57	3265.48	3332.06	3399.31	3467.27	3535.94	.36
	38	3070.92	3135.59	3200,88	3266.81	3333.40	3400.66	3468.63	3537.32	.38
I.	40	3072.21	3136.89	3202.19	3268.14	3334.74	3402.02	3470.00	3538.70	.40
I.	42	3073.50	3138.19	3203.51	3269.46	3336.08	3403.37	3471.37	3540.09	.42
	44	3074.79	3139.49	3204.82	3270.79	3337.41	3404.72	3472.73	3541.47	.44
ŀ	46	3076.08	3140.79	3206.13	3272.11	3338.75	3406.08	3474.10	3542.85	.46
١.	48	3077.36	3142.09	3207.44	3273.44	3340.09	3407.43	3475.47	3544.23	.48
	50	3078.65	3143.39	3208.76	3274.76	3341.43	3408.78	3476.84	3545.62	.50
Ŀ	52	3079.94	3144.69	3210.07	3276.09	3342.77	3410.14	3478.20	3547.00	.52
	54	3081.23	3146.00	3211.39	3277.42	3344.11	3411.49	3479.57	3548.38	-54
	56	3082.52	3147.30	3212.70	3278.75	3345.46	3412.85	3480.94	3549.76	.56
	58	3083.81	3148.60	3214.01	3280.07	3346.80	3414.20	3482.31	3551.15	.58
	60	3085.10	3149.90	3215.33	3281.40	3348.14	3415.56	3483.68	3552.53	.60
	62	3086.39	3151.20	3216.64	3282.73	3349.48	3416.91	3485.05	3553.92	.62
	64 66	3087.68 3088.97	3152.51 3153.81	3217.96 3219.27	3284.06 3285.39	3350.82 3352.16	3418,27 3419.62	3486.42 3487.79	3555.30 3556.69	.64 .66
	68				3286.72					.68
	70	3090.26 3091.55	3155.11 3156.42	3220.59 3221.91	3288.04	3353.51 3354.85	3420.98 3422.34	3489.16 3490.53	3558.07 3559.46	.70
	72	3092.84	3157.72	3223.22	3289.37	3356.19	3423.69	3491.90	3560.84	.72
	74	3094.13	3159.02	3224.54	3290.70	3357.53	3425.05	3493.27	3562.23	.74
	76	3095.43	3160.33	3225.86	3292.03	3358.88	3426.41	3494.65	3563.62	.76
L	78	3096.72	3161.64	3227.17	3293.36	3360.22	3427.77	3496.02	3565.01	.78
L	80	3098.01	3162.94	3228.49	3294.69	3361.57	3429.12	3497.39	3566.39	.80
L.	82	3099.30	3164.24	3229.81	3296.03	3362.91	3430.48	3498.77	3567.78	.82
	84	3100.60	3165.55	3231.13	3297.36	3364.26	3431.84	3500.14	3569.17	.84
	.86	3101.89	3166.85	3232.45	3298.69	3365.60	3433.20	3501.51	3570.56	.86
	88	3103.18	3168.16	3233.76	3300.02	3366.94	3434.57	3502.89	3571.95	.88
	.90	3104.48	3169.46	3235.08	3301.35	3368.29	3435.92	3504.26	3573.33	.90
	.92	3105.77	3170.77	3236.40	3302.68	3369.64	3437.28	3505.63	3574.72	.92
	.94	3107.06	3172.08	3237.72	3304.02	3370.98	3438.64	3507.01	3576.11	.94
	.96 .98	3108.36	3173.38 3174.69	3239.04 3240.36	3305.35 3306.68	3372.33 3373.67	3440.00 3441.36	3508.38 3509.76	3577.50 3578.89	.96 .98
	.00	3109.65	3174.09	3241.68	3308.0I	3375.02	3442.72	3511.14	3580.28	1.00
Ľ	.00	3110.95	3170.00	3241.08	3300.01	33/3.02	3442.72	3311.14	3500.28	1.00

TABLE II. — (Continued)

. 1			660	C 0	600	C . 0	0	0	
I	64°	65°	66°	67°	68°	69°	70°	71°	I
.00	3580.28	3650.19	3720.88	3792.37	3864.70	3937.88	4011.94	4086.92	.00
.02	3581.67	3651.60	3722.30	3793.81	3866.15 3867.61	3939.35	4013.43	4088.43	.02
.04	3583.06 3584.46	3653.00 3654.41	3723.72 3725.15	3795.25 3796.69	3869.06	3940.82 3942.30	4014.93 4016.42	4089.94	.04
					3870.52				
.08	3585.85 3587.24	3655.82 3657.22	3726.57 3727.99	3798.13 3799.57	3871.98	3943.77 3945.25	4017.91	4092.96 4094.47	.08
.12	3588.63	3658.63	3729.41	3801.01	3873.43	3946.72	4020.89	4095.98	.12
.14	3590.02	3660.04	3730.84	3802.45	3874.89	3948.19	4022.39	4097.49	.14
.16	3591.42	3661.45	3732.26	3803.89	3876.35	3949.67	4023.88	4099.00	.16
.18	3592.81	3662 86	3733.69	3805.33	3877.81	3951.15	4025.37	4100.51	.18
.20	3594.20	3664.26	3735.11	3806.77	3879.27	3952.62	4026.86	4102.03	.20
.22	3595.60	3665.67	3736.54	3808.21	3880.72	3954.10	4028.36	4103.54	.22
.24	3596.99	3667.08	3737.96	3809.65	3882.18	3955.57	4029.85	4105.05	.24
.26	3598.39	3668.49	3739 - 39	3811.10	3883.67	3957.05	4031.35	4106.57	.26
.28	3599.78	3669.88	3740.81	3812.54	3885.10	3958.53	4032.84	4108.08	.28
.30	3601.17	3671.3 1	3742.24	3813.98	3886.56	3960.00	4034.34	4109.59	.30
.32	3602.57	3672.72	3743.67	3815.42	3888.02	3961.48	4035.84	4111.11	.32
.34	3603.96	3674.13	3745.09	3816.87	3889.48	3962.96	4037.33	4112.62	-34
.36	3605.36	3675.55	3746.52	3818.31	3890.94	3964.44	4038.83	4114.14	.36
.38	3606.76	3676.96	3747.95	3819.76	3892.40	3965.92	4040.33	4115.65	.38
.40	3608.15	3678.37	3749.38	3821.20	3893.87	3967.40	4041.82	4117.17	.40
.42	3609.55	3679.78	3750.81	3822.65	3895.33	3968.88	4043.32	4118.69	.42
.44 .46	3610.95 3612.34	3681.20 3682.61	3752.24 3753.66	3824.09 3825.54	3896.79 3898.25	3970.36 3971.84	4044.82	4I20.20 4I2I.72	.44 .46
							-		
.48 .50	3613.74 3615.14	3684.02 3685.43	3755.09 3756.52	3826.98 3828.43	3899.73 3901.18	3973.32 3974.80	4047.82	4123.24	.48 .50
.52	3616.54	3686.85	3757.95	3829.88	3902.64	3976.28	4050.82	4126.28	.52
.54	3617.94	3688.26	3759.38	3831.32	3904.11	3977.76	4052.32	4127.80	.54
.56	3619.34	3689.68	3760.81	3832.77	3905.57	3977.70	4053.82	4129.31	.56
.58	3620.74	3691.09	3762.24	3834.22	3907.04	3980.73	4055.32	4130.83	.58
.60	3622.14	3692.51	3763.68	3835.67	3908.50	3982.21	4056.82	4132.35	.60
.62	3623.54	3693.92	3765.11	3837.12	3909.97	3983.69	4058.32	4133.87	.62
.64	3624.93	3695.34	3766.54	3838.56	3911.43	3985.18	4059.82	4135.40	.64
.66	3626.34	3696.76	3767.97	3840.01	3912.90	3986.66	4061.32	4136.92	.66
.68	3627.74	3698.17	3769.41	3841.46	3914.37	3988.15	4062.83	4138.44	.68
.70	3629.14	3699.59	3770.84	3842.91	3915.83	3989.63	4064.33	4139.96	.70
.72	3630.54	3701.01	3772.27	3844.36	3917.30	3991.12	4065.83	4141.48	.72
.74	3631.94	3702.42	3773.7I	3845.81	3918.77	3992.60	4067.34	4143.00	.74
.76 .78	3633.34	3703.84 3705.26	3775.14 3776.57	3847.26 3848.71	3920.24	3994.09 3995.57	4068.84	4144.53	.76
.70	3634.74	3706.68	3778.0I	3850.17		3995.57	4071.85	4148.57	.80
.80	3636.15			3851.62	3923.17				.82
.82	3637.55 3638.95	3708.10 3709.52	3779·44 3780.88	3851.02	3924.04	3998.55	4073.36	4149.10	.82
.86	3640.36	3710.93	3782.31	3854.52	3927.58	4001.52	4076.37	4152.15	.86
.88	3641.76	3712.35	3783.75	3855.97	3929.05	4003.01	4077.87	4153.67	.88
.90	3643.16	3713.77	3785.19	3857.43	3930.68	4004.50	4079.38	4155.20	.90
.92	3644.57	3715.19	3786.62	3858.88	3931.99	4005.99	4080.89	4156.73	.92
.94	3645.97	3716.61	3788.06	3860.33	3933.46	4007.48	4082.39	4158.25	.94
.96	3647.38	3718.04	3789.50	3861.79	3934.94	4008.96	4083.90	4159.78	.96
.98	3648.78	3719.46	3790.93	3863.24	3936.41	4010.45	4085.41	4161.31	.98
1.00	3650.19	3720.88	3792.37	3864.70	3937.88	4011.94	4086.92	4162.83	1.00

TABLE II. — (Continued)

I	72°	73°	74°	75°	76°	77°	78°	I
.00	4162.83	4239.72	4317.60	4396.52	4476.50	4557.56	4639.78	.00
.02	4164.36	4241.27	4319.17	4398.11	4478.10	4559.20	4641.44	.02
.04	4165.89	4242.81	4320.74	4399.69	4479.72	4560.84	4643.09	.04
.06	4167.42	4244.36	4322.31	4401.28	4481.33	4562.47	4644.75	. об
.08	4168.95	4245.91	4323.88	4402.87	4482.94	4564.10	4646.41	.08
.10	4170.48	4247.46	4325.45	4404.46	4484.55	4565.74	4648.06	.10
.12	4172.01	4249.01	4327.02	4406.06	4486.16	4567.37	4649.72	.12
.14	4173.54	4250.56	4328.59	4407.65	4487.78	4569.01	4651.38	.14
.16	4175.07	4252.11	4330.16	4409.24	4489.39	4570.65	4653.04	.16
.18	4176.60	4253.66	4331.73	4410.83	4491.01	4572.28	4654.70	.18
.20	4178.13	4255.21	4333.30	4412.42	4492.62	4573.92	4656.36	.20
.22	4179.66	4256.77	4334.87	4414.02	4494.23	4575.56	4658.02	.22
.24	4181.20	4258.32	4336.45	4415.63	4495.85	4577.19	4659.68	.24
.26	4182.73	4259.87	4338.02	4417.21	4497 - 47	4578.83	4661.34	.26
.28	4184.26	4261.42	4339.59	4418.80	4499.09	4580.47	4663.01	.28
.30	4185.80 4187.33	4262.98 4264.53	4340.97	4420.39 4421.99	4500.70	4582.11	4664.67	.30
			4342.74		4502.32	4583.75	4666.33	.32
-34	4188.87	4266.09	4344.32	4423.59	4503.94	4585.39	4668.00	.34
.36	4190.40	4267.64 4269.19	4345.89	4425.18	4505.55	4587.03 4588.67	4669.66	.36 .38
.40			4347 . 47		4507.17		4671.32	
	4193.47	4270.85	4349.04	4428.38	4508.79	4590.31	4672.99	.40
.42	4195.01 4196.54	4272.31	4350.62	4429.97	4510.41	4591.96	4674.65	.42
.46	4198.08	4273.86 4275.42	4352.19 4353.77	4431.57 4433.17	4512.03 4513.65	4593.60 4595.24	4676.32	.44
.48								
.50	4199.62 4201.15	4276.98 4278.53	4355.35 4356.93	4434.77 4436.37	4515.27 4516.89	4596.89 4598.53	4679.65	.48
.52	4202.69	4280.09	4358.51	4430.37	4518.51	4590.53	4682.99	.50
.54	4204.23	4281.65	4360.08	4439.57	4520.14	4601.82	4684.66	
. 56	4204.23	4283.21	4361.66	4439.37	4521.76	4603.47	4686.32	.54
.58	4207.31	4284.77	4363.24	4442.77	4523.38	4605.19	4687.99	.58
.60	4208.85	4286.33	4364.81	4444.37	4525.01	4606.76	4689.67	.60
.62	4210.39	4287.89	4366.40	4445.97	4526.63	4608.40	4691.33	.62
.64	4211.93	4289.45	4367.98	4447.58	4528.25	4610.05	4693.00	.64
.66	4213.47	4291.01	4369.56	4449.18	4529.88	4611.70	4694.68	.66
.68	4215.01	4292.57	4371.15	4450.78	4531.50	4613.35	4696.35	.68
.70	4216.55	4294.13	4372.73	4452.39	4533.13	4614.99	4698.02	.70
.72	4218.09	4295.69	4374.31	4453.99	4534.76	4616.64	4699.69	.72
.74	4219.63	4297.25	4375.90	4455.59	4536.38	4618.29	4701.37	.74
.76	4221.18	4298.82	4377.48	4457.20	4538.01	4619.94	4703.04	.76
.78	4222.72	4300.38	4379.06	4458.81	4539.64	4621.59	4704.71	.78
.80	4224.26	4301.94	4380.65	4460.41	4541.27	4623.24	4706.39	.80
.82	4225.81	4303.51	4382.23	4462.02	4542.89	4624.90	4708.06	.82
.84 .86	4227.35	4305.07	4383.82	4463.62	4544.52	4626.55	4709.74	.84
	4228.90	4306.64	4385.40	4465.23	4546.15	4628.20	4711.41	.86
.88	4230.44	4308.20	4386.99	4466.84	4547.78	4629.85	4713.09	.88
.90	4231.98	4309.77	4388.58	4468.45	4549.41	4631.51	4714.77	.90
	4233.53	4311.33	4390.16	4470.05	4551.04	4633.16	4716.45	.92
.94 .96	4235.08	4312.90	4391.75	4471.66	4552.67	4634.81	4718.12	.94
.98	4236.62 4238.17	4314.46	4393.34	4473.27	4554.31	4636.47 4638.12	4719.80	.96 .98
1.00	4239.72		4394.93	4474.88	4555.94		4721.48	1.00
1.00	4239.72	4317.60	4396.52	4476.50	4557.56	4639.78	4723.16	1.00

TABLE II. — (Continued)

I	79°	80°	81°	82°	83°	84°	85°	I
.00	4723.16	4807.85	4893.58	4980.71	5069.17	5159.00	5250.26	.00
.02	4724.84	4809.45	4895.31	4982.47	5070.95	5160.80	5252.10	.02
.04	4726.52	4811.16	4897.04	4984.22	5072.73	5162.62	5253.94	.04
.06	4728.20	4812.86	4898.78	4985.98	5074.52	5164.43	5255.78	.06
.08	4729.88	4814.57	4900.51	4987.74	5076.30	5166.25	5257.62	.08
.10	4731.56	4816.27	4902.24	4989.49	5078.09	5168.06	5259.46	.10
. 12	4733.25	4817.98	4903.97	4991.25	5079.87	5169.88	5261.30	.12
.14	4734.93	4819.69	4905.70	4993.01	5081.66	5171.69	5263.15	.14
.16	4736.61	4821.40	4907.44	4994.77	5083.45	5173.50	5264.99	.16
.18	4738.29	4823.10	4909.17	4996.53	5085.23	5175.32	5266.84	.18
.20	4739.98	4824.81	4910.90	4998.29	5087.02	5177.14	5268.68	.20
.22	4741.66	4826.52	4912.64	5000.05	5088.81	5178.95	5270.53	.22
.24	4743.35	4828.23	4914.37	5001.82	5090.60	5180.77	5272.38	.24
.26	4745.03	4829.94	4916.11	5003.58	5092.39	5182.59	5274.22	.26
.28	4746.72	4831.65	4917.83	5005.34	5094.18	5184.41	5276.07	.28
.30	4748.41	4833.36	4919.58	5007.10	5095.97	5186.23	5277.92	.30
.32	4750.09	4835.08	4921.32	5008.87	5097.76	5188.05	5279.77	.32
-34	4751.78	4836.79	4923.06	5010.63	5099.55	5189.87	5281.62	.34
.36	4753.47	4838.50	4924.80	5012.40	5101.34	5191.69	5283.47	.36
.38	4755.16	4840.22	4926.54	5014.16	5103.14	5193.51	5285.32	.38
.40	4756.85	4841.93	4928.28	5015.93	5104.93	5195.33	5287.17	.40
.42	4758.54	4843.64	4930.02	5017.70	5106.73	5197.15	5289.02	.42
-44	4760.23	4845.36	4931.76	5019.46	5108.52	5198.98	5290.87	.44
.46	4761.92	4847.08	4933.50	5021.23	5110.32	5200.80	5292.73	.46
.48	4763.61	4848.79	4935.24	5023.00	5112.11	5202.62	5294.58	.48
.50	4765.30	4850.51	4936.98	5024.77	5113.91	5204.45	5296.42	.50
. 52	4766.99	4852.22	4938.73	5026.54	5115.70	5206.27	5298.29	.52
.54	4768.69	4853.94	4940.47	5028.31	5117.50	5208.10	5300.13	.54
. 56	4770.38	4855.66	4942.21	5030.08	5119.30	5209.93	5302.00	.56
. 58	4772.07	4857.38	4943.96	5031.85	5121.10	5211.75	5303.86	.58
.60	4773.76	4859.10	4945.70	5033.62	5122.90	5213.58	5305.71	.60
.62	4775.46	4860.82	4947 - 45	5035.39	5124.70	5215.41	5307.57	.62
.64	4777.15	4862.54	4949.19	5037.17	5126.50	5217.24	5309.43	.64
.66	4778.85	4864.26	4950.94	5038.94	5128.30	5219.07	5311.29	.66
.68	4780.55	4865.98	4952.68	5040.71	5130.10	5220.90	5313.15	.68
.70	4782.24	4867.70	4954 . 43	5042.49	5131.90	5222.73	5315.01	.70
.72	4783.94	4869.42	4956.18	5044.26	5133.70	5224.56	5316.87	.72
.74	4785.64	4871.14	4957 93	5046.04	5135.51	5226.39	5318.73	.74
.76	4787.33	4872.87	4959.68	5047.81	5137.31	5228.22	5320.59	.76
.78	4789.03	4874.59	4961.63	5049.59	5139.12	5230.06	5322.46	.78
.80	4790.73	4876.31	4963.18	5051.37	5140.92	5231.89	5324.32	.80
.82	4792.43	4878.04	4964.93	5053.14	5142.73	5233.72	5326.18	.82
.84	4794.13	4879.76	4966.68	5054.92	5144.53	5235.56	5328.05	.84
.86	4795.83	4881.49	4968.43	5056.70	5146.34	5237.39	5329.91	1
.88	4797.53	4883.22	4970.18	5058.48	5148.15	5239.23	5331.78	.88
.90	4799.23	4884.94	4971.94	5060.26	5149.95	5241.07	5333.65	.90
.92	4800.93	4886.67	4973.69	5062.04	5151.76	5242.90	5335.51	.92
.94	4802.64	4888.40	4975.44	5063.82	5153.57	5244.74	5337.38	.94
.96	4804.34	4890.13	4977.20	5065.60	5155.38	5246.58 5248.42	5339.25	.96
.98	4806.04	4891.85	4978.95	5067.38	5157.19	5240.42	5341.12	1.00
1.00	4807.85	4893.58	4980.71	5069.17	5159.00	5250.20	5342.99	1.00

TABLE II. — (Continued)

I	86°	87°	88°	89°	90°	91°	92°	I
.00	5342.99	5437.24	5533.06	5630.51	5729.65	5830.53	5933.23	.00
.02	5344.85	5439.14	5534.99	5632.48	5731.65	5832.57	5935.30	.02
.04	5346.73	5441.04	5536.92	5634.44	5733.65	5834.61	5937.37	.04
.06	5348.60	5442.94	5538.86	5636.41	5735.65	5836.64	5939 - 45	.06
.08	5350.46	5444.84	5540.79	5638.38	5737.65	5838.68	5941.52	.08
.10	5352.34	5446.75	5542.73	5640.35	5739.66	5840.72	5943.60	.10
.12	5354.21	5448.65	5544.67	5642.32	5741.66	5842.76	5945.67	.12
.14	5356.09	5450.55	5546.60	5644.29	5743.67	5844.80	5947.75	.14
.16	5357.96	5452.46	5548.54	5646.26 5648.23	5745.67 5747.68	5846.84	5949.83	.16
.18	5359.84	5454.37	5550.48				5951.91	.18
.20	5361.71	5456.27	5552.42	5650.20	5749.69	5850.93	5953.99	.20
.22	5363.59	5458.18	5554.36	5652.18	5751.69	5852.97	5956.07	.22
.24	5365.46	5460.09 5462.00	5556.30 5558.24	5654.15 5656.12	5753.70 5755.71	5855.01 5857.05	5958.15 5960.23	.24
	5367.34						1	
.28	5369.22	5463.91 5465.81	5560.18	5658.10	5757.72	5859.10	5962.31	.28
.30	5371.10 5372.98	5405.81	5562.12 5564.06	5660.07 5662.05	5759.73 5761.74	5861.15 5863.20	5964.40	.30
-34	5374.86 5376.74	5469.64 5471.55	5566.01 5567.95	5664.03 5666.00	5763.75 5765.76	5865.24 5867.29	5968.56	-34
.36 .38	5370.74	5471.55	5569.90	5667.98	5767.78	5869.34	5970.65 5972.74	.36 .38
.40	5380.50	5475.37	5571.84	5669.96	5769.79	5871.38	5974.82	.40
.42	5382.38 5384.26	5474.29 5479.20	5573.79 5575.73	5671.94 5673.92	5771.80 5773.82	5873.44 5875.49	5976.91	.42
.46	5386.15	5481.12	5577.68	5675.90	5775.84	5877.54	5981.09	.46
.48	5388.03	5483.03	5579.63	5677.88	5777.85	5879.60	5983.18	.48
.50	5389.92	5484.95	5581.58	5679.87	5777.05	5881.65	5985.27	.50
.52	5391.80	5486.86	5583.53	5681.85	5781.89	5883.71	5987.36	.52
.54	5393.69	5488.78	5585.48	5683.83	5783.91	5885.76	5989.46	-54
.56	5395.57	5490.70	5587.43	5685.82	5785.93	5887.82	5991.55	.56
.58	5397.46	5492.62	5589.38	5687.80	5787.95	5889.87	5993.64	.58
.60	5399.35	5494.54	5591.33	5689.79	5789.97	5891.93	5995.74	.60
.62	5401.24	5496.46	5593.29	5691.78	5791.99	5893.98	5997.83	.62
.64	5403.13	5498.38	5595.24	5693.76	5794.01	5896.05	5999.93	.64
.66	5405.02	5500.30	5597.19	5695.75	5796.03	5898.10	6002.02	.66
.68	5406.91	5502.22	5599.15	5697.74	5798.06	5900.16	6004.12	.68
.70	5408.80	5504.14	5601.10	5699.73	5800.08	5902.23	6006.22	.70
.72	5410.69	5506.07	5603.06	5701.72	5802.11	5904.29	6008.32	.72
.74	5412.58	5507.99	5605.01	5703.71	5804.13	5906.35	6010.42	.74
.76	5414.47	5509.92	5606.97	5705.70	5806.16	5908.41	6012.52	.76
.78	5416.37	5511.84	5608.93	5707.69	5808.19	5910.48	6014.62	.78
.80	5418.26	5513.77	5610.89	5709.68	5810.21	5912.54	6016.72	.80
.82	5420.16	5515.69	5612.85	5711.68	5812.24	5914.61	6018.83	.82
.84 .86	5422.05	5517.62	5614.81	5713.67	5814.27	5916.67	6020.93	.84 .86
	5423.95	5519.55	5616.77	5715.67	5816.30	5918.74	6023.04	
.88	5425.84	5521.48	5618.73	5717.66	5818.33	5920.81	6025.14	.88
.90 .92	5427.74 5429.64	5523.40 5525.33	5620.69 5622.65	5719.66 5721.65	5820.37 5822.40	5922.87	6027.25	.90 .92
						5924.94		
.94 .96	5431.54	5527.26 5529.19	5624.62 5626.58	5723.65 5725.65	5824.43 5826.47	5927.01	6031.46	.94
,98	5433.44 5435.34	5531.13	5628.55	5725.65	5828.50	5929.08 5931.15	6033.57 6035.68	.96 .98
1.00	5437.24	5533.06	5630.51	5729.65	5830.53	5933.23	6037.79	1.00
1.00	3431.24	3333.00	3030.31	3129.03	3030.33	3933.23	0037.79	1.00

TABLE II. — (Continued)

I	93°	94°	95°	96°	97°	98°	99°	I
.00	6037.79	6144.30	6252.82	6363.42	6476.19	6591.21	6708.56	.00
.02	6039.90	6146.45	6255.01	6365.66	6478.47	6593.53	6710.93	.02
.04	6042.01	6148.60	6257.20	6367.89	6480.75	6595.86	6713.30	.04
.06	6044.12	6150.75	6259.39	6370.13	6483.03	6598.18	6715.67	.06
.08	6046.25	6152.90	6261.59	6372.36	6485.31	6600.51	6718.05	.08
.10	6048.35	6155.06	6263.78	6374.60	6487.59	6602.84	6720.42	.IO
.12	6050.47	6157.21	6265.98	6376.84	6489.87	6605.16	6722.80	.12
.14	6052.58	6159.37	6268.16	6379.08	6492.16	6607.49	6725.18	.14
.16	6054.70	6161.52	6270.37	6381.32	6494.44	6609.83	6727.56	.16
.18	6056.82	6163.68	6272.57	6383.56	6496.73	6612.16	6729.93	.18
.20	6058.96	6165.84	6274.77	6385.80	6499.01	6614.49	6732.32	.20
.22	6061.05	6168.00	6276.97	6388.04	6501.30	6616.82	6734.70	.22
.24	6063.17	6170.15	6279.17	6390.29	6503.59	6619.17	6737.08	.24
.26	6065.29	6172.32	6281.37	6392.53	6505.88	6621.49	6739.46	.26
.28	6067.42	6174.48	6283.57	6394.77	6508.17	6623.83	6741.85	.28
.30	6069.55	6176.64	6285.78	6397.02	6510.46	6626.16	6744.23	.30
.32	6071.66	6178.80	6287.98	6399.27	6512.75	6628.50	6746.62	.32
-34	6073.78	6180.96	6290.18	6401.52	6515.04	6630.84	6749.00	.34
.36	6075.91	6183.13	6292.39	6403.76	6517.33	6633.18	6751.39	.36
.38	6078.03	6185.29	6294.60	6406.01	6519.63	6635.52	6753.78	.38
.40	6080.16	6187.46	6296.80	6408.26	6521.92	6637.86	6756.17	.40
.42	6082.28	6189.63	6299.01	6410.52	6524.22	6640.21	6758.56	.42
.44	6084.41	6191.79	6301.22	6412.77	6526.62	6642.55	6760.96	.44
.46	6086.54	6193.96	6303.43	6415.02	6528.81	6644.90	6763.35	.46
.48	6088.67	6196.13	6305.64	6417.28	6531.11	6647.24	6765.74	.48
.50	6090.80	6198.30	6307.85	6419.53	6533.41	6649.59	6768.14	.50
.52	6092.93	6200.47	6310.07	6421.79	6535.71	6651.93	6770.53	.52
-54	6095.06	6202.64	6312.28	6424.04	6538.02	6654.28	6772.93	-54
.56	6097.19	6204.81	6314.49	6426.30	6540.32	6656.63	6775.33	.56
.58	6099.32	6206.99	6316.71	6428.56	6542.62	6658.98	6777.73	.58
.60	6101.46	6209.16	6318.92	6430.82	6544.93	6661.33	6780.12	.60
.62	6103.59	6211.34	6321.14	6433.08	6547.23	6663.69	6782.53	.62
.64	6105.73	6213.51	6323.36	6435.34	6549.54	6666.04	6784.93	.64
.66	6107.86	6215.69	6325.58	6437.60	6551.85	6668.39	6787.33	.66
.68	6110.00	6217.87	6327.80	6439.86	6554.15	6670.75	6789.73	.68
.70	6112.14	6220.04	6330.02	6442.13	6556.46	6673.10	6792.14	.70
.72	6114.28	6222.22	6332.24	6444.39	6558.77	6675.46	6794.55	.72
.74	6116.42	6224.40	6334.46	6446.66	6561.08	6677.82	6796.95	.74
.76	6118.55	6226.58	6336.68	6448.93	6563.39	6680.18	6799.36	.76
.78	6120.70	6228.77	6338.90	6451.19	6565.71	6682.54	6801.77	.78
.80	6122.84	6230.95	6341.13	6453.46	6568.02	6684.90	6804.18	.80
.82	6124.98	6233.13	6343.35	6455.73	6570.34	6687.26	6806.59	.82
.84 .86	6127.12	6235.31	6345.58	6458.00	6572.65	6689.62	6809.00	.84
	6129.27	6237.50	6347.81	6460.27	6574.97	6691.99	6811.41	.86
.88	6131.42	6239.69	6350.04	6462.54	6577.29	6694.35	6813.83	.88
.90	6133.56 6135.70	6241.87	6352.26	6464.81	6579.60 6581.92	6696.72 6699.08	6816.24 6818.66	.90
.92		6244.06	6354.49					.92
.94	6137.85	6246.25	6356.72	6469.36	6584.24	6701.45	6821.07	.94
.96 .98	6140.00 6142.15	6248.44 6250.63	6358.96 6361.19	6471.64	6586.56 6588.89	6703.82 6706.19	6823.49 6825.91	.96 .98
1.00	6144.30	6252.82		6473.91	6591.21	6708.56	6828.33	1.00
1.00	0144.30	0252.82	6363.42	0470.19	0591.21	0708.50	0020.33	1.00

TABLE III. — TANGENT DISTANCE CORRECTIONS $T_D = T_{10}/D + \text{tabular correction}$

I D	2°	4°	6°	8°	10°	12°	14°	16°	18°	20°	D_I
ů	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	i
2	.00	.00	.01	.01	.01	.02	.02	.02	.02	.03	2
4 6	.00	.01	.or	.02	.03	.03	.04	.04	. 05	.05	4
6	.01	.OI	.02	.03	.04	.05	.05	.06	.07	.08	6
8	.01	.02	.03	.04	.05	.06	.07	.08	.09	.10	8
10	0.01	0.02	0.04	0.05	0.06	0.08	0.09	0.10	0.11	0.13	10
12	.01	.03	.04	.06	.08	.09	.II	.12	.14	.15	12
14	.01	.03	.05	.07	.09	.11	.13	14	.16	.18	14
16	.02	.04	.06	.08	.10	.12	.14	.16	.18	.20	16
18	.02	.04	.07	.09	.II	.14	.16	. 18	.21	.23	18
20	0.02	0.05	0.07	0.10	0.13	0.15	0.18	0.21	0.23	0.26	20
											1
22	.02	.05	.08	.II	.14	.17	.20	.23	.25 .28	.29	22
24	.02	.06	.09	.12	.15	.20		.25	l.	.31	24
26	.03	.06	.10	.13	.17		.24	.27	.30	-34	26
28	.03	.07	.II.	.14	.18	.22	.25	.29	-33	.36	28
30	0.03	0.07	0.11	0.15	0.19	0.23	0.27	0.31	0.35	0.39	30
32	.03	.08	.12	.16	.21	.25	.29	-33	.38	.42	32
34	.03	.08	.13	.18	.22	.27	.31	.36	.40	.45	34
36	.04	.09	.14	.19	.23	. 28	-33	.38	-43	-47	36
38	.04	.09	.15	20	25	.30	-35	40	-45	.50	38
40	0.04	0.10	0.15	0.21	0.26	0.32	0.37	0.42	0.47	0.53	40
42	.04	.10	.16	.22	.28	-33	-39	-45	.50	.56	42
44	.04	.II	.17	.23	.29	-35	.41	-47	-53	.59	44
46	.05	.12	.18	.24	.31	-37	-43	.49	.56	.62	46
48	.05	.12	.19	.26	.32	-39	-45	.52	-59	.65	48
50	0.05	0.13	0.20	0.27	0.34	0.40	0.47	0.54	0.61	0.68	50
52	.05	.13	.21	.28	·35	.42	.50	-57	.64	.71	52
54	.06	.14	.22	.29	.37	-44	.52	-59	.67	.74	54
56	.06	. 15	.23	.30	.38	.46	-54	.62	.70	.77	56
58	.06	.15	.24	.32	.40	.48	.56	.64	.73	.80	58
60	0.06	0.16	0.24	0.33	0.42	0.50	0.58	0.67	0.75	0.84	60
62	.07	.16	.25	-34	.43	.52	.61	.70	.79	.87	62
64	.07	.17	.27	.36	-45	.54	.64	-73	.82	.91	64
66	.07	.18	.28	-37	-47	.56	.66	-75	.85	.95	66
68	.07	.18	.29	-39	.49	-59	.69	.78	.88	.98	68
70	0.08	0.19	0.30	0.40	0.50	0.61	0.71	0.81	0.91	1.02	70
72	.08	.20	.31	.42	.52	.63	.74	.84	.95	1.06	72
74	.08	.21	.32	.43	-54	.65	.77	.87	.99	1.10	74
76	.09	.21	.33	-45	.56	.68	.79	.91	1.02	1.14	76
78	.09	.22	-34	.46	.58	.70	.82	.94	1.06	1.18	78
80	0.09	0.23	0.36	0.48	0.60	0.73	0.84	0.97	1.10	I.22	80
82	.09	.24	-37	.50	.63	.75	.88	1.01	1.14	1.27	82
84	.10	.25	.38	.52	.65	.78	.91	1.05	1.18	1.31	84
86	.10	.25	.40	-53	.67	.81	.95	1.08	1.22	1.36	86
88	.II	.26	.41	-55	.70	.84	.98	1.12	1.26	1.41	88
90	0.11	0.27	0.42	0.57	0.72	0.87	1.02	1.16	1.31	1.45	90
92	.II.	.28	-44	-59	.75	.90	1.05	1.20	1.36	1.50	92
94	.12	.29	.46	.61	.77	.93	1.09	1.24	1.40	1.56	94
96	.12	.30	-47	.64	.80	.96	1.13	1.29	1.45	1.62	96
98	.13	.31	-49	66	.83	1.00	1.17	1.34	1.51	1.68	98
100	0.13	0.33	0.51	0.68	0.86	1.03	1.21	1.38	1.56	1.74	100

TABLE IV. — External Distances for a 1° Curve $E_D = E_{1^{\circ}}/D \ ({\rm approx.})$

I	o°	10°	20°	30°	40°	50°	60°	70°	8o°	90°
.0	.0	21.9	88.4	202.I	367.7	592.3	886.4	1265.0	1749.9	2373.3
.2	.0	22.8	90.2	04.9	71.6	97.5	93.1	73.5	60.9	87.5
.4	.0	23.7	92.0	07.7	75.5	602.7	99.8	82.1	71.9	2401.8
.6	ı.	24.6	93.8	10.5	79.4	07.9	906.5	90.8	83.0	16.1
.8	.1	25.5	95.7	13.4	83.4	13.1	13.3	99.5	94.1	30.5
1.0	.2	26.5	97.6	216.2	387.4	618.4	920.1	1308.2	1805.3	2444.9
.2	.3	27.5	99.5	19.1	91.4	23.7	27.0	17.0	16.6	59.5
.4	.4	28.5	101.4	22.0	95.4	29.0	33.9	25.8	27.9	74.2
.6	.6	29.5	103.3	25.0	99.5	34.4	40.8	34.7	39.3	88.8
.8	.7	30.5	105.3	27.9	403.5	39.8	47.8	43.6	50.7	2503.6
2.0	.9	31.6	107.2	230.9	407.6	645.2	954.8	1352.6	1862.2	2518.5
.2	I.I	32.6	9.2	33.9	11.8	50.6	61.8	61.6	73.8	33.4
.4	1.3	33.7	11.2	36.9	15.9	56.1	68.8	70.6	85.4	48.5
.6	1.5	34.8	13.3	39.9	20.I	61.6	75.9	79.7	97.0	63.6
.8	1.7	35.9	15.3	43.0	24.3	67.1	83.1	88.9	1908.7	78.7
3.0	2.0	37.I	117.4	246.1	428.5	672.7	990.2	1398.0	1920.5	2594.0
.2	2.2	38.2	19.5	49.2	32.7	78.2	97.4	1407.3	32.4	2609.4
.4	2.5	39.4	21.6	52.3	37.0	83.9	1004.7	16.5	44.3	24.8
.6	2.8	40.6	23.7	55.4	41.3	89.5	12.0	25.9	56.3 68.3	40.3
.8	3.2	41.8	25.8	58.6	45.6	95.2	19.3	35.3		55.9
4.0	3.5	43.0	128.0	261.8	450.0	700.9	1026.6	1444.6	1980.4	2671.6
.2	3.9	44.3	30.2	65.0	54.3	06.6	34.0	54.I	92.5	87.4
.4	4.2	45.5 46.8	32.4	68.2	58.7	12.4	41.4	63.6	2004.7 17.0	2703.3
.6	4.6		34.6	71.5	63.2			73.2		19.2
.8	5.0 5.5	48.I 49.4	36.9 139.1	74.8 278.1	67.6 472.1	24.0 729.9	56.4	82.8 1492.4	29.3	35.2 2751.3
5.0	5.5	50.8	41.4	81.4	76.6	35.7	71.5	1492.4 1502.1	54.2	67.5
	6.4	52.1	43.7	84.7	81.1	41.6	79.1	11.8	66.7	83.8
.4	6.8	53.5	46.0	88.1	85.6	47.6	86.8	21.7	79.3	2800.I
.8	7.3	54.9	48.4	91.5	90.2	53.6	94.5	31.5	91.9	16.6
6.0	7.9	56.3	150.7	294.9	494.8	759.6	1102.2	1541.4	2104.6	2833.2
.2	8.4	57.7	53.I	98.3	99.4	65.6	09.9	51.3	17.4	49.8
.4	8.9	59.2	55.5	301.7	504.1	71.7	17.7	61.3	30.3	66.5
.6	9.5	60.6	57.9	05.2	08.8	77.8	25.6	71.3	43.2	83.4
.8	10.1	62.1	60.4	08.7	13.5	83.9	33.5	81.4	56.2	2900.3
7.0	10.7	63.6	162.8	312.2	518.2	790.I	1141.4	1591.6	2169.2	2917.3
.2	11.3	65.2	65.3	15.8	22.9	96.3	49.3	1601.8	82.4	34.4
.4	12.0	66.7	67.8	19.3	27.7	802.5	57.3	12.0	95.5	51.6
.6	12.6	68.3	70.3	22.9	32.5	08.8	65.4	22.3	2208.8	68.9
.8	13.3	69.8	72.8	26.5	37.4	15.2	73.4	32.6	22.1	86.3
8.0	14.0	71.4	175.4	330.1	542.2	821.4	1181.6	1643.0	2235.5	3003.8
.2	14.7	73.0	78.0	33.8	47.I	27.7	89.7	63.5	48.9	21.4
.4	15.4	74.7	80.6	37.5	52.0	34.1	97.9 1206.1	64.0	62.5 76.1	39.1
.6	16.2	76.3	83.2	41.2	57.0	40.5	ł	74.5		56.8
.8	16.9	78.0	85.8 188.5	44.9 348.6	61.9 566.9	47.0 853.5	14.4	85.1 1695.8	89.8	74.7 3092.7
9.0	17.7 18.5	79.7 81.4	91.2	52.4	72.0	60.0	31.1	1706.5	17.3	3110.8
		83.1		56.2	77.0	66.5	39.5	17.3	31.2	28.9
.4 .6	19.3	84.8	93.9 96.6	60.0	82.1	73.I	48.0	28.1	45.I	47.2
.8	21.0	86.6	99.4	63.9	87.2	79.7	56.4	39.0	59.2	65.6
10.0	21.9	88.4	202.1	367.7	592.3	886.4	1265.0	1749.9	2373.3	3184.1
I	0°	10°	20°	30°	40°	50°	60°	70°	80°	90°

TABLE V. — LONG CHORDS AND ACTUAL ARCS

					-				
Degree	Actual		_	_	_		1 -	1	Degree
of	arc, one	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of
curve	station								curve
0.2	100.000	200.0	300.0	400.0	500.0	600.0	700.0	800.0	0.2
-4	.000	00.0	00.0	00.0	00.0	00.0	699.9	799.9	.4
.6	.000	00.0	00.0	00.0	499.9	599.9	699.8	799.8	.6
.8	.001	00.0	00.0	00.0	99.9	99.8	99.7	99.6	.8
1.0	100.001	200.0	300.0	399.9	499.8	599.7	699.6	799.4	1.0
.2	,002	00.0	00.0	99.9	99.8	99.6	99.4	99.1	.2
-4	.002	00.0	299.9	99.9	99.7	99.5	99.2	98.8	.4
.6	.003	00.0	99.9	99.8	99.6	99.3	98.9	98.4	.6
.8	.004	00.0	99.9	99.8	99.5	99.1	98.6	97.9	.8
2.0	100.005	200.0	299.9	399.7	499.4	598.9	698.3	797.4	2.0
. 2	.006	00.0	99.9	99.6	99.3	98.7	97.9	96.9	.2
.4 .6	.007	00.0	99.8	99.6	99.1	98.5	97.5	96.3	.4
	.009		99.8	99.5	99.0	98.2	97.1	95.7	.6
.8	.010	199.9	99.8	99.4	98.8	97.9	96.7 696.2	95.0	.8
3.0	.013	199.9 99.9	299.7 99.7	399.3	498.6	597.6 97.3	95.6	794·3 93·5	3.0
					98.2	96.9	1	92.6	
.4 .6	.015	99.9 99.9	99.6 99.6	99.1 99.0	98.0	96.6	95.I 94.5	92.0	.6
.8	.010	99.9	99.6	98.9	97.8	96.2	93.9	90.8	.8
4.0	100.020	199.9	299.5	398.8	497.6	595.7	693.2	789.8	4.0
.2	.022	99.9	99.5	98.7	97.3	95.3	92.5	88.8	
.4	.022	99.9	99.5	98.5	97.3 97.1	95.3	92.3	87.7	.2
.6	.023	99.8	99.4	98.4	96.8	94.4	91.0	86.5	.6
.8	.029	99.8	.99.3	98.2	96.5	93.9	90.2	85.3	.8
5.0	100.032	199.8	299.2	398.I	496.2	593.4	689.4	784.1	5.0
.2	.034	99.8	99.2	97.9	95.9	92.8	88.5	82.8	. 2
.4	.037	99.8	99.1	97.8	95.6	92.3	87.6	81.5	.4
.6	.040 ″	99.8	99.0	97.6	95.2	91.7	86.7	80.1	.6
.8	.043	99.7	99.0	97.4	94.9	91.1	85.7	78.7	.8
6.0	100.046	199.7	298.9	397.3	494.5	590.4	684.7	777.2	6.0
.2	.049	99.7	98.8	97.1	94.2	89.8	83.7	75.6	.2
.4	.052	99.7	98.8	96.9	93.8	89.1	82.7	74.0	.4
.6	.055	99.7	98.7	96.7	93.4	88.5	81.6	72.4	.6
.8	.059	99.6	98.6	96.5	93.0	87.7	80.4	70.7	.8
7.0	.066	199.6 99.6	298.5 98.4	396.3 96.1	492.6 92.1	587.0 86.3	679.3 78.1	769.0 67.2	7.0
		99.6	98.3	95.8	91.7	85.5	76.9	65.4	
.4	.070	99.6	98.2	95.6	91.7	84.7	75.6	63.5	.6
.8	.073	99.5	98.1	95.4	90.8	83.9	74.3	61.6	.8
8.0	100.081	199.5	298.I	395.I	490.3	583.I	673.0	759.7	8.0
.2	.085	99.5	98.0	94.9	89.8	82.2	71.7	57.7	.2
-4	.090	99.5	97.9	94.6	89.3	81.4	70.3	55.6	.4
.6	.094	99.4	97.8	94.4	88.8	80.5	68.9	53.5	.6
.8	. 098	99.4	97.6	94.1	88.3	79.6	67.4	51.4	.8
9.0	100.103	199.4	297.5	393.9	487.7	578.6	666.0	749.2	9.0
.2	.108	99.4	97.4	93.6	87.2	77.7	64.4	46.9	.2
.4 .6	.112	99.3	97.3	93.3	86.6 86.1	76.7	62.9 61.3	44.6	.6
.6	.117	99·3 99·3	97.2 97.1	93.0	85.5	75.7 74.7	59.7	42.3 39.9	.8
10.0	100.127	199.2	297.0	392.4	484.9	573.7	658.1	737.5	10.0
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree
Degree	rictual arc	2 Dia.	Jula.	4 Dua.	J Dia.	J Dia.	, 000.	o bua.	Degree

	Degree of curve	Actual arc, one station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
	10.0	100.127	199.2	297.0	392.4	484.9	573.7	658.1	737.5	10.0
ı	.2	.132	99.2	96.8	92.1	84.3	72.6	56.5	35.I	.2
ı	-4	.137	99.2	96.7	91.8	83.7	71.6	54.8	32.5	.4
ı	.6	. 143	99.1	96.6	91.5	83.1	70.5	53.0	30.0	.6
ı	.8	.148	99.1	96.5	91.2	82.4	69.4	51.3	27.4	.8
ı	11.0	100.154	199.1	296.3	390.8	481.8	568.2	649.5	724.8	11.0
ı	.2	.159	99.0	96.2	90.5	81.1	67.1	47.7	22.I	. 2
	.4	. 165	99.0	96.1	90.2	80.4	65.9	45.8	19.4	.4 .6
	.6 .8	.171	99.0	95.9 95.8	89.8 89.5	79.7 79.0	64.8 63.5	44.0 42.1	16.6	.8
		.177							13.8	
ı	12.0	100.183	198.9	295.6	389.1	478.3	562.3	640.1	710.9	12.0
	.2	. 189	98.9 98.8	95.5	88.7 88.4	77.6 76.9	61.1 59.8	38.2	08.1	.2
	·4 .6	. 195	98.8	95.3 95.2	88.0	76.2	58.5	36.2 34.2	05.I 702.2	.4 .6
	.8	.208	98.8	95.0	87.6	75.4	57.2	32.I	699.2	.8
	13.0	100.215	198.7	294.9	387.2	474.6	555.9	630.1	696.I	13.0
1	.2	. 222	98.7	94.7	86.8	73.9	54.6	28.0	93.0	.2
ı	.4	. 228	98.6	94.6	86.5	73.I	53.2	25.8	89.9	.4
	.6	. 235	98.6	94.4	86.0	72.3	51.9	23.7	86.7	.6
	.8	. 242	98.5	94.2	85.6	71.5	50.5	21.5	83.5	.8
	14.0	100.249	198.5	294.I	385.2	470.6	549.I	619.3	680.3	14.0
	.2	. 256	98.5	93.9	84.8	69.8	47.6	17.0	77.0	. 2
	.4	. 264	98.4	93.7	84.4	69.0	46.2	14.8	73.7	.4
ı	.6	.271	98.4	93.5	83.9	68.1	44.7	12.5	70.3	.6
	.8	. 279	98.3	93.4	83.5	67.3	43.2	10.2	66.9	.8
	15.0	100.286	198.3	293.2	383.I 82.6	466.4	541.7	607.8	663.5	15.0
	.2	. 294	98.2	93.0		65.5	40.2	05.4	60.0	.2
	.4 .6	.302	98.2 98.2	92.8 92.6	82.2	64.6	38.7 37.1	03.0 600.6	56.5	.4 .6
ı	.8	.318	98.1	92.0	81.2	62.8	35.6	598.2	49.4	.8
	16.0	100.326	198.1	292.3	380.8	461.9	534.0	595.7	645.8	16.0
ı	.2	-334	98.0	92.I	80.3	60.9	32.4	93.2	42.2	,2
ı	.4	.342	98.0	91.9	79.8	60.0	30.7	90.7	38.5	.4
ı	.6	.351	97.9	91.7	79.3	59 0	29.I	88.1	34.8	.6
ı	.8	-359	97.9	91.5	78.8	58.0	27.5	85.5	31.1	.8
ı	17.0	100.368	197.8	291.3	378.3	457.I	525.8	582.9	627.3	17.0
ı	.2	.376	97.8	91.1	77.8	56.1	24.I	80.3	23.5	.2
ı	.4	.385	97.7	90.8	77.3	55.I	22.4	77.7	19.6	-4
	.6	-394	97.6	90.6	76.8	54.I	20.7	75.0	15.8	.6
ı	.8	.403	97.6	90.4	76.3	53.0	18.9	72.3	11.9	.8
ı	18.0	100.412	197.5	290.2	375.7	452.0	517.2	569.6	608.0	18.0
ı	.2	.422	97.5	90.0	75.2	51.0	15.4	66.8	04.0	.2
ı	·4 .6	.431	97.4	89.8 89.6	74.7 74.1	49.9 48.9	13.6	64.1 61.3	596.0	.4 .6
	.8	.440	97.4	89.3	73.6	47.8	10.0	58.5	92.0	.8
	19.0	.450 100.460	97.3 197.3	289.1	373.0	446.7	508.1	555.6	587.9	19.0
	.2	.469	97.2	88.9	72.5	45.6	06.3	52.8	83.8	.2
	.4	.479	97.1	88.6	71.9	44.5	04.4	49.9	79.7	.4
	.6	.489	97.1	88.4	71.3	43.4	02.5	47.0	75.5	.6
	.8	. 499	97.0	88.2	70.7	42.3	500.6	44.I	71.3	.8
	20.0	100.510	197.0	287.9	370.2	44I.I	498.7	541.1	567.1	20.0
	Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE VI. — MIDDLE ORDINATES

Degree of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
0.2	.04	.17	.39	.70	1.09	1.57	2.14	2.79	0.2
.4	.09	-35	. 78	1.40	2.18	3.14	4.28	5.58	-4
.6	.13	.52	1.18	2.09	3.27	4.71	6.41	8.38	.6
.8	.17	.70	1.57	2.79	4.36	6.28	8.55	11.17	.8
1.0	. 22 .26	.87	1.96	3.49	5.45	7.85	10.69	13.96	1.0
.2	.30	1.05	2.36	4.19	6.54 7.63	9.42	12.82	16.75	.2
.6	.35	1.40	3.14	5.58	8.72	12.56		19.53	.4
.8	.39	1.57	3.14	6.28	9.81	12.50	17.09	22.32 25.10	.6 .8
2.0	.44	1.75	3.93	6.98	10.90	15.69	21.36	27.88	2.0
.2	.48	1.92	4.32	7.68	11.99	17.26	23.48	30.66	.2
.4	.52	2.09	4.71	8.37	13.08	18 83	25.61	33.43	.4
.6	-57	2.27	5.10	9.07	14.17	20.39	27.74	36.21	.6
.8	.61	2.44	5.50	9.77	15.25	21.95	29.86	38.98	.8
3.0	.65	2.62	5.89	10.46	16.34	23.52	31.98	41.74	3.0
.2	.70	2.79	6.28	11.16	17.43	25.08	34.10	44.50	.2
.4	.74	2.97	6.67	11.86	18.51	26.64	36.22	47.26	-4
.6	.78 .83	3.14	7.06	12.55 13.25	19.60	28.20	38.34	50.01	.6
4.0	.87	3.49	7.85	13.94	21.77	29.75 31.31	40.45	52.76	4.0
.2	.92	3.66	8.24	14.64			42.56	55.50	
.4	.92	3.84	8.63	15.33	22.85 23.93	32.86 34.4I	44.66	58.24 60.97	.2
.6	1.00	4.01	9.02	16.03	25.01	35.96	48.87	63.69	.6
.8	1.05	4.19	9.42	16.72	26.09	37.51	50.96	66.42	.8
5.0	1.09	4.36	9.81	17.42	27.17	39.06	53.05	69.13	5.0
.2	1.14	4.54	10.20	18.11	28.25	40.60	55.14	71.84	.2
-4	1.18	4.71	10.59	18.80	29.33	42.15	57.23	74.54	.4
.6 .8	I.22	4.89	10.98	19.49	30.40	43.69	59.31	77.23	.6
	I.27	5.06	11.37	20.19	31.48	45.22	61.38	79.92	.8
6.0	1.31	5.23	11.76	20.88	32.55	46.76	63.46	82.60	6.0
.2	I.35 I.40	5.4I 5.58	12.15 12.54	21.57 22.26	33.63	48.29	65.52	85.27	.2
.6	I.44	5.76	12.54	22.95	34.70 35.77	49.82 51.35	67.58 69.64	87.93 90.59	.4 .6
.8	1.48	5.93	13.32	23.64	36.84	52.88	71.70	93.23	.8
7.0	1.53	6.11	13.71	24.33	37.91	54.40	73.74	95.87	7.0
.2	I.57	6.28	14.10	25.02	38.97	55.92	75.79	98.50	,2
-4	1.62	6.45	14.49	25.71	40.04	57.44	77.82	101.12	.4
.6	1.66	6.63	14.88	26.39	41.10	58.95	79.85	103.73	.6
.8	1.70	6.80	15.27	27.08	42.17	60.46	81.88	106.33	.8
8.0	1.75	6.98	15.66	27.77	43.23	61.97	83.90	108.92	8.0
.2	1.79	7.15	16.05	28.45	44.29	63.47	85.92	111.50	.2
.4 .6	1.83	7.32	16.44	29.14 29.82	45.35 46.40	64.97 66.47	87.92 89.92	114.06	.4 .6
.8	1.92	7.67	17.22	30.51	47.46	67.97	91.92		.8
9.0	1.92	7.85	17.61	31.19	48.51	69.46	91.92	119.17	. 8 9.0
.2	2.00	8.02	18.00	31.87	49.56	70.95	95.89	124.23	.2
.4	2.05	8.19	18.38	32.56	50.61	72.43	97.87	126.75	.4
.6	2.10	8.37	18.77	33.24	51.66	73.91	99.83	129.25	.6
.8	2.14	8.54	19.16	33.92	52.71	75.39	101.80	131.74	.8
10.0	2.18	8.72	19.55	34.60	53.75	76.86	103.75	134.22	10.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE VI. — (Continued)

1	D 1									1.70
ı	Degree of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
ı	10.0	2.18	8.72	19.55	34.60	53.75	76.86	103.75	134.22	10.0
ı	.2	2.23	8.89	19.94	35.28	54.79	78.33	105.70	136.68	.2
ı	.4	2.27	9.06	20.32	35.96	55.83	79.79	107.64	139.14	.4
ı	.6	2.31	9.24	20.71	36.63	56.87	81.25	109.57	141.58	.6
ı	.8	2.36	9.41	21.10	37.31	57.91	82.71	111.49	144.00	.8
ı	11.0	2.40	9.59	21.48	37.99	58.94	84.16	113.41	146.41	11.0
ľ	.2	2.44	9.76	21.87	38.66	59.98	85.61	115.32	148.81	.2
ı	.4	2.49	9.93	22.25	39.34	61.01	87.05	117.21	151.20	.4
ı	.8	2.53 2.58	10.11	22.64	40.0I 40.68	62.04 63.06	88.49 89.92	119.11	153.57 155.93	.6 .8
ı	12.0	2.62		23.41		64.09	91.36	122.87	158.27	12.0
ı			10.45		41.36					
1	.2	2.66 2.7I	10.63	23.80 24.18	42.03 42.70	65.11 66.13	92.78 94.20	124.73	160.59 162.91	.2
ı	.6	2.75	10.80	24.10	43.37	67.14	95.62	128.43	165.21	.6
ł	.8	2.80	11.15	24.95	44.03	68.16	97.03	130.27	167.49	.8
ı	13.0	2.84	11.32	25.33	44.70	69.17	98.43	132.10	169.75	13.0
ı	.2	2.88	11.49	25.72	45.37	70.18	99.83	133.92	172.01	.2
ı	.4	2.93	11.67	26.10	46.03	71.19	101.23	135.73	174.24	.4
ı	.6	2.97	11.84	26.48	46.70	72.19	102.62	137.53	176.46	.6
ł	.8	3.01	12.01	26.87	47.36	73.20	104.00	139.33	178.67	.8
ı	14.0	3.06	12.19	27.25	48.02	74.20	105.38	141.11	180.85	14.0
ı	.2	3.10	12.36	27.63	48.69	75.20	106.76	142.88	183.02	.2
ı	-4	3.15	12.53	28.01	49.35	76.19	108.12	144.64	185.17	.4
ı	.6	3.19	12.71	28.40	50.01	77.18	109.49	146.40	187.31	.6
ı	.8	3.23	12.88	28.78	50.66	78.17	110.85	148.14	189.43	.8
ı	15.0	3.28	13.05	29.16	51.32	79.16	112.20	149.87	191.53	15.0
ı	. 2	3.32	13.23	29.54	51.98	80.14	113.54	151.59	193.62	.2
ı	.4	3.36	13.40	29.92	52.63	81.12	114.88	153.30	195.68	.6
ı	.8	3.4I 3.45	13.57 13.74	30.30	53.29 53.94	82.10 83.08	116.22	155.00	197.73	.8
ľ	16.0	3.50	13.92	31.06	54.59	84.05	118.87	158.37	201.77	16.0
ı	.2	3.54	14.00	31.44	55.24	85.02	120.19	160.03	203.77	.2
ı	.4	3.58	14.26	31.82	55.89	85.99	121.50	161.69	205.74	.4
ı	.6	3.63	14.44	32.20	56.54	86.95	122.80	163.33	207.70	.6
ı	.8	3.67	14.61	32.57	57.19	87.91	124.10	164.96	209.64	.8
ı	17.0	3.72	14.78	32.95	57.83	88.87	125.39	166.59	211.55	17.0
ı	.2	3.76	14.95	33.33	58.48	89.83	126.68	168.20	213.46	.2
	.4	3.80	15.13	33.71	59.12	90.78	127.96	169.79	215.33	-4
ı	.6 .8	3.85	15.30	34.08	59.76	91.73	129.23	171.38	217.20	.6 .8
ı	18.0	3.89	15.47	34.46	60.40	92.67	130.49	172.95	219.03	18.0
ı		3.94	15.64	34.84	61.04	93.62	131.75	174.52	220.86	
	.2	3.98	15.82	35.21	61.68	94.55	133.01	176.07	222.65	.2
	.4	4.02	15.99 16.16	35.59 35.96	62.32 62.96	95.49 96.42	134.25	177.60	224.43	.6
	.8	4.11	16.33	36.34	63.59	97.35	136.72	180.64	227.93	.8
	19.0	4.16	16.51	36.71	64.22	97.35	137.95	182.15	229.65	19.0
	.2	4.20	16.68	37.09	64.85	99.20	139.17	183.64	231.35	.2
	.4	4.24	16.85	37.46	65.48	100.12	140.38	185.11	233.03	.4
	.6	4.29	17.02	37.83	66.11	101.03	141.58	186.57	234.69	.6
	.8	4.33	17.19	38.20	66.74	101.95	142.78	188.02	236.33	.8
	20.0	4.37	17.37	38.58	67.37	102.86	143.97	189.46	237.94	20.0
	Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

CHAPTER II

THE SPIRAL

The railroad spiral is a curve of varying radius connecting a main or central curve with a tangent or connecting the two branches of a compound curve. If it is a true spiral its change in "degree" is proportionate to its length. Thus at the point of junction with the tangent (T, S) in Fig. 22) the degree is zero; at the junction with the main or central curve of degree D (S. C. in Fig. 22) it is D; at its midpoint it is $\frac{1}{2}D$... etc. The radius is closely inversely as the length. Knowing the degree of the central curve the first quantity to determine is the length L, the second is Δ , the central angle consumed by the spiral. If these two can be conveniently chosen the other functions can be had from tables.

The length of the spiral is determined as follows: For curves of 6° or over on which track is canted 8 inches, L=240 feet as a minimum.

For curves flatter than 6° likely sometime to limit speed, $L = \frac{587}{\sqrt{D}}$ feet,

D being the degree of the central curve. For minor curves not likely to limit speed, $L=\frac{2}{3}SE$ or 30 E in feet, in which S is speed in miles per hour and E is the difference in elevation of the two rails in inches.

If the maximum allowable cant is 6 inches, $L = \frac{380}{\sqrt{D}}$ feet for curves

flatter than 4.5° likely to limit speed. For curves of 4.5° and over the minimum length will be 180 feet.

For minor curves, $L = \frac{2}{3} SE$ or 30 E, as above.

It will be well to select lengths that are round numbers of feet not less than the required minimums and such that the resulting Δ may be whole degrees or a whole number of tenths of a degree divisible by 3. This is merely for convenience in computing.

$$\Delta = \frac{LD}{200}$$
.

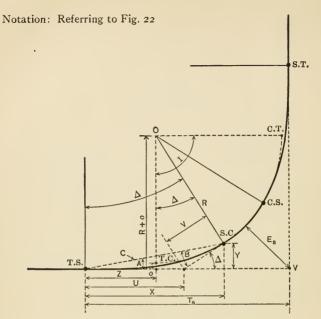


FIG. 22.

T. S. = Tangent-Spiral. S. C. = Spiral-Curve. C. S. = Curve-Spiral. S. T. = Spiral-Tangent. T. C. = Tangent-Curve. C. T. = Curve-Tangent.

 Δ = central angle of the spiral.

A = deflection angle T. S. to S. C.

B =deflection angle S. C.to T. S.

C = the long chord of the spiral.

X = abscissa with T. S. as origin.

Y = ordinate with T. S. as origin.

U =spiral long tangent.

V =spiral short tangent.

o = curve offset.

Z = distance on tangent from T. S. to T. C. of the offset curve.

 T_s = tangent distance of the spiraled curve.

 $E_{\mathbf{s}}$ = external distance of the spiraled curve.

R = radius of central curve.

The Chord Spiral. — If the spiral be laid out by equal chords it is approximately true that the deflection angles from the tangent at the T. S. to the several chord points are as the squares of the chord numbers, and the final deflection A of the long chord is one-third the central angle Δ .

If the spiral be divided into N chords, the deflection angle for the first chord will closely approximate $\frac{\Delta}{3 N^2}$ and the angles that the several chords (produced) will make with the tangent will be approximately Δ

1, 7, 19, 37, 61, 91, 127, 169, 217, 271, etc., times $\frac{\Delta}{3 N^2}$

The chord spiral is a curve passing through the chord points of a series of equal chords for which the relations of the preceding paragraph are exactly true. It is not a curve of uniformly varying radius or degree, but differs from such a curve by an inappreciable amount.

The spiral may be divided into any number of chords. Tables for a division into ten chords have been devised by Mr. Jenks B. Jenkins for the American Railway Engineering Association, and have been approved as good practice by that association.

Table VIII gives values for the quantities noted below. Excepting o and Z the linear quantities vary as L and hence the tabular quantities are coefficients by which the L's of any given cases are to be multiplied to find the functions C, X, Y, U, and V. The use of the table to get o and Z will be evident from the table headings.

Referring to Fig. 22, the tabulated quantities are Δ , A, $\frac{C}{L}$, $\frac{X}{L}$, $\frac{Y}{L}$,

 $\frac{U}{L}$, $\frac{V}{L}$, coefficients for o and Z. The following formulas give these quantities:

$$\Delta = \frac{LD}{200}, A = \frac{1}{3}\Delta - 0.000000825\Delta^3, B = \Delta - A.$$

$$\frac{C}{L} = \cos 0.3 \Delta + 0.004 \operatorname{exsec} \frac{3}{4} \Delta \text{ (approx.)}.$$

$$\overline{X} = C \cos A$$
.

$$Y = C \sin A$$
.

$$Z = X - R \sin \Delta$$
.

$$U = C \frac{\sin B}{\sin \Delta}.$$

$$V = C \frac{\sin A}{\sin \Delta}.$$

$$o = Y - R \text{ vers } \Delta.$$

Exactly,
$$X = \frac{L}{10} \left(\cos \frac{\Delta}{300} + \frac{7\Delta}{300} + \cos \frac{19\Delta}{300} + \cos \frac{37\Delta}{300} + \cos \frac{61\Delta}{300} + \cos \frac{61\Delta}{300} + \cos \frac{91\Delta}{300} + \cos \frac{127\Delta}{300} + \cos \frac{169\Delta}{300} + \cos \frac{217\Delta}{300} + \cos \frac{271\Delta}{300} \right)$$
.
Exactly, $Y = \frac{L}{10} \left(\sin \frac{\Delta}{300} + \sin \frac{7\Delta}{300} + \dots \right)$.

The following formulas give the tangent distance and external distance of the curve:

$$T_s = (R + o) \tan \frac{1}{2} I + Z$$

 $E_s = (R + o) \operatorname{exsec} \frac{1}{2} I + o.$

The central δ subtended by any portion, l feet, of the spiral is the average "degree" of the portion multiplied by $\frac{l}{100}$. The average "degree" is the initial and final degree of the portion divided by 2. The degree at any point distant l feet from the T.S. is $\frac{l}{L}D$. The degree at the end of any chord p (p being the number of the chord) is $\frac{p}{10}D$ for the 10-chord spiral or $\frac{p}{N}D$ for the N-chord spiral.

For precise computation of positions of points on line, A should be computed from $A = \frac{1}{3}\Delta - 0.000000825 \Delta^3$ or taken from Table VIII, or Tables IX to XXIII. The deflection a_1 for the first chord is always $\frac{\Delta}{300}$ for the 10-chord spiral.

For field use the deflection from the T. S. to any chord point should be taken as a_1 times the square of the number of the chord point to be located so long as δ does not exceed 15°. A may be taken as $1/3 \Delta$ for $\Delta \equiv 15^\circ$. When Δ is more than 15° one or more intermediate transit points should be used. Such points should be so chosen that the δ from the T. S. to the first intermediate point shall not exceed 15°, and so that δ from any occupied point to the next transit point less the δ from the T. S. to the occupied point shall not exceed 15°. With this procedure the deflections from the tangent at any intermediate point may be taken as in Table VII, which gives the coefficients by which a_1 is to be multiplied to give deflections to points both forward and back as indicated. This procedure is not exact but results in angular errors less than can be measured by the transit. It is probable that 90 or more per cent of the cases in practice will involve Δ s of less than 10° and an error of 3 seconds or less than 0.001° if A is taken as $\frac{1}{3}\Delta$.

For $\Delta = 15^{\circ}$ the error is 10 seconds or less than 0.003°. If it is desired to find the deflection from the T. S. to any point to which the δ exceeds 15° it may be done by finding the δ and then the corresponding A from Table VIII. If convenient spirals have been chosen, Tables IX to XXIII may be used.

To Select and Lay Out the Spiral. — Knowing I and D, determine L and Δ : from Table VIII find coefficients for and determine o and Z and substitute in the equation for T₈. Knowing the P. I. the station of the T. S. can be found. There are now four ways of locating the

curve.

1. The curve may be run from the T. S. to the S. C. by deflection angles and chord measurements, using Table VII for multiples of a₁ and setting on intermediate points if necessary as advised in the preceding article. To lay out by 5 chords use the deflection coefficients for

every second point computing a_1 as for 10 chords.

2. The tangent may be continued from the T. S. for Z feet, o laid off and the curve D run in for the full central angle I, using an offset back sight for the direction of the offset tangent, locating the S. C. at a distance corresponding to Δ , and which will be nearly L-Z, and the C. S. at a distance from the S. C. corresponding to $I - 2\Delta$, and offsetting o to the forward tangent and proceeding, locating the spirals later by deflection angles, or by offsets as in 4 below, when staking out for construction.

3. Measure U from the T.S.; establish a transit point, turn the angle Δ and measure V and establish the S. C.; run the spiral by deflections from either end; continue the central curve to the C. S.; lay out V and U to get the S. T. and run in the final spiral by deflections from either end.

4. Many times it will be sufficiently exact after running the central curve as in 2, to bisect the offset o for a point on the spiral and then set over such points as may be desired from tangent and curve respectively, making the offsets from the tangent half proportional to the cube of the distance from T.S. and from the curve half proportional to the cube of the distance from the S. C. Thus the quarter points would be offset 1/8 of $\frac{1}{2}o$ or o/16 from tangent and curve respectively.

Time may be saved if a spiral that can be found in one of the Tables IX to XXIII can be chosen. Thus if a 1.5-degree curve is to be connected and the speed to be considered is 90 miles an hour or less, Table X gives all required quantities for the necessary spiral which is 500 feet long. It may be laid out in ten chords of 50 feet each, for which deflection angles are found under the A column. If pluses are to be

located they may be interpolated between the tabular values which are given for each 10 feet on the spiral. But if the speed considered is only 65 miles an hour Table XIII may be used, the length of the spiral being 200 feet. It may be laid out in 10 chords of 20 feet for which the deflection angles or coordinates are given in the table or it may be laid out by 5 chords of 40 feet. Pluses may be interpolated as indicated above. If the speed is 60 miles an hour, Table XIV may be used and the length of spiral will be found to be 150 feet. It may be laid out in 10 chords of 15 feet interpolating in the table, or better, by 5 chords of 30 feet, with quantities taken directly from the table. Thus each table is good for many different spiral lengths connecting curves of various degrees. Any table may be used in which the degree of the central curve can be found in the column headed D provided the speed for which the table is adapted is that for which the curve is to be spiraled or the track canted. Shorter spirals found in tables for slower maximum speed than that for which the track is canted may be used but are not recommended except where it is necessary materially to save cost of construction or to fit cramped situations in cities or on high embankments or in deep cuts when relining old track.

Spiraling a Compound Curve. — The length of spiral to connect the two branches of a compound curve may be found just as for a

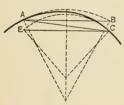


Fig. 23.

tangent and simple curve by substituting the difference of "degrees" $(D_1 - D_2)$ in the equation for length. It is also practically true that the deflections at the junction points with the two branches to the various chord points of the spiral are the same as for corresponding chord points of the spiral between tangent and simple curve of degree $(D_1 - D_2)$ if the deflections are considered as turned from equivalent

chord points on the respective curves rather than from the tangent. Thus in Fig. 23, the deflection from chord AB to chord AC of the spiral is $\frac{1}{3}\Delta$ (Δ being the central angle for spiral of length L connecting a tangent and $(D_1-D_2)^\circ$ curve) if arc AB=L, and from chord CE to chord CA it is the same. These relations are closely approximate. The deflection from the tangent at A is, if D_2 be the degree of the larger radius curve and D_1 of the shorter, $\frac{LD_2}{200}+\frac{1}{3}\Delta-C$, when $\Delta=$

 $\frac{(D_1 - D_2) L}{200}$ and C is the correction to be used when necessary or when

 Δ is more than 15°. Or the curve may be considered as part of a spiral from a tangent to the curve of degree D_2 and the deflection coefficients of Table VII may be used.

Illustrative Example. — A 4° curve is to connect with an 8° curve the offset coming at Sta. 464 of the 4° curve. $D_2=4^\circ;\ D_1=8^\circ;\ D_1-D_2=4^\circ;\ L=\frac{600}{\sqrt{D_1-D_2}}=300.\ \Delta=\frac{(D_1+D_2)}{2}\times\frac{L}{100}=18^\circ.$ For computing o and Z we use $D=D_1-D_2=4^\circ,\$ and $L=300,\$ whence $\Delta=6^\circ,\$ and from the tables for $D=4,\ L=300,\$ and $\Delta=6^\circ$ we find o=2.62 and Z=149.92. Therefore C.S.=5ta. 464—149.92 ft. = Sta. 462 + 50.08. If the 300 feet is part of a spiral connecting a tangent and an 8° curve and covers a difference of 4° in its length the whole spiral would be $L_8=\frac{8\,L}{D_1-D_2}=2\,L=600\,{\rm feet}$ covering a Δ of 24°. Therefore Sta. 462 + 50.08 = C.S. is the fifth chord point of the spiral. Since the central angle consumed by the spiral to be run is 18° and the central angle up to the fifth point of the 600-foot spiral is 6°, the difference is 12° or less than 15° and it will be proper to use Table VII with the transit at the fifth chord point. Hence the deflections to the several chord points are 16, 34, 54, 76, and 100 times a_1 , which is $\frac{\Delta}{300}=0.08^\circ$ or:

The chords are 60 feet and the deflections from tangent at A to the corresponding points on the 4° curve extended would be:

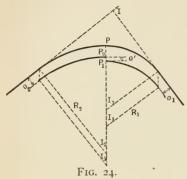
which would be the deflections from corresponding chord points on the D_1 curve, are the deflections for the chord points of a five-chord spiral of 300 feet connecting a tangent and $4^{\circ} = (D_1 - D_2)$ degree curve.

Setting up on the S. C., the compounding point with the 8° curve, the deflection from the long chord of the spiral to the tangent is from Table VII, $125 \times a_1$ or 10°. It is also $\frac{LD_1}{200} - 2$ ° or, stated otherwise,

the angle between the long chord of $\frac{L}{100}$ stations of curve D_2 and the chord of the spiral is 2° , which is the deflection angle of a 300-foot spiral connecting a tangent and $4^{\circ} = (D_1 - D_2)$ degree curve.

Considering the whole spiraled curve, and referring to Fig. 24, in which R_1 is the shorter radius and R_2 is the longer radius, the compound curve is supposed connected first directly to the tangents. To introduce the spirals, the arc of R_1 must be thrown in along the line of common radius $PP_1 = o_1 \sec I_1$. The arc of R_2 must be thrown $PP_2 = o_2 \sec I_2$. $PP_1 - PP_2$ must equal o', the proper offset for the connecting spiral. Therefore determine L_2 to find o_2 and PP_2 ; to

 PP_2 add o' previously found and find a trial value for $o_1 = \frac{PP_2 + o'}{\sec I_1}$; if found too small, o_2 or o' or both may be increased, which will



necessitate increase in L_2 or L' or both; if found too large no harm will result unless in relining track the shift is too great. The tangent distances are increased by $o_2 \tan \Delta_2$ and $o_1 \tan \Delta_1$, respectively.

To lessen the movement of existing track the following procedure may be had: Conceive the larger radius curve moved outward along the common radius line, and the smaller radius curve moved inward, each by $\frac{1}{2}o'$, the

proper offset for the chosen spiral; find new radii for the curves such that

$$R_{2}' = R_{2} - \frac{\frac{1}{2} o' \cos I_{2} + o_{2}}{\text{vers } I_{2}}$$

$$R_{1}' = R_{1} - \frac{o_{1} - \frac{1}{2} o' \cos I_{1}}{\text{vers } I_{1}}.$$

Both tangent points will be moved toward the vertex by

$$t_2 = (R_2 - R_2' + \frac{1}{2} o') \sin I_2$$

 $t_1 = (R_1 - R_1' - \frac{1}{2} o') \sin I_1$.

TABLE VII. — COEFFICIENTS OF a_1 FOR DEFLECTION ANGLES TO CHORD POINTS

Deflection				Tran	sit at c	hord-pe	oint nu	mber			
angle to chord-point number	r. s.	1	2	3	4	5	6	7	8	9	10 S. C.
o T. S.	0	2	8	18	32	50	72	98	128	162	200
I	1	0	5	14	27	44	65	90	119	152	189
2	4	4	0	8	20	36	56	80	108	140	176
3	9	10	7	0	11	26	45	68	95	126	161
4	16	18	16	10	0	14	32	54	80	110	144
4 5 6	25	28	27	22	13	0	17	38	63	92	125
	36	40	40	36	28	16	0	20	44	72	104
7 8	49	54	55	52	45	34	19	0	23	50	81
	64	70	72	70	64	54	40	22	0	26	56
9	81	88	91	90	85	76	63	46	25	0	29
10 S. C.	100	108	112	112	108	100	88	72	52	28	0

TABLE VIII. - GENERAL FUNCTIONS - TEN-CHORD SPIRAL

	-	C	v	V	U	V	o=mL	_nD	Z=mL	-»D	
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L_1}$	$\frac{\partial}{L}$	$\frac{r}{L}$					Δ
								<u>n</u>			-
0.0	0.000	1.00000	1.00000	.00000	.66667	.33333	.00000	,0000	.50000	,0000	0.0
Ι.	.033	.00000	.00000	.00058	.66667	.33333	.00015	.0000	.50000	.0001	ı.
.2	.067	.00000	.00000	.00116	.66667	-33333	.00029	.0000	.50000	.0003	.2
-3	.100	.00000	.00000	.00175	.66667	-33333	.00044	.0000	.50000	.0004	-3
-4	.133	.00000	.00000	.00233	.66667	.33333	.00058	.0000	.50000	.0005	-4
.5	.167	.00000	0.99999	.00291	.66667	.33334	.00073	.0000	.50000	.0006	.5
.6	.200	,00000	.99999	.00349		-33334	1		-		.6
.7 .8	.233	.99999	.99999	.00407	.66667	·33334 ·33334	.00102	.0000	.50000	.0009	.7 .8
.9	.300	.99999	.99998	.00524	.66668	.33334	.00131	.0000	.50000	.0011	.9
1.0	-333	.99999	.99997	.00582	.66668	-33334	.00145	.0000	.50000	.0013	1.0
				.00562	.66668		,00160	.0000		.0014	
.I	.367	. 99998	.99996 .99996	.00040	.66668	·33335 ·33335	.00175	.0000	.49999 .49999	.0014	. I . 2
.3	.433	.99998	-99995	.00756	.66668	-33335	.00189	.0000	.49999	.0017	.3
.4	.467	.99997	.99994	.00814	.66669	-33335	.00204	.0000	. 49999	.0018	.4
.5	.500	.99997	.99994	.00873	.66669	.33336	.00218	.0000	.49999	.0019	.5
.6	•533	.99997	.99992	.00931	.66669	.33336	.00233	.0000	.49999	.0020	.6
.7	.567	.99996	.99991	.00989	.66670	.33336	.00247	.0000	.49999	.0022	.7
.8	.600	.99996	.99990	.01047	.66670	-33337	.00262	.0000	.49998	.0023	.8
.9	.633	.99995	.99989	.01105	.66671	.33337	.00276	.0000	.49998	.0024	.9
2.0	.667	.99995	.99988	.01163	.66671	-33337	.00291	.0000	.49998	.0025	2.0
. І	.700	.99994	.99987	.01222	.66671	-33338	.00305	,0000	.49998	.0027	.1
.2	.733	.99994	.99985	.01280	.66672	.33338	.00320	.0001	.49998	.0028	.2
-3	.767	.99993	.99984	.01338	.66672	.33338	.00335	.0001	-49997	.0029	-3
.4	.800	.99992	.99983	.01396	.66673	-33339	.00349	.0001	.49997	.0031	.4
.5	.833	.99992	.99981	.01454	.66673	.33339	.00364	.0001	-49997	.0032	.5
.6	.867	.99991	.99980	.01512	.66674	-33340	.00378	.0001	-49997	.0033	.6
.7	.900	.99990	.99978	.01571	.66674	.33340	.00393	.0001	.49996	.0034	.7
.8	.933	.99990	.99976	.01629	.66675	.33341	.00407	.0001	.49996	.0036	.8
.9	.967	.99989	-99975	.01687	.66676	-33342	.00422	.0001	-49996	.0037	.9
3.0	1.000	.99988	.99973	.01745	.66676	-33342	.00436	.0001	-49996	.0038	3.0
.1	1.033	.99987	.99971	.01803	.66677	·33343	.00451	.0001	-49995	.0039	. 1
.2	1.067			.01861	.66678	-33343	.00465	.0001	-49995	.0041	. 2
-3	1.100			.01919	.66678	-33344	.00480	.0001	-49995	.0042	.3
-4	1.133			.01978	.66679	-33345	.00494	.0001	-49994	.0043	-4
5	1.167	.99984		.02036	.66680	•33345	.00509	.0001	-49994	.0045	·5
.6	1,200			.02094	.66681	.33346	1	10001	•49994	.0046	
.7	1.233			.02152	.66681	-33347	.00538		-49993	.0047	.7 .8
.0	1.300			.02210	.66683	·33347 ·33348		.0002	·49993 ·49993	.0048	.9
4.0					.66684			.0002	.49992	.0051	4.0
	1.333			.02326		-33349	I				
ı,	1.367	.99978		.02384	.66685	.33350		.0002	.49992	.0052	. I
.2	1.433			.02443	.66686	·33351 ·33351	.00625	.0002	.49991	.0053	.2
.3	1.455	1		1	.66687		.00640	.0002	.49991	.0056	.4
.4	1.407			.02559	.66688	.33352 .33353		.0002	.49991	.0050	.5
·5 .6	1.533			.02675	.66689	-33354	.00669	.0002	.49990	.0059	.6
.7	1.567	1		.02733	.66690	-33355	.00683	.0002	.49989	.0060	.7
.8	1.600			.02733	.66691	.33356	.00698	.0003	.49989	.0061	.8
.9	1.633			.02849	.66692	-33357	.00713	.0003	.49988	.0062	.9
5.0	1.667			.02907	.66693	.33358	.00727	.0003	. 49988	.0064	5.0
		1 55551	1 . 5 5 5 5 19	1 -5-1		, 55000	-,-,-,	1		-	

		-									_
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=m1	L-nD	Δ
		L	L	L	L	L	m	n	m	n	
5.0	1.667	.99967	.99924	.02907	.66693	.33358	.00727	.0003	.49988	.0064	5.0
Ι.	1.700	.99965	.99921	.02965	.66695	-33359	.00742	.0003	.49987	.0065	.1
.2	1.733	.99964	.99918	.03023	.66696	.33360	.00756	.0003	.49987	.0066	.2
.3	1.767	.99962	.99915	.03082	.66697	.33361	.00771	.0003	.49986	.0067	.3
.4	1.800	.99961	.99912	.03140	.66698	.33362	.00785	.0003	. 49986	.0069	.4
.5	1.833	,99960	.99908	.03198	.66699	.33363	.00800	.0003	.49985	.0070	.5
.6	1.867	.99958	.99905	.03256	.66700	.33364	.00814	.0003	-49985	.0071	.6
.7	1.900	.99957	.99902	.03314	.66702	. 33365	.00829	.0004	.49984	.0073	.7
.8	1.933	.99955	.99898	.03372	.66703 .66704	.33366 .33367	.00843	.0004	.49984	.0074	.8
6.0		-99953		.03488	.66705		.00872		.49983	.0075	.9
	2.000	.99952	.99891			.33369		.0004	.49982	.0076	6.0
I.	2.033	.99950	.99887	.03546	.66707	.33370	.00887	.0004	.49982	.0078	.I
.2	2.100	.99949	.99884	.03662	.66708 .66709	.33371	.00901	.0004	.49981	.0079	.2
	1	-99947	.99876	.03720	.66711		.00910	.0004	.49981		-3
.4 .5	2.133	.99945	.99870	.03720	.66712	·33373 ·33375	.00930	.0005	.4998o .49979	.0081	.4
.6	2.200	.99944	.99868	.03778	.66713	.33376	.00959	.0005	.49979	.0084	.5
.7	2.233	.99940	.99864	.03894	.66715	-33377	.00974	.0005	.49979	.0085	
.8	2.267	.99938	.99860	.03952	.66716	.33379	.00974	.0005	.49978	.0086	.7
.9	2.300	.99936	.99856	.04010	.66718	.33380	.01003	.0005	-49977	.0088	.9
7.0	2.333	.99935	.99852	.04068	.66719	.33381	.01018	.0005	-49976	.0089	7.0
.1	2.367	.99933	.99847	.04126	.66721	.33383	.01032	.0006	·49975	.0090	.1
.2	2.400	.99933	.99843	.04120	.66722	.33384	.01032	.0006	·49975 ·49975	.0090	.1
.3	2.433	.99931	.99839	.04242	.66724	.33385	.01061	.0006	.49973	.0093	.3
.4	2.467	.99927	.99834	.04300	.66725	-33387	.01076	.0006	.49973	.0094	.4
.5	2.500	.99925	.99830	.04358	.66727	.33388	.01090	.0006	.49972	.0095	.5
.6	2.533	.99923	.99825	.04416	.66729	. 33390	.01105	.0006	-49972	.0097	.6
.7	2.567	.99921	.99821	.04474	.66730	.33391	.01119	.0007	.49971	.0098	.7
.8	2.600	.99919	.99816	.04532	.66732	.33393	.01134	.0007	.49970	.0099	.8
.9	2.633	.99917	.99811	.04590	.66734	.33394	.01148	.0007	.49969	.0100	.9
8.0	2.666	.99914	.99806	.04648	.66735	.33396	.01163	.0007	.49969	.0102	8.0
. I	2.699	.99912	.99801	.04706	.66737	.33398	.01177	.0007	.49968	.0103	.1
.2	2.733	.99910	.99797	.04764	.66739	.33399	.01192	.0007	. 49967	.0104	.2
.3	2.766	.99908	.99792	,04822	.66741	.33401	.01206	.0008	.49966	.0105	.3
.4	2.799	.99906	.99786	.04880	.66742	.33402	.01221	.0008	. 49965	.0107	.4
.5 .6	2.833	.99903	.99781	.04937	.66744	.33404	.01235	.0008	.49965	.0108	.5
	2.866	.99901	.99776	.04995	.66746	.33406	.01250	.0008	.49964	.0109	.6
.7	2.899	.99899	.99771	.05053	.66748	.33407	.01264	.0008	. 49963	.0110	.7
.8	2.933	.99897	.99766	.05111	.66750	.33409	.01279	.0009	.49962	.0112	.8
.9	2.966	.99894	.99760	.05169	.66752	.33411	.01293	.0009	49961	.0113	.9
9.0	2.999	.99892	.99755	.05227	.66754	.33413	.01308	.0009	.49960	.0114	.9.0
.I	3.033	.99889	.99749	.05285	.66756	.33414	.01322	.0009	49959	.0116	.I
.2	3.066	.99887	-99744	.05343	.66758	.33416	.01337	.0009	49959	.0117	.2
-3	3.099	.99884	.99738	.05400	.66760	.33418	.01351	.0010	49958	.0118	.3
.4	3.133	.99882	.99733	.05458	.66762	.33420	.01366	.0010	49957	.0119	-4
.5 .6	3.100	.99879	.99727	.05516	.66764	.33422	.01381	.0010	.49956	.0120	.6
))			ł	-49955		
-7 .8	3.232	.99874	.99715	.05632	.66768	.33425	.01410	.0010	49954	.0123	.7 .8
.9	3.299	.99869	.99709	.05090	.66772	.33427	.01424	.0011	.49953 .49952	.0124	.9
10.0	3.332	.99866	.99698	.05805	.66774			.0011			10.0
20.0	3.332	.99000	.99090	.050051	.007/4	.33431	.01453	.0011	49951	.0127	10.0

		C 1	v l	v I	77	V.	o=mL	_m η	Z=mI	"D	
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$					Δ
								n		n	
10.0	3.332	.99866	.99698	.05805	.66774	.33431	.01453	.0011	.49951	.0127	10.0
ı.	3.366	.99864	.99691	.05863	.66776	-33433	.01468	.0011	.49950	.0128	.1
.2	3.399	.99861	.99685	.05921	.66779	-33435	.01482	.0012	49949	.0129	.2
-3	3.432	.99858	.99679	.05979	.66781	-33437	.01497	.0012	.49948	.0131	.3
-4	3.466	.99856	.99673	.06036	.66783	.33439	.01511	.0012	-49947	.0132	.4
.5	3.499	.99853	.99667	.06094	.66785	.33441	.01526	.0012	.49946	.0133	.5
.6	3.532	.99850	.99660	.06152	.66787	.33443	.01540	.0012	-49945	.0134	.6
.7 .8	3.566	.99847	.99654	.06210	.66790	.33446	.01555	.0013	-49944	.0136	.7
.9	3.599 3.632	.99844	.99647	.06325	.66792	.33448	.01569	.0013	·49943 ·49942	.0137	.8
11.0	3.666			.06383	.66797			.0013			11.0
		.99838	.99634			33452	.01598		-49941	.0139	
.I .2	3.699 3.732	.99835	.99627 .99621	.06441	.66799 .66802	·33454 ·33456	.01612	.0014	49940	.0141	.I
.3	3.765	.99829	.99614	.06556	.66804	.33459	.01641	.0014	·49939 ·49937	.0142	.2
		.99826	.99607	.06614	.66806		.01656	.0014			
.4 .5	3.799 3.832	.99823	.99600	.06671	.66809	.33461	.01670	.0014	.49936 .49935	.0144	.4
.6	3.865	.99820	.99593	.06729	.66811	.33465	.01685	.0015	·49935 ·49934	.0140	.6
.7	3.899	.99817	.99586	.06787	.66814	.33468	.01699	.0015	.49933	.0148	.7
.8	3.932	.99814	.99579	.06844	.66816	.33470	.01714	.0015	.49933	.0149	.8
.9	3.965	.99811	.99572	.06902	.66819	.33472	.01728	.0016	.49931	.0151	.9
12.0	3.999	.99808	.99565	.06960	.66822	-33475	.01743	.0016	.49929	.0152	12.0
Ι.	4.032	.99804	.99557	.07017	.66824	-33477	.01757	.0016	.49928	.0153	°.I
.2	4.052	.99801	.99550	.07075	.66827	.33479	.01737	.0016	.49928	.0153	.2
.3	4.098	.99798	.99543	.07133	.66830	.33482	.01786	.0017	.49927	.0156	.3
.4	4.132	.99795	.99535	.07190	.66832	.33484	.01801	.0017	-49925	.0157	.4
.5	4.165	.99791	.99528	.07248	.66835	.33487	.01815	.0017	.49923	.0158	.5
.6	4.198	.99788	.99520	.07305	.66838	.33489	.01830	.0018	.49922	.0159	.6
.7	4.232	.99785	.99513	.07363	.66840	.33492	.01844	.0018	.49921	.0160	.7
.8	4.265	.99781	.99505	.07421	.66843	.33494	.01859	.0018	.49920	.0162	.8
.9	4.298	.99778	.99497	.07478	.66846	-33497	.01873	.0018	.49918	.0163	.9
13.0	4.331	.99774	.99489	.07536	.66849	.33499	.01888	.0019	.49917	.0164	13.0
ı.	4.365	.99771	.99481	.07593	.66852	.33502	.01902	.0019	.49916	.0165	.1
.2	4.398	.99767	.99474	.07651	.66854	.33504	.01917	.0019	.49915	.0167	.2
.3	4.431	.99764	.99467	.07708	.66857	-33507	.01931	.0020	.49913	.0168	.3
.4	4.465	.99760	.99457	.07766	.66860	.33510	.01946	.0020	.49912	.0169	.4
.5	4.498	-99757	.99449	.07823	.66863	.33512	.01960	.0020	.49911	.0170	
.6	4.531	∙99753	.99441	.07881	.66866	.33515	.01974	.0020	.49909	.0172	.6
.7	4.564	.99749	.99433	.07938	.66869	.33518	.01989	.0021	.49908	.0173	.7
.8	4.598	.99746	.99425	.07996	.66872	.33520	.02003	.0021	-49907	.0174	.8
.9	4.631	.99742	.99416	.08053	.66875	-33523	.02018	.0021	.49905	.0175	.9
14.0	4.664	.99738	.99408	.08111	.66878	-33526	.02032	.0022	.49904	.0177	14.0
.I	4.698	-99735	.99399	.08168	.66881	-33529	.02047	.0022	.49903	.0178	I.
.2	4.731	.99731	.99391	.08226	.66884	·33531	.02061	.0022	.49901	.0179	.2
1 .3	4.764	.99727	.99382	.08283	.66887	• 3 3534	.02076	.0023	.49900	.0180	.3
.4	4.797	.99723	.99374	.08340	.66890	-33537	.02090	.0023	.49898	.0182	.4
.5	4.831	.99719	.99365	.08398	.66893	.33540		.0023	.49897	.0183	.5
	4.864	.99715	.99356	.08455	.66897	•33543	.02119	.0024	.49896	.0184	ı
.7 .8	4.897	.99711	-99347	.08513	.66900	.33546		.0024	.49894	.0185	.7 .8
.9	4.930	.99708	.99339	.08570	.66903 .66906	-33549	.02148	.0024	.49893	.0186	.9
	4.964	.99704	.99330	ļ		-33552					
15.0	4.997	.99700	.99321	. 08685	. 66909	-33555	.02177	.0025	.49890	.0189	15.0

r								o=mL	"D	Z=mL	#D	
ı	Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	0=mL	-110	Z=mL	-10	Δ
L			L			L		m	n	m	n	
ı	15.0	4.997	.99700	.99321	.08685	.66909	.33555	.02177	.0025	.49890	.0189	15.0
ı	.1	5.030	.99696	.99312	.08742	.66913	.33558	.02191	.0025	.49888	.0190	.I
ı	.2	5.064	.99692	.99302	.08799	.66916	.33561	.02206	.0026	.49887	.0191	.2
ı	-3	.5.097	.99687	.99293	.08857	.66919	.33564	.02220	.0026	.49885	.0193	.3
ı	.4	5.130	.99683	.99284	.08914	.66923	.33567	.02235	.0026	.49884	.0194	.4
ı	-5	5.163	.99679	.99275	.08971	.66926	.33570	.02249	.0027	.49882	.0195	·5
ı	.6	5.197	.99675	.99265	.09028	.66929	-33573					- 1
ı	.7 .8	5.230	.99671	.99256	.09086	.66933	.33576	.02278	.0027	.49879	.0198	·7
ı	.9	5.296	.99662	.99237	.09200	.66940	.33582	.02307	.0028	.49876	.0200	.9
ı	16.0	5.330	.99658	.99227	.09257	.66943	-33585	.02321	.0028	.49875	.0201	16.0
ı	.1	5.363	.99654	,99218	.09315	.66947	-33588	.02336	.0029	.49873	.0202	.1
ı	.2	5.303	.99650	.99218	.09372	.66950	.33592	.02350	.0029	.49872	.0204	.2
ı	.3	5.429	.99645	.99198	.09429	.66954	-33595	.02365	.0029	.49870	.0205	-3
ı	.4	5.463	.99641	.99188	.09486	.669571	.33598	.02379	.0030	.49868	.0206	.4
ı	.5	5.496	.99637	.99178	.09543	.66961	.33601	.02393	.0030	.49867	.0207	-5
ı	.6	5.529	.99632	.99169	.09600	.66964	.33605	.02408	.0030	.49865	.0209	.6
i	.7	5.563	.99628	.99159	.09658	.66968	.33608	.02422	.0031	.49863	.0210	.7
ı	.8	5.596	.99623	.99148	.09715	.66972	.33611	.02437	.0031	.49862	.0211	.8
ı	.9	5.629	.99619	.99138	.09772	.66975	.33615	.02451	.0032	.49860	.0212	.9
ı	17.0	5.662	.99614	.99128	.09829	.66979	.33618	.02466	.0032	.49859	.0213	17.0
ı	.I	5.696	.99610	.99118	.09886	.66983	.33621	.02480	.0032	.49857	.0215	. I
ı	.2	5.729	.99605	.99108	.09943	.66986	.33625	.02494	.0033	.49855	.0216	.2
ı	-3	5.762	.99601	.99097	.10000	.66990	.33628	.02509	.0033	.49853	.0217	-3
ı	.4	5.796	.99596	.99087	.10057	.66994	.33632	.02523	.0033	.49852	.0218	-4
ı	-5	5.829	.99591	.99076	.10114	.66998	.33635	.02538	.0034	.49850	.0220	.5
ı	.6	5.862	.99587	.99066	.10171	.67002	.33639	.02552	.0034	.49848	.0221	.6
ı	.8	5.896	.99582	.99055	.10228	.67005	.33642 .33646	.02567	.0035	.49847	.0222	.7
ı	.9	5.929 5.962	.99577	.99044	.10205	.67009	.33649	.02595	.0035	.49843	.0223	.9
ı	18.0	5.995	.99568	.99023	.10399	.67017	.33653	.02610	.0036	.49841	.0226	18.0
ı		6.028		.99023	.10399	.67021	.33657	.02624	.0036	.49840	.0227	.1
ı	. I . 2	6.062	.99563	.99012	.10450	.67021	.33650	.02639	.0030	.49838	.0227	.2
ı	.3	6,095	.99553	.98990	.10570	.67029	.33664	.02653	.0037	.49836	.0229	-3
ı	.4	6.128	.99548	98979	.10627	.67033	.33667	.02667	.0037	.49834	,0230	.4
ı	.5	6.161	•99543	.98968	.10684	.67037	.33671	.02682	.0038	.49833	.0232	.5
ı	.6	6.194	.99538	.98957	.10741	.67041	.33675	.02696	.0038	.49831	.0233	.6
ı	.7	6.228	.99533	.98946	.10798	.67045	.33679	.02711	.0039	.49829	.0234	-7
ı	.8	6.261	.99528	.98935	.10855	.67049	.33682	.02725	.0039	.49827	.0235	.8
ı	.9	6.294	.99523	.98923	.10912	.67053	.33686	.02739	.co39	.49825	.0236	.9
ı	19.0	6.328	.99518	.98912	.10968	.67058	.33690		.0040	.49823	.0238	19.0
ı	.I	6.361	.99513		.11025		.33694	.02768	.0040	.49821	. 0239	.I
ı	.2	6.394			.11082		.33697	.02783	.0041	.4982C	.0240	.2
	.3	6.427			.11139			1	.0041	.49818	.0241	-3
	.4	6.461		1	.11196		.33705		.0041	.49816	.0242	.4
ı	.5 .6	6.494			.11252		.33709	1 .	.0042	.49814	.0244	·5
		1				1	1		.0043	.49810	1	.7
	.7 .8	6.560	.99482	.98831	.11366		.33717		.0043	.49810	.0240	.8
	.9	6.627	.99477		.11423		.33725		.0043	.49806	.0248	.9
	20.0	6.660			.11536		.33729		.0044	.49804	.0250	20.0
	20.5	0.000	.99400	1 .90193	1 .11330	.07200	1 .33129	102090		1 17504	1 30	

		-								_	
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	\underline{U}	\underline{V}	o=mL	-nD	Z=mL	-nD	Δ
Δ	A	\overline{L}	L	L	L	L	m	n	m	n	
20.0	6.660	.99466	.98795	.11536	.67100	.33729	.02898	.0044	.49804	.0250	20.0
. т	6.693	.99461	.98783	.11593	.67105	.33733	.02912	.0044	.49802	.0251	. г
.2	6.727	.99456	.98771	.11649	.67109	.33737	.02926	.0045	.49800	.0252	.2
.3	6.759	.99450	.98759	.11706	.67114	.33741	.02941	.0045	.49798	.0253	-3
.4	6.793	.99445	.98747	.11763	.67118	33745	.02955	.0046	.49796	.0254	-4
.5	6.826	.99439	.98734	.11819	.67123	-33749	.02969	.0046	49794	.0256	.5
.6	6.859	•99434	.98722	.11876	.67127	.33753	.02984	.0047	.49792	.0257	.6
.7 .8	6.892 6.926	.99428	.98710	.11932	.67132 .67136	.33757	.02998	.0047	.49790	.0258	.7
.9	6.959	.99423	.98685	.12046	.67141	.33766	.03013	.0048	.49786	.0259	.9
21.0	6.992	.99412	.98672	.12102	.67145	-33770	.03041	.0048	.49784	.0262	21.0
.1	7.026	.99412	.98660	.12159	.67150	-33774	.03041	.0049	.49782	.0263	. I
.2	7.059	.99400	.98647	.12159	.67155	.33778	.03050	.0049	.49780	.0264	.1
-3	7.092	.99395	.98634	.12272	.67159	.33783	.03084	.0050	.49778	.0265	.3
.4	7.125	.99389	.98622	.12328	.67164	.33787	.03099	.0050	.49776	.0266	.4
.5	7.158	.99383	.98609	.12385	.67169	.33791	.03113	.0051	.49774	.0267	.5
.6	7.192	.99378	.98596	.12441	.67173	.33796	.03127	.0051	.49772	.0269	.6
-7	7.225	.99372	.98583	.12497	.67178	.33800	.03142	.0052	.49770	.0270	.7
.8	7.258	.99366	.98570	.12554	.67183	.33804	.03156	.0052	.49768	.0271	.8
.9	7.291	.99360	.98557	.12610	.67188	_33809	.03170	.0053	.49765	.0272	.9
22.0	7.324	-99354	98544	.12667	.67193	33813	.03185	.0053	.49763	.0273	22.0
.1	7.358	.99349	.98531	.12723	.67197	.33818	.03199	.0054	.49761	.0275	.ı
.2	7.391	.99343	.98517	.12779	.67202	.33822	.03213	.0054	-49759	.0276	.2
-3	7.424	.99337	.98504	. 12836	.67207	.33827	.03228	.0055	-49757	.0277	.3
-4	7.458	.99331	.98491	.12892	.67212	.33831	.03242	.0055	-49755	.0278	-4
·5 .6	7.491 7.524	.99325	.98477 .98464	.12948	.67217 .67222	.33836	.03256	.0056	.49752	.0279	·5 ·6
			.98450	.13061	.67227	.33845	.03271		1	.0282	
.7 .8	7.557 7.590	.99313	.98437	.13001	.67232	.33849	.03205	.0057	.49748 .49746	.0283	·7
.9	7.623	.99301	.98423	.13173	.67237	.33854	.03314	.0058	-49744	.0284	.9
23.0	7.657	.99295	.98409	.13230	.67242	.33859	.03328	.0058	.49741	.0285	23.0
.1	7.690	.99288	.98396	.13286	.67247	.33863	.03342	.0059	-49739	.0286	. т
.2	7.723	.99282	.98382	.13342	.67252	.33868	.03357	.0059	.49737	.0288	.2
-3	7.756	.99276	.98368	.13398	.67258	.33873	.03371	.0060	-49735	.0289	.3
.4	7.789	.99270	.98354	.13454	.67263	.33877	.03385	.0060	.49732	.0290	.4
.5	7.822	.99264	.98340	.13510	.67268	.33882	.03400	.0061	.49730	.0291	-5
.6	7.856	.99257	.98326	.13567	.67273	.33887	.03414	.0061	.49728	.0292	.6
.7	7.889	.99251	.98312	. 13623	.67278	.33892	.03428	.0062	.49725	.0293	.7
.8	7.922	.99245	.98298	.13679	.67284 .67289	.33896	.03443	.0062	.49723	.0295	.8
.9	7.955	.99238	.98283	.13735		.33901	.03457	.0063	.49721	.0296	.9
24.0	7.989	.99232	.98269	.13791	.67294	.33906	.03471	.0063	.49718	.0297	24.0
.I	8,022 8.055	.99226	.98255	.13847	.67300 .67305	.33911	.03485	.0064	.49716	.0298	.I
.3	8.088	.99219	.98226	.13903	.67310	.33916	.03500	.0064	.49714	.0300	.2
.4	8.121	.99213	.98211	.14015	.67316	.33926	.03528	.0065	.49709	. 0302	.4
-5	8.154	.99200	.98197	.14013	.67321	.33931	.03543	.0066	.49709	.0302	.5
.6	8.188	.99193	.98182	.14127	.67327	.33936	.03557	,0066	.49704	.0304	.6
.7	8.221	.99187	.98167	.14183	.67332	.33941	.03571	.0067	.49702	.0305	.7
.8	8.254	.99180	.98153	.14239	.67338	.33946	.03585	.0067	.49699	.0306	.8
.9	8.287	99174	.98138	.14295	.67343	.33951	.03600	.0068	.49697	.0307	.9
25.0	8.321	.99167	.98123	.14350	.67349	.33956	.03614	.0068	.49695	.0309	25.0

	$C \mid X \mid V \mid II \mid V \mid o=mL-nD \mid Z=mL-nD$										
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$					Δ
								n		n	
25 [°] .0	8.321	.99167	.98123	.14350	.67349	.33956	.03614	.0068	.49695	.0309	25.0
. r	8.354	.99160	.98108	.14406	.67354	.33961	.03628	.0069	.49692	.0310	.I
.2	8.387	.99154	.98093	.14462	.67360	.33966	.03643	.0069	.49690	.0311	. 2
-3	8.420	.99147	.98078	.14518	.67365	.33971	.03657	.0070	.49687	.0312	•3
.4	8.453 8.486	.99140	.98063 .98048	.14574	.67371	.33976	.03671	.0071	.49685	.0313	.4 .5
·5	8.519	.99133	. 98033	.14685	.67382	.33987	.03700	.0072	.49680	.0314	.6
.7	8.553	.99120	.98017	.14741	.67388	.33992	.03714	.0072	.49677	.0317	.7
.8	8.586	.99113	.98002	.14797	.67394	-33997	.03728	.0073	.49675	.0318	.8
.9	8.619	.99106	.97987	.14852	.67400	.34002	.03742	.0073	.49672	.0319	.9
26.0	8.652	.99099	.97971	.14908	.67405	. 34008	.03757	.0074	.49670	.0320	26.0
ı.	8.685	.99092	.97956	.14964	.67411	.34013	.03771	.0074	.49667	.0321	ı,
.2	8.719	.99085	.97940	.15019	.67417	.34018	.03785	.0075	.49665	.0322	.2
.3	8.752	.99078	.97925	.15075	.67423	.34024	.03800	.0076	.49662	.0323	.3
.4	8.785 8.818	.99071	.97909	.15131	.67429 .67435	.34029	.03814	.0076	.49660 .49657	.0325	.4
·5	8.851	.99004	.97878	.15160	.67441	.34035	.03842	.0077	.49654	.0326	·5
.7	8.884	.99050	.97862	.15297	.67447	.34045	.03857	.0078	.49652	.0328	
.8	8.917	.99030	.97846	.15353	.67452	.34043	.03871	.0078	.49649	.0320	.7
.9	8.951	.99036	.97830	.15408	.67458	.34056	.03885	.0079	.49647	.0330	.9
27.0	8.984	.99029	.97814	.15464	.67465	.34062	.03899	.0080	.49644	.0331	27.0
. т	9.017	.99022	.97798	.15519	.67471	.34067	.03913	.0080	.49641	.0333	.I
.2	9.050	.99014	.97782	.15575	.67477	.34073	.03929	.0081	.49639	.0334	.2
.3	9.083	.99007	.97766	.15630	.67483	.34079	.03942	.0081	.49636	.0335	-3
-4	9.116	.99000	.97749	.15686	.67489	.34084	.03956	.0082	.49633	.0336	.4
.5	9.149	.98993	•97733	.15741	.67495	.34090	.03970	.0082	.49631	.0337	.5
.6	9.183	.98985	.97717	.15796	.67501	.34095	.03985	.0083	.49629	.0338	.6
.7 .8	9.216 9.249	.98978 .98971	.97700	.15852	.67507 .67514	.34101	.03999	.0084	.49625	.0339	.7
.9	9.249	.98963	.97667	.15962	.67520	.34113	.04027	.0085	.49620	.0342	.9
28.0	9.315	.98956	.97651	,16018	.67526	.34118	.04041	.0085	.49617	.0343	28.0
1.	9.348	.98948	.97634	,16073	.67532	.34124	.04056	.0086	.49615	.0344	.1
.2	9.381	.98941	.97617	.16128	.67539	.34130	.04070	.0087	.49612	.0345	.2
.3	9.415	.98933	.97601	.16183	.67545	.34136	.04084	.0087	.49609	.0346	-3
.4	9.448	.98926	.97584	. 16239	.67551	.34141	.04098	.0088	.49606	.0347	-4
-5	9.481	.98918	.97567	.16294	.67558	-34147	.04113	.0088	.49604	.0348	.5
.6	9.514	.98911	.97550	.16349	.67564	.34153	.04127	.0089	.49601	.0349	.6
.7	9.547	.98903	.97533	.16404	.67571	.34159	.04141	.0090	.49598	.0351	.7 .8
. 8	9.580	.98895	.97516	.16459 .16514	.67577	.34165	.04155	.0090	.49595 .49592	.0352	.9
29.0	9.647	.98880	.97482	.16569	.67590	.34177	.04184	.0092	.49590	.0354	29.0
.I	9.680	.98872	.97465	.16624	.67597	.34183	.04198	.0092	.49587	.0355	.1
.1	9.713	.98865	.97403	.16679	.67603	.34189	.04198	.0092	.49584	.0356	.2
.3	9.746	.98857	.97430	.16734	.67610	.34195	.04226	.0093	.49581	.0357	.3
.4	9.779	.98849	.97413	.16789	.67616	.34201	.04240	.0094	.49578	.0358	.4
.5	9.812	.98841	.97395	.16844	.67623	.34207	.04254	.0095	.49575	.0359	.5
.6	9.845	.98833	.97378	.16899	.67630	.34213	.04269	.0095	.49573	.0361	.6
.7	9.878	.98826	.97360	.16954	.67636	.34219	.04283	.0096	.49570	.0362	.7
.8	9.911	.98818	.97343	.17009	.67643	.34225	.04297	.0097	.49567	.0363	.8
.9 30.0	9.945		.97325	.17064	67650	.34232	.04311	.0097	.49561	.0365	30.0
30.0	9.978	98802	.97307	.17119	.67657	.34238	.04325	.0098	.49501	.0305	30.0

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ı	Δ	A	C L	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=m1	Δ	
L	4		L	L	L	L	L	m	n	m	n	
3(0.0	9.978	.988c2	.97307	.17119	.67657	.34238	.04325	.0098	.49561	.0365	30.0
	.I	10.011	.98794	.97290	.17174	.67663	.34244	.04339	.0098	.49558	.0366	.I
	.2	10.044	.98786	.97272	.17229	.67670	.34250	.04354	.0099	49555	.0367	.2
1	-3	10.077	.98778	.97254	.17283	.67677	34257	.04368	.0100	-49552	.0368	.3
L	-4	10.110	.98770	.97236	.17338	.67684	.34263	.04382	.0100	49549	.0369	-4
•	.5	10.143	.98762	.97218	.17393	.67691	.34269	.04396	.0101	.49546	.0371	.5
	- 1	10.176	.98754	.97200	.17448	.67698	.34276	.04410	.0102	-49543	.0372	i
ı	·7	10.209	.98745	.97182	.17502	.67705 .67712	.34282	.04424	.0102	.49540 .49537	.0373	.7
ı	.9	10.276	.98729	.97146	.17612	.67719	.34295	.04453	.0103	49534	.0375	.9
31	1.0	10.309	.98721	.97127	.17666	.67726	.34301	.04467	.0104	·49531	.0376	31.0
1	.1	10.342	.98713	.97109	.17721	.67733	.34308	.04481	.0105	.49528	.0377	1.
1	.2	10.375	.98704	.97091	.17776	.67740	.34314	.04495	.0106	.49525	.0378	.2
1	-3	10.408	.98696	.97072	.17830	.67747	.34321	.04509	.0106	.49522	.0379	-3
•	.4	10.441	.98688	.97054	. 17885	.67754	.34327	.04523	.0107	-49519	.0380	.4
	.5	10.474	.98680	.97035	.17939	.67761	.34334	.04538	.0108	.49516	.0381	-5
ı	.6	10.507	.98671	.97017	. 17994	.67768	.34340	.04552	.0108	-49513	.0383	.6
	-7	10.540	.98663	.96998	. 18048	.67775	-34347	.04566	.0109	.49510	.0384	.7
	.8	10.573	.98654	.96979	.18103	.67783	·34353	.04580	.0110	49507	.0385	.8
	.9	10.607	.98646	.96960	.18157	.67790	.34360	.04594	.0110	49504	.0386	.9
32	1.0	10.640	.98637	.96942	.18212	.67797	.34367	.04608	.0111	.49501	.0387	32.0
	.I	10.673	.98629	.96923	.18266	.67804	.34373	.04622	.0112	49498	.0388	. I
1	.2	10.706	.98620	.96904	.18320	.67812	.34380	.04636	.0112	+49495	.0389	.2
	.3	10.739	.98612	.96885	.18375	.67819	.34387	.04650	.0113	-49491	.0390	-3
1	·4 ·5	10.772 10.805	.98603	.96866	.18429	.67826 .67834	·34394 ·34400	.04665	.0114	.49488	.0391	-4
1	.6	10.838	.98586	.96828	. 18538	.67841	.34407	.04693	.0115	.49482	.0392	·5
ı	.7	10.871	.98577	.96808	. 18592	.67849	.34414	.04707	.0116	.49479	.0394	.7
ı	.8	10.904	.98569	.96789	. 18646	.67856	.34421	.04721	.0116	.49476	.0395	.8
	.9	10.937	.98560	.96770	.18700	.67864	.34428	.04735	.0117	-49473	.0397	.9
33	3.0	10.970	.98551	.96750	.18754	.67871	-34435	.04749	.0118	.49469	.0398	33.0
ı	ı.	11.003	.98543	.96731	.18809	.67879	.34442	.04763	.0118	.49466	.0399	. т
ì	.2	11.036	.98534	.96712	.18863	.67886	.34448	.04777	.0119	.49463	.0400	.2
1	-3	11.069	.98525	.96692	.18917	.67894	-34455	.04791	.0120	.49460	.0401	-3
	-4	11.103	.98516	.96672	. 18971	.67901	.34462	.04805	.0121	-49457	.0402	.4
	.5	11.136	.98507	.96653	.19025	.67909	.34469	.04820	.0121	-49453	.0403	.5
	.6	11.169	.98499	.96633	.19079	.67917	-34477	.04834	.0122	-49450	.0404	.6
1	·7	11.202	.98490	.96613	.19133	.67925	.34484	.04848	.0123	-49447	.0405	.7
	.9	11.235 11.268	.98481	.96593 .96574	.19187	.67932 .67940	.34491	.04802	.0123	-49443 -49440	.0406	.9
24	1.0	11.301	.98463	.96554	.19295	.67948	.34505	.04890	.0125	•49437	.0408	34.0
		11.334	.98454	.96534	.19349	.67956	.34512	.04904	.0126	49434	.0409	.1
1	.I	11.367	.98445	.96514	.19349	.67963	.34519	.04904	.0126	.49434	.0409	.2
1	.3	11.400	.98436	.96494	.19457	.67971	-34527	.04932	.0127	.49427	.0411	-3
	.4	11.433	.98427	.96473	.19510	.67979	-34534	.04946	.0128	.49424	.0412	.4
1	.5	11.456	.98417	.96453	.19564	.67987	.34541	.04960	.0128	.49420	.0413	.5
	.6	11.499	. 98408	.96433	.19618	.67995	.34548	.04974	.0129	.49417	.0415	.6
	.7	11.532	.98399	.96413	.19672	.68003	-34556	.04988	.0130	.49414	.0416	.7
i	.8	11.565	.98390	.96392	.19726	.68011	.34563	.05002	.0131	.49410	.0417	.8
١.	.9	11.598	.98381	.96372	.19779	.68019	-34570	.05016	.0131	.49407	.0418	.9
3	5.0	11.631	.98371	.96351	.19833	.68027	.34578	.05030	.0132	.49404	.0419	35.0

TABLE VIII. — (Continued)

			-				o=mL	#D	77	"D	
Δ	A	$\frac{C}{L}$	$\frac{X}{}$	$\frac{Y}{L}$	$\frac{U}{L}$	\underline{V}	0=mL	- 10	Z=mI	-nD	Δ
_	•	L	\overline{L}	L		L	m	n	m	n	
35°.0	11.631	.98371	.96351	. 19833	.68027	.34578	.05030	.0132	.49404	.0419	35.0
.I	11.664	.98362	. 96331	.19887	.68035	.34585	.05044	.0133	. 49400	.0420	.1
.2	11.698	.98353	.96310	. 19940	. 68043	-34593	.05058	.0133	.49397	.0421	.2
-3	11.731	.98344	.96290	.19994	.68051	.34600	.05072	.0134	-49393	.0422	-3
-4	11.764	. 98334	.96269	.20047	.68059	.34608	.05086	.0135	.49390	.0423	.4
.5	11.797	.98325	.96248	.20101	.68068	.34615	.05100	.0136	.49387	.0424	.5
.6	11.830	.98315	.96227	.20155	.68076	.34623	.05115	.0136	.49383	.0425	.6
.7	11.863	.98306	. 96207	. 20208	.68084	.34630	.05129	.0137	.49380	.0426	.7
.8	11.896	.98297	.96186	,20262	.68092	.34638	.05143	.0138	.49376	.0427	.8
.9	11.929	. 98287	.96165	.20315	.68101	.34645	.05157	.0139	-49373	.0428	.9
36.0	11.961	.98278	.96144	.20368	.68109	.34653	.05171	.0139	. 49369	.0429	36.0
	11.994	.98268	.96123	.20422	.68117	.34661	.05185	.0140	.49366	.0430	.1
.I .2	12.027	.98259	.96102	.20422	.68126	.34668	.05199	.0140	.49362	.0431	.2
.3	12.061	.98249	.96080	.20529	.68134	.34676	.05213	.0142	49359	.0432	.3
			.96059	.20582	.68142	.34684	.05227	.0142			
-4	12.094 12.127	.98239	.96038	.20502	.68151	.34692	.05241	.0142	.49355 .49352	.0433	·4 ·5
.5 .6	12.127	.98230	.96017	.20689	.68159	.34699	.05255	.0144	.49332	.0435	.6
		.98210		.20742	.68168	.34707	.05269	.0145	. 49345	.0436	.7
.7 .8	12.192 12.226	.98201	·95995 ·95974	.20742	.68176	.34715	.05282	.0145	.49343	.0430	.8
.9	12.259	.98191	.95952	.20848	.68185	.34723	.05296	.0146	. 49338	.0437	.9
37.0				.20901	.68194	-34731	.05310	.0147			37.0
	12.292	.98181	.95931						49334	.0439	
ı.	12.324	.98171	.95909	.20955	.68202	·34739	.05324	.0148	.49330	.0440	ı,ı
.2	12.358	.98162	.95887 .95866	.21008	.68211	·34747 ·34754	.05338	.0149	.49327	.0441	.2
-3	12.391	.98152					.05352		. 49323	.0442	
.4	12.424	.98142	.95844	.21114	.68228	.34762	.05366	.0150	.49320	.0443	-4
.5	12.456	.98132	.95822	.21167	.68246	.34770	.05380	.0151	.49316	.0444	.5
.6	12.489	.98122	.95800			-34779	.05394	.0152	.49312	.0445	
.7	12.523	.98112	.95778	.21273	.68254	.34787 .34795	.05408	.0152	.49309	.0446	.7
.8	12.556	.98102	.95756 .95734	.21320	.68272	.34803	.05422	.0153	.49305	.0447	.9
.9					.68281	.34811					38.0
38.0	12,621	.98082	.95712	.21432			.05450	.0155	.49298	.0449	
ı.	12.654	.98072	.95690	.21485	.68290	.34819	.05464	.0156	.49294	.0450	I.
.2	12.687	.98062	.95668	.21537	.68299	.34827	.05478	.0156	.49291	.0451	.2
-3	12.720	.98052	.95646	.21590			.05492		.49287	.0452	-3
-4	12.753	.98042	.95623	.21643	.68316 .68325	.34844	.05506	.0158	.49283	.0453	.4
·5	12.786	.98032	.95601	.21696	.68334	.34852	.05520	.0159	.49279	.0454	.6
		-			.68343			.0159			
.7	12.852	.98011	.95556	. 21801	.68353	.34869	.05548	.0161	.49272	.0456	.7 .8
.8 .8	12.885	.98001	.95533	.21907	.68362	.34885	.05575	.0162	.49265	.0457	.9
					.68371			.0163			39.0
39.0	12.951	.97981	.95488	. 21959		.34894	.05589		.49261	.0459	
ı.	12.984	.97970	.95466	.22012	.68380	.34902	.05603	.0163	.49257	.0460	I.
.2	13.017	. 97960	.95443	.22005	.68398	.34911	.05617	.0165	.49253	.0461	.2
-3	13.050	.97950	.95420			.34919			.49250	.0462	.3
.4	13.083	.97939	.95397	.22170	.68408	.34928	.05645	.0166	.49246	.0463	.4
·5	13.116	.97929	.95374 .95351	.22222	.68417	.34936 .34945	.05659	.0167	.49242	.0464	·5
		.97919									
.7	13.182	.97908	.95328	. 22327	.68435 .68445	34953	.05687	.0168	. 49234	.0466	.7
.8	13.215 13.247	.97898	.95305 .95282	.22379	.68454	.34962	.05701	.0170	.49231	.0468	.9
40.0	1			,22484	.68464		.05728	.0170	.49227	.0469	
40.0	13.281	.97877	.95259	. 22404	.00404	+34979	.05/28	.01/1	.49223	.0409	20.0

TABLE IX. — Spiral Functions for Change of 0.2° per 100 Feet Suitable for Speeds of 104 Miles an Hour or Less and Curves of 1° or Less

L D	CURVES OF I OR LESS											
10	L	D	Δ	A	Z	0	С	X	Y	U	V	
20		•	•	•	,			-				
20	10	0.02	0.001	0,000	5.00	0.00	10.00	10.00	0.00	6.67	3.33	
30	20	.01	.004	.001		.00	20.00	20.00	.00	13.33		
40						.00	30.00	30.00	.00			
10			-	-			-					
60 .12 .036 .012 30.00 .00 60.00 60.00 .01 40.00 20.00 70 .14 .049 .016 35.00 .00 70.00 70.00 .02 46.67 23.33 26.67 90 .18 .081 .027 45.00 .01 80.00 80.00 .03 53.33 26.67 90 .18 .081 .027 45.00 .01 100.00 .06 66.67 33.33 26.67 100 .20 .101 .055 .00 .20 100.00 .06 66.67 33.33 36.67 20 .24 .144 .048 60.00 .03 20.00 .10 80.00 40.00 30 .225 .055 .050 .05 .50.00 .50.00 .10 93.33 46.67 50 .32 .225 .085 80.00 .05 50.00 50.00 .22 100.00												
70 1.14 0.09 0.016 35.00 0.00 70.00 70.00 0.02 46.67 23.33 26.67 80 .16 0.61 .021 40.00 .01 80.00 80.00 .03 53.33 26.67 90 .18 .081 .027 45.00 .01 100.00 100.00 .04 60.00 30.00 100 .20 .101 .040 55.00 .02 10.00 100.00 .06 66.67 33.33 36.67 20 .24 .144 .048 60.00 .03 20.00 20.00 .10 80.00 40.00 30 .26 .166 .056 65.00 .03 30.00 .13 86.67 43.33 46.67 50 .30 .225 .075 75.00 .05 50.00 .20 .10 .20 .24 46.67 23.33 46.67 70 .34 .289 .096												
86 .16 .064 .021 49.00 .01 80.00 80.00 .03 53.33 26.67 90 .18 .081 .027 45.00 .01 90.00 90.00 .04 66.00 30.00 100 .22 .121 .040 55.00 .02 10.00 100.00 .08 73.33 36.67 20 .24 .144 .048 60.00 .03 20.00 20.00 .10 80.00 40.00 30 .26 .169 .056 65.00 .03 30.00 30.00 .13 86.67 43.33 46.67 50 .30 .225 .075 75.00 .05 50.00 50.00 .10 93.33 46.67 80 .36 .324 .108 90.00 .88.00 .60 60.00 60.00 .24 66.67 .53.33 76.67 80 .36 .34 .289 .096 85.00		1 1	- 1		-							
90												
100						1						
10	90	.18	.081	.027	45.00	.01	90.00	90.00		60.00	30.00	
20	100	.20	.100	.033	50.00	.01	100.00	100.00	.06	66,67	33.33	
30	10	.22	. 121	.040	55.00	.02	10.00	10.00	.08	73.33	36.67	
40	20	.24	. 144	.048	60.00	.03	20.00	20.00	.10	80.00	40.00	
40	30	26	160	.056	65.00	.03	30,00	30.00	,13	86.67		
50 .30 .225 .075 75.00 .05 \$0.00 \$50.00 .20 \$100.00 \$50.00 60 .32 .256 .085 80.00 .06 60.00 60.00 .24 06.67 \$3.33 70 .34 .289 .096 85.00 .07 70.00 .28 \$13.33 \$56.67 80 .36 .324 .108 99.00 .08 80.00 80.00 .34 20.00 60.00 90 .38 .361 .120 95.00 .10 90.00 90.00 .40 26.67 63.33 200 .40 .400 .133 100.00 .15 200.00 200.00 .47 133.33 66.67 20 .44 .484 .161 110.00 .15 20.00 20.00 .62 46.67 73.33 30 .46 .529 .176 115.00 .18 30.00 30.00 .71 53.33												
60 .32 .256 .085 80.00 .06 60.00 60.00 .24 66.67 53.33 70 .34 .289 .096 85.00 .07 70.00 70.00 .28 13.33 56.67 80 .36 .324 .108 90.00 .08 80.00 80.00 .34 20.00 60.00 60.00 .36.67 60.00 .33 .361 .120 95.00 .10 90.00 .90.00 .40 .46.67 60.00 .60.00 .40 .40 .43 .10 .10 .12 200.00 .20 .47 133.33 .66.67 73.33 .30 .46 .529 .176 115.00 .18 .30.00 .30 .00 .51 200.00 .54 .40.00 .70.00 40 .48 .576 .192 120.00 .22 .40.00 .80.60 .80.00 .71 .53.33 .76.67 40 .48 .576 .192 .120.00 <th></th> <th></th> <th></th> <th>- 1</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>				- 1								
70 .34 .289 .096 85.00 .07 70.00 70.00 .28 13.33 \$6.67 80 .36 .324 .108 99.00 .08 80.00 80.00 .34 20.00 60.00 90 .38 .361 .120 95.00 .10 99.00 .40 .40 .133 100.00 .12 200.00 200.00 .40 .26.67 6.33 10 .42 .441 .147 105.00 .13 10.00 10.00 .54 40.00 70.00 20 .44 .484 .161 110.00 .15 20.00 20.00 .62 46.67 73.33 76.67 40 .48 .576 .192 120.00 .20 40.00 40.00 .80 60.00 80.00 80.00 .91 66.67 83.33 66 72 .676 .225 130.00 .26 60.00 60.00 10.00 .14 80.00 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th>- 1</th> <th></th> <th></th> <th>1</th> <th></th> <th></th>						- 1			1			
80 .36 .324 .108 90.00 .08 80.00 80.00 .34 20.00 60.00 90 .38 .361 .120 95.00 .10 90.00 90.00 .40 26.67 63.33 10 .42 .441 .147 105.00 .13 100.00 10.00 100.00 .54 40.00 70.00 20 .44 .484 .161 110.00 .15 20.00 20.00 .62 46.67 73.33 30 .46 .529 .176 115.00 .18 30.00 30.00 .71 53.33 76.67 40 .48 .576 .192 120.00 .20 40.00 .40.00 .80 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 60.00 90 90.00 80.00 70.90 1.14 80.00 90.00 80 .56 .784 .225 1												
90 38 .36f .120 95.00 .10 90.00 90.00 .40 26.67 63.33 200 .40 .400 .133 100.00 .12 200.00 200.00 .47 133.33 66.67 10 .42 .441 .147 105.00 .13 10.00 10.00 .54 40.00 70.00 20 .44 .484 .161 110.00 .15 20.00 20.00 .62 46.67 73.33 76.67 40 .48 .576 .192 120.00 .20 40.00 40.00 .80 60.00 80.00 50 .625 .676 .225 130.00 .23 50.00 .50.00 .91 .66.67 83.33 60 .52 .676 .225 130.00 .26 60.00 60.00 10.22 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00<												
200 .40 .4co .133 100.00 .12 200.00 200.00 .47 133.33 66.67 10 .42 .441 .147 105.00 .13 10.00 10.00 .54 40.00 70.00 20 .44 .484 .161 I10.00 .15 20.00 20.00 .62 46.67 73.33 76.67 40 .48 .576 .192 120.00 .20 40.00 40.00 .80 60.00 80.00 50 .50 .625 .208 125.00 .23 50.00 50.00 .91 66.67 83.33 60 .52 .676 .225 .130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 1.14 80.00 90.00 80 .56 .784 .261 .140.00 .32 80.00 79.99 1.28<		- 1			_							
10 .42 .441 .147 105.00 .13 10.00 10.00 .54 40.00 70.00 20 .44 .484 .161 110.00 .15 20.00 20.00 .62 46.67 73.33 30 .46 .529 .176 115.00 .18 30.00 30.00 .62 46.67 73.33 76.67 40 .48 .576 .192 120.00 .20 20.00 40.00 .80 60.00 80.00 50 .50 .625 .208 125.00 .23 50.00 50.00 .91 66.67 83.33 60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 1.014 80.00 99 1.28 86.67 93.34 90 .58 .841 .280 145.00 .32												
20 .44 .484 .161 I10.00 .15 20.00 20.00 .62 46.67 73.33 30 .46 .529 .176 I15.00 .18 30.00 30.00 .71 53.33 76.67 40 .48 .576 .192 I20.00 .20 40.00 .80 60.00 80.00 .71 53.33 76.67 50 .625 .208 I25.00 .23 50.00 50.00 .91 66.67 83.33 60 .52 .676 .225 I30.00 .29 770.00 70.00 1.14 80.00 90.00 80 .56 .784 .280 I45.00 .32 80.00 79.99 I.28 86.67 93.34 90 .58 .841 .280 I45.00 .35 90.00 89.99 I.57 200.00 100.00 10 .62 .961 .320 I55.00 .43 10.00 39.99 1.9			-									
30 .46 .529 .176 115.00 .18 30.00 30.00 .71 53.33 76.67 40 .48 .576 .192 120.00 .20 40.00 40.00 .80 60.00 80.00 50 .50 .625 .208 125.00 .23 50.00 .50.00 .91 66.67 83.33 60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80 .56 .784 .261 140.00 .32 80.00 79.99 1.28 86.67 93.34 90 .58 .841 .280 145.00 .32 80.00 79.99 1.28 86.67 93.33 96.67 300 .60 .900 .330 150.00 .48 20.00 1.73 <th>10</th> <th>-42</th> <th>.441</th> <th>.147</th> <th>105.00</th> <th>.13</th> <th>10.00</th> <th>10.00</th> <th></th> <th>40.00</th> <th>70.00</th>	10	-42	.441	.147	105.00	.13	10.00	10.00		40.00	70.00	
40 .48 .576 .192 120.00 .20 40.00 40.00 .80 60.00 80.00 50 .50 .625 .208 125.00 .23 50.00 .50.00 .91 66.67 83.33 60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80 .56 .784 .261 140.00 .32 80.00 79.99 1.28 86.67 93.34 90 .58 .841 .280 145.00 .35 90.00 89.99 1.42 93.33 96.67 300 .60 .900 .300 150.00 .39 300.00 99.99 1.57 200.00 100.00 10 .62 .961 .320 155.00 .43 10.00 309.99 1.73 06.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 131 3.3 106.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99 39.99 2.29 20.00 110.00 40 .68 1.156 .385 170.00 .62 49.99 49.98 2.49 33.34 116.67 60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98 2.95 46.67 123.34 80 .76 1.444 .481 189.99 .80 79.99 79.98 3.19 53.34 126.67 90 .78 1.521 1.507 194.99 86 89.99 89.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.52 266.68 133.34 40 .88 1.936 6.645 219.99 1.08 19.98 19.96 4.01 73.35 136.68 50 .90 2.025 6.675 224.99 1.33 49.98 49.94 5.30 30.00 2 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86.66 133.35 40 .88 1.936 6.45 219.99 1.24 39.98 39.95 6.04 4.33 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86.66 133.35 40 .85 1.936 68 23.04 .768 234.99 1.51 69.97 69.93 6.04 13.36 156.69 50 .90 2.025 6.75 224.99 1.31 49.98 49.94 5.30 30.00 2 150.02 60 .92 2.116 .7	20	.44	. 484							46.67		
50 .50 .625 .208 125.00 .23 50.00 .50.00 .91 66.67 83.33 60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80.99 1.28 86.67 93.34 90.05 89.99 1.28 86.67 93.34 96.67 30.00 89.99 1.28 86.67 93.34 96.67 30.34 90.00 89.99 1.57 200.00 100.00 300 .60 .900 .320 155.00 .43 10.00 39.99 1.73 06.67 103.34 10.00 30 300.00 99.99 1.57 200.00 100.00 30 300.00 99.99 1.57 200.00 100.00 30 300.00 99.99 1.57 200.00 100.00 30 300.00 99.99 1.	30	.46	.529								76.67	
60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80 .56 .784 .280 145.00 .32 80.00 79.99 1.28 86.67 93.34 96.67 300 .60 .900 .300 150.00 .39 300.00 99.99 1.57 200.00 100.00 10 .62 .961 .320 155.00 .43 10.00 309.99 1.73 66.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 106.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 2.00 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99	40	.48	.576	.192	120.00	.20	40.00	40.00	.80	60.00	80.00	
60 .52 .676 .225 130.00 .26 60.00 60.00 1.02 73.33 86.67 70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80 .56 .784 '.261 140.00 .32 80.00 79.99 1.28 86.67 93.34 90 .58 .841 .280 145.00 .35 90.00 89.99 1.42 93.33 96.67 300 .60 .900 .300 150.00 .39 300.00 99.99 1.57 200.00 100.00 10 .62 .961 .320 155.00 .43 10.00 399.99 1.73 66.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.99 13.33 106.67 30 .66 1.024 .341 160.00 .57 39.99 39.99	50	.50	.625	.208	125.00	.23	50.00	50.00	.91	66.67	83.33	
70 .54 .729 .243 135.00 .29 70.00 70.00 1.14 80.00 90.00 80 .56 .784 .261 140.00 .32 80.00 79.99 1.28 86.67 93.34 96.67 300 .58 .841 .280 145.00 .35 90.00 89.99 1.42 93.33 96.67 300 .60 .900 .320 155.00 .43 10.00 309.99 1.73 06.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 166.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 2.09 20.00 110.33 40 .68 1.156 .385 170.00 .57 39.99 39.99 2.99 20.00 110.33 50 .70 1.225 .408 175.00 .62 49.99				.225	130.00	.26	60.00	60.00	1.02	73.33		
80 .56 .784 .261 140.00 .32 80.00 79.99 1.28 86.67 93.34 90 .58 .841 .280 145.00 .35 90.00 89.99 1.42 93.33 96.67 300 .60 .900 .300 150.00 .39 300.00 99.99 1.57 200.00 100.00 10 .62 .961 .320 155.00 .43 10.00 309.99 1.73 06.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 106.67 30 .66 1.089 .363 165.00 .52 29.99 2.99 2.09 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99 39.99 2.29 26.67 113.34 116.00 50 .70 1.225 .408 175.00 .62 49.99	70			.243	135.00	.29	70.00	70.00	1.14		90.00	
90	85			° 26т	T40.00	32	80.00	70 00	T 28	86 67		
300 .60 .900 .300 150.00 .39 300.00 99.99 1.57 200.00 100.00 10 .62 .961 .320 155.00 .43 10.00 309.99 1.73 66.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 106.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 2.09 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99 39.99 2.29 26.67 113.34 50 .70 1.225 .408 175.00 .62 49.99 49.98 2.49 33.34 116.67 60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98												
10 .62 .961 .320 155.00 .43 10.00 399.99 1.73 .66.67 103.34 20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 106.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 2.09 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99 39.99 2.29 26.67 113.34 50 .70 1.225 .408 175.00 .62 49.99 49.98 2.49 23.34 116.67 60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98 2.95 46.67 123.34 80 .75 1.444 .481 189.99 .80 79.99 79.98												
20 .64 1.024 .341 160.00 .48 20.00 19.99 1.91 13.33 166.67 30 .66 1.089 .363 165.00 .52 29.99 29.99 2.09 20.00 110.00 40 .68 1.156 .385 170.00 .57 39.99 2.29 26.67 113.34 116.00 50 .70 1.225 .408 175.00 .62 49.99 49.98 2.49 33.34 116.67 60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98 2.95 46.67 123.34 80 .76 1.444 .481 189.99 .80 79.99 79.98 3.19 53.34 126.67 90 .78 1.521 .507 194.99 .80 89.99 89.97					-		_	1	1			
30												
40												
50 .70 1.225 .408 175.00 .62 49.99 49.98 2.49 33.34 116.67 60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98 2.95 46.67 123.34 80 .76 1.444 .481 189.99 .80 79.99 79.99 73.45 60.01 133.34 126.67 90 .78 1.521 .507 194.99 .80 79.99 79.99 73.45 60.01 133.34 126.67 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.72 266.68 133.34 10 .82 1.681 .560 204.99 1.00 499.98 499.96 40.01 73.35 136.68 20 .84 1.764 .588 299.99 1.									-			
60 .72 1.296 .432 180.00 .68 59.99 59.98 2.71 40.01 120.01 70 .74 1.369 .456 185.00 .74 69.99 69.98 2.95 46.67 123.34 80 .76 1.444 .481 189.99 .80 79.99 79.98 3.19 53.34 126.67 90 .78 1.521 5.57 194.99 .86 89.99 89.97 3.45 60 133.34 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.72 266.68 133.34 10 .82 1.681 .560 204.99 1.00 409.98 409.96 4.01 73.35 136.68 20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96												
70												
80 .76 I .444 .481 189.99 .80 79.99 79.98 3.19 53.34 126.67 90 .78 I .521 1.507 194.99 .86 89.99 89.97 3.45 60.01 130.01 400 .80 I.600 .533 199.99 .93 99.99 99.97 3.72 266.68 133.34 10 .82 1.681 .550 204.99 1.00 49.98 499.96 4.01 73.35 136.68 20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86,68 143.35 146.68 50 .99 2.025 .675 224.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .92 2.16 .705 229.99 1.32 59.		.72							1			
90 .78 1.521 1.507 194.99 .86 89.99 89.97 3.45 60.01 130.01 400 .80 1.600 .533 199.99 .93 99.99 99.97 3.72 266.68 133.34 10 .82 1.681 .560 204.99 1.00 409.98 409.96 4.01 73.35 136.68 20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86.68 143.35 40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.42 59.97 59.94 5.66 66.69 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36			1.369							46.67		
400			1.444									
10 .82 1.681 .560 204.99 1.00 409.98 409.96 4.01 73.35 136.68 20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86,68 143.35 40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.24 59.97 59.94 5.66 66.69 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.	90	.78	1.521	.507	194.99	.86	89.99	89.97	3.45	60.01	130.01	
10 .82 1.681 .560 204.99 1.00 409.98 409.96 4.01 73.35 136.68 20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86.68 143.35 40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.42 59.97 59.94 5.66 66.69 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.02 80 .96 2.304 .768 239.98 1.61 79.97 79.	400	.80	1.600	-533	199.99	.93	99.99	99.97	3.72	266.68	133.34	
20 .84 1.764 .588 209.99 1.08 19.98 19.96 4.31 80.02 140.01 30 .86 1.849 .618 214.99 1.16 29.98 29.96 4.63 86.68 143.35 40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.42 59.97 59.94 5.66 0.66 0.66 6.69 7.36 234.99 1.51 69.97 69.93 36.04 13.36 156.39 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70	10	.82			204.99		409.98	409.96		73.35		
40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.42 59.97 59.94 -5.66 66.66 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36	20	.84	1.764	-588	209.99	1.08	19.98	19.96	4.31	80.02	140.01	
40 .88 1.936 .645 219.99 1.24 39.98 39.95 4.96 93.35 146.68 50 .90 2.025 .675 224.99 1.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 1.42 59.97 59.94 -5.66 66.66 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36	30	.86	1.840	.618	214.99	1.16	29.98	29.96	4.63	86.68	143.35	
50 .90 2.025 .675 224.99 I.33 49.98 49.94 5.30 300.02 150.02 60 .92 2.116 .705 229.99 I.42 59.97 59.94 5.66 66.69 153.35 70 .94 2.209 .736 234.99 I.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 I.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 I.71 89.96 89.91 6.84 26.70 163.36												
60 .92 2.116 .705 229.99 1.42 59.97 59.94 5.66 66.69 153.35 70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36												
70 .94 2.209 .736 234.99 1.51 69.97 69.93 6.04 13.36 156.69 80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36			1								_	
80 .96 2.304 .768 239.98 1.61 79.97 79.92 6.43 20.03 160.02 90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36										-		
90 .98 2.401 .800 244.98 1.71 89.96 89.91 6.84 26.70 163.36												
				i .		1						
1.00 2.500 .033 249.90 1.02 499.90 499.91 7.27 333.37 100.70									1			
	000	1.00	2.500	.033	249.98	1.62	499.90	499.91	1.21	333.37	100.70	

TABLE X. — Spiral Functions for a Change of 0.3° per 100 Feet. Suitable for Speeds of 91 Miles an Hour or Less, or Curves of 1.5° or Less

L	D	Δ	A	Z	0	C	X	Y	U	V
	•	-								
10	0.03	0.001	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.06	.006	.002	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.09	.013	.005	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.12	.024	.008	20.00	.00	40.00	40.00	.00	26.67	13.33
50	.15	.037	.013	25.00	.00	50.00	50.00	.01	33.33	16.67
60	.18	.054	.018	30.00	.00	60.00	60.00	.02	40.00	20.00
70	.21	.073	.025	35.00	.01	70.00	70.00	.03	46.67	23.33
80	.24	.096	.032	40.00	.01	80.00	80.00	.04	53.33	26.67
90	.27	.121	.041	45.00	.02	90.00	90.00	.06	60.00	30.00
100	.30	.150	.050	50.00	.02	100,00	100.00	.09	66.67	33.33
10	-33	.181	.061	55.00	.03	110.00	110.00	.12	73.33	36.67
20	.36	.216	.072	60.00	.04	120.00	120.00	.15	80.00	40.00
30	-39	.253	.085	65.00	.05	130.00	130.00	.19	86.67	43.33
40	.42	.294	.098	70.00	.06	140.00	140.00	.24	93.33	46.67
50 60	· 45	-337 -384	.113	75.00 80.00	.07	150.00	150.00	.29	100.00	50.00
				85.00			1	-		53.33
70 80	.51 .54	· 433 · 486	.145	90.00	.11	170.00 180.00	170.00	.43 .51	113.33	56.67
90	.57	.541	.181	95.00	.13	190.00	190.00	.60	126.67	63.33
200	.60	.600	.200	100.00	.17	200.00	200.00	.70	133.33	66.67
10	.63	.661	.221	105.00	.20	210.00	210.00	.8I		
20	.66	.726	.242	110.00	.23	220.00	220.00	.93	140.00	70.00
30	.69	.793	.265	115.00	.27	230.00	230.00	1.06	153.33	76.67
40	.72	.864	.288	120.00	.30	240.00	240.00	1.21	160.00	80.00
50	.75	.937	.313	125.00	.34	250.00	250.00	1.36	166.67	83.34
60	.78	1.014	.338	130.00	.38	260.00	259.99	1.53	173.34	86.67
70	.81	1.093	.365	135.00	.43	269.99	269.99	1.72	180.00	90.00
8o	.84	1.176	.392	140.00	.48	279.99	279.99	1.92	186.67	93.34
90	.87	1.261	.421	145.00	-53	289.99	289.99	2.13	193.34	96.67
300	.90	1.350	.450	150.00	.59	299.99	299.98	2.36	200.0I	100.01
10	.93	1.441	.481	155.00	.65	309.99	309.98	2.60	206.67	103.34
20	.96	1.536	.512	160.00	.71	319.99	319.98	2.86	213.34	106.67
30	.99	1.633	-545	165.00	.79	329.99	329.97	3.14	220.01	110.01
40	1.02	1.734	.578	170.00	.86	339.99	339.97	3.43	226.68	113.34
50	1.05	1.837	.613	175.00	.93	349.99	349.96	3.74	233.35	116.68
60	1.08	1.944	.648	180.00	1.02	359.98	359.96	4.07	240.02	120.01
70	I.II	2.053	.685	184.99	1.11	369.98	369.95	4.42	246.68	123.35
80	1.14	2.166	.722	189.99	1.20	379.98	379.94	4.79	253.35	126.68
90 400	1.17	2.281	.761	194.98	1.29	389.97	389.94	5.18	260.02	130.02
	1.20	2.400	.800	199.98	1.40	399.97	399.93	5.58	266.69	133.36
10	1.23	2.521	.841	204.98	1.50	409.96	409.92	6.01	273.36	136.69
20 30	1.26	2.646 2.773	.882	209.98	1.62	419.96 429.96	419.91	6.46	280.03	140.03
	1.32	2.773	.925	214.93	1.74					143.37
40 50	1.32	3.937	1.013	219.98	1.80	439.95 449.95	439.89	7.43	293.37 300.04	146.70
60	1.38	3.174	1.058	229.97	2.13	459.95	459.86	8.49	306.72	153.38
70	1.41	3.313	1.105	234.97	2.27	469.93	469.84	9.06	313.39	156.72
80	1.44	3.456	1.152	239.96	2.41	479.92	479.83	9.65	320.06	160.06
90	1.47	3.601	1.201	244.96	2.57	489.92	489.81	10.27	326.74	163.40
500	1.50	3.750	1.250	249.96	2.72	499.90	499.79	10.91	333.41	166.74

TABLE XI. — SPIRAL FUNCTIONS FOR A CHANGE OF 0.4° PER 100
FEET. SUITABLE FOR SPEEDS OF 83 MILES AN HOUR OR
LESS, OR CURVES OF 2.0° OR LESS

										_
L	D	Δ	A		0	C	X	Y	U	V
	0	۰	0							
10	0.04	0.002	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.08	.008	.003	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.12	.018	.006	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.16	.032	.011	20.00	.00	40.00	40.00	.01	26.67	13.33
50	.20	.050	.016	25.00	.00	50.00	50.00	.02	33.33	16.67
60	.24	.072	.024	30.00	.01	60.00	60.00	.03	40.00	20.00
70	.28	.098	.033	35.00	.01	70.00	70.00	.04	46.67	23.33
80	.32	.128	.043	40.00	.01	80.00	80.00	.06	53.33	26.67
90	.36	.162	.054	45.00	.02	90.00	90.00	.08	60.00	30.00
100	.40	.200	.067	50.00	.03	100.00	100.00	.12	66.67	33.33
10	.44	.242	.081	55.00	.04	110.00	110.00	.16	73.33	36.67
20	.48	.288	.096	60.00	.05	120.00	120.00	.20	80.00	40.00
30	.52	.338	.113	65.00	.06	130.00	130.00	.26	86.67	43.33
40	. 56	.392	.131	70.00	.08	140.00	140.00	.32	93.33	46.67
50	.60	.450	.150	75.00	.10	150.00	150.00	-39	100.00	50.00
60	.64	.512	.171	80.00	.12	160.00	160.00	.48	106.67	53.33
70	. 68	.578	.193	85.00	.14	170.00	170.00	-57	113.33	56.67
80	.72	.648	.216	90.00	.17	180.00	180.00	.68	120.00	60.00
90	.76	.722	.241	95.00	.20	190.00	190.00	.80	126.67	63.33
200	.80	.800	.267	100.00	.23	200.00	200.00	.93	133.33	66.67
10	.84	.882	.294	105.00	.27	210.00	210.00	1.08	140.00	70.00
20	.88	.968	.323	110.00	.31	220.00	219.99	1.24	146.67	73.33
30	.92	1.058	-353	115.00	-35	230.00	229.99	1.41	153.34	76.67
40	.96	1.152	.384	120.00	.40	240.00	239.99	1.61	160.00	80.00
50	1.00	1.250	.417	125.00	.46	250.00	249.99	1.82	166.67	83.34
60	1.04	1.352	.451	130.00	.51	259.99	259.98	2.04	173.34	86.67
70	1.08	1.458	.486	135.00	.57	269.99	269.98	2.29	180.01	90.01
80	1.12	1.568	.523	140.00	.64	279.99	279.98	2.55	186.67	93.34
90	1.16	1.682	.561	144.99	.71	289.99	289.97	2.84	193.34	96.67
300	1.20	1.800	.600	149.99	.79	299.99	299.97	3.14	200.01	100.01
10	1.24	1.922	.641	154.99	.86	309.98	309.97	3.47	206.68	103.34
20	1.28	2.048	. 683	159.99	.95	319.98	319.96	3.81	213.35	106.68
30	1.32	2.178	.726	164.99	1.05	329.98	329.95	4.18	220.02	110.02
40	1.36	2.312	.771	169.99	1.14	339.98	339.95	4.57	226.68	113.35
50	1.40	2.450	.817	174.98	1.25	349.97	349.94	4.99	233.36	116.69
60	1.44	2.592	.864	179.98	1.36	359.97	359.93	5.43	240.03	120.02
70	1.48	2.738	.913	184.98	1.48	369.96	369.91	5.89	246.69	123.36
80	1.52	2.888	.963	189.98	1.60	379.96	379.90	6.38	253.37	126.70
90	1.56	3.042	1.014	194.98	1.72	389.95	389.89	6.90	260.04	130.03
400	1.60	3.200	1.067	199.97	1.86	399.94	399.88	7.44	266.71	133.37
10	1.64	3.362	1.121	204.97	2.00	409.94	409.86	8.02	273.38	136.71
20	1.68	3.528	1.176	209.97	2.15	419.93	419.84	8.61	280.06	140.05
30	1.72	3.698	1.233	214.96	2.31	429.92	429.82	9.25	286.73	143.39
40	1.76	3.872	1.291	219.96	2.48	439.91	439.80	9.90	293.41	146.73
50	1.80	4.050	1.350	224.95	2.65	449.90	449.78	10.60	300.08	150.07
60	1.84	4.232	1.411	229.95	2.83	459.89	459.75	11.32	306.76	153.41
70	1.88	4.418	1.473	234.95	3.02	469.88	469.72	12.07	313.43	156.75
80	1.92	4.608	1.533	239.94	3.22	479.87	479.69	12.86	320.11	160.10
90	1.96	4.802	1.601	244.93	3.42	489.85	489.66	13.68	326.79	163.44
500	2.00	5.000	1.667	249.93	3.63	499.84	499.62	14.54	333.47	166.79

TABLE XII. — SPIRAL FUNCTIONS FOR A CHANGE OF 0.5° PER 100
FEET. SUITABLE FOR SPEEDS OF 77 MILES AN HOUR OR
LESS, OR CURVES OF 2.0° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
	0	0	0							
10	0.05	0.002	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.10	.010	.003	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.15	.025	.008	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.20	.040	.013	20.00	.00	40.00	40.00	.01	26.67	13.33
50	.25	.062	.021	25.00	.00	50.00	50.00	.02	33.33	16.67
60	.30	.090	.030	30.00	.01	60.00	60.00	.03	40.00	20.00
70	.35	.122	.041	35.00	.01	70.00	70.00	.05	46.67	23.33
80	.40	. 160	.053	40.00	.02	80.00	80.00	.07	53.33	26.67
90	-45	. 202	.067	45.00	.03	90.00	90.00	.II	60.00	30.00
100	.50	.250	. 083	50.00	.04	100.00	100.00	.15	66.67	33.33
10	. 55	.302	.ioi	55.00	.05	110.00	110.00	. 19	73.33	36.67
20	.60	. 360	.120	60.00	.06	120.00	120.00	.25	80.00	40.00
30	.65	.422	.141	65.00	.08	130.00	130.00	.32	86.67	43.33
40	.70	. 490	. 163	70.00	.10	140.00	140.00	.40	93.33	46.67
50	- 75	. 562	. 187	75.00	.12	150.00	150.00	. 49	100.00	50.00
60	.80	.640	.213	80.00	. 15	160.00	160.00	.60	106.67	53.33
70	.85	.722	.241	85.00	. 18	170.00	170.00	.71	113.33	56.67
80	.90	.810	.270	90.00	.21	180.00	180.00	.85	120.00	60.00
90	.95	.902	.301	95.00	. 25	190.00	189.99	1.00	126.67	63.33
200	1.00	1.000	-333	100.00	. 29	200.00	199.99	1.16	133.34	66.67
10	.05	I.I02	.367	105.00	.34	210.00	209.99	1.35	140.00	70.00
20	. 10	1.210	. 403	110.00	- 39	220.00	219.99	1.55	146.67	73.34
30	. 15	I.322	.441	115.00	-44	230.00	229.99	1.77	153.34	76.67
40	.20	1.440	. 480	120.00	- 50	239.99	239.99	2.01	160.01	80.00
50	.25	1.562	.521	125.00	-57	249.99	249.98	2.27	166.67	83.34
60	.30	1.690	. 563	129.99	.64	259.99	259.98	2.56	173.34	86.67
70	-35	1.822	. 607	134.99	.72	269.99	269.97	2.86	180.01	90.01
80	.40	1.960	.653	139.99	.80	279.99	279.97	3.19	186.68	93.34
90	-45	2.102	.701	144.99	. 88	289.98	289.96	3.55	193.35	96.68
300	1.50	2.250	.750	149.99	.98	299.98	299.96	3.93	200.02	100.01
10	.55	2.402	.801	154.99	1.08	309.98	309.95	4.33	206.69	103.35
20	.60	2.560	.853	159.98	1.19	319.97	319.94	4.76	213.36	106.69
30	.65	2.722	. 907	164.98	1.31	329.97	329.93	5.23	220.02	110.02
40	.70	2.890	.963	169.98	1.43	339.96	339.92	5.72	226.70	113.36
50	.75	3.062	1.021	174.98	1.56	349.96	349.90	6.23	233.37	116.70
60	.80	3.240	1.080	179.97	1.70	359.95	359.88	6.78	240.04	120.03
70	.85	3.422	1.141	184.97	1.84	369.94	369.87	7.37	246.71	123.38
80	.90	3.610	1.203	189.97	2.00	379.94	379.85	7.98	253.39	126.71
90	.95	3.802	1.267	194.96	2.16	389.93	389.83	8.63	260.06	130.05
400	2.00	4.000	1.333	199.96	2.33	399.92	399.81	9.30	266.74	133.40

TABLE XIII. — Spiral Functions for a Change of 0.75° per 100 Feet. Suitable for Speeds of 67 Miles an Hour or Less, or Curves of 3.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
	•	٥	٥					1		
10	0.075	0.004	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	. 150	.015	.005	10.00	.00	20.00	20.00	.00	13.33	6.67
30	,225	.034	.012	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.300	.060	.020	20.00	.00	40.00	40.00	.01	26.67	13.33
50	.375	.094	.031	25.00	.01	50.00	50.00	.03	33.33	16.67
60	.450	. 135	.045	30.00	.01	60.00	60.00	.05	40.00	20.00
70	. 525	. 184	.061	35.00	.02	70.00	70.00	.07	46.67	23.33
80	.600	.240	.080	40.00	.03	80.00	80.00	.II	53.33	26.67
90	.675	.304	.101	45.00	.04	90.00	90.00	. 16	60.00	30.00
100	.750	.375	.125	50.00	.06	100.00	100.00	.22	66.67	33.33
10	.825	. 454	. 151	55.00	.07	110.00	110.00	. 29	73.33	36.67
20	. 900	.540	.180	60.00	.09	120.00	120.00	.38	80.00	40.00
30	.975	.634	.211	65.00	.12	130.00	130.00	.48	86.67	43.33
40	1.050	.735	.245	70.00	.15	140.00	140.00	.60	93.33	46.67
50	1.125	.844	.281	75.00	.18	150.00	150.00	.74	100.00	50.00
60	1.200	.960	.320	80.00	. 22	160.00	160.00	.89	106.67	53.33
70	1.275	1.084	.361	85.00	. 27	170.00	169.99	1.07	113.33	56.67
80	1.350	1.215	.405	90.00	.32	180,00	179.99	1.27	120.00	60.00
90	1.425	1.354	.451	95.00	- 37	189.99	189.99	1.50	126.67	63.34
200	1.500	1.500	.500	100.00	.44	199.99	199.99	1.75	133.34	66.67
10	1.575	1.654	.551	104.99	.51	209.99	209.98	2.02	140.01	70.01
20	1.650	1.815	.605	109.99	.58.	219.99	219.98	2.32	146.67	73.34
30	1.725	1.984	.661	114.99	.66	229.99	229.97	2.65	153.34	76.68
40	1.800	2.160	.720	119.99	.73	239.99	239.97	3.02	160.01	80.01
50	1.875	2.344	.781	124.99	.85	249.98	249.96	3.41	166.68	83.34
60	1.950	2.535	.845	129.99	.96	259.98	259.95	3.84	173.35	86.68
70	2.025	2.734	.911	134.98	1.07	269.97	269.94	4.30	180.02	90.02
80	2,100	2.940	.980	139.98	1.20	279.97	279.93	4.79	186.69	93.36
90	2.175	3.154	1.051	144.98	1.33	289.96	289.91	5.32	193.37	96.69
300	2.250	3.375	1.125	149.97	1.47	299.96	299.90	5.86	200.04	100.03
10	2.325	3.604	1.201	154.97	1.63	309.95	309.88	6.50	206.71	103.37
20	2.400	3.840	1.280	159.97	1.79	319.94	319.86	7.15	213.38	106.71
30	2.475	4.084	1.361	164.96	1.96	329.93	329.83	7.84	220.06	110.04
40	2.550	4.335	1.445	169.96	2.14	339.92	339.81	8.57	226.73	113.39
50	2.625	4.594	1.531	174.95	2.34	349.90	349.78	9.35	233.41	116.74
60	2.700	4.860	1.620	179.94	2.54	359.88	359.74	10.17	240.09	120.09
70	2.775	5.134	1.711	184.93	2.76	369.87	369.70	11.04	246.77	123.43
80	2.850	5.415	1.805	189.93	2.99	379.85	379.67	11.97	253.45	126.78
90	2.925	5.704	1.901	194.92	3.24	389.83	389.62	12.93	260.14	130.12
400	3.000	6.000	2.000	199.91	3.49	399.81	399.56	13.95	266.82	138.34

TABLE XIV. — Spiral Functions for a Change of 1.0° per 100 Feet. Suitable for Speeds of 61 Miles an Hour or Less, or Curves of 4.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	ħ.
	0	0	0							
10	0.10	0.005	0.002	5.00	0.00	10.00	10.00	.00	6.67	3.33
20	.20	.020	.007	10.00	.00	20.00	20.00	.00	13.33	6.66
30	.30	.045	.015	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.40	.080	.027	20.00	.00	40.00	40.00	.02	26.67	13.33
50	.50	. 125	.0.12	25.00	.01	50.00	50.00	.04	33.33	16.67
60	.60	. 180	.060	30.00	.02	60.00	60.00	.06	40.00	20.00
70	.70	.245	.082	35.00	.03	70.00	70.00	.10	46.67	23.33
80	.80	.320	.107	40.00	.03	80.00	80.00	.15	53-33	26.67
90	.90	.405	. 135	45.00	.05	90.00	90.00	.21	60.00	30.00
100	1.00	.500	.167	50.00	.07	100.00	100.00	.29	66.67	33.33
10	1.10	.605	.202	55.00	.10	110.00	110.00	-39	73.33	36.67
20	I.20	.720	. 240	60.00	.13	120.00	120.00	.50	80.00	40.00
30	1.30	.845	. 282	65.00	.16	130.00	130.∞	. 64	86.67	43.33
40	1.40	.980	.327	70.00	.20	140.00	140.00	.80	93.34	46.67
50	1.50	1.125	-375	75.00	.25	150.00	149.99	.98	100.00	50.00
60	1.60	1.280	. 427	80.00	.30	160.00	159.99	1.19	106.67	53.34
70	1.70	I.445	.482	85.∞	.36	169.99	169.99	1.43	113.34	56.67
80	1.80	1.620	. 540	90.00	.42	179.99	179.99	1.70	120.00	60.00
90	1.90	1.805	.602	94.99	.50	189.99	189.98	1.99	126.67	63.34
200	2.00	2.000	.667	99.99	. 58	199.99	199.98	2.33	133.34	66.67
10	2.10	2.205	-735	104.99	.67	209.99	209.97	2.69	140.CI	70.01
20	2.20	2.420	.807	109.99	-77	219.98	219.96	3.10	146.68	73.35
30	2.30	2.645	.882	114.99	.89	229.98	229.95	3.54	153.35	76.68
40	2.40	2.880	.960	119.98	1.01	239.97	239.94	4.02	160.02	80.02
50	2.50	3.125	1.042	124.98	1.14	249.97	249.93	4.54	166.69	83.36
60	2.60	3.380	1.127	129.97	1.28	259.96	259.91	5.11	173.37	86.70
70	2.70	3.645	1.215	134.97	1.43	269.95	269.89	5.72	180.04	90.03
80	2.80	3.920	1.307	139.97	1.60	279.94	279.87	6.38	186.71	93.37
90	2.90	4.205	1.402	144.96	1.77	289.93	289.85	7.09	193.39	96.72
300	3.00	4.500	1.500	149.95	1.96	299.92	299.82	7.85	200.06	100.06
10	3.10	4.805	1.602	154.95	2.16	309.90	309.78	8.66	206.74	103.40
20	3.20	5.120	1.707	159.94	2.38	319.89	319.75	9.53	213.42	106.75
30	3.30	5 - 445	1.815	164.93	2.61	329.87	329.70	10.44	220.10	110.09
40	3.40	5.780	1.927	169.92	2.86	339.85	339.66	II.42	226.79	113.44
50	3.50	6.125	2.042	174.91	3.12	349.82	349.60	12.46	233.47	116.80
60	3.60	6.480	2.160	179.89	3.39	359.80	359-54	13.56	240.16	120.15
70	3.70	6.845	2.282	184.88	3.68	369.77	369.47	14.71	246.85	123.50
80	3.80	7.220	2.407	189.87	3.99	379.73	379.40	15.94	253.54	126.86
90	3.90	7.605	2.535	194.85	4.31	389.70	389.32	17.23	260.24	130.22
400	4.00	8.000	2.667	199.84	4.65	399.66	399.22	18.59	266.94	133.58

Table XV.—Spiral Functions for a Change of 1\frac{1}{3}\circ per 100 Feet. Suitable for a Speed of 55 Miles an Hour or Less, or Curves of 4.0\circ or Less

			A	Z	0	С	X	Y	U	V
	0	0	•							
10	0.133	0.007	0.002	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	. 267	.027	.009	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.400	.060	.020	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.533	.107	.036	20.00	.oı	40.00	40.00	.02	26.67	13.33
50	.667	.167	.056	25.00	.01	50.00	50.00	.05	33.33	16.67
60	.800	.240	.080	30.00	.02	60.00	60.00	.08	40.00	20.00
70	.933	.327	.109	35.00	.03	70.00	70.00	.13	46.67	23.33
	1.067	.427	.142	40.00	.05	80.00	80.00	. 20	53.33	26.67
	1.200	.540	. 180	45.00	.07	90.00	90.00	. 28	60.00	30.00
-	1.333	.667	.222	50.00	.10	100.00	100.00	-39	66.67	33.33
-	1.467	.807	. 269	55.00	.13	110.00	110.00	.52	73.33	36.67
1	1.600	.960	.320	60.00	.17	120.00	120.00	.67	80.00	40.00
1	1.733	1.127	.376	65.00	.21	130.00	129.99	.85	86.67	43.34
				_						46.67
	1.867	1.307	.436	70.00	. 27	140.00	139.99 149.99	1.06	93.34	50.00
	2.000	1.500	.500	74.99 79.99	-33 .40	159.99	159.99	1.59	106.67	53.34
	2.267	1.927	.642	84.99	.48	169.99	169.98	1.91	113.34	56.67
1	2.400	2.160	.720	89.99	-57	179.99	179.97	2.26	120.01	60.01
-	2.533	2.407	.802	94.99	.66	189.98	189.97	2.66		63.34
200	2.667	2.667	.889	99.98	.78	199.98	199.96	3.10	133.35	66.68
10	2.800	2.940	.980	104.98	.90	209.97	209.94	3.59	140.02	70.02
20 :	2.933	3.227	1.076	109.98	1.03	219.97	219.93	4.12	146.69	73-35
30	3.067	3.527	1.176	114.97	1.18	229.95	229.91	4.71	153.36	76.69
40	3.200	3.840	1.280	119.97	1.34	239.95	239.89	5.35	160.04	80.03
50	3.333	4.167	1.389	124.96	1.51	249.94	249.87	6.05	166.72	83.38
60 ;	3.467	4.507	I.502	129.95	1.70	259.93	259.84	6.81	173.39	86.72
70	3.600	4.860	1.620	134.95	1.91	269.91	269.81	7.62	180.07	90.06
80	3.733	5.227	1.742	139.94	2.13	279.90	279.77	8.50	186.75	93.41
90	3.867	5.607	1.869	144.94	2.36	289.88	289.72	9.43	193.43	96.76
300	4.000	6.000	2.000	149.92	2.61	299.86	299.67	10.46	200.12	100.11

TABLE XVI. — SPIRAL FUNCTIONS FOR A CHANGE OF 1.5° PER 100 FEET. SUITABLE FOR SPEEDS OF 53 MILES AN HOUR OR LESS, OR CURVES OF 4.5° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
	•	۰	0							
10	0.15	0.008	0.002	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.30	.030	.010	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.45	.068	.022	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.60	.120	.040	20.00	.01	40.00	40.00	.03	26.67	13.33
50	.75	. 188	.062	25.00	.01	50.00	50.00	.05	33.33	16.67
60	.90	. 270	.090	30.00	.02	60.00	60.00	.09	40.00	20.00
70	1.05	. 368	. 122	35.00	.04	70.00	70.00	.15	46.67	23.33
80	1.20	.480	.160	40.00	.06	80.00	80.00	.22	53.33	26.67
90	1.35	.608	. 202	45.00	.08	90.00	90.00	.32	60.00	30.co
100	1.50	.750	. 250	50.00	.II	100.00	100.00	-44	66.67	33.33
10	1.65	.908	.302	55.00	.15	110.00	110.00	.58	73.33	36.67
20	1.80	1.080	.360	60.00	.19	120.CO	120.00	-75	80.00	40.00
30	1.95	1.268	.422	65.00	.24	130.00	129.99	.96	86.67	43.34
40	2.10	1.470	.490	69.99	.30	140.00	139.99	1.20	93.34	46.67
50	2.25	1.688	. 562	74.99	.37	149.99	149.99	1.47	100.00	50.00
60	2.40	1.920	.640	79.99	.45	159.99	159.98	1.79	106.67	53.34
70	2.55	2.168	.722	84.99	.54	169.99	169.97	2.14	113.34	56.67
80	2.70	2.430	.810	89.99	.64	179.99	179.97	2.54	120.01	60.01
90	2.85	2.708	.902	94.98	.75	189.98	189.96	2.99	126.68	63.35
200	3.00	3.000	1.000	99.98	.87	199.98	199.95	3.49	133.35	66.68
10	3.15	3.308	1.102	104.98	I.OI	209.97	209.93	4.04	140.02	70.02
20	3.30	3.630	1.210	109.97	1.16	219.96	219.91	4.64	146.70	73.36
30	3.45	3.968	1.322	114.96	1.33	229.95	229.89	5.30	153.37	76.70
40	3.60	4.320	1.440	119.96	1.51	239.94	239.87	6.03	160.05	80.04
50	3.75	4.688	1.562	124.95	1.70	249.93	249.83	6.81	166.73	83.39
60	3.90	5.070	1.690	129.94	1.92	259.91	259.80	7.66	173.41	86.73
70	4.05	5.468	1.822	134.93	2.15	269.89	269.76	8.58	180.09	90.08
80	4.20	5.880	1.960	139.92	2.39	279.87	279.71	9.55	186.77	93.43
90	4.35	6.308	2.102	144.91	2.66	289.85	289.65	10.61	193.46	96.78
300	4.50	6.750	2.250	149.90	2.94	299.82	299.59	11.77	200.15	100.13

TABLE XVII. — Spiral Functions for a Change of 2.0° per 100 Feet. Suitable for a Speed of 48 Miles an Hour or Less, and Curves of 6.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
	•	0	•							
10	0.20	0.010	0.003	5.00	0.00	10.00	10.00	0.00	6.97	3.33
20	.40	.040	.013	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.60	.090	.030	15.00	.00	30.00	30.00	.02	20.00	10.00
40	.80	.160	.053	20.00	.01	40.00	40.00	.04	26.67	13.33
50	1.00	.250	.083	25.00	.02	50.00	50.00	.07	33.33	16.67
60	.20	.360	.120	30.00	.03	60.00	60.00	.13	40.00	20.00
70	.40	.490	.163	35.00	.05	70.00	70.00	.20	46.67	23.33
80	.60	.640	.213	40.00	.07	80.00	80.00	.30	53.33	26.67
90	.80	.810	.270	45.00	.11	90.00	90.00	.42	60.00	30.00
100	2.00	1.000	-333	50.00	.14	100.00	100.00	.58	66.67	33.33
10	.20	1.210	.403	55.00	.19	110.00	109.99	.77	73.33	36.67
20	.40	1.440	.480	59.99	.25	120.00	119.99	1.00	80.00	40.00
30	.60	1.690	.563	64.99	-34	129.99	129.99	1.28	86.67	43.34
40	.80	1.960	.653	69.99	.40	139.99	139.98	1.60	93.34	46.67
50	3.00	2.250	.750	74.99	.49	149.99	149.98	1.96	100.01	50.01
60	.20	2.560	.853	79.98	.60	159.99	159.97	2.38	106.68	53.34
70	.40	2.890	.963	84.98	.71	169.98	169.96	2.86	113.35	56.68
8o	.60	3.240	1.080	89.98	.85	179.97	179.94	3.39	120.02	60.02
90	.80	3.610	1.203	94.97	1.00	189.97	189.93	3.99	126.69	63.36
200	4.00	4.000	1.333	99.96	1.16	199.96	199.90	4.65	133.37	66.70
10	.20	4.410	1.470	104.96	1.35	209.95	209.88	5.38	140.04	70.04
20	.40	4.840	1.613	109.95	1.55	219.93	219.84	6.19	146.72	73.38
30	.60	5.290	1.763	114.94	1.77	229.91	229.80	7.07	153.40	76.73
40	.80	5.760	1.920	119.93	2.01	239.89	239.76	8.03	160.09	80.08
50	5.00	6.250	2.083	124.91	2.27	249.87	249.70	9.08	166.77	83.43
60	.20	6.760	2.253	129.90	2.55	259.84	259.64	10.21	173.46	86.78
70	.40	7.290	2.430	134.88	2.86	269.81	269.57	11.44	180.15	90.14
8o	.60	7.840	2.613	139.86	3.19	279.77	279.48	12.75	186.85	93.50
90	.80	8.410	2.802	144.84	3.54	289.73	289.38	14.17	193.55	96.87
300	6.00	9.000	2.999	149.81	3.92	299.68	299.26	15.68	200.26	100.24

TABLE XVIII. — SPIRAL FUNCTIONS FOR A CHANGE OF 2.5°
PER 100 FEET. SUITABLE FOR SPEEDS OF 45 MILES AN
HOUR OR LESS, AND CURVES OF 7.5° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
		•	۰							
10	0.25	0.012	0.004	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	. 50	.050	.017	10.00	.00	20.00	20.00	.01	13.33	6.67
30	. 75	.112	.037	15.00	.00	30.00	30.00	.02	20.00	10.00
40	1.00	. 200	.067	20.00	.01	40.00	40.00	.05	26.67	13.33
50	. 25	.312	. 104	25.00	.02	50.00	50.00	.09	33.33	16.67
60	.50	. 450	. 150	30.00	.04	60.00	60.00	. 16	40.00	20.00
70	.75	.612	. 204	35.00	.c6	70.00	70.00	.21	46.67	23.33
80	2.00	.800	.267	40.00	.09	80.00	80.00	.37	53.33	26.67
90	.25	1.012	-337	45.00	.13	90.00	90.00	53	60.00	30.00
100	.50	1.250	.417	50.00	.18	100.00	100.00	.73	66.67	33.34
10	.75	T.512	.504	54.99	.24	110.00	109.99	.97	73.34	36.67
20	3.00	1.800	.600	59.99	.31	120.00	119.99	1.26	80.00	40.00
30	. 25	2.112	.704	64.99	.40	129.99	129.98	1.60	86.67	43.34
40	.50	2.450	.817	69.98	.50	139.99	139.97	2.00	93.34	46.67
50	-75	2.812	.937	74.98	.61	149.98	149.96	2.45	100.01	50.01
60	4.00	3.200	1.067	79.98	.74	159.98	159.95	2.98	106.68	53.35
70	.25	3.612	1.204	84.97	.89	169.97	169.93	3.57	113.36	56.69
80	.50	4.050	1.350	89.96	1.06	179.96	179.91	4.24	120.03	60.03
90	.75	4.512	1.504	94.95	1.25	189.95	189.88	4.99	126.71	63.37
200	5.00	5.000	1.667	99.94	1.45	199.93	199.85	5.81	133.39	66.72
10	.25	5.512	1.837	104.93	1.68	209.91	209.81	6.73	140.07	70.06
20	.50	6.050	2.017	109.92	1.93	219.89	219.76	7.74	146.76	73.41
30	-75	6.612	2.204	114.90	2.21	229.87	229.70	8.84	153.44	76.76
40	6.00	7.200	2.400	119.89	2.51	239.83	239.62	10.04	160.13	80.12
50	.25	7.812	2.604	124.86	2.84	249.80	249.54	11.35	166.83	83.48
60	.50	8.450	2.816	129.84	3.19	259.75	259.44	12.76	173.53	86.85
70	.75	9.112	3.036	134.81	3.57	269.70	269.32	14.29	180.24	90.22
80	7.00	9.800	3.266	139.78	3.98	279.64	279.19	15.93	186.96	93.60
90	.25	10.512	3.503	144.75	4.42	289.57	289.03	17.69	193.68	96.98
300	7.50	11.250	3.749	149.71	4.89	299.49	298.85	19.58	200.41	100.37

TABLE XIX. — SPIRAL FUNCTIONS FOR A CHANGE OF 3.0° PER 100 FEET. SUITABLE FOR SPEEDS OF 41 MILES AN HOUR OR LESS, AND CURVES OF 9.0° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
	•	•								
10	0.30	0.015	0.005	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.60	.060	.020	10.00	.00	20.00	20.00	.01	13.33	6.67
30	.90	. 135	.045	15.00	.01	30.00	30.00	.02	20.00	10.00
40	1.20	.240	.080	20.00	.01	40.00	40.00	.06	26.67	13.33
50	.50	.375	.125	25.00	.03	50.00	50.00	.II	33.33	16.67
60	.80	. 540	.180	30.00	.05	60.00	60.00	.19	40.00	20,00
70	2.10	.735	. 245	35.00	.07	70.00	70.00	.30	46.67	23.33
80	.40	.960	.320	40.00	.11	80.00	80.00	. 45	53.34	26.67
90	.70	1.215	. 405	45.00	.16	90.00	90.00	.64	60.00	30.00
100	3.∞	1.500	. 500	49.99	.22	100.00	99.99	.87	66.67	33.34
10	.30	1.815	.605	54.99	.29	109.99	109.99	1.16	73.34	36.67
20	.60	2.160	.720	59.99	.36	119.99	119.98	1.51	80.01	40.01
30	.90	2.535	.845	64.98	.48	129.99	129.98	1.92	86.67	43.34
40	4.20	2.940	.980	69.98	.60	139.98	139.96	2.39	93.35	46.68
50	.50	3.375	1.125	74.97	.74	149.98	149.95	2.94	100.02	50.02
60	.80	3.840	1.280	79.97	.89	159.97	159.93	3.57	106.69	53.36
70	5.10	4.335	1.445	84.96	1.07	169.96	169.90	4.28	113.37	56.70
80	.40	4.860	1.620	89.95	1.27	179.94	179.87	5.08	120.05	60.04
90	.70	5.415	1.805	94.93	1.49	189.92	189.83	5.98	126.73	63.39
200	6.00	6.000	2.000	99.92	1.74	199.90	199.78	6.98	133.41	66.74
10	.30	6.615	2.205	104.90	2.02	209.88	209.72	8.06	140.10	70.09
20	.60	7.260	2.420	109.88	2.32	219.85	219.65	9.26	146.79	73.45
30	.90	7.935	2.645	114.86	2.65	229.81	,229.56	10.59	153.49	76.81
40	7.20	8.640	2.879	119.83	3.01	239.76	239.46	12.04	160.19	80.17
50	.50	9.375	3.124	124.80	3.40	249.71	249.34	13.60	166.90	83.55
60	.80	10.140	3.379	129.77	3.82	259.64	259.19	15.30	173.62	86.93
70	8.10	10.935	3.644	134.73	4.28	269.57	269.03	17.11	180.35	90.32
80	.40	11.760	3.919	139.69	4.77	279.48	278.83	19.08	187.08	93.71
90	.70	12.615	4.203	144.64	5.30	289.39	288.61	21.20	193.83	97.12
300	9.00	13.500	4.498	149.58	5.86	298.70	298.35	23.47	200.59	100.54

TABLE XX. — Spiral Functions for a Change of 4.0° per 100 Feet. Suitable for Speeds of 35 Miles an Hour or Less, or Curves of 10.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
		•								
10	0.40	0.020	0.007	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.80	.080	.027	10.00	.00	20.00	20.00	.01	13.33	6.67
30	1.20	. 180	. 060	15.00	.01	30.00	30.00	.03	20.00	10.00
40	.60	.320	. 107	20.00	.02	40.00	40.00	.07	26.67	13.33
50	2.00	.500	.167	25.00	.04	50.00	50.00	.15	33.33	16.67
60	.40	.720	.240	30.00	.06	60.00	60.00	.25	40.00	20,00
70	.80	.980	.327	35.00	.10	70.00	70.00	.40	46.67	23.33
8o	3.20	1.280	.427	39.99	.15	80.00	80.00	.60	53.33	26.67
90	.60	1.620	. 540	44.99	.21	90.00	89.99	.85	60.00	30.00
100	4.00	2,000	.667	49.99	.29	99.99	99.99	1.16	66.67	33.34
10	.40	2.420	.807	54.98	-39	109.99	109.98	1.55	73.33	36.67
20	.80	2.880	.960	59.98	.50	119.99	119.97	1.84	80.01	40.01
30	5.20	3.380	1.127	64.97	.64	129.98	129.95	2.56	86.68	43.35
40	.60	3.920	1.307	69.96	.80	139.97	139.93	3.19	93.36	46.69
50	6.00	4.500	1.500	74.95	.98	149.96	149.91	3.93	100.03	50.03
60	.40	5.120	1.707	79.94	1.19	159.94	159.87	4.76	106.71	53.37
70	.80	5.780	1.927	84.92	1.43	169.92	169.83	5.71	113.40	56.72
80	7.20	6.480	2.160	89.90	1.77	179.90	179.77	6.78	120.08	60.08
90	.60	7.220	2.407	94.88	1.99	189.87	189.70	7.97	126.77	63.43
200	8.00	8.000	2.667	99.86	2.32	199.83	199.61	9.30	133.47	66.79
10	.40	8.820	2.939	104.83	2.68	209.78	209.51	10.76	140.18	70.16
20	.80	9.680	3.222	109.79	3.09	219.72	219.38	12.38	146.89	73.54
30	9.20	10.580	3.526	114.75	3.52	229.66	229.22	14.11	153.61	76.92
40	.60	11.520	3.839	119.70	4.00	239.57	239.03	16.03	160.34	80.31
250	10.00	12.500	4.165	124.65	4.52	249.48	248.82	18.12	167.09	83.72

TABLE XXI. — Spiral Functions for a Change of 5.0° per 100 Feet. Suitable for Speeds of 32 Miles an Hour or Less, or Curves of 12.5° or Less

L	D	Δ	A	Z	o	С	X	Y	U	V
	-	•				-				
10	0.50	0.025	0,008	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	1.00	.100	.033	10.00	2.00	20,00	20.00	.01	13.33	6.67
30	.50	.225	.075	15.00	.01	30.00	30.00	.04	20.00	10.00
40	2.00	.400	.133	20.00	.02	40.00	40.00	.09	26.67	13.33
50	.50	.625	,208	25.00	.05	50.00	50.00	.18	33.33	16.67
60	3.00	.900	.300	30.00	.08	60.00	60.00	.31	40.00	20.00
	1							1		
70 80	4.00	1.225	.408	34.99	.13	70.00	70.00	.50	46.67 53.34	23.33
90	.50	2.025	.533 .675	39.99	.19	90.00	89.99	1.06	60.00	30.00
-				44.99			l			
100	5.00	2.500	.833	49.98		99.99	99.98	1.45	66.67	33.34
10	.50	3.025	1.008	54.97	.48	109.99	109.97	1.93	73.34	36.68
20	6.00	3.600	1.200	59.97	.63	119.98	119.95	2.51	80.02	40.02
30	.50	4.225	1.408	64.95	.80	129.97	129.93	3.19	86.69	43.36
40	7.00	4.900	1.633	69.94	1.00	139.96	139.90	3.99	93.37	46.70
50	.50	5.625	1.875	74.92	1.20	149.94	149.86	4.90	100.05	50.05
60	8.00	6.400	2.133	79.90	1.48	159.91	159.80	5.94	106.74	53.40
70	.50	7.225	2.408	84.88	1.78	169.88	169.73	7.13	113.43	56.75
80	9.00	8.100	2.699	89.85	2.11	179.84	179.64_	8.46	120.13	60.12
90	.50	9.025	3.008	94.82	2.48	189.79	189.53	9.95	126.83	63.48
200	10.00	10.000	3.332	99.78	2.90	199.73	199.40	11.61	133.55	66.86
10	.50	11.025	3.674	104.73	3.35	209.66	209.23	13.41	140.27	70.25
20	11.00	12,100	4.032	109.67	3.82	219.57		15.42	147.01	73.65
30	.50	13.225	4.406	114.61	4.40	229.46	228.79	17.62	153.76	77.06
40	12.00	14.400	4.797	119.54	5.99	239.34	238.50	20.02	160.54	80.49
250	12.50	15.625	5.205	124.46	5.64	249.18	248.16	22.62	167.32	83.94

TABLE XXII.—Spiral Functions for a Change of 7.5° per 100 Feet. Suitable for a Speed of 26 Miles an Hour or Less, or a Curve of 18.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
		•	0							
10	0.75	0.0375	0.012	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	1.50	.1500	.050	10.00	.00	20.00	20.00	.02	13.33	6.67
30	2.25	.3375	.113	15.00	.01	30.00	30.00	.06	20.00	10.00
40	3.00	.6000	.200	20.00	.03	40.00	40.00	.14	26.67	13.33
50	3.75	.9375	.313	25.00	.07	50.00	50.00	.27	33.33	16.67
60	4.50	1.3500	-450	29.99	.12	60.00	60.00	.47	40.00	20.00
70	5.25	1.8375	.613	34.99	.19	70.00	69.99	.75	46.67	23.34
80	6.00	2.4000	.800	39.98	.28	79.99	79.99	1.12	53.34	26.67
90	6.75	3.0375	1.013	44.97	.40	89.99	89.97	1.59	60.01	30.01
100	7.50	3.7500	1.250	49.96	-54	99.98	99.96	2.18	66.68	33.35
10	8.25	4.5375	1.513	54.94	.71	109.97	109.93	2.90	73.36	36.69
20	9.00	5.4000	1.800	59.92	.94	119.95	119.89	3.77	80.04	40.03
30	9.75	6.3375	2.113	64.90	1.19	129.93	129.84	4.78	86.72	43.38
40	10.50	7.3500	2.450	69.86	1.49	139.90	139.77	5.98	93.41	46.74
50	11.25	8.4375	2.812	74.83	1.83	149.86	149.68	7.35	100.11	50.10
60	12.00	9.6000	3.199	79.78	2.22	159.80	159.55	8.92	106.83	53.48
70	12.75	10.8375	3.612	84.73	2.66	169.73	169.40	10.67	113.55	56.86
80	13.50	12.1500	4.049	89.66	3.15	179.64	179.20	12.66	120.29	60.26
90	14.25	13.5375	4.511	94.59	3.51	189.54	188.95	14.89	127.04	63.68
200	15.00	15.0000	4.997	99.50	4.32	199.40	198.64	17.37	133.82	67.11
10	15.75	16.5375	5.509	104.40	4.99	209.23	208.27	19.86	140.62	70.57
20	16.50	18.1500	6.045	109.27	5.73	219.03	217.82	22.72	147.45	74.05
30	17.25	19.8375	6.607	114.13	6.54	228.79	227.28	25.91	154.31	77.56
240	18.∞	21.6000	7.192	118.97	7.41	238.51	236.63	30.01	161.22	81.11

TABLE XXIII. — Spiral Functions for a Change of 10.0° per 100 Feet. Suitable for Speeds of 22 Miles an Hour or Less, or Curves of 25.0° or Less

L	D	Δ	A	Z	0	C	X	Y	U	V
	۰									
10	1.00	0.050	0.017	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	2.00	.200	.067	10.00	.01	20.00	20.00	.02	13.33	6.67
30	3.00	.450	.150	15.00	.02	30.00	30.00	.c8	20.00	10.00
40	4.00	.800	.267	20.00	.05	40.00	40.00	.19	26.67	13.33
50	5.00	1.250	.417	24.99	.09	50.00	50.00	.36	33.33	16.67
60	6.00	1.800	.600	29.98	.16	60.00	59.99	.63	40.00	20,00
70	7.00	2.450	.817	34.98	.25	69.99	69.99	.98	46.67	23.34
80	8.00	3.200	1.067	39.96	-37	79.99	79.97	1.49	53.34	26.67
90	9.00	4.050	1.350	44.95	-53	89.98	89.96	2.12	60.02	30.01
100	10.00	5.000	1.667	49.92	.72	99.97	99.92	2.91	66.69	33.36
10	11.00	6.050	2.017	54.89	.98	109.95	109.88	3.87	73.38	36.71
20	12.00	7.200	2.400	59.86	1.25	119.92	119.81	5.02	80.07	40.06
30	13.00	8.450	2.816	64.81	1.59	129.88	129.72	6.38	86.77	43.42
40	14.00	9.800	3.266	69.76	1.98	139.82	139.59	7.97	93.48	46.80
50	15.00	11.250	3.749	74.69	2.43	149.74	149.43	9.78	100.20	50.19
60	16.00	12.80C	4.265	79.61	2.95	159.65	159.21	11.87	106.95	53.59
70	17.00	14.450	4.814	84.52	3.53	169.53	168.93	14.21	113.72	57.01
8o	18.00	16.200	5.396	89.40	4.18	179.37	178.57	16.87	120.45	60.47
90	19.00	18.050	6.012	94.26	4.91	189.18	188.13	19.78	127.34	63.94
200	20.00	20,000	6.660	99.11	5.71	198.93	197.59	23.07	134.20	67.46
10	21.00	22.050	7.341	103.92	6.69	208.64	206.93	26.60	141.11	71.01
20	22.00	24.200	8.055	108.71	7.56	218.28	216.13	30.59	148.07	74.62
30	23.00	26.450	8.802	113.46	8.51	227.86	225.17	34.77	155.09	78.27
40	24.00	28.800	9.580	118.18	9.76	237.35	234.04	39.50	162.18	82.00
250	25.00	31.250	10.392	122.86	10.99	246.75	242.70	44.67	169.36	85.79
		1								

CHAPTER III

LOGARITHMS AND TRIGONOMETRIC FUNCTIONS

TABLE XXIV. — COMMON LOGARITHMS OF NUMBERS

USE OF THE TABLE OF LOGARITHMS The logarithm of a number is the exponent denoting the power to

which some fixed base number must be raised to equal the number whose logarithm is considered. There are two base numbers in use. but almost all operations are performed by one system, known as Common Logarithms, in which the base is 10. The logarithm of 1 in any system is o because any number raised to the o power is I. Thus $\frac{x^1}{x^1} = x^{1-1} = x^0 = 1$. The logarithm of 10 in the common system is 1; of 100, 2; of 1000, 3; etc., since $10^1 = 10$, $10^2 = 100$, $10^3 = 1000$, etc. Numbers between I and IO, IO and IOO, IOO and IOOO, etc., will have fractional logarithms. Thus, the logarithm of 8 is 0.90309; of 13 is 1.11394; of 126 is 2.10037, etc., since $10^{0.90309} = 8$, $10^{1.11394} = 13$, $10^{2.10037}$ = 126. etc. The fraction is called the mantissa and is always the same for the same sequence of figures and is incommensurable, being given to 3, 5, 6, 7, or 10 decimal places, according to the precision required. Thus $\log 1.263 = 0.10140$; $\log 12.63 = 1.10140$; and $\log 126.3 =$ 2.10140, all of 5 decimal places. The whole number, called the characteristic, varies. The characteristic is always I less than the number of digits to the left of the decimal point of the number whose logarithm is being found. In the tables only the mantissas are given. The whole number must be known by the computer from the number of digits in the number whose logarithm is wanted.

To find the logarithm of a number look in the table for the mantissa and prefix the proper characteristic, determined from the number of digits to the left of the decimal point in the number in question. Thus, on page 76, line 27, we find the mantissa for the sequence 1263 in the fifth column to be 0.10140; then for 1.263 the log is 0.10140; for 12.63 and 126.3 as given above.

In the table the first three figures of a four-figure number appear in the first column, the fourth figure at the heads of the 10 numbered columns. The first two figures of the mantissa appear in the second column, the last three in the column under the fourth digit of the number whose logarithm is sought. If the first two figures change in going across the page, that fact is indicated by an asterisk; which, to economize space, stands for the first two figures of the second column in the *line below the asterisk*. Thus, the logarithm of 1445 (see p. 76) is 3.15987, while that of 1446 is 3.16017. For numbers of 3 figures or less, the mantissa is found in the column headed 0, since the mantissas for 1, 10, 100, or for 2, 20, 200, or for 15, 150, 1500, etc., are respectively the same.

The logarithm of a number of more than four figures is found as indicated in the following example: What is the log of 382.568? On page 81, line 33, columns 2 and 7, find log 382.5 to be 2.58263. Note that log 382.6 is 2.59274, a difference of 11 in the log for a difference of I in the last place of the sequence in the number. Assuming that the log increases in proportion to the number, the log of 382.568 may be said to be $\frac{68}{100}$ of 11 larger than log 382.5 since 382.568 is $\frac{68}{100}$ of 1 in the last place (the place of the 5) greater than 382.5. To facilitate this computation, a table of proportional parts is found alongside the log table. Thus, in the case just given, for a difference of 11 we find, from the table of proportional parts, that an increase of 0.6 of one in the last place of the number makes a difference in the log of 6.6, an increase of 0.08 in the number increases the log by 0.88, found by moving the decimal point I digit to the left in the tabular value for 0.8, so that an increase of 0.68 of 1 in the last place increases the log of 382.5 by 6.6 + 0.88, or 7.48; or, since we make the fifth figure the nearest whole number, we find $\log 382.568 = 2.58263 + 7 = 2.58270$.

To find the number corresponding to a given logarithm we reverse the process. Thus, the number corresponding to the logarithm 2.58270 is found as follows: The next smaller mantissa is 0.58263 for the sequence 3825 and it is smaller than 0.58270 by 7. The difference for a whole unit in the last place is 11 and in the table of proportional parts under 11 find 6.6, corresponding to 0.6 of 1 in the last place of the number, as the next smaller difference to 7, leaving still a difference of 7-6.6=0.4 to be used, which, by moving the decimal point one digit to the left, is found to correspond most nearly to 0.04 of 1 in the last place of the number. Therefore, the whole number is 382.564. But we found that 2.58270 is the logarithm of 382.568. We see by this that this table cannot be depended on to give more than a sequence of 5 significant

figures correctly. This is true of all tables of logarithms: that as many significant figures in sequence may be correctly determined as there are decimal places in the tabular mantissas. A 5-place table gives five significant figures, a 6-place table, six significant figures, etc.

To multiply a by b we add the logarithms of a and b, written $\log a$

and log b, and find the number corresponding to the sum.

To divide a by b, we subtract $\log b$ from $\log a$ and find the number corresponding to the difference.

It may often occur in computations that the fifth place in a resulting logarithm, found by adding two or more logarithms, may be in error by one unit, thus making the quantity determined certain to one less significant figure than the number of places in the logarithm.

To find the product a^2b^3 . Find the logarithm of a and multiply it by 2; find the logarithm of b and multiply it by 3; add the two results for the logarithm of the product and find the corresponding number. Thus:

What is the product $1.2^2 \times 4.3^3$? p. 76, line 21, col. 2, log $1.2 = 0.07918 \times 2 = 0.15836$ p. 82, line 31, col. 2, log $4.3 = 0.63347 \times 3 = 1.90041$ p. 76, line 15, col. 6 and 7 $= 2.05877 = \log 114.49$.

Ans.

This example, checked by a 7-place table, gives the same result to the fifth significant figure even though both logarithms were multiplied and then added.

The following example, worked by 5-place and 7-place logarithms, shows the uncertainty of the last figure in computations made by any set of tables, by showing the uncertainty of the fifth figure in the computations made with the 5-place tables. Required the product 1.65² × 1.8³.

Log I.65 = 0.21748
$$\times$$
 2 = 0.43496
Log I.8 = 0.25527 \times 3 = 0.76581
1.20077 = log I5.877. Ans.
7-Place
Log I.65 = 0.2174839 \times 2 = 0.4349678
Log I.8 = 0.2552725 \times 3 = 0.7658175
1.2007853 = log I5.8776. Ans.

Thus 15.878 is nearer right than 15.877, although the error of the latter is only about 0.6 of one in the last place and the error of the former is

about 0.4 of one in the last place. Greater differences can occur so that the fifth place is not certain within I unit.

Logarithms of fractions. The logarithm of $I = \frac{10}{10} = I0^{1-1} = I0^0$ is 0.00000. Similarly the logarithm of $0.I = \frac{1}{10} = I0^{0-1}$ is -1.00000; the logarithm of $\frac{1}{10}$ is -2; of $\frac{1}{1000}$ is -3; etc. Therefore, if the sequence is all fractional the characteristic is minus and with a numerical value expressed by the number of the place on the right of the decimal point in which the first significant figure appears. Thus the logarithm of 0.00126 is -3 + 0.10037, usually written $\frac{1}{3}.10037$. The mantissa is not minus, only the characteristic is minus. This sometimes gives the beginner trouble, but need not if he remembers that the mantissa is always plus, while the characteristic is plus or minus according as the number corresponding is equal to or greater than I or is less than I, and that in general the two must be treated separately. The following examples will make the use of the signs clear:

Required the product 43.0×0.43 .

Required the product 43.0×0.43^2 .

Log
$$43.0 = 1.63347$$
 Log $0.43^2 = \overline{1}.63347 \times 2$ Log $0.43^2 = \overline{1}.26694$ Log $7.951 = 0.90041$ Log $0.43^2 = \overline{1}.26694 = \overline{1}.26694$

Required the product $43.0 \times 0.43^{\frac{1}{2}}$.

Log
$$0.43^{\frac{1}{2}} = \overline{1}.816735$$
 found thus: Add 10 to the characteristic and subtract 10 before dividing by 2, getting
$$1.45021$$
Log $0.43^{\frac{1}{2}} = \overline{1}.816735$
Log $0.43^{\frac{1}{2}} = \overline{1}.816735$
Log $0.43^{\frac{1}{2}} = \overline{1}.816735$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

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$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

$$1.45021$$

Instead of adding and subtracting 10 in the preceding example, only enough may be added and subtracted to make the negative characteristic divisible by the divisor. Thus: In the foregoing example add and subtract 1, getting $\frac{\overline{1}.63347 - \overline{1} + \overline{1}}{2} = \frac{\overline{2} + \overline{1}.63347}{2} = \overline{1}.816735$, as before, without the necessity of considering the 4 and -5. If the 1/3 power has been required, the divisor would have been 3, and 2 should be added and subtracted getting $\frac{\overline{1}.63347 - 2 + 2}{3} = \frac{\overline{3} + 2.63347}{3} = 1.877823 +$. This work need not be written out in full in an exam-

ple, as the computer can see the figures mentally. Thus, he knows the characteristic will be $\bar{1}$ so he writes this down and then imagines a 2, or whatever number is to be added, at the left of the decimal and at once writes down the quotient after the $\bar{1}$. In handling very small numbers when the negative characteristic is large, it may be necessary to write out the operation to guard against error.

In making the tables, when the remainder after the fifth figure was more than 0.5, the fifth figure was increased by 1; when less than 0.5,

the fifth figure was not changed.

When the computer is finding a logarithm, and the operation brings a 5 in the place following the last place of the table (as the sixth place when using the tables of this book) and the 5 is followed by ciphers, a good rule to adopt is to make the last place the nearest *even* number. Thus in getting log $0.43^{\frac{1}{2}}$ in the example above we add 5 in the sixth place. This rule will tend to balance inaccuracies in a long series of computations.

To divide 3.68×4.21 we find (page 81) log 3.68 = 0.56585 (page 82) log 4.21 = 0.62428

Now to subtract, we may add and subtract

10 from the log 3.68, getting 10.56585 - 10 0.62428

 $\frac{9.94157 - 10}{9.94157} = \overline{1}.94157$

or, we may add the arithmetical complement of log 4.21 instead of subtracting the log 4.21. That is, we may multiply by $\frac{I}{4.21}$ instead

of dividing by 4.21. The logarithm of $\frac{1}{4.21}$ is 0.00000 - 0.62428, or

1.37572 and is called the arithmetical complement of the log 4.21. It is the logarithm of the reciprocal of 4.21. In a series of operations, where several factors are to be multiplied and the product divided by the product of several factors, the arithmetical complements of the divisor factors are used to avoid the double operation of two additions and one subtraction, since the arithmetical complements may be written down from the logs almost as readily as the logs themselves. Each digit of the mantissa of the log is subtracted from 9 except the last, which is subtracted from 10. The characteristic is negative and one greater than the characteristic of the log when the log characteristic is positive; and is positive and one less than the characteristic of the log if that characteristic is negative. Thus:

Log 8.364 is 0.92241; its complement is **1.07759** Log 83.64 is 1.92241; its complement is **2.07759** Log 836.4 is $\overline{2.92241}$; its complement is $\overline{3.07759}$ Log 0.8364 is $\overline{1.92241}$; its complement is 0.07759 Log 0.08364 is $\overline{2.92241}$; its complement is 1.07759

Instead of thinking of the characteristic by the rule above, the log may be subtracted from 10 instead of zero when a characteristic of 9 in the complement will correspond to $\overline{1}$; 8 to $\overline{2}$, etc. And the computer can as readily think of 9 as indicating that the first significant figure of the result is in the first or tenths' place of the decimal; 8, that it is in the second or hundredths' place, etc., and this will cause no confusion unless very large quantities are being dealt with, so that the 8 or 9 might sometimes be a positive characteristic not standing in the place of a $\overline{2}$ or $\overline{1}$; but this difficulty is not likely to arise in using 5- or 6-place tables, since such tables would not be used with such large numbers.

When the first figures are small. When the first three figures of a number of five or more places are between 100 and 110 inclusive use pages 94 and 95, which give 7-place logarithms for five digits directly.

N	L	0	1	2	3	4	5	6	7	8	9		PP	
100	00	000	043	087	130	173	217	260	303	346	389			
101		432	475	518	561	604	647	689	732	775	817	44	43	42
102	۱	860	903	945	988	*030	*072	*115	*157	*199	*242		20	10
103	OI		326	368	410	452	494	536	578	620	662	I 4.4 2 8.8	4.3 8.6	4.2
104	02	703	745 160	· 787	828	870 284	912	953 366	995	*036	*078	2 8.8 3 I3.2	12.9	8.4
105	02	119 531	572	612	243 6 5 3	694	325 735	776	407 816	449 857	490 898	4 17.6	17.2	16.8
107		938	979	*010	*060	*100	*141	*181	*222	*262	*302	5 22.0	21.5 25.8	2I.0 25.2
108	0,3	342	383	423	463	503	543	583	623	663	703	7 30.8	30.I	29.4
109	ľ	743	782	822	862	902	941	981	*021	*060	*100	8 35.2 9 39.6	34.4	33.6
110	04	139	179	218	258	297	336	376	415	454	493	9139.0	38.7	37.8
III		532	571	610	650	689	727	766	805	844	883	41	40	39
112		922	961	999	*038	*077	*115	*154	*192	*231	*269	41	40	39
113	05	308	346	385	423	461	500	538	576	614	652	1 4.1	4.0	3.9
114		690	729	767	805	843	881	918	956	994	*032	2 8.2 3 I2.3	8.0	7.8 II.7
115	06		108	145	183	221	258	296	333	371	408	4 16.4	16.0	15.6
116		446	483	521	558	595	633	670	707	744	781	5 20.5	20.0	19.5
117	07	188	856	893	930	967	*004 372	*041 408	*078	*115 482	*151 518	6 24.6 7 28.7	24.0 28.0	23.4 27.3
110	0,	555	591	628	664	335	737	773	445 800	846	882	8 32.8	32.0	31.2
120		918	954	990	*027	*063	*099	*135	*171	*207	*243	9 36.9	36.0	35.I
121	08	279	314	350	386	422	458	493	520	565	600	38	37	36
122	00	636	672	707	743	778	814	849	884	920	955	38	37	36
123		991	*026	*061	*096	*132	*167	*202	*237	*272	*307	1 3.8	3.7	3.6
124	009	342	377	412	447	482	517	552	587	621	656	2 7.6 3 II.4	7.4 II.I	7.2
125	_	691	726	760	795	830	864	899	934	968	*003	4 15.2	14.8	I4.4
126	10	037	072	106	140	175	209	243	278	312	346	5 19.0	18.5	18.0
127		380	415	449	483	517	551	585	619	653	687	6 22.8 7 26.6	22.2 25.9	21.6
128		721	755	789	823	857	890	924	958	992	*025	8 30.4	29.6	28.8
129	II		093	126	160	193	227	261	294	327	361	9 34.2	33.3	32.4
130		394	428	461	494	528	561	594	628	661	694			
131		727	760	793	826	860	893	926	959	992	*024	35	34	33
132	12	057	090	123	156	189	222	254 581	287 613	320	352	1 3.5	3.4	3.3
133		385		450	483 808	516 840	548 872	-	-	646 969	678	2 7.0	6.8	6.6
134	13	710	743 066	775	130	162	104	9 0 5	937 258	290	*001 322	3 10.5	10.2 13.6	9.9 13.2
136	-3	354	386	418	450	481	513	545	577	600	640	5 17.5	17.0	16.5
137		672	704	735	767	799	830	862	893	925	956	6 21.0	20.4 23.8	19.8 23.1
138		988	*019	*051	*082	*114	*145	*176	*208	*239	*270	8 28.0	27.2	26.4
139	14	301	_333	364	395	426	457	489	520	551	582	9 31.5	30.6	29.7
140		613	644	675	706	737	768	799	829	860	891	00	04	20
141		922	953	983	*014	*045	*076	*106	*137	*168	*198	32	31	30
142	15	229	259	290	320	351	381	412	442	473	503	1 3.2	3.I	3.0
143		534	564	594	625	655	685	715	746	776	806	2 6.4	6.2 9.3	9.0
144	76	836	866 167	897	927	957	987 286	*017	*047	*077	*107	4 12.8	12.4	12.0
145 146	10	137 435	465	197 495	227 524	256 554	584	316 613	346 643	376 673	406 702	5 16.0	15.5	15.0 18.0
147		732	761	791	820	850	879	000	938	067	997	6 19.2 7 22.4	18.6	21.0
148	17	026	056	085	114	143	173	202	231	260	289	8 25.6	24.8	24.0
149		319	348	377	406	435	464	493	522	551	580	9 28.8	27.9	27.0
150	17	609	863	667	696	725	754	782	811	840	869			
N	L	0		2	3	4	5	6	7	8	9		PP	

155	2.8 5.6 8.4 11.2 14.0 16.8 19.6 22.4 25.2 7.8 13.0 15.6 15.2 7.8 13.0 15.6 22.3 23.4
151	2.8 5.6 8.4 11.2 14.0 16.8 19.6 22.4 25.2 26 2.6 5.2 7.8 10.4 13.0 15.6 15.2 20.8
153	5.6 8.4 11.2 14.0 16.8 19.6 22.4 25.2 26 5.2 7.8 10.4 13.0 15.6 18.2 20.8
154	8.4 11.2 14.0 16.8 19.6 22.4 25.2 26 2.6 5.2 7.8 10.4 13.0 15.0 18.2 20.8
155	14.0 16.8 19.6 22.4 25.2 26 2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
156	16.8 19.6 22.4 25.2 26 2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
158 866 893 921 948 976 970 303 303 358 385	22.4 25.2 26 2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
159	25.2 26 2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
160	2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
161	2.6 5.2 7.8 10.4 13.0 15.6 18.2 20.8
162	5.2 7.8 10.4 13.0 15.6 18.2 20.8
163	5.2 7.8 10.4 13.0 15.6 18.2 20.8
164	7.8 10.4 13.0 15.6 18.2 20.8
165	13.0 15.6 18.2 20.8
166	15.6 18.2 20.8
170	20.8
170	
170	
171 300 325 350 376 401 426 452 477 502 528 172 553 578 603 629 654 679 704 729 754 779 1 2 2 173 805 830 855 880 905 930 955 980 *005 *030 3 7 7 7 7 7 7 8 2 3 53 378 403 428 452 477 502 527 512 176 551 576 601 625 650 674 699 724 748 773 7 177 797 822 846 871 805 920 944 969 993 *018 7 7 178 25 042 066 091 115 139 164 188 212 237 261 201 179 228 310 334 358 352 406 431 455 479 503 180 527 551 575 600 624 648 672 696 720 744 748	
172	
173	=
174	0
175	
177	
178	
178	
180	
181 768 792 816 840 864 888 912 935 959 983 182 26 007 031 055 079 102 126 150 174 198 221 1 2.4 183 245 269 293 316 340 364 387 411 435 458 2 4.8 184 482 505 529 553 576 600 623 647 670 694 4 0.6	
182 26 007 031 055 079 102 126 150 174 198 221 1 2.4 183 245 269 293 316 340 364 387 411 435 458 2 4.8 184 482 505 529 553 576 600 623 647 670 694 3 7.2 0.6	23
183 245 269 293 316 340 364 387 411 435 458 2 4.8 184 482 505 529 553 576 600 623 647 670 694 4 7.6	2.3
184 482 505 529 553 576 600 623 647 670 694 3 7.2	2.3 4.6
	6.9 9.2
185 717 741 764 788 811 834 858 881 905 928 5 12.0 186 951 975 998 921 945 968 901 114 138 161 6 14.4	11.5
186 951 975 998 *021 *045 *068 *091 *114 *138 *161 6 14.4	13.8 16.1
107 27 184 207 231 254 277 300 323 340 370 393 8 19.2	18.4
188 416 439 462 485 508 531 554 577 600 623 9 21.6 189 646 669 692 715 738 761 784 807 830 852	20.7
100 875 808 021 044 067 080 *010 *025 *058 *081	
191 28 103 126 149 171 194 217 240 262 285 307	21
192 330 353 375 398 421 443 466 488 511 533 I 2.2	2.I
193 556 578 601 623 646 668 691 713 735 758 2 4.4	4.2
194 780 803 825 847 870 892 914 937 959 981 4 8.8	6.3 8.4
195 29 003 026 048 070 092 115 137 159 181 203 5 11.0	
	10.5
197 447 409 491 513 535 557 579 001 023 045 8 17.6	10.5 12.6
198	10.5 12.6 14.7 16.8
200 30 103 125 146 168 190 211 233 255 276 298	10.5 12.6 14.7
N L O I 2 3 4 5 6 7 8 9 PP	10.5 12.6 14.7 16.8

ı	N	L O	1	2	3	4	5	6	7	8	9	PP
ı	200	30 103	125	146	168	190	211	233	255	276	298	
ı	201	320	341	363	384	406 621	428	449 664	47I 685	492	514	22 21
ı	202	535 750	557 771	578 792	814	835	643 856	878	899	707	728	I 2.2 2.I 2 4.4 4.2
ı	204	963	984	*006	*027	*048	*060	*091	*112	*133	*154	3 6.6 6.3
ı	205	31 175	197	218	239	260	281	302	323	345	366	4 8.8 8.4 5 II.O 10.5
1	206	387	408	429	450	471	492	513	534	555	576	6 13.2 12.6
ı	207	597 806	618	639 848	869	681 890	702 QII	723	744	765	785	7 15.4 14.7 8 17.6 16.8
ı	200	32 015	035	056	077	098	118	931 139	952 160	973 181	994 201	9 19.8 18.9
I	210	222	243	263	284	305	325	346	366	387	408	
ı	211	428	449	400	490	510	531	552	572	593	613	20
ı	212	634	654	675	695	715	736	756	777	797	818	I 2.0
ı	213	838	858	879	899	919	940	960	980	*001	*C2I	2 4.0 3 6.0
ı	214	33 04I 244	062 264	082 284	304	325	143 345	163 365	183	203	224 425	4 8.0
ı	216	445	465	486	506	526	546	566	586	606	626	5 IO.0 6 I2.0
ı	217	646	666	686	706	726	746	766	786	806	826	7 14.0 8 16.0
ı	218	846	866	885	905	925	945	965	985	*005	*025	9 18.0
ı	219 220	34 044	064	282	104	124	143	163	183	203	223	
ı	221	242	262		301	321	341	361	380	400	420	19
ı	222	439 635	459 655	479 674	694	713	537 733	557 753	577 772	596 792	811	1 1.9
ı	223	830	850	869	889	908	928	947	967	986	*005	2 3.8
ı	224	35 025	044	064	083	102	122	141	160	180	199	3 5.7 4 7.6
I	225	218	238	257	276	295	315	334	353	372	392	5 9.5 6 II.4
I	226	603	430 622	449	468 660	488 679	507 698	526	545	564	583	7 13.3
ı	227	793	813	641 832	851	870	889	908	736	755 946	774	8 15.2 9 17.1
ı	229	984	*003	*021	*040	*059	*078	*097	*116	*135	*154	9 1/.1
ı	230	36 173	192	211	229	248	267	286	305	324	342	18
ı	231	361	380	399	418	436	455	474	493	511	530	1 1.8
ı	232	549 736	568 754	586 773	791	624 810	642 829	847	68o 866	698 884	717	2 3.6
ı	234	Q22	940	959	977	996	*014	*033	*051	*070	*088	3 5-4 4 7-2
ı	235	37 107	125	144	162	181	199	218	236	254	273	5 9.0
ı	236	291	310	328	346	365	383	401	420	438	457	
1	237	475	493	511	530	548	566	585	603	621	639	7 12.6 8 14.4 9 16.2
I	238	658 840	676 858	694 876	712 894	73I 9I2	749 931	767 949	785 967	803 985	822 *co3	9 10.2
I		38 021	039	057	075	093	112	130	148	166	184	17
	241	202	220	238	256	274	292	310	328	346	364	
1	242	382	399	417	435	453	471	489	507	525	543	2 3.4
	243	561	578	596	614	632	650	668	686	703	721	3 5.1 4 6.8
I	244	739 917	757 934	775 952	792 970	987	828 *005	846 *023	863 *041	881 *058	899 *076	5 8.5
1		39 094	111	129	146	164	182	199	217	235	252	
I	247	270	287	305	322	340	358	375	393	410	428	8 13.6
1	248	445	463	480	498	515	533	550	568	585	602	9 15.3
1	249 250	620	637 811	6 <u>55</u> 829	846	863	707	724 898	742	759	777	
F		39 794			_	-	_		915	933	950	
L	N	L O	1	2	3	4	5	6	7_	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
250	39 79		829	846	863	881	898	915	933	950	40
251	96		*002	*019	*037	*054	*071	*088	*106	*123	18
252 253	40 140		175 346	192 364	381	398	243 415	261 432	278	²⁹⁵	I 1.8 2 3.6
254	48		518	535	552	560	586	603	620	637	3 5.4
255	652		688	705	722	739	756	773	790	807	4 7.2
256	824		858	875	892	909	926	943	960	976	6 10.8
257	993		*027	*044	*061	*078	*095	*111	*128	*145	7 12.6
258	41 16:		196	380	,229	246	263	280	296	313 481	8 14.4 9 16.2
²⁵⁹ 260	330		363		397	581	430	447 614	464		
261	497 662		531	547	564		597 764	780	631	647	17
262	830		863	714 880	731 896	747	929	946	797 963	814 979	I 1.7
263	996		*029	*045	*062	*078	*095	*111	*127	*144	2 3.4
264	42 160	177	193	210	226	243	259	275	292	308	3 5.I 4 6.8
265	325		357	374	390	406	423	439	455	472	5 8.5
266	488		521	537	553	570	586	602	619	635	6 10.2
267 268	651 813		684 846	700 862	716 8 7 8	732 894	749	765	781 943	797 959	8 13.6
269	975		*008	*024	*040	*056	*072	*088	*104	*120	9 15.3
270	43 136		169	185	201	217	233	249	265	281	16
271	297	313	329	345	361	377	393	409	425	441	
272	457	473	489	505	521	537	553	569	584	600	I 1.6 2 3.2
273	616		648	664	680	696	712	727	743	759	3 4.8
274 275	775 933		807 965	823 981	838	854 *012	870 *028	886 *044	902 *059	917 *075	4 6.4 5 8.0
276	44 001	107	122	138	154	170	185	201	217	232	6 9.6
277	248	264	279	295	311	326	342	358	373	389	7 11.2 8 12.8
278	404	420	436	451	467	483	498	514	520	545	9 14.4
279	560		592	607	623	638	654	669	685	700	
280	716		747	762	778	793	800	824	840	855	15
281 282	871 45 025	886	902 056	917 071	932 086	948	963	979 133	994	*010	I 1.5
283	170		200	225	240	255	271	286	301	317	2 3.0 3 4.5
284	332		362	378	393	408	423	439	454	469	4 6.0
285	484	500	515	530	545	561	576	591	606	621	5 7.5 6 9.0
286	637	652	667	682	697	712	728	743	758	773	7 10.5
287 288	788 939		969	834 984	849 *000	864 *015	879 *030	894 *045	909 *060	924 *075	8 12.0 9 13.5
289	46 090		120	135	150	165	180	195	210	225	,
290	240		270	285	300	315	330	345	359	374	14
291	380	404	419	434	449	464	479	494	500	523	1 1.4
292	538 687	553	568	583	598	613	627	642	657	672	2 2.8
293			716	731	746	761	776	790	805	820	3 4.2 4 5.6
294 295	835 982	850	*012	879 *026	894 *041	909 *056	923	938 *085	953	967 *114	5 7.0 6 8.4
296	47 129		159	173	188	202	217	232	246	261	5 7.0 6 8.4 7 9.8
297	276		305	310	334	349	363	378	302	407	8 11.2
298	422	436	451	465	480	494	500	524	538	553	9 12.6
299	567	-	596	611	625	640	654	669	683	698	
300	47 713		741	756	770	784	799	813	828	842	
N	L 0	1	2	3	4	5	6	7	8	9	PP

N	L	. 0	1	2	3	4	5	6	7	8	9	PP
300	1 '''	712	727	741	756	770	784	799	813	828	842	
301		857	871	885	900	914	929	943	958	972 116	986	
302 303	40	144	159	029 173	187	202	973 216	230	244	259	130 273	4.0
304		287	302	316	330	344	359	373	387	401	416	15
305		430	444	458	473	487	501	515	530	544	558	I I.5 2 3.0
306		572	586 728	601	756	770	643 785	657	671 813	686 827	700	3 4.5
307 308		714 855	869	742 883	897	911	926	799 940	954	968	841 982	5 7.5
309		996	*010	*024	*038	*052	*066	*080	*094	*108	*122	
310	49	136	150	164	178	192	206	220	234	248	262	8 12.0
311		276 415	290 429	3 0 4 443	318 457	332 471	346 485	36 o 499	374 513	388 527	402 541	9 13.5
313		554	568	582	596	610	624	638	651	665	679	
314		693	707	721	734	748	762	776	790	803	817	
315		831	845	859	872	886	900	914	927	941	955 *092	14
316	50	969	982	996	*010	*024 161	*037 174	188	*065 202	*079	220	I I.4 2 2.8
318		243	256	270	284	297	311	325	338	352	365	3 4.2
319		379	393	406	420	433	447	461	474	488	501	4 5.6 5 7.0 6 8.4
320		515	529	542	556	569	583	596	610	623	637	
32I 322		651 786	799	678	691 826	705 840	718 853	732 866	745 880	759 893	772 907	8 11.2
323		920	934	947	961	974	987	*001	*014	*028	*041	9 12.6
324	51	055	068	081	095	108	121	135	148	162	175	
325 326		188	202	348	228 362	242	255 388	268	282 415	295 428	308	
327		455	335 468	481	495	375 508	521	534	548	561	574	13
328		587	601	614	627	640	654	667	680	693	706	I I.3
329		720	733	746	759	772	786	799	812	825	838	2 2.6 3 3.9
330	1	851	865	878	891	904	917	930	943	957	970	4 5-2
33I 332		983	996	*009	*022 153	*035	* 0 48	*061	*075 205	*088 218	*101	5 6.5 6 7.8
333	3-	244	257	270	284	297	310	323	336	349	362	7 9.1 8 10.4
334		375	388	401	414	427	440	453	466	479	492	9 11.7
335		504 634	517	530 660	543 673	556 686	569	582	595 724	608 737	750	
337		763	776	789	802	815	827	840	853	866	879	
338		892	905	917	930	943	956	969	982	994	*007	12
339		020	033	046	058	071	084	097	110	122	135	I I.2
340		148	161	173	186	199	212	224	237	250	263	3 3.6
34I 342		275 403	288	301 428	314	326 453	339 466	35 ² 479	364 491	377 504	390	4 4.8
343		529	542	555	567	580	593	605	618	631	643	5 6.0 6 7.2
344		656	668	681	694	706	719	732	744	757 882	769	7 8.4 8 9.6
345 346		782 908	794	933	945	958	970	983	870 995	*008	895 *020	9 10.8
347		033	045	058	070	083	095	108	120	133	145	
348		158	170	183	195	208	220	233	245	258	270	
349	- 1	283	295	307	320	332	345	357	370	382	394	
350	_	407	419	432	444	456	469	481	494	506	518	
N	L	. 0	1	2	3	4	5	6	7	8	9	PP

N	LO	ı	2	3	4	5	6	7	8	9	PP
350	54 407	419	432	444	456	469	481	494	506	518	
351	531	543 667	555	568 691	580	593	605	617	630	642	
352 353	654 777	790	802	814	704	839	728 851	741 864	753 876	765	13
354	900	913	925	937	949	962	974	986	998	*011	
355	55 023	035	047	060	072	084	096	108	121	133	2 2.6
356	145	157	169	182	194	206	218	230	242	255	3 3.9 5.2
357 358	267 388	279 400	291 413	303 425	315 437	328 449	340 461	35 ² 473	364	376 497	4 5.2 5 6.5 6 7.8
359	509	522	534	546	558	570	582	594	606	618	0 7.8 7 9.1
360	630	642	654	666	678	691	703	715	727	739	8 10.4
361	751 871	763	775	787	799	811	823	835	847	859	9 11.7
362 363	991	883 *003	895 *015	907 *027	919 *038	931 *050	943 *062	955 *074	967 *o86	979 *098	
364	56 110	122	134	146	158	170	182	194	205	217	
365	229	241	253	265	277	289	301	312	324	336	12
366	348	360	372	384	396	407	419	431	443	455	I I.2
367 368	467 585	478	490 608	502 620	514	526	538	549	561	573	3 3.6
369	703	597	726	738	750	644 761	773	785	797	808	4 4.8
370	820	832	844	855	867	879	891	902	914	926	6 7.2
37I	937	949	961	972	984	996	*008	*019	*031	*043	6 7.2 7 8.4 8 9.6
372	57 054	066	078	089	101	113	124	136	148	159	9 10.8
373	171 287	183	194	206	217	229	241	252	264	276	
374 375	403	299 415	310 426	322 438	334	345 461	357 473	368 484	380 496	392 507	
376	519	530	542	553	565	576	588	600	611	623	11
377	634	646	657	669	680	692	703	715	726	738	1 1.1
378 379	749 864	875	772 887	784 898	795	921	933	830 944	955	852 967	2 2.2
380	978	990	*001	*013	*024	*035	*047	*058	*070	*081	3 3.3
381	58 092	104	115	127	138	149	161	172	184	195	4 4.4 5 5.5 6 6.6
382	206	218	229	240	252	263	274	286	297	309	7 7.7
383	320	331	343	354	365	377	388	399	410	422	7 7.7 8 8.8 9 9.9
384 385	433 546	444 557	456 569	467 580	478 591	490 602	501	512 625	524 636	535 647	9 9.9
386	659	670	681	692	704	715	726	737	749	760	
387	771	782	794	805	816	827	838	850	861	872	
388 389	883 995	894 *006	906 *017	917 *028	928 *040	939 *051	950 *062	961 *073	973 *084	984	10
390	59 106	118	120	140	151	162	173	184	195	*095 207	1 1.0
391	218	220	240	251	262	273	284	295	306	318	2 2.0 3 3.0
392	329	340	351	362	373	384	395	406	417	428	4 4.0
393	439	450	461	472	483	494	506	517	528	539	5 5.0 6 6.0
394 395	550 660	561 671	572 682	583 693	594 704	605 715	726	627	638	649	7 7.0 8 8.0
395	770	780	791	802	813	824	835	737 846	748 857	759 868	9 9.0
397	879	890	901	912	923	934	945	956	966	977	
398	988	999	*010	*021	*032	*043	*054	*065	*076	*o86	
399	60 097	108	119	130	141	152 260	163	173 282	184	195	
400 N	L 0	217	228	239 3	249 4	5	6	7	293 8	304 9	PP
14	LU	1		0		0	O	-	0	9	P P

N	L	0	1	2	3	4	5	6	7	8	9	PP
400	60	206	217	228	239	249	260	271	282	293	304	
401		314	325	336	347	358	369	379	390	401	412	
402 403		423 531	433 541	444 552	455 563	466 574	477 584	487 595	498 606	509	520 627	
404		638	649	660	670	681	692	703	713	724	735	
405		746	756	767	778	788	799	810	821	831	842	
406		853	863	874	885	895	906	917	927	938	949	11
407 408	6т	959 066	970	981 087	991	*002 100	*013	*023 130	*034 140	*045 151	*055 162	I I.I 2 2.2
409	"	172	183	194	204	215	225	236	247	257	268	3 3.3
410		278	289	300	310	321	331	342	352	363	374	4 4.4 5 5.5
411		384	395	405	416	426	437	448	458	469	479	0.0
412 413		490 595	500 606	511	521 627	532 637	542 648	553 658	563 669	574 679	584 690	7 7.7 8 8.8
414		700	711	721	731	742	752	763	773	784	794	9 9.9
415		805	815	826	836	847	857	868	878	888	899	
416	6.	909	920	930	941	951	962	972	982 086	993	*003	
417 418	02	014	024	034	045	055	066	076	100	201	211	
419		221	232	242	252	263	273	284	294	304	315	
420		325	335	346	356	366	377	387	397	408	418	10
421		428	439	449	459	469	480	490	500	511	521	1 1.0
422 423		531 634	542 644	552 655	562 665	572 675	583 685	593 696	706	716	624 726	2 2.0
424		737	747	757	767	778	788	798	808	818	820	3 3.0
425		839	849	859	870	880	890	900	910	921	931	5 5.0
426		941	951	961	972	982	992	*002	*012	*022	*033	7 7.0 8 8.0
427	63	043 144	053	063 165	073 175	083	195	205	215	124	236	8 8.0
429		246	256	266	276	286	296	306	317	327	337	, , , , ,
430		347	357	367	377	387	397	407	417	428	438	
431		448	458	468	478	488	498	508	518	528	538	
432		548 649	558	568 669	579 6 7 9	589 689	599 699	700	719	729	739	
433	i	749	759	769	779	780	799	800	810	829	839	
435		849	859	869	879	889	899	909	919	929	939	9
436		949	959	969	979	988	998	*008	*018	*028	*038	1 0.9
437	64	048	058	068	078	088	098	108	118	128	137	3 2.7
438		147 246	256	266	276	286	296	306	316	326	335	4 3.6 5 4.5 6 5.4
440		345	355	365	375	385	395	404	414	424	434	
441		444	454	464	473	483	493	503	513	523	532	7 6.3 8 7.2
442		542	552 650	562 660	572 670	582 680	591 689	699	700	719	729	8 7.2 9 8.1
443		640 738	748	758	768	777	787	797	807	816	826	
444		836	846	856	865	875	885	895	904	914	924	
446		933	943	953	963	972	982	992	*002	*011	*021	
447	65	031	040	050	060	167	176	089	196	108	118	
448		225	137 234	147 244	254	263	273	283	292	302	312	
450	65	321	331	341	350	360	369	379	389	398	408	
N	L	0	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
450	65 321	331	341	350	360	369	379	389	398	408	
451	418	427	437	447	456	466	475	485	495	504	
452	514 610	523 619	533 629	543 639	552 648	562 658	571 667	581 677	591 686	600 696	
453 454	706	715	725	734	744	753	763	772	782	792	
455	801	811	820	830	839	849	858	868	877	887	
456	896	9 0 6	916	925	935	944	954	963	973	982	10
457	992	*001	*011	*020	*030	*039	*049	*058	*068	*077	1 1.0
458	66 0 87	096	200	115 210	124 210	134 220	143 238	153 247	162 257	172 266	2 2.0 3.0
459 460	276	285	295	304	314	323	332	342	351	361	4 4.0
461	370	380	389	398	408	417	427	436	445	455	5 5.0 6 6.0
462	464	474	483	492	502	511	521	530	539	549	7 7.0 8 8.0
463	558	567	577	586	596	605	614	624	633	642	8 8.0 9 9.0
464	652	661	671	680	689	699	708	717	727	736	9 9.0
465 466	745	755 848	764	773 867	783 876	792 885	801 804	904	913	829 922	
467	839		857	960	969	978	987	997	*006	*015	
468	932 67 025	94I 934	950 043	052	062	071	080	080	099	108	
469	117	127	136	145	154	164	173	182	191	201	
470	210	219	228	237	247	256	265	274	284	293	9
471	302	311	321	330	339	348	357	367	376	385	
472	394	403	413	422	431	440	449	459	468	477	I 0.9 2 1.8
473	486	495	504	514 605	523 614	532 624	54I 633	550 642	560 651	569 660	3 2.7
474 475	578 669	587 679	596 688	697	706	715	724	733	742	752	4 3.6 5 4.5
476	761	770	779	788	797	806	815	825	834	843	6 5.4
477	852	861	870	879	888	897	906	916	925	934	7 6.3 8 7.2
478	943	952	961	970	979	988	997	*006	*015	*024	8 7.2 9 8.1
479	68 034	043	052	061	070	079	088	097	106	115	
480	124	133	142	151	160	169	178	187	196	205	
481 482	305	314	233 323	242 332	25I 34I	260 350	269 359	368	377	296 386	
483	395	404	413	422	431	440	449	458	467	476	
484	485	494	502	511	520	529	538	547	556	565	
485	574	583	592	601	610	619	628	637	646	655	8
486	664	673	681	69 0	699	708	717	726	735	744	1 0.8
487 488	753 842	762 851	771 860	780 860	789 878	797 886	806	904	824	833	2 I.6 3 2.4
489	931	940	949	958	966	975	984	993	*002	*011	4 3.2
490	69 020	028	037	046	055	064	073	082	090	099	5 4.0 6 4.8
491	108	117	126	135	144	152	161	170	179	188	7 5.6 8 6.4
492	197	205	214	223	232	241	249	258	267	276	9 7.2
493	285	294	302	311	320	329	338	346	355	364	
494 495	373 461	381 469	390 478	399 487	408 496	417 504	425 513	434 522	443 531	45 ² 539	
496	548	557	566	574	583	592	601	609	618	627	
497	636	644	653	662	671	679	688	697	705	714	
498	723	732	740	749	758	767	775	784	793	801	
499	810	819	827	836	845	854	862	871	966	888	
500		906	914	923	932	940	949	958	-	975	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	L	0	1	2	3	4	5	6	7	8	9	PP
500	69	897	906	914	923	932	940	949	958	966	975	
501		984	992	*001	*010	*018	*027	*036	*044	*053	*062	
502	70	070	079	088	096	105	114	122	131	140	148	
503		157	165	174	183	191	200	209	217	226	234	
504 505		243 329	252 338	260 346	269 355	278 364	286 372	295 381	3 0 3 389	312	32I 406	
506		415	424	432	441	449	458	467	475	484	492	9
507		501	500	518	526	535	544	552	561	569	578	
508		586	595	603	612	621	629	638	646	655	663	I 0.9 2 I.8
509		672	680	689	697	706	714	723	731	740	749	3 2.7
510		757	766	774	783	791	800	808	817	825	834	4 3.6 5 4.5 6 5.4
511 512		842 927	851 935	859 944	868 952	876 961	885 969	893 978	9 0 2 986	910 995	919 * 00 3	6 5.4
513	71	0I2	020	029	037	046	054	o63	071	079	088	7 6.3 8 7.2
514	ľ	096	105	113	122	130	139	147	155	164	172	8 7.2 9 8.1
515		181	189	198	206	214	223	231	240	248	257	
516		265	273	282	290	299	307	315	324	332	341	
517		349	357	366	374	383	391	399	408	416	425	0
518 519		433	525	45° 533	458 542	466 550	475 559	483 567	492 575	500 584	508	4
520		600	600	617	625	634	642	650	659	667	675	
521		684	692	700	709	717	725	734	742	750	759	8
522		767	775	784	792	800	809	817	825	834	842	1 0.8
523		850	858	867	875	883	892	900	9 0 8	917	925	2 I.6 3 2.4
524		933	941	950	958	966	975	983	991	999	*008	4 3.2
525 526	72	000	024 107	032	041	049	057	066	156	165	090	5 4.0 6 4.8
527		181	180	108	206	214	222	230	239	247		7 5.6
528		263	272	280	288	296	304	313	321	329	²⁵⁵	8 6.4
529		346	354	362	370	378	387	395	403	411	419	911.
530		428	436	444	452	460	469	477	485	493	501	
531		509	518	526	534	542	550	558	567	575	583	
532		591	599 681	680	616	624	632	640	648	656	665	
533		673	762	_	697	705	713	722 803	730	738	746 827	
534 535		754 835	843	770 852	779 860	868	795 876	884	802	900	008	7
536		916	925	933	941	949	957	965	973	981	989	1 0.7
537		997	*006	*014	*022	*030	*038	*046	*054	*062	*070	2 I.4
538	73	078	086	094	102	III	119	127	135	143	151	3 2.I 4 2.8
539 540		159	167	175	183	191	199	207	215	223	231	5 3.5
		239	247	255	263	272			296	304	312	6 4.2
541 542		320 400	328 408	336	344 424	352 432	360 440	368 448	376 456	464	39 ² 47 ²	7 4.9 8 5.6 9 6.3
543		480	488	496	50.1	512	520	528	536	544	552	9 6.3
544		560	568	576	584	592	600	608	616	624	632	
545		640	648	656	664	672	679	687	695	703	711	
546		719	727	735	743	751	759	767	775	783	791	
547 548		799 878	807	815	823	830	838	926	933	862	870	
549		957	965	973	981	989	997	*005	*013	*020	*028	
550	74	036	044	052	060	068	076	084	002	099	107	
N	L	. 0	T	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
550	74 036	044	052	060	o 68	076	084	092	099	107	
551	115	123	131	139	147	155	162	170	178	186	
552 552	194 273	202	210	218 296	304	233	320	249	257	265	
553 554	351	359	367	374	382	312	398	327 406	335	343	
555	429	437	445	453	461	468	476	484	492	500	
556	507	515	523	531	539	547	554	562	570	578	
557	586	593	601	600	617	624	632	640	648	656	
558 559	663 741	749	679 757	687 764	772	702 780	710	718	803	733 811	
560	819	827	834	842	850	858	865	873	881	889	
561	896	904	QI 2	020	927	935	943	950	958	966	
562	974	981	989	997	*005	*012	*020	*028	*035	*043	8
563	75 051	059	o 66	074	082	089	097	105	113	120	1 0.8 2 1.6
564 565	128	136	143	151 228	159	166	174	182	189	197	3 2.4
566	282	213	220	305	236	243 320	328	259 335	343	274 351	4 3.2 5 4.0 6 4.8
567	358	366	374	381	389	397	404	412	420	427	6 4.8
568	435	442	450	458	465	473	481	488	496	504	7 5.6 8 6.4
569	511	519	526	534	542	549	557	565	572	580	9 7.2
570	587	595	603	610	618	626	633	641	648	656	
571 572	664 740	671 747	679 755	686 762	694 770	702 778	709 785	717	724 800	732 808	
573	815	823	831	838	846	853	861	868	876	884	
574	891	899	906	914	921	929	937	944	952	959	
575	967	974	982	989	997	*005	*012	*020	*027	*035	
576	76 042	050	057	065	072	080	087	095	103	110	
577 578	1 193	125	208	215	148	230	163 238	245	178 253	185	
579	268	275	283	290	298	305	313	320	328	335	
580	343	350	358	365	373	380	388	395	403	410	7
581	418	425	433	440	448	455	462	470	477	485	I 0.7
582 583	492 567	500	507 582	515 589	522 597	530	537	545 619	552 626	559 634	2 I.4 3 2.1
584	641	649	656	664	671	678	686	693	701	708	
585	716	723	730	738	745	753	760	768	775	782	4 2.8 5 3.5 6 4.2
586	790	797	805	812	819	827	834	842	849	856	7 4.9 8 5.6 9 6.3
587	864	871	879	886	893	901	908	916	923	930	9 6.3
588 589	938	945	953 026	960 034	967	975	982 056	989 063	997	*004 078	
590	085	093	100	107	115	122	120	137	144	151	
591	159	166	173	181	188	195	203	210	217	225	
592	232	240	247	254	262	269	276	283	291	298	
593	305	313	320	327	335	342	349	357	364	371	
594 595	379 452	386 459	393 466	401 474	408 481	415	422	430 503	437	444 517	
596	525	532	539	546	554	561	568	576	583	590	
597	597	605	612	619	627	634	641	648	656	663	
598	670	677	685	692	699	706	714	721	728	735	
599 600	743 77 815	750 822	757 830	764 837	772 844	779 851	786 859	793 866	801	808	
N	L 0	1	2	3	4	5	6	7	8	9	PP
14	LU			0	-	0	0	1	0	9	P P

N	LO	1	2	3	4	5	6	7	8	9	PP
600	77 815	822	830	837	844	851	859	866	873	880	
601	887	895	902	909	916	924	931	938	945	952	
602	960	967	974	981	988	996	*003	*010	*017	*025	
603-	78 032	039	046	053	061	068	075	082	o 89	097	
604	104	III	118	125	132	140	147	154	161	168	
605 606	176 247	183	190 262	197 260	204	211	219	226	233	240	
607		326		-	1 -	_	362	369	305	312	8
608	319 390	398	333	340 412	347	355	433	440	376	383	1 0.8 2 1.6
609	462	469	476	483	490	497	504	512	519	526	3 2.4
610	533	540	547	554	561	569	576	583	590	597	4 3.2
611	604	611	618	625	633	640	647	654	661	668	5 4.0 6 4.8
612	675	682	689	696	704	711	718	725	732	739	7 5.6
613	746	753	760	767	774	781	789	796	803	810	8 6.4
614	817	824	831	838	845	852	859	866	873	880	9 1 7.2
615 616	888 958	895	902	909	916	923	930	937	944	951 *021	
617	79 029	036	972	979 050	057	993	071	078	085		
618	000	106	113	120	127	134	141	148	155	162	
619	169	176	183	190	197	204	211	218	225	232	
620	239	246	253	260	267	274	281	288	295	302	_
621	300	316	323	330	337	344	351	358	365	372	7
622	379	386	393	400	407	414	421	428	435	442	I 0.7
623	449	456	463	470	477	484	491	498	505	511	2 I.4 3 2.1
624	518	525	532	539	546	553	560	567	574	281	4 2.8
625 626	588 657	595	602 671	6 0 9	616	623	630	706	713	720	5 3.5 6 4.2
627	727	734	741	748		761	768		782	780	7 4.9
628	796	803	810	817	754 824	831	837	775 844	851	858	8 5.6 9 6.3
629	865	872	879	886	893	900	906	913	920	927	9 0.3
630	934	941	948	955	962	969	975	982	989	996	
631	80 003	OIO	017	024	0,30	037	044	051	058	065	
632	072	079	085	092	099	106	113	120	127	134	
633	140	147	154	161	168	175	182	188	195	202	
634	209	216	223	229	236	243	250	257	264	271	
635 636	277 346	284 3 5 3	291 359	298 366	3 0 5 3 7 3	312	318	325 393	332	339	6
637	414	421	428	434	441	448	455	462	468	475	I 0.6 2 I.2
638	482	489	496	502	500	516	523	530	536	543	3 1.8
639	550	557	564	570	577	584	591	598	604	611	4 2.4
640	618	625	632	638	645	652	659	665	672	679	5 3.0 6 3.6
641	686	693	699	706	713	720	726	733	740	747	7 4.2
642	754	760	767	774	781	787	794	801	808	814	8 4.8
643	821	828	835	841	848	855	862	868	875	882	9 1 3.4
644 645	889	895	902	909	916	922	929	936	943 *010	949	
646	956 81 0 23	963	969 937	976	983 050	990	996 064	*003	077	*017	
647	000	007	104	111	117	124	131	137	144	151	
648	158	164	171	178	184	191	198	204	211	218	
649	224	231	238	245	251	258	265	271	278	285	
650	81 291	298	305	311	318	325	331	338	345	351	
N	L 0	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
650	81 291	298	305	311	318	325	331	338	345	351	
651	358	365	371	378	385	391	398	405	411	418	
652 653	425 491		438 505	445 511	451 518	458 525	465 531	471 538	478 544	485	
654	558		571	578	584	591	598	604	611	551	
655	624	631	637	644	651	657	664	671	677	684	
656	690		704	710	717	723	730	737	743	750	
657	757	763	770	776	783	790	796	803	809	816	
658	823	829	836	842	849	856	862	869	875	882	
659 660	889		902 968	908	915	921	928	935	941	948	
661	82 9 54			974	981	987	994 060	*000	*007	*014	7
662	086		033	040	046	053	125	132	138	079	
663	151		164	171	178	184	191	197	204	210	I 0.7 2 I.4
664	217	223	230	236	243	249	256	263	269	276	3 2.1
665	282		295	302	3 0 8	315	321	328	334	341	4 2.8 5 3.5
666	347	1	360	367	373	380	387	393	400	406	6 4.2
667 668	413	419	426	432	439	445	452	458	465	471	7 4.9 8 5.6
669	543		491 556	497 562	569	510	517 582	523 588	530 595	536	8 5.6 9 6.3
670	607		620	627	633	640	646	653	659	666	
671	672		685	602	698	705	711	718	724	730	
672	737	743	750	756	763	769	776	782	789	795	
673	802		814	821	827	834	840	847	853	860	
674	866		879	885	892	898	905	911	918	924	
675 676	930		943	950 *014	956 *020	963	969 *033	975	982 *046	988	
677	83 059		072	078	085	001	097	104	110	117	
678	123	120	136	142	149	155	161	168	174	181	
679	187	193	200	206	213	219	225	232	238	245	
680	251	257	264	270	276	283	289	296	302	308	6
681	315	321	327	334	340	347	353	359	366	372	1 0.6
682 683	378 442		391	398	404	410	417	423	429	436	2 I.2 3 I.8
684	500		455 518	525	531	537	544	550	556	499 563	
685	560		582	588	594	601	607	613	620	626	4 2.4 5 3.0 6 3.6
686	632		645	651	658	664	670	677	683	689	7 4.2
687	690		708	715	721	727	734	740	746	753	
688	759	765	771	778	784	790	797	803	809	816	9 5.4
689 690	82:	891	835	841	910	853 916	860	866	872	879	
691	94		960	901			923	929	935	942 *004	
692	84 01		023	020	973	979	c48	055	061	067	
693	07.		086	092	098	105	III	117	123	130	
694	130		148	155	161	167	173	180	186	192	
695	19		211	217	223	230	236	242	248	255	
696	26:		273	280	286	292	298	305	311	317	
697 698	32,		3 36	342	348	354	361 423	367	373 435	379 442	
699	44		460	466	473	479	485	491	497	504	
700			522	528	535	541	547	553	559	566	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	L	0	i	2	3	4	5	6	7	8	9	PP
700	84	510	516	522	528	535	541	547	553	559	566	
701		572	578	584	590	597	603	600	615	621	628	
702 703		634	702	708	652	658	665 726	733	677	683	689	
704	-		763	770	776	782	788	794	739 800	745 807	751 813	
704		757 819	825	831	837	844	850	856	862	868	874	
706		880	887	893	899	905	911	917	924	930	936	7
707		942	948	954	960	967	973	979	985	991	997	
708	85	003	0009	016	022	028	034	040	046	052	058	I 0.7 2 I.4
709 710		065	071	138			095	163	169	114	181	3 2.1
711		187	132	100	205	211	156	224	230	236	242	4 2.8 5 3.5 6 4.2
711		248	254	260	266	272	278	285	291	297	303	6 4.2
713		309	315	321	327	333	339	345	352	358	364	7 4.9 8 5.6
714		370	376	382	388	394	400	406	412	418	425	8 5.6 9 6.3
715		431	437	443	449	455	461	467	473	479	485	
716		491	497	503	509	516	522	528	534	540	546 606	
717 718		552 612	558 618	564 625	570 631	576 637	643	649	594 655	661	667	
719		673	679	685	691	697	703	700	715	721	727	
720		733	739	745	751	757	763	769	775	781	788	
721		794	800	806	812	818	824	830	836	842	848	6
722		854	860	866	872	878	884	890	896	902	908	I 0.6 2 1.2
723		914	920	926	932	938	944	950	956 *016	962 *022	968	3 1.8
724 725	86	974 034	980 040	986 046	992 052	998 058	*004	070	076	082	*028 088	4 2.4
726	00	094	100	106	112	118	124	130	136	141	147	5 3.0 6 3.6
727		153	159	165	171	177	183	189	195	201	207	7 4.2 8 4.8
728		213	219	225	231	237	243	249	255	261	267	9 5.4
729		273	279	285	291	297	303	308	314	320	326	
730		332	338	344	350	356	362	368	374	380	386	
731 732		392 451	398 457	404 463	410 469	415	42I 48I	427	433	439	445 504	
733		510	516	522	528	534	540	546	552	558	564	
734		570	576	581	587	593	599	605	611	617	623	
735		629	635	641	646	652	658	664	670	676	682	5
736		688	694	700	705	711	717	723	729	735	741	1 0.5
737 738		747 806	753 812	759 817	764 823	770 829	776 835	782 841	788 847	794 853	800 859	2 I.O 3 I.5
739		864	870	876	882	888	894	900	906	911	917	4 2.0
740		923	929	935	941	947	953	958	964	970	976	5 2.5 6 3.0
741		982	988	994	999	*005	*011	*017	*023	*029	*035	7 3.5
742	87	040	046	052	058	064	070	075	081	087	093	8 4.0
743		099	105	III	116	122	128	134	140	146	151	
744 745		157 216	163	169 227	175 233	181	245	192 251	198 256	204	210	
746		274	280	286	291	297	303	309	315	320	326	
747		332	338	344	349	355	361	367	373	379	384	
748		390	396	402	408	413	419	425	431	437	442	
749 750	Q=	506	454	<u>460</u> 518	466	471	477	483 541	489	495	558	
N N	<u>07</u> L	0	512	2	523 3	529 4	535	6	547 7	552 8	9	PP
1A	L	U		4	J	_	3	J	-	9	0	

N	LO		2	3	4	5	6	7	8	9	PP
750	87 506	512	518	523	529	535	541	547	552	558	
751	564	570	576	581	587	593	599	604	610	616	
752 753	622 679	628 685	633	639 697	703	651 708	656 714	720	668 726	674 731	
754	737	743	749	754	760	766	772	777	783	789	
755	795	800	806	812	818	823	829	835	841	846	
756	852	858	864	869	875	88 1	887	892	898	904	
757	910 967	915	921 978	927 984	933	938	944	950 *007	955	961	
758 759	88 024	973	036	904 0 41	990	996 05 3	*001	064	*013 070	*018 076	
760	081	087	093	098	104	110	116	121	127	133	
761	138	144	150	156	161	167	173	178	184	190	6
762	195	201	207	213	218	224	230	235	241	247	1 0.6
763	252	258	264	270	275	281	287	292	298	304	2 1.2 3 1.8
764 765	309 366	315 372	321	326 383	332 389	338	343	349 406	355 412	360 417	3 1.8 4 2.4
766	423	429	377 434	440	446	395 451	457	463	468	474	5 3.0
767	480	485	491	497	502	508	513	519	525	530	7 4.2
768	536	542	547	553	559	564	570	576	581	587	8 4.8 9 5.4
769	593	598	604	610	615	621	627	632	638	643	9 3.4
770	649	655	660	666	672	677	683	689	694	700	
77I 772	705 762	711 767	717 773	722 779	728 784	734 790	739 795	745 801	807	756 812	
773	818	824	829	835	840	846	852	857	863	868	
774	874	880	885	891	897	902	908	913	919	925	
775	93 0 98 6	936	941	947	953	958	964	969	975	981	
776		992	997	*003	*009	*014	*020	*025 081	*031	*037	
777	89 042	048	053	059	064	126	076	137	087	092 148	
779	154	159	165	170	176	182	187	193	198	204	
780	209	215	221	226	232	237	243	248	254	260	5
781	265	271	276	282	287	293	298	304	310	315	1 0.5
782 783	321 376	326 382	332 387	337	343 398	348 4 0 4	354 4 0 9	360 415	365 421	371 426	2 1.0
784	432	437	443	393 448	454	459	465	470	476	481	4 2.0
785	487	492	498	504	500	515	520	526	531	537	5 2.5 6 3.0
786	542	548	553	559	564	570	575	581	586	592	7 3.5
787	597	603	609	614	620	625	631	636	642	647	8 4.0 9 4.5
788 789	653 708	658 713	664 719	669 724	675 730	68o 735	686 741	691 7 46	697 752	702 757	7 1 4.5
790	763	768	774	779	785	790	796	801	807	812	
791	818	823	829	834	840	845	851	856	862	867	
792	873	878	883	889	894	900	905	911	916	922	
793	927	933	938	944	949	955	960	966	971	977	
794	982	988	993	998	*004	*009	*015	*020	*026	*031 086	
795 796	90 037 091	042 097	048	053 108	059	119	124	075	135	140	
797	146	151	157	162	168	173	179	184	189	195	
798	200	206	211	217	222	227	233	238	244	249	
799	255	260	266	271	276	282	287	293	298	304	
800	90 309	314	320	325	331	336	342	347	352	358	
N	LO	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
800	90 300	314	320	325	331	336	342	347	352	358	
801	363		374	380	385	390	396	401	407	412	
802 803	417		428	434 488	439 493	445	450 504	455 509	461 515	466 520	
804	520	_	536	542	547	553	558	563	560	574	
805	580	585	590	596	601	607	612	617	623	628	
806	632		644	650	655	660	666	671	677	682	
807 808	687 741		698 752	703	709 763	714	720	725 779	730	736	
809	795		806	811	816	822	827	832	838	843	
810	849	854	859	865	870	875	881	886	891	897	
811	902		913	918	924	929	934	940	945	950	6
812 813	950		966	972	977	982 036	988	993 0 46	998	*004 057	I 0.6 2 1.2
814	062		073	078	084	080	004	100	105	110	3 1.8
815	116	121	126	132	137	142	148	153	158	164	4 2.4 5 3.0
816	169	1	180	185	190	196	201	206	212	217	6 3.6
817 818	222 275		233	238	243 297	249 302	254 3 0 7	259 312	265 318	323	7 4.2 8 4.8
819	328		339	344	350	355	360	365	371	376	9 5.4
820	381		392	397	403	408	413	418	424	429	
821	434		445	450	455	461	466	471	477	482	
822 823	487 549		498	503 556	508 561	514 566	519 572	524 577	529 582	535 587	
824	593		603	600	614	619	624	630	635	640	
825	645		656	661	666	672	677	682	687	693	
826	698	1	700	714	719	724	730	735	740	745	
827 828	751 803		761 814	766 819	772 824	777 829	782 834	787 840	793 845	798 850	
829	855		866	871	876	882	887	892	897	903	
830	908		918	924	929	934	939	944	950	955	
831	960		971	976	981	986	991	997	*002	*007	5
8 ₃₂ 8 ₃₃	92 OI 2 O65		023	028	033	038	044	049	106	059	I 0.5 2 I.0
834	117	1 '	127	132	137	143	148	153	158	163	3 I.5 4 2.0
835	169		179	184	189	195	200	205	210	215	5 2.5
836	221		231	236	241	247	252	257	262	267	6 3.0 7 3.5 8 4.0
837 838	273 324		283 335	288 340	293 345	298 350	3 0 4	3 0 9 361	314	319 371	
839	376		387	392	397	402	407	412	418	423	9 4.5
840	428		438	443	449	454	459	464	469	474	
841	480		490	495	500	505	511	516	521	526	
842 843	531 583		542	547 598	552 603	557 609	562 614	567	572 624	578 629	
844	634		645	650	655	660	665	670	675	681	
845	686	691	696	701	706	711	716	722	727	732	
846	737		747	752	758	763	768	773	778	783	
847 848	788 840		799 850	804 855	809 860	814 865	819	824 875	829	834 886	
849	891		901	906	911	916	921	927	932	937	
850	92 942	947	952	957	962	967	973	978	983	988	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
850	92 942	947	952	957	962	967	973	978	983	988	
851	993	998	*003	*008	*013	*018	*024	*029	*034	*039	
852	93 044	100	054	059	064	069	075	080	085	090	
8 ₅₃ 8 ₅₄	095	151	105	161	115	171	125	131	136 186	141	
855	197	202	207	212	217	222	227	232	237	242	
856	247	252	258	263	268	273	278	283	288	293	6
857	298	303	3 0 8	313	318	323	328	334	339	344	1 0.6
858 859	349	354	359 4 0 9	364 414	369 420	374 425	379 430	384 435	389	394	2 I.2
860	399 450	455	460	465	470	475	480	485	440	445	3 1.8 4 2.4
861	500	505	510	515	520	526	531	536	541	546	5 3.0
862	551	556	561	566	571	576	581	586	591	596	
863	601	606	611	616	621	626	631	636	641	646	8 4.8
864	651	656	661	666	671	676	682	687	692	697	9 5.4
865 866	702 752	707	712 762	717 767	722 772	727 777	732 782	737 787	742 792	747 797	
867	802	807	812	817	822	827	832	837	842	847	
868	852	857	862	867	872	877	882	887	892	897	
869	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	5
871 872	94 002 052	007	012 062	017	022 072	027	032	037	042	047 096	1 0.5
873	101	106	111	116	121	126	131	136	141	146	2 1.0
874	151	156	161	166	171	176	181	186	191	196	3 I.5 4 2.0
875	201	206	211	216	221	226	231	236	240	245	5 2.5
876	250	255	260	265	270	275	280	285	290	295	6 3.0 7 3.5 8 4.0
877 878	300	305	359	315 364	320 369	325 374	330	335	340	345 394	
879	399	404	409	414	419	424	429	433	438	443	9 4.5
880	448	453	458	463	468	473	478	483	488	493	
881	498	503	507	512	517	522	527	532	537	542	
88 ₂ 88 ₃	547	552 601	557 606	562 611	567	571 621	576	581	586	591	
884	596 645	650	655	660	665	670	675	680	635	680	
885	694	699	704	709	714	719	724	729	734	738	4
886	743	748	753	758	763	768	773	778	783	787	I 0.4 2 0.8
887	792	797	802	807	812	817	822	827	832	836	
888 889	841 890	846	900	856	861	866	871	924	880	885 934	4 1.6
890	1	944	949	954	959	963	968	973	978	983	5 2.0 6 2.4
891	988	993	998	*002	*007	*012	*017	*022	*027	*032	7 2.8
892	95 036	041	046	051	056	061	066	071	075	080	8 3.2 9 3.6
893	085	090	095	100	105	100	114	119	124	129	, , , ,
894	134 182	139	143	148	153	158	163	168	173	177	
895 896	231	187	192	197	250	207	260	265	270	274	
897	279	284	289	294	299	303	308	313	318	323	
898	328	332	337	342	347	352	357	361	366	371	
899	376		386	390	395	400	405	410	415	410	1
900			434	439	444	448	453	458	463	468	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
900	95 42	4 429	434	439	444	448	453	458	463	468	
901	47		482	487	492	497	501	506	511	516	
902	52 56		530	535 583	540	545	550	554	559	564	
903	61		626	631	636	641	646	650	655	660	
905	66		674	679	684	689	694	698	703	708	
906	71	- 1 -	722	727	732	737	742	746	751	756	
907	76		770	775	780	785	789	794	799	804	
908	80 85		866	823	828	832 880	837	842	847	852	
910	90.		914	918	923	928	933	938	942	947	•
911	95	957	961	966	971	976	980	985	990	995	5
912	99		*000	*014	*019	*023	*028	*033	*038	*042	1 0.5
913	96 04		104	061	066	071	076	080	085	090	2 I.O 3 I.5
914 915	09. 14:		152	109	114	118	123	128	133	137	4 2.0
916	190		199	204	209	213	218	223	227	232	5 2.5 6 3.0
917	23'		246	251	256	261	265	270	275	280	7 3.5
918	28.	. 1 -	294	298	303	308	313	317	322	327	8 4.0 9 4.5
919 920	33 379		341	346	350	355 402	360	365	369	374	
921	420		435	393 440	398 445	450	454	459	464	421	
922	47.		483	487	445	497	501	506	511	515	
923	520		530	534	539	544	548	553	558	562	
924	56		577	581	586	591	595	600	605	600	
925 926	66:		624	628	633 680	638	689	647	652	703	
927	708	1	717	722	727	731	736	741	745	750	
928	75	759	764	769	774	778	783	788	792	797	
929	80		811	816	820	825	830	834	839	844	
930	848		858	862	867	872	876	881	886	890	4
931 932	895 943		904	909	914	918	923	928	932	937	1 0.4
933	988	993	997	*002	*007	*011	*016	*021	*025	*030	2 0.8 3 1.2
934	97 035	039	044	049	053	058	063	067	072	077	
935	081		090	095	100	104	109	114	118	123	5 2.0 6 2.4
936	128	1 -	137	142	146	151	155	160 206	165	169	7 2.8
937 938	172		183	234	239	197 243	202	253	211	262	8 3.2 9 3.6
939	26		276	280	285	290	294	299	304	308	
940	313		322	327	331	336	340	345	350	354	
941	359		368	373	377	382	387	391	396	400	
942 943	405 451		414	419 46 5	424 470	428 474	433	437 483	442 488	447 493	
944	497		506	511	516	520	525	520	534	539	
945	543	548	552	557	562	566	571	575	580	585	
946	589		598	603	607	612	617	621	626	630	
947	635 681		644	649	653	658	663	667	672	676	
948	727		736	695 740	699 745	704 749	708	713 759	717	722	
950	97 77		782	786	791	795	800	804	809	813	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	L O	1	2	3	4	5	6	7	8	9	PP
950	97 772	777	782	786	791	795	800	804	800	813	
951	818	823	827	832	836	841	845	850	855	859	
952	864	868	873	877	882	886	891	896	900	905	
953	909	914	918	923	928	932	937	941	946	950	
954 955	955	959	964 00 9	968 014	973 010	978 023	982 028	987 032	991 037	996 041	
956	046	050	055	059	064	068	073	078	082	087	
957	091	006	100	105	100	114	118	123	127	132	
958	137	141	146	150	155	159	164	168	173	177	
959	182	186	191	195	200	204	209	214	218	223	
960	227	232	236	241	245	250	254	259	263	268	5
961	272	277	281	286	290	295	299	304	308	313	
962 963	318 363	322	327 372	331	336 381	340 385	345 390	349 394	354 399	358 4 0 3	I 0.5 2 I.0
964	408	412	417	421	426	430	435	439	444	448	3 1.5
965	453	457	462	466	471	475	480	484	489	493	4 2.0 5 2.5
966	498	502	507	511	516	520	525	529	534	538	6 3.0
967	543	547	552	556	561	565	570	574	579	583	7 3.5 8 4.0
968	588	592	597	646	605	610	614	664	668	628	8 4.0
969 970	$\frac{632}{677}$	682	686	691	650	700	659 704	709		717	
	722	726							713	762	
97 I 972	767	771	731	735 780	740 784	744 789	749 793	753 798	758 802	807	
973	811	816	820	825	829	834	838	843	847	851	
974	856	860	865	869	874	878	883	887	892	896	
975	900	905	909	914	918	923	927	932	936	941	
976	945	949	954	958	963	967	972	976	981	985	
977 978	989	994 038	998	*003	*007 052	*012 056	*016	*021 C65	*025 060	*029 074	
979	078	083	043	047	096	100	105	100	114	118	
980	123	127	131	136	140	145	149	154	158	162	4
981	167	171	176	180	185	189	193	198	202	207	
982	211	216	220	224	229	233	238	242	247	251	1 0.4 2 0.8
983	255	260	264	269	273	277	282	286	291	295	3 1.2
984	300	304	308	313	317	322	326	330	335	339	4 1.6
985 986	344 388	348	35 ² 396	357 401	361 4 05	366 410	370 414	374	379 423	383	6 2.4
987	432	436	441	445	449	454	458	463	467	471	7 2.8 8 3.2
988	476	480	484	489	493	498	502	506	511	515	9 3.6
989	520	524	528	533	537	542	546	550	555	559	
990	564	568	572	577	581	585	590	594	599	603	
991	607	612	616	621	625	629	634	638	642	647	
992	651	656	704	708	669	673	721	726	686 730	691	
993 994	739	743	747	752	756	760	765	760	774	734	
995	782	787	791	795	800	804	808	813	817	822	
996	826	830	835	839	843	848	852	856	861	865	
997	870	874	878	883	887	891	896	900	904	909	- 1
998	913	917	922	926	930	935	939	944	948	952	
999	00 000	961	965	970	974	978	983	987	991	996	
1000 N	L 0	004	2	3	017	5	6	7	8	9	
N	LU		1 2	ರ	4	5	0		8	9	PP

N	L	0	1	2	3	4	5	6	7	8	9
1000	000	0000	0434	0869	1303	1737	2171	2605	3039	3473	3907
1001		4341	4775	5208	5642	6076	6510	6943	7377	7810	8244
1002		8677-	9111	9544	9977	*0411	*0844	*1277	*1710	*2143	*2576
1003	001	3009	3442	3875	4308	4741	5174	5607	6039	6472	6905
1004		7337	7770	8202	8635	9067	9499	9932	*0364	*0796	*1228
1005	002	1661	2003	2525	2957	3389	3821	4253	4685	5116	5548
1006		5980	6411	6843	7275	7706	8138	8569	9001	9432	9863
1007	003	0295	0726	1157	1588 5898	2019 6328	2451	2882	3313 7620	3744 8051	4174 8481
1008		4605 8012	5036	54 ⁶ 7 977 ²	*0203	* o 633	6759 *1 0 63	7190 *1493	*1924	*2354	*2784
1010			9342						6223	6652	7082
	004	3214	3644	4074	4504	4933	5363	5793			
IOII		7512	7941	8371	8800	9229	9659	*0088	*0517	*0947	*1376
1012	005	1805	2234	2663	3092 7380	7800	39 50 8238	43 7 9 8666	4808	5237 9523	5666 9951
1013		6094	6523 0808	6952	1664	2002				3805	4233
1014	000	0380 4660	5088	1236 5516	5944	6372	2521 6799	2949 7227	3377 7655	8082	8510
1015		8937	9365	9792	*0219	*0647	*1074	*1501	*1928	*2355	*2782
1017	007	3210	3637	4064	4490	4017	5344	5771	6108	6624	7051
1017	007	7478	7904	8331	8757	9184	0610	*0037	*0463	*0880	*1316
1010	008	1742	2168	2594	3020	3446	3872	4298	4724	5150	5576
1020		6002	6427	6853	7279	7704	8130	8556	8981	9407	9832
1021	000	0257	0683	1108	1533	1959	2384	2800	3234	3659	4084
1022		4500	4934	5359	5784	6208	6633	7058	7483	7907	8332
1023		8756	9181	9605	*0030	*0454	*0878	*1303	*1727	*2151	*2575
1024	010	3000	3424	3848	4272	4696	5120	5544	5967	6391	6815
1025		7239	7662	8086	8510	8933	9357	9780	*0204	*0627	*1050
1026	OII	1474	1897	2320	2743	3166	3590	4013	4436	4859	5282
1027		5704	6127	6550	6973	7396	7818	8241	8664	9086	9509
1028		9931	*0354	*0776	*1198	*1621	*2043	*2465	*2887	*3310	*3732
1029	012	4154	4576	4998	5420	5842	6264	6685	7107	7529	7951
1030		8372	8794	9215	9637	*0059	*0480	*0901	*1323	*1744	*2165
1031	013	2587	3008	3429	3850	4271	4692	5113	5534	5955	6376
1032	1	6797	7218	7639	8059	8480	8901	9321	9742	*0162	*0583 4785
1033	014	1003	1424	1844	2264	2685	3105	3525	3945	4365 8564	8084
1034		5205	5625	6045 *0243	6465 * o 662	6885 *1082	7305	7725 *1920	*2340	*2759	*3178
1035	OTE	9403 3598	9823	4436	4855	5274	5693	6112	6531	6050	7369
1030	513	7788	8206	8625	0044	0462	0881	*0300	*0718	*1137	*1555
1037	016	1974	2392	2810	3229	3647	4065	4483	4901	5319	5737
1039	010	6155	6573	6001	7409	7827	8245	8663	9080	9498	9916
1040	017	0333	0751	1168	1586	2003	2421	2838	3256	3673	4090
1041		4507	4924	5342	5759	6176	6593	7010	7427	7844	8260
1042	1	8677	9094	9511	9927	*0344	*0761	*1177	*1594	*2010	*2427
1043	018	2843	3259	3676	4092	4508	4925	5341	5757	6173	6589
1044		7005	7421	7837	8253	8669	9084	9500	9916	*0332	*0747
1045	019	1163	1578	1994	2410	2825	3240	3656	4071	4486	4902
1046		5317	5732	6147	6562	6977	7392	7807	8222	8637	9052
1047		9467	9882	*0296	*0711	*1126	*1540	*1955	*2369 6513	*2784 6927	*3198 7341
1048	020	3613	4027	4442	4856	5270	5684 9824	* 0 238	*0652	*1066	*1479
1049	021	7755	2307	8583	8997 3134	3547	3961	4374	4787	5201	5614
	L	0	-	2	3	4	5	6	7	8	9
N		0	1	2	3	4	- 3		1		

N	L	0	1	2	3	4	5	6	7	8	9
1050	021	1893	2307	2720	3134	3547	3961	4374	4787	5201	5614
1051		6027	6440	6854	7267	7680	8093	8506	8919	9332	9745
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1053		4284	4696	5100	5521	5933	6345	6758 *0878	7170 *1280	7582	7994
1054	022	8406 2525	8818	9230 3348	9642 3759	*0054 4171	*0466 4582	4994	5405	*1701 5817	*2113 6228
1056	023	6639	7050	7462	7873	8284	8695	0106	9517	9928	*0339
1057	024	0750	1161	1572	1982	2393	2804	3214	3625	4036	4446
1058	,	4857	5267	5678	6088	6498	6909	7319	7729	8139	8549
1059		8960	9370	9780	*0190	*0600	*1010	*1419	*1829	*2239	*2649
1060	025	3059	3468	3878	4288	4697	5107	5516	5926	6335	6744
1061	,	7154	7563	7972	8382	8791	9200	9609	*0018	*0427	*0836
1062	020	1245	1654	2063	2472	2881 6967	3289	3698	4107	4515 8600	4924
1063		5333 9416	574I 9824	6150 *0233	6558 *0641	*1049	7375 *1457	7783 *1865	*2273	*2680	9008 *3088
1004	027	3496	3904	4312	4719	5127	5535	5942	6350	6757	7165
1066	,	7572	7979	8387	8794	9201	9609	*0016	*0423	*0830	*1237
1067	028	1644	2051	2458	2865	3272	3679	4086	4492	4899	5306
1068		5713	6119	6526	6932	7339	7745	8152	8558	8964	9371
1069		9777	*0183	*0590	* o 996	*1402	*1808	*2214	*2620	*3026	*3432
1070	029	3838	4244	4649	5055	5461	5867	6272	6678	7084	7489
1071	000	7895	8300	8706	9111	9516	9922	*0327	*0732	*1138	*1543
1072	030	1948 5997	2353	6807	3163 7211	3568 7616	3973 8020	4378 8425	4783 8830	5188 9234	5592 9638
1073	031	0043	0447	0851	1256	1660	2064	2468	2872	3277	3681
1075	-5-	4085	4489	4893	5296	5700	6104	6508	6912	7315	7719
1076		8123	8526	8930	9333	9737	*0140	*0544	*0947	*1350	*1754
1077	032	2157	2560	2963	3367	3770	4173	4576	4979	5382	5785
1078	022	6188	0590	1010	7396	7799 1824	8201	8604 2629	9007	9409	9812
1080	033	4238	4640	5042	1422 5444	5846	6248	6650	303 I 705 2	3433 7453	3835 7855
1081		8257	8650	9060	0462	9864	*0265	*0667	*1068	*1470	*1871
1082	034	2273	2674	3075	3477	3878	4279	4680	5081	5482	5884
1083		6285	6686	7087	7487	7888	8289	8690	9091	9491	9892
1084	035	0293	0693	1094	1495	1895	2296	2696	3096	3497	3897
1085		4297	4698	5098	5498	5898	6298	6698	7098	7498	7898
1086	016	8298	8698 2695	90 98	9498 3494	9898	*0297 4293	*0697 4692	*1097	*1496	*1896
1087	030	6280	6688	7087	7486	7885	8284	8683	5091 9082	5491 9481	9880
1089	037	0279	0678	1076	1475	1874	2272	2671	3070	3468	3867
1090		4265	4663	5062	5460	5858	6257	6655	7053	7451	7849
1091		8248	8646	9044	9442	9839	*0237	*0635	*1033	*1431	*1829
1092	038	2226	2624	3022	3419	3817	4214	4612	5009	5407	5804
1093		6202	6599	6996	7393	7791	8188	8585	8982	9379	9776
1094	039	0173 4141	0570	0967	1364	1761 5727	2158 6124	2554 6520	2951 6017	3348	3745 7709
1095		8106	4538 8502	4934 8898	5331 9294	9690	*0086	*0482	*0878	7313 *1274	*1670
1097	040	2066	2462	2858	3254	3650	4045	4441	4837	5232	5628
1098		6023	6419	6814	7210	7605	8001	8396	8791	9187	9582
1099		9977	*0372	*0767	*1162	*1557	*1952	*2347	*2742	*3137	*3532
1100	041	3927	4322	4716	5111	5506	5900	6295	6690	7084	7479
N	L	0	1	2	3	4	5	6	7	8	9

TABLE XXV. — LOGARITHMS OF SINES, TANGENTS, COSINES, AND COTANGENTS FOR EACH 0.01° OF THE QUADRANT

In this table whenever the trigonometric function is fractional, as it always is for sines and cosines, except when it is I, the logarithms have been increased by IO to avoid the negative characteristic. But where the function is greater than I, as are cotangents and tangents for certain parts of the circle, the logarithm is given without the IO. Thus in the column headed cot at the top of the page the logarithms are unaugmented; in all other columns they are augmented. This must be remembered in working with them.

To find the square root of the sine of 26.32° we find on page 151, line 33, the log sin to be 9.64678, which must be divided by 2 to give the logarithm of the square root; the operation is performed thus:

$$\frac{2)9.64678 - 10}{4.82339 - 5} = \overline{1}.82339.$$

Whence $\sqrt{\sin 26.32^{\circ}}$ = the number whose log is $\overline{1.82339}$ or 0.66587+. But to find the square root of the cotangent of 26.32° , page 151, line 33, we have $0.30569 \div 2 = 0.152845$, which corresponds to the number 1.4218+.

The numbering of the pages. — On each page there will be found four-degree numbers which are to be used as follows: the upper left-hand figure is used with the headings at the tops of the columns and the fractions running down the left side of the page. The lower right-hand figure is used with the headings at the bottoms of the columns, and fractions running up the right-hand side of the page. The upper right-hand figure is used with headings at the tops of the columns and fractions running up the right-hand side of the page. The lower left-hand figure is used with headings at the bottom of the page and fractions running down the left-hand side of the page. Generally stated the figures are used with the headings and fractions nearest them.

Example. — See pages 163-164. The log sin of 32.4° is found in the 2nd column, page 163, 41st line, to be 9.72902, while the log sin of 122.4° is found in the 7th column of the same page and line to be 9.92651. The log sin of 147.4° is found in the 2nd column on page 164, 41st line from the bottom, to be 9.73140, while the log sin 57.4° is found in the 7th column of the same page and line to be 9.92555.

When the function or angle sought is not in the table, as when the log sin of 14.436° or the angle whose sine is 9.34220 is wanted, we must interpolate between the tabular quantities. Thus:

- (a) Log sin 14.43° is found on page 127, line 44, to be 9.39654 with a tabular difference of 30 for a change of 0.01 given in the column headed d. Then the addition for 6 tenths of 0.01° is found by multiplying 30 × 0.6 = 18, and adding to 9.39654 giving 9.39672 as the required sine. When the quantities are less simple the proportional part given in the right-hand column of the page may be used. If the angle is 14.4362° the table of proportional parts is convenient even for the simple difference of 30. Thus, from the values in the right-hand column headed "30" we find 18 opposite 6; moving the decimal point one place to the left, we find 0.6 opposite 2; adding we get .000186, or .00019, to be added to the log sin 14.43° to give log sin 14.4362°. The figures are uncertain beyond five places and may be a fraction of one in error in the fifth place.
- (b) For the angle whose log sine is 9.34220 we find on page 124 the next smaller log sin = 9.34212 = log sin 12.70°; the difference is 9.34220 9.34212 = 8 in the last place. The tabular difference is 34. Looking in the column of proportional parts under 34 we find 6.8 next smaller number than 8 corresponding to 0.002 and leaving 1.2 unused; moving the decimal point one place to the left in the tabular quantities, the next smaller and nearest number is 1.02 opposite 3. Therefore the angle is 12.7023°. The last figure is uncertain.

For fractional angles near 0° and 90°, the differences are changing so rapidly that linear interpolation is not sufficiently exact. The right-hand columns of pages 99 to 104 show what to do. Thus to find the log sin 0.1246° we find (pages 76 and 99)

Log. 0.1246 =
$$\overline{1}.09552$$

 $S = \underbrace{1.75812}_{7.33740}$

To find log cos and log cot we find log sin and tangents of complementary angles. Thus, to get log cos 89.367°, we get log sin 0.633°. Conversely, to find the angle whose log sin is 7.33740, we refer to page 99, and find that the angle is between 0.12° and 0.13° and hence

$$S = 1.75812$$

$$\log \sin = 7.33740 - 10$$
(page 76) log 0.1246° = 9.09552 - 10 = $\overline{1}$.09552.

TABLE XXVI. — LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS FOR EACH 0.02° OF THE QUADRANT

The use of this table will be evident except the interpolation for small angles and for external secants for angles near 90°.

For small angles use the quantity V for versed sines and E for external secants as follows:

Log vers
$$\alpha = 2 \log \alpha^{\circ} + V$$
.
Log exsec $\alpha = 2 \log \alpha^{\circ} + E$.

Interpolate for V and E when necessary. Example. — Required log vers 1.354°.

Log 1.354 = 0.13162

$$V \text{ for } 1.36^{\circ} = \frac{2}{0.26324}$$

 $V \text{ for } 1.36^{\circ} = \frac{6.18270}{6.44594}$.
Log $v \text{ ers } 1.354^{\circ} = \frac{6.44594}{6.44594}$.

For external secants near 90° the interpolation is as follows: Log exsec A = log vers A - log sin (90 - A).

0,							179°	
	Sin	d.	Tan	d. c.	Cot	Cos		
00							100	S
or	6.24188		6.24188		3.75812	0.00000	99	
02	6.54291	30103	6.54291	30103	3.45709	0.00000	98	° 1.758
03	6.71900	17609	6.71900	17609	3.28100	0,00000	97	.0 123
04	6.84394	12494	6.84394	12494	3.15606	0.00000	96	.1 123
05	6.94085	9691	6.94085	9691	3.05915	0.00000	95	.2 124
06	7.02003	7918	7.02003	7918	2.97997	0.00000	94	.3 125
07	7.08698	6695	7.08698	6695	2.91302	0.00000	93	.4 126
08	7.14497	5799	7.14497	5799	2.85503	0,00000	92	.5 128
09	7.19612	5115	7.19612	5115	2.80388	0.00000	91	
10	7.24188	4576	7.24188	4576	2.75812	0.00000	90	
11	7.28327	4139	7.28327	4139	2.71673	0.00000	89	
12	7.32106	3779	7.32106	3779	2.67894	0.00000	88	
13	7.35582	3476	7.35582	3476	2.64418	0,00000	87	
14	7.38800	3218	7.38801	3219	2.61199	0.00000	86	
15	7.41797	2997	7.41797	2996	2.58203	0.00000	85	ئب
16	7.44600	2803	7.44600	2803	2.55400	0.00000	84	T;
	7.47233	2633	7.47233	2633	2.52767	0,00000	83	re small: β ; log tan $\alpha = \log \alpha^{\circ} - T$; $\beta = \log \tan \alpha + T$. sin and tan of complement.
17	7.47233	2482	7.47233	2482	2.50285	0.00000	82	are small: S; log tan $\alpha = \log \alpha^{\circ} -$ $+S = \log \tan \alpha + T$. e sin and tan of compler
19	7.52063	2348	7.52063	2348	2.47937	0.00000	81	gg t
20		2228	7.54291	2228		0.00000	80	α - α f c
	7.54291	2119	7.56410	2119	2.45709			n c
21	7.56410	2020		2020	2.43590	0.00000	79	l: n o g t; ta
22	7.58430	1930	7.58430	1931	2.41570	0.00000	78	ta ta 10, nd
23	7.60360	1849	7.60361	1848	2.39639	0.00000	77	Smr logo
24	7.62209	1773	7.62209	1773	2.37791	0.00000	76	re S; 1 F S sir
25	7.63982	1703	7.63982	1703	2.36018	0.00000	75	les a - S - S - use
26	7.65685	1639	7.65685	1639	2.34315		74	To interpolate when angles are small: $\log \sin \alpha = \log \alpha^{\circ} - S$; $\log \tan \alpha = \log \sin \alpha + S = \log \cos \alpha \cos \alpha$ For $\cos and \cot \cos \alpha$ we sin and t
27	7.67324	1579	7.67324	1580	2.32676	0.00000	73	g s s s s s s s s s s s s s s s s s s s
28	7.68903	1524	7.68904	1524	2.31096	9.99999	72	ar logar
29	7.70427	1473	7.70428	1472	2.29572	9.99999	71	To interpolate when ang $ \alpha = \log \alpha^{\prime}$ for $ \alpha = \log \alpha^{\prime}$ For $ \alpha = \log \alpha$
30	7.71900	1424	7.71900	1424	2.28100	9.99999	70	olate whe sin α = log α° = log α° = nd cot n
31	7.73324	1379	7.73324	1379	2.26676	9.99999	69	lat si si log d c
32	7.74703	1336	7.74703	1337	2.25297	9.99999	68	an an
3 3	7.76039	1296	7.76040	1296	2.23960	9.99999	67	os
34	7.77335	1259	7.77336	1259	2.22664	9.99999	66	in
35	7.78594	1239	7.78595	1239	2.21405	9.99999	65	To F
36	7.79818	1190	7.79819	1190	2.20181	9.99999	64	
37	7.81008	1158	7.81009	1158	2.18991	9.99999	63	
38	7.82166	1128	7.82167	1128	2.17833	9.99999	62	
39	7.83294	1099	7.83295	1099	2.16705	9.99999	61	
40	7.84393	1073	7.84394	1073	2.15606	9.99999	60	
41	7.85466	1	7.85467		2.14533	9.99999	59	
42	7.86512	1046	7.86513	1046	2.13487	9.99999	58	T
43	7.87534	1022	7.87535	1022 999	2.12465	9.99999	57	
44	7.88533	999	7.88534		2.11466	9.99999	56	° 1.758
45	7.89509	976	7.89510	976	2.10490	9.99999	55	.0 123
46	7.90463	954	7.90464	954	2.09536	9.99999	54	.I I22
47	7.91397	934	7.91398	934	2.08602	9.99999	53	.2 121
48	7.92311	914	7.92313	915	2.07687	9.99998	52	.3 119
49	7.93207	896	7.93208	895 878	2.06792	9.99998	51	:4 116
50	7.94084	877	7.94086	070	2.05914	9.99998	50	.5 112
	Cos	d.	Cot	d. c.	Tan	Sin		
90°							89°	
90							09	

	1 0:	-		1	0.			
_	Sin	d.	Tan	d.c.	Cot	Cos		
50	7.94084	860	7.94086	860	2.05914	9.99998	50	S
51	7.94944	843	7.94946	843	2.05054	9.99998	49 48	
52	7.95787	828	7.95789	828	2.04211	9.99998		1.758
53	7.96615	811	7.96617	811	2.03383	9.99998	47	.5 128
54	7.97426	797	7.97428	797	2.02572	9.99998	46	.6 131
55	7.98223	783	7.98225	783	2.01775	9.99998	45	.7 133
56	7.99006	769	7.99008	769	2.00992	9.99998	44	.8 137
57	7.99775	755	7.99777	755	2.00223	9.99998	43	.9 140 1.0 145
58	8.00530	742	8.00532	742	1.99468	9.99998	42	210 243
59	8.01272	730	8.01274	730	1.98726	9.99998	41	
60	8.02002	718	8,02004	718	1.97996	9.99998	40	
61	8.02720	706	8.02722	707	1.97278	9.99998	39	
62	8.03426	695	8.03429	695	1.96571	9.99997	38	
63	8.04121	684	8.04124	684	1.95876	9.99997	37	
64	8.04805	673	8.04808	673	1.95192	9.99997	36	ıt.
65	8.05478	663	8.05481	663	1.94519	9.99997	35	; ner
66	8.06141	653	8.06144	653	1.93856	9.99997	34	thes are small: $-S_i \text{ log tan } \alpha = \log \alpha^o - T_i,$ $-S_i \text{ log tan } \alpha + T = -1 \text{ og tan } \alpha + T.$ use sin and tan of complement.
67	8.06794	644	8.06797	644	1.93203	9.99997	33	- Idu
68	8.07438 8.08072	634	8.07441	634	1.92559	9.99997	32	is are small: S; log $\tan \alpha = \log \alpha^{\circ}$ S and $\tan \alpha + T$. Is sin and $\tan \alpha + T$.
69		624	8.08075	625	1.91925	9.99997	31	sare small: S; log tan $\alpha = \log 2$ Log tan $\alpha + \log 2$ Log tan $\alpha + \log 2$ Log tan of c
70	8.08696	616	8.08700	616	1.91300	9.99997	30	an c
71	8.09312	608	8.09316	607	1.90684	9.99997	29	11: 1 α 1 ta
72	8.09920	599	8.09923	599	1.90077	9.99997	28	ma tar log an
73	8.10519	591	8.10522	591	1.89478	9.99996	27	in II s
74	8.11110	583	8.11113	583	1.88887	9.99996	26	ar
75	8.11693	575	8.11696	576	1.88304	9.99996	25	les S + t
76	8.12268	568	8.12272	567	1.87728	9.99996	24	when angle = $\log \alpha^{\circ} - 1$ = $\log \sin \alpha$ = 1 = $\log \sin \alpha$ of near 90° u
77	8.12836	560	8.12839	561	1.87161	9.99996	23	n a g or g si gr g
78	8.13396	553	8.13400	553	1.86600 1.86047	9.99996	22 21	log log
79	8.13949	546	8.13953	547		9.99996		t
80	8.14495	540	8.14500	539	1.85500	9.99996	20	To interpolate when angles are small: $\log \sin \alpha = \log \alpha^{\circ} - S_i$, fog $\tan \alpha$ $\log \alpha^{\circ} = \log \sin \alpha + S = \log \tan \alpha$ For \cos and \cot near 9° use \sin and \tan
81	8.15035	533	8.15039	533	1.84961	9.99996	19	pol g si log log and
82	8.15568	526	8.15572	527	1.84428	9.99996	18	log log s
83	8.16094	520	8.16099	520	1.83901	9.99995	17	in
84	8.16614	514	8.16619	514	1.83381	9.99995	16	For
85	8.17128 8.17636	508	8.17133 8.17641	508	1.82867 1.82359	9.99995	15	`
86	8.18138	502		502		9.99995	14	
87 88	8.18138	496	8.18143 8.18639	496	1.81857	9.99995 9.99995	13 12	
89	8.19125	491	8.19130	491	1.80870	9.99995	II	
90	8.19610	485	8.19616	486	1.80384		10	
		480		480		9.99995		
91 92	8.20090 8.20565	475	8.20096 8.20570	474	1.79904	9.99995	o9 o8	
93	8.21034	469	8.21040	470	1.79430	9.99994 9.99994	07	T
94	8.21499	465	8.21504	464	1.78496	9.99994	06	° 1.758
95	8.21499	459	8.21964	460	1.78490	9.99994	05	.5 112
96	8.22413	455	8.22419	455	1.77581	9.99994	04	.6 107
97	8.22863	450	8.22869	450	1.77131	9.99994	03	.7 101
98	8.23308	445	8.23315	446	1.76685	9.99994	03	8 094
99	8.23749	441	8.23756	441	1.76244	9.99994	OI	9 087
100	8.24186	437	8.24192	436	1.75808	9.99993	00	1.0 079
	Cos	d.	Cot	d. c.	Tan	Sin		
	003	u.	000	u. c.	Tall	OIII		

					- 0			
	Sin	d.	Tan	d. c.	Cot	Cos		
00	8.24186	432	8.24192	432	1.75808	9.99993	100	
01	8.24618	1	8.24624	428	1.75376	9.99993	99	S
02	8.25045	427 424	8.25052	424	1.74948	9.99993	98	° 1.758
43	8.25469	424	8.25476	424	1.74524	9.99993	97	1.0 145
04	8,25889	1	8.25896		1.74104	9.99993	96	.1 149
05	8.26304	415	8.26312	416	1.73688	9.99993	95	.2 154
oõ	8.26716	412 408	8.26723	411	1.73277	9.99993	94	.3 160
07	8.27124		8.27131		1.72869	9.99992	93	.4 166
08	8.27528	404	8.27535	404	1.72465	9.99992	92	.5 172
09	8.27928	400 396	8.27936	401	1.72064	9.99992	91	
10	8.28324		8.28332	396	1.71668	9.99992	90	
II	8.28717	393	8.28725	393	1.71275	9.99992	89	
12	8.29107	390	8.29115	390	1.70885	9.99992	88	
13	8.29493	386	8.29501	386	1.70499	9.99992	87	
	8.29875	382	8.29884	383	1.70116	9.99991	86	nt.
14	8.30255	380	8.30263	379	1.69737	9.99991	85	ne
15 16	8.30631	376	8.30639	376	1.69361	9.99991	84	ler
		372		373	1.68988			di
17	8.31003	370	8.31012 8.31382	370	1.68618	9.99991	8 ₃ 8 ₂	T;
18	8.31373	366		367	1.68251	9.99991	81	1 5
19	8.31739	364	8.31749	363		9.99991		α" – T. an of
20	8.32103	360	8.32112	361	1.67888	9.99990	80	on angles are small: $= \log \alpha^{\bullet} - T;$ $= \log \sin \alpha + \log \tan \alpha = \log \alpha^{\bullet} - T;$ $= \log \sin \alpha + S = \log \tan \alpha + T.$ angles near 90° use sin and tan of complement.
21	8.32463	_	8.32473	357	1.67527	9.99990	79	= 1 nd
22	8.32820	357	8.32830	357	1.67170	9.99990	78	1 3 2
23	8.33175	355 352	8.33185	352	1.66815	9.99990	77	an og t sir
24	8.33527		8.33537		1.66463	9.99990	76	3. tz
25	8.33875	348	8.33886	349	1.66114	9.99990	75	log log
26	8.34221	346	8.34232	346	1.65768	9.99989	74	S: SI 90,06
27	8.34565	344	8.34575	343	1.65425	9.99989	73	34 7 34
28	8.34905	340	8.34916	341	1.65084	9.99989	72	ne ne se
29	8.35243	338	8.35254	338	1.64746	9.99989	71	lgi lgi
30	8.35578	335	8.35590	336	1.64410	9.99989	70	olate when angles are sm log $\sin \alpha = \log \alpha' - S$; it $\log \alpha' = \log \sin \alpha + S$ d cot of angles near 90°
		333		332	1.64078			a = = a
31	8.35911	330	8.35922	331		9.99989	69 68	te whe
32	8.36241	328	8.36253	328	1.63747	9.99988	67	sii sii
33	8.36569	325	8.36581	325	1.63419	9.99988		latilogical plate of d
34	8.36894	323	8.36906	323	1.63094	9.99988	66	an an
35	8.37217	321	8.37229	321	1.62771	9.99988	65	os te
36	8.37538	318	8.37550	318	1.62450	9.99988	64	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - S$; $\log \omega = \log \sin \alpha + S = \log \omega$. For \cos and \cot of angles near \cos use
37	8.37856	315	8.37868	316	1.62132	9.99988	63	To
38	8.38171	314	8.38184	314	1.61816	9.99987	62	
39	8.38485	311	8.38498	311	1.61502	9.99987	61	
40	8.38796	309	8.38809	309	1.61191	9.99987	60	
41	8.39105		8.39118		1.60882	9.99987	59	
42	8.39412	307	8.39425	307	1.60575	9.99987	58	
43	8.39717	305	8.39730	305	1.60270	9.99986	57	T
44	8.40019	302	8.40033	303	1.59967	9.99986	56	° 1.758
45	8.40320	301	8.40334	301	1.59666	9.99986	55	
46	8.40618	298	8.40532	298	1.59368	9.99986	54	1.0 079
47	8.40915	297	8.40929	297	1.59071	9.99986	53	.1 069
48	8.41209	294	8.41224	295	1.58776	9.99986	52	.2 059
49	8.41501	292	8.41516	292	1.58484	9.99985	51	.4 036
50	8.41792	291	8.41807	291	1.58193	9.99985	50	.4 036
			Cot	4 .	Tan	Sin		.3 . 023
	Cos	d.	Cot	d. c.	lan	Sin		

91º

1							110	
	Sin	d.	Tan	d. c.	Cot	Cos		
50	8.41792	288	8.41807	288	1.58193	9.99985	50	0
51	8.42080	287	8.42095	287	1.57905	9.99985	49	S
52	8.42367	285	8.42382	285	1.57618	9.99985	48	° 1.758
53	8.42652	283	8.42667	283	1.57333	9.99985	47	1.5 172
54	8.42935	281	8.42950	282	1.57050	9.99984	46	.6 179
55	8.43216	279	8.43232	279	1.56768	9.99984	45	.7 186
56	8.43495	277	8.43511	278	1.56489	9.99984	44	.8 194
57	8.43772	276	8.43789	275	1.56211	9.99984	43	.9 202
58	8.44048	274	8.44064	275	1.55936	9.99983	42	2.0 211
59	8.44322	272	8.44339	272	1.55661	9.99983	41	
60	8.44594	271	8.44611	271	1.55389	9.99983	40	
61	8.44865	268	8.44882	269	1.55118	9.99983	39	
62	8.45133	268	8.45151	267	1.54849	9.99983	38	
63	8.45401	265	8.45418	266	1.54582	9.99982	37	<u>;</u>
64	8.45666	26.1	8.45684	26.4	1.54316	9.99982	36	nen
65	8.45930	262	8.45948	263	1.54052	9.99982	35	len
66	8.46192	261	8.46211	261	1.53789	9.99982	34	T_i
67	8.46453	259	8.46472	259	1.53528	9.99982	33	1 8
68	8.46712	259	8.46731	259	1.53269	9.99981	32	(α° – Τ. n of α
69	8.46970	256	8.46989	256	1.53011	9.99981	31	γ α In
70	8.47226	255	8.47245	255	1.52755	9.99981	30	n angles are small: = $\log \alpha^{\circ} - S$; $\log \tan \alpha = \log \alpha$ = $\log \sin \alpha + S = \log \tan \alpha + T$; ungles near 90° use sin and \tan
71	8.47481		8.47500		1.52500	9.99981	29	n o
72	8.47734	253	8.47754	254	1.52246	9.99980	28	ta ta
73	8.47986	252 250	8.48006	252 250	1.51994	9.99980	27	tar
74	8.48236		8.48256		1.51744	9.99980	26	all: og = 1
75	8.48485	249	8.48505	249 248	1.51495	9.99980	25	e sma . S; lo . + S =
76	8.48732	247 246	8.48753	246	1.51247	9.99980	24	S + 8
77	8.48978		8.48999		1.51001	9.99979	23	n a ear
78	8.49223	245 243	8.49244	245 243	1.50756	9.99979	22	gles s a s n
79	8.49466	242	8.49487	242	1.50513	9.99979	21	angles α log α° log sin gles ne:
80	8.49708	240	8.49729	241	1.50271	9.99979	20	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - 5; \log 1$ $\log \alpha' = \log \sin \alpha + S = 1$ For \cos and \cot of angles near 90° use
81	8.49948		8.49970		1.50030	9.99978	19	e where $\sin \alpha$ log α ° sot of α
82	8.50188	240	8.50209	239	1.49791	9.99978	18	e w sir og
83	8.50425	237 237	8.50448	239 236	1.49552	9.99978	17	lat log
84	8.50662		8.50684		1.49316	9.99978	16	pool.
85	8.50897	235 234	8.50920	236 234	1.49080	9.99977	15	ter
86	8.51131	233	8.51154	233	1.48846	9.99977	14	in or c
87	8.51364		8.51387	232	1.48613	9.99977	13	To Fo
88	8.51596	232 230	8.51619	232 23I	1.48381	9.99977	12	
89	8.51826	229	8.51850	229	1.48150	9.99976	II	
90	8.52055	228	8.52079	228	1.47921	9.99976	10	
91	8.52283	227	8.52307	227	1.47693	9.99976	09	
92	8.52510	227	8.52534	227	1.47466	9.99976	08	T
93	8.52735	225	8.52760	225	1.47240	9.99975	07	° \ 1.75
94	8.52960	223	8.52985	223	1.47015	9.99975	06	1.5 8023
95	8.53183	223	8.53208	223	1.46792	9.99975	05	.6 8010
96	8.53405	221	8.53430	221	1.46570	9.99975	04	.7 7995
97	8.53626	220	8.53651	221	1.46349	9.99974	03	.8 7980
98	8.53846	218	8.53872	219	1.46128	9.99974	02	.9 7963
99	8.54064	218	8.54091	217	1.45909	9.99974	OI	2.0 7946
100	8.54282		8.54308		1.45692	9.99974	00	
	Cos	d.	Cot	d. c.	Tan	Sin		
-								THE RESERVE TO THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN

	Sin	d.	Tan	d. c.	Cot	Cos	_	
		<u>u.</u>		<u>u. c.</u>			100	
00	8.54282	216	8.54308	217	1.45692	9.99974		S
OI	8.54498	216	8.54525	216	1.45475	9.99973	99	
02	8.54714	214	8.54741	215	1.45259	9.99973	98	° 1.758
03	8.54928	214	8.54956	213	1.45044	9.99973	97	2.0 211
04	8.55142	212	8.55169	213	1.44831	9.99972	96	.1 220
05	8.55354	211	8.55382	213	1.44618	9.99972	95	.2 229
06	8.55565	210	8.55593	211	1.44407	9.99972	94	.3 239
07	8.55775	210	8.55804		1.44196	9.99972	93	.4 250
08	8.55985	208	8.56013	209	1.43987	9.99971	92	.5 260
09	8.56193	207	8.56222	207	1.43778	9.99971	91	
10	8.56400	206	8.56429	207	1.43571	9.99971	90	
11	8.56606		8.56636		1.43364	9.99971	89	
12	8.56811	205	8.56841	205	1.43159	9.99970	88	
13	8.57016	205 203	8.57046	205	1.42954	9.99970	87	it.
14	8.57219		8.57249	-	1.42751	9.99970	86	ne
15	8.57421	202	8.57452	203	1.42548	9.99969	85	ler
16	8.57623	202	8.57654	202	1.42346	9.99969	84	du
17	8.57823		8.57854	200	1.42146	9.99969	83	$T_{\rm ;}$
18	8.58023	200	8.58054	200	1.41946	9.99969	82	J . 45
19	8.58222	199	8.58253	199	1.41747	9.99968	81	n T a
20	8.58419	197	8.58451	198	1.41549	9.99968	80	all: $\cos t$ and $\alpha = \log \alpha^{\circ} - T$; $\beta = \log \tan \alpha + T$. use sin and \tan of complement.
21	8.58616	197	8.58649	198	1.41351	9.99968	79	u d
22	8.58812	196	8.58845	196	1.41155	9.99967	78	e small: S; log tanα +S = log ts 90° use sin ε
23	8.59007	195	8.59040	195	1.40960	9.99967	77	tar log
24	8.59201	194	8.59235	195	1.40765	9.99967	76	all:
25	8.59395	194	8.59428	193	1.40572	9.99967	75	Sing i lo i lo o
26	8.59587	192	8.59621	193	1.40379	9.99966	74	8 4 8
	8.59779	192	8.59813	192	1.40187	9.99966	73	n o ear
27 28	8.59970	191	8.60004	191	1.39996	9.99966	73	S Si C C
29	8.60160	190	8.60194	190	1.39806	9.99965	71	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
30	8.60349	189	8.60384	190	1.39616	9.99965	70	្ត្រ = ដូច្នា
		188	8.60572	188	1.39428	9.99965	69	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - S; \log t$ $\log \sin \alpha + S = \log \sin \alpha + S$ For \cos and \cot of angles near 90° use
31	8.60537 8.60725	188	8.60760	188	1.39420	9.99964	68	siis og ot
32	8.60911	186	8.60947	187	1.39240	9.99964	67	ate og 1
33	8.61097	186	8.61133	186	1.38867	9.99964	66	pol l anc
34	8.61282	185	8.61319	186	1.38681	9.99963	65	ter os :
35 36	8.61467	185	8.61504	185	1.38496	9.99963	64	in o
	8.61650	183	8.61687	183	1.38313	9.99963	63	To Fo
37 38	8.61833	183	8.61870	183	1.38130	9.99963	62	
39	8.62015	182	8.62053	183	1.37947	9.99962	61	
40	8.62196	181	8.62234	181	1.37766	9.99962	60	
	8.62377	181	8.62415	181	1.37585	9.99962	59	
41	8.62556	179	8.62595	180	1.37505	9.99961	58	T
42	8.62735	179	8.62774	179	1.37403	9.99961	57	- 1
		179	8.62953	179	1.37047	9.99961	56	I.757
44	8.62914 8.63091	177	8.63131	178	1.37047	9.99960	55	2.0 946
45 46	8.63268	177	8.63308	177	1.36692	9 .99960 9 .99960	54	.1 928
		176	8.63484	176	1.36516	9.99960	53	.2 909
47	8.63444	175	8.63660	176	1.36340	9.99959	53	.3 889
48	8.63794	175	8.63835	175	1.36165	9.99959	51	.4 869
49 50	8.63968	174	8.64009	174	1.35991	9.99959	50	.5 847
	Cos	d.	Cot	d. c.	Tan	Sin		
	Cos	u.	COL	a. c.	1 (111	UIII		

	Sin	d.	Tan	d. c.	Cot	Cos		
50	8.63968	<u>u.</u>	8.64009	- a. c.			50	
		173		174	1.35991	9.99959		S
51	8.64141	173	8.64183 8.64356	173	1.35817	9.99958	49 48	
52	8.64314 8.64486	172	8.64528	172	1.35644	9.99958		° 1.758
53		171		172	1.35472	9.99958	47	2.5 260
54	8.64657	170	8.64700 8.64870	170	1.35300	9.99957	46	.6 272
55 56	8.64827	170	8.65041	171	1.35130	9.99957	45	.7 283
	8.64997	169		169	1.34959	9.99957	44 43	.8 296
57 58	8.65166 8.65335	169	8.65210 8.65379	169	1.34790	9.99956		.9 308
59	8.65503	168	8.65547	168	1.34621 1.34453	9.99956 9.99956	42 41	3.0 321
60		167		168				
	8.65670	167	8.65715	167	1.34285	9.99955	40	
61	8.65837	166	8.65882	166	1.34118	9.99955	39 38	
62	8.66003	165	8.66048	166	1.33952	9.99955		
63	8.66168	165	8.66214	165	1.33786	9.99954	37	nt
64	8.66333	164	8.66379	164	1.33621	9.99954	36	m
65 66	8.66497	163	8.66543	164	1.33457	9.99954	35	ple
	8.66660	163	8.66707	163	1.33293	9.99953	34	all: $ \log \alpha^\circ - T; $ = $\log \tan \alpha + T. $ use sin and tan of complement.
67 68	8.66823	162	8.66870	163	1.33130	9.99953	33	-T;
69	8.66985	162	8.67033	162	1.32967	9.99952	32	م کر د
	8.67147	161	8.67195	161	1.32805	9.99952	31	tan tan
70	8.67308	160	8.67356	161	1.32644	9.99952	30	mall: $S = \log \alpha$ $S = \log \tan \alpha + T$ • use sin and tan (a)
71	8.67468	160	8.67517	160	1.32483	9.99951	29	an a
72	8.67628	160	8.67677	160	1.32323	9.99951	28	n n c
73	8.67788	158	8.67837	159	1.32163	9.99951	27	1: 1: 10 se s
74	8.67946	158	8.67996	158	1.32004	9.99950	26	lag log si = s
75	8.68104	158	8.68154	158	1.31846	9.99950	25	S: Su
76	8.68262	157	8.68312	158	1.31688	9.99950	24	late when angles are small: $\log \sin \alpha = \log \alpha^\circ - S$; $\log \tan \alpha = \log \alpha \circ - S$; $\log \tan \alpha + S = \log \tan \alpha + T$. d $\cot \alpha$ angles near 90° use sin and $\tan \alpha$
77	8.68419	156	8.68470	156	1.31530	9.99949	23	ne nee
78	8.68575	156	8.68626	157	1.31374	9.99949	22	lg lg s s s s s s s
79	8.68731	155	8.68783	155	1.31217	9.99948	21	ar in the last
80	8.68886	155	8.68938	155	1.31062	9.99948	20	a len
81	8.69041		8.69093	155	1.30907	9.99948	19	W in a solution
82	8.69195	154 154	8.69248	154	1.30752	9.99947	18	g si col
83	8.69349	153	8.69402	153	1.30598	9.99947	17	lo lo
84	8.69502	152	8.69555	153	1.30445	9.99947	16	di a
85	8.69654	152	8.69708	152	1.30292	9.99946	15	co ut
86	8.69806	152	8.69860	152	1.30140	9.99946	14	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - S$; $\log t$ $\log \alpha' = \log \sin \alpha + S = 1$ For \cos and \cot of angles near 90° use
87	8.69958	151	8.70012	152	1.29988	9.99945	13	H H
88	8.70109	150	8.70164	150	1.29836	9.99945	12	
89	8.70259	150	8.70314	151	1.29686	9.99945	11	
90	8.70409	149	8.70465	149	1.29535	9.99944	10	
91	8.70558	{	8.70614	150	1.29386	9.99944	09	
92	8.70707	149 149	8.70764	148	1.29236	9.99944	.08	T
93	8.70856	149	8.70912	149	1.29088	9.99943	07	° 1.757
94	8.71003	148	8.71061	147	1.28939	9.99943	06	2.5 847
95	8.71151	140	8.71208	147	1.28792	9.99942	05	2.5 847 .6 824
96	8.71298	146	8.71356	146	1.28644	9.99942	04	.7 801
97	8.71444	146	8.71502	147	1.28498	9.99942	03	.8 777
98	8.71590	145	8.71649	147	1.28351	9.99941	02	.9 752
99	8.71735	145	8.71794	146	1.28206	9.99941	01	3.0 725
100	8.71880		8.71940		1.28060	9.99940	00	
	Cos	d.	Cot	d.c.	Tan	Sin)	

	Sin	d.	Tan	d.c.	Cot	Cos			P. P.	
									145	143
00	8.71880	144	8.71940	144	1.28060	9.99940	100	1	14.5	14.3 28.6
01	8.72024	144	8.72084	145	1.27916	9.99940	99	3	29.0 43.5	28.6 42.9
02	8.72168	144	8.72229	144	1.27771	9.99940	98	4	58.0	57.2
03	8.72312	143	8.72373	143	1.27627	9.99939	97	5 6	72.5	71.5
04	8.72455	142	8.72516	143	1.27484	9.99939	96		87.0	85.8 100.1
05	8.72597	142	8.72659	142	1.27341	9.99938	95	7 8	116.0	114.4
06	8.72739	142	8.72801	142	1.27199	9.99938	94	9	130.5	128.7
07	8.72881	141	8.72943	142	1.27057	9.99938	93	1	141 14.1	139 13.9
08	8.73022	141	8.73085	141	1.26915	9.99937	92	2	28.2	27.8
09	8.73163	140	8.73226	140	1.26774	9.99937	91	3	42.3	41.7
10	8.73303	139	8.73366	140	1.26634	9.99936	90	4	56.4 70.5	55.6 69.5
11	8.73442	140	8.73506	140	1.26494	9.99936	89	5 6	84.6	83.4
12	8.73582	139	8.73646	139	1.26354	9.99936	88	7 8	98.7	97.3
13	8.73721	138	8.73785	139	1.26215	9.99935	87	8 9	112.8	111.2 125.1
14	8.73859	138	8.73924		1.26076	9.99935	86	9	138	137
15	8.73997	137	8.74063	139	1.25937	9.99934	85	1	13.8	13.7
16	8.74134	138	8.74201	137	1.25799	9.99934	84	2	27.6	27.4
17	8.74272	136	8.74338	!	1.25662	9.99933	83	3 4	4I.4 55.2	41.1 54.8
18	8.74408	136	8.74475	137	1.25525	9.99933	82	5	69.0	68.5
19	8.74544	136	8.74612	136	1.25388	9.99933	81		82.8 96.6	82.2 95.9
20	8.74680	136	8.74748	136	1.25252	9.99932	80	7 8	110.4	109.6
21	8.74816	-	8.74884		1.25116	9.99932	79	9	124.2	123.3
22	8.74950	134	8.75019	135	1.24981	9.99931	78	1	135	133
23	8.75085	135	8.75154	135	1.24846	9.99931	77	2	13.5	13.3 26.6
24	8.75219		8.75289	}	1.24711	9.99931	76	3	40.5	39.9
25	8.75353	134	8.75423	134	1.24577	9.99930	75	4	54.0	53.2 66.5
26	8.75486	133	8.75556	133	1.24444	9.99930	74	5 6	67.5 81.0	79.8
27	8.75619	ł	8.75690	134	1.24310	9.99929	73	7 8	94.5	93.1
28	8.75751	132	8.75823	133	1.24177	9.99929	72		108.0	106.4
29	8.75883	132 132	8.75955	132 132	1.24045	9.99928	71	9	121.5 131	119.7 129
30	8.76015		8.76087		1.23913	9.99928	70	1	13.1	12.9
31	8.76146	131	8.76219	132	1.23781	9.99927	69	2	26.2	25.8
32	8.76277	131	8.76350	131	1.23650	9.99927	68	3 4	39.3 52.4	38.7
33	8.76408	131	8.76481	131	1.23519	9.99927	67	5 6	65.5 78.6	51.6 64.5
34	8.76538	130	8.76612	131	1.23388	9.99926	66		78.6	77.4
35	8.76667	129	8.76742	130	1.23258	9.99926	65	7 8	91.7	90.3
36	8.76797	130	8.76871	129	1.23129	9.99925	64	9	117.9	116.1
37	8.76926	129	8.77001	130	1.22999	9.99925	63	1	128	127
38	8.77054	128	8.77130	129	1.22870	9.99923	62	I 2	12.8 25.6	12.7 25.4
39	8.77182	128	8.77258	128	1.22742	9.99924	61	3	38.4	38.1
40	8.77310		8.77387	129	1.22613	9.99923	60	4	51.2 64.0	50.8
41	8.77438	128	8.77514	127	1.22486			5 6	76.8	63.5
42	8.77565	127	8.77642	128	1.22480	9.99923 9.99923	59 58	7 8	89.6	76.2 88.9
43	8.77691	126	8.77769	127	1.22331	9.99923	57		102.4	101.0
44	8.77817	126	8.77896	127	1.22104	9.99922	56	9	115.2 125	114.3 124
45	8.77943	126	8.78022	126	1.22104	9.99921	55	I	12.5	12.4
46	8.78069	126	8.78148	126	1.21978	9.99921	54	2	25.0	24.8
47	8.78194	125	8.78274	126	1.21726			3	37.5 50.0	37.2 49.6
48	8.78319	125	8.78399	125	1.21720	9.99920	53 52		02.5	49.6 62.0
49	8.78443	124	8.78524	125	1.21476	9.99920	51	5	75.0 87.5	74 · 4 86 · 8
50	8.78568	125	8.78649	125	1.21351	9.99919	50	7 8	87.5 100.0	86.8 99.2
	0.70300		0.70049		1.21351	9.99919	00	9	112.5	111.6
	Cos	d.	Cot	d. c.	Tan	Sin			P. P.	

3 *							176°			
	Sin	d.	Tan	d. c.	Cot	Cos			P. P.	
50	8.78568		8.78649		r oragr	0.00070	50		123	122
		123		124	1.21351	9.99919		I 2	12.3	12.2 24.4
51	8.78691	124	8.78773	124	1.21227	9.99918	49	3	36.9	36.6
52	8.78815	123	8.78897	123	1.21103	9.99918	48	4	49.2	48.8
53	8.78938	122	8.79020	123	1.20980	9.99918	47	5	61.5	61.0 73.2
54	8.79060	123	8.79143	123	1.20857	9.99917	46		73.8 86.1	85.4
55	8.79183	122	8.79266	123	1.20734	9.99917	45	7 8	98.4	85.4 97.6
56	8.79305	121	8.79389	122	1.20611	9.99916	44	9	110.7	109.8
57	8.79426	122	8.79511	122	1.20489	9.99916	43	1	121 12.1	119 11.9
58	8.79548	121	8.79633	121	1.20367	9.99915	42	2	24.2	23.8
59	8.79669	120	8.79754	121	1.20246	9.99915	41	3	36.3	35.7
60	8.79789	121	8.79875	121	1.20125	9.99914	40	4 5	48.4	47.6 59.5
61	8.79910		8.79996		1.20004	9.99914	39	5	60.5 72.6	71.4
62	8.80030	120	8.80116	120	1.19884	9.99913	38	7 8	84.7 96.8	83.3
63	8.80149	119	8.80237	121	1.19763	9.99913	37	8	96.8	95.2 107.1
64	8.80269		8.80356		1.19644	9.99912	36	9	1118	117
65	8.80388	119	8.80476	120	1.19524	9.99912	35	I	11.8	11.7
66	8.80506	118	8.80595	119	1.19405	9.99911	34	2	23.6	23.4
67	8.80625	119	8.80714	119	1.19286	9.99911	33	3 4	35.4 47.2	35.I 46.8
68	8.80743	118	8.80832	118	1.19168	9.99910	32	5	59.0	58.5
69	8.80860	117	8.80950	118	1.19050	9.99910	31	5 6	70.8 82.6	70.2
70	8.80978	118	8.81068	118	1.18932	9.99909	30	7 8	94.4	81.9 93.6
		117		118				9	106.2	105.3
71	8.81095 8.81212	117	8.81186 8.81303	117	1.18814	9.99909	29 28		116	115
72 73	8.81328	116	8.81420	117	1.18697	9.99908	27	1	11.6	11.5
		116		117	-			3	23.2	23.0 34.5
74	8.81444	116	8.81537	116	1.18463	9.99907	26	4	34.8 46.4	46.0
75 76	8.81675	115	8.81653 8.81769	116	1.18347	9.99907	25	5	58.0	57.5
		116		116		9.99906	24		69.6	69.0 80.5
77	8.81791	114	8.81885	115	1.18115	9.99906	23	7 8	92.8	92.0
78	8.81905	115	8.82000	115	1.18000	0.99905	22	9	104.4	103.5
79		114		115	1.17885	9.99905	21	_	114	113
80	8.82134	114	8.82230	114	1.17770	9.99904	20	1 2	11.4	11.3 22.6
81	8.82248		8.82344		1.17656	9.99904	19	3	34.2	33.9
82	8.82362	114	8.82458	114	1.17542	9.99903	18	4	45.6	45.2
83	8.82475	113	8.82572	114	1.17428	9.99903	17	5 6	57.0 68.4	56.5 67.8
84	8.82588		8.82686		1.17314	9.99902	16		79.8	79.1
85	8.82701	113	8.82799	113	1.17201	9.99902	15	7 8	91.2	90.4
86	8.82814	113	8.82912	113	1.17088	9.99901	14	9	102.6	101.7
87	8.82926		8.83025		1.16975	9.99901	13	1	II.2	II.I
88	8.83038	II2	8.83137	112	1.16863	9.99900	12	2	22.4	22.2
89	8.83149	III2	8.83249	112	1.16751	9.99900	11	3	33.6	33.3
90	8.83261		8.83361		1.16639	9.99899	10	4 5	44.8 56.0	44.4 55.5
91	8.83372	111	8.83473	II2	1.16527	9.99899	09	5 6	67.2	55.5 66.6
92	8.83482	110	8.83584	III	1.16416	9.99898	08	7 8	78.4	77.7 88.8
93	8.83593	III	8.83695	III	1.16305	9.99898	07	9	89.6	99.9
94	8.83703	110	8.83806	111	1.16194	9.99897	06	3	109	108
95	8.83813	110	8.83916	110	1.16084	9.99897	05	1	10.9	10.8
96	8.83923	110	8.84026	110	1.15974	9.99896	04	3	21.8	2I.6 32.4
97	8.84032	109	8.84136	110	1.15864	9.99896	03	4	32.7 43.6	43.2
98	8.84141	109	8.84246	110	1.15754	9.99895	03	5	54.5	54.0 64.8
99	8.84250	109	8.84355	109	1.15645	9.99895	OI		65.4	75 6
100	8.84358	108	8.84464	109	1.15536	9.99894	00	7 8	87.2	75.6 86.4
100								9	98.1	97.2
	Cos	d.	Cot	d. c.	Tan	Sin			P. P.	

	Sin	d.	Tan	d. c.	Cot	Cos	1		P. P.	
-							_		109	108
00	8.84358	109	8.84464	109	1.15536	9.99894	100	I	10.9	10.8
OI	8.84467	108	8.84573	109	I.I5427	9.99894	99	2 3	21.8 32.7	21.6 32.4
02	8.84575	107	8.84682	108	1.15318	9.99893	98	4	43.6	43.2
03	8.84682	108	8.84790	108	1.15210	9.99892	97	5 6	54.5	54.0
04	8.84790	107	8.84898	108	1.15102	9.99892	96	7	65.4	64.8 75.6
05	8.84897	107	8.85006	103	1.14994	9.99891	95	7 8	87.2	86.4
06	8.85004	107	8.85113	107	1.14887	9.99891	94	9	98.1	97.2
07	8.85111	106	8.85220	107	1.14780	9.99890	93	1	107	106 10.6
08	8.85217	106	8.85327	107	1.14673	9.99890	92	2	21.4	21.2
09	8.85323	106	8.85434	106	1.14566	9.99889	91	3	32.I	31.8
10	8.85429	106	8.85540	106	1.14460	9.99889	90	4	42.8 53.5	42.4 53.0
11	8.85535		8.85646		1.14354	9.99888	89	5 6	64.2	63.6
12	8.85640	105	8.85752	106	1.14248	9.99888	88	7 8	74.9	74.2
13	8.85745	105	8.85858	100	1.14142	9.99887	87	9	85.6 96.3	84.8
14	8.85850	_	8.85963		1.14037	9.99887	86	9	105	95.4 104
15	8.85955	105	8.86069	106	1.13931	9.99886	85	I	10.5	10.4
16	8.86059	104	8.86173	104	1.13827	9.99885	84	2	21.0	20.8
17	8.86163		8.86278		1.13722	9.99885	83	3 4	31.5 42.0	31.2 41.6
18	8.86267	104	8.86383	105	1.13617	9.99884	82	5 6	52.5	52.0
19	8.86370	103	8.86487	10.4	1.13513	9.99884	81	6	63.0	62.4
20	8.86474		8.86591		1.13409	9.99883	80	7 8	73.5 84.0	72.8 83.2
21	8.86577	103	8.86694	103				9	94.5	93.6
21	8.86680	103	8.86798	104	1.13306 1.13202	9.99883 9.99882	79 78		103	102
23	8.86782	102	8.86901	103	1.13202	9.99882	77	I	10.3	10.2
		103		103				2 3	20.6 30.9	20.4 30.6
24 25	8.86885 8.86987	102	8.87004 8.87106	102	1.12996	9.99881	76	4	41.2	40.8
26	8.87089	102	8.87209	103	1.12094	9.99880	75 74	5 6	51.5	51.0
		101		102			i		61.8 72.1	61.2 71.4
27 28	8.87190 8.87292	102	8.87311	102	1.12689	9.99879	73	7 8	82.4	81.0
29	8.87393	IOI	8.87515	102	1.12587	9.99879 9.99878	72 71	9	92.7	91.8
		IOI		IOI				1	101 10.1	100 10.0
30	8.87494	100	8.87616	IOI	1.12384	9.99878	70	2	20.2	20.0
31	8.87594	IOI	8.87717	102	1.12283	9.99877	69	3	30.3	30.0
32	8.87695	100	8.87819	100	1.12181	9.99876	68	4	40.4	40.0
33	8.87795	100	8.87919	101	1.12081	9.99876	67	5	50.5 60.6	50.0 60.0
34	8.87895	100	8.88020	100	1.11980	9.99875	66	7 8	70.7	70.0
35	8.87995	99	8.88120	100	1.11880	9.99875	65		80.8	80.0
36	8.88094	100	8.88220	100	1.11780	9.99874	64	9	90.9	90.0 98
37	8.88194	99	8.88320	100	1.11680	9.99874	63	I	9.9	9.8
38	8.88293	99	8.88420	99	1.11580	9.99873	62	2	19.8	19.6
39	8.88392	98	8.88519	99	1.11481	9.99872	61	3	29.7 39.6	29.4 39.2
40	8.88490	99	8.88618	99	1.11382	9.99872	60	4 5 6	49.5	49.0
41	8.88589		8.88717		1.11283	9.99871	59		59.4	58.8
42	8.88687	98	8.88816	99	1.11184	9.99871	58	7 8	69.3 79.2	68.6 78.4
43	8.88785	98 98	8.88915	99 98	1.11085	9.99870	57	9	89.1	88.2
44	8.88883		8.89013	-	1.10987	9.99869	56		97	96
45	8.88980	97	8.89111	98	1.10889	9.99869	55	I 2	9.7 19.4	9. 6 19.2
46	8.89077	97 97	8.89209	98 98	1.10791	9.99868	54	3	29.I	28.8
47	8.89174		8.89307		1.10693	9.99868	53	4	38.8	38.4
48	8.89271	97	8.89404	97	1.10596	9.99867	52	5	48.5	48.0
49	8.89368	97 96	8.89501	97	1.10499	9.99867	51		58.2 67.9	57.6 67.2
50	8.89464	90	8.89598	97	1.10402	9.99866	50	7 8	77.6 87.3	76.8
		-d.						9	P. P	86.4
-	Cos	u,	Cot	d. c.	Tan	Sin	-		F. P	

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	8.89464		8.89598		1.10402	9.99866	50	
51	8.89561	97	8.89695	97	1.10305	9.99865	49	97 96
52	8.89657	\ 96	8.89792	97	1.10208	9.99865	48	I 9.7 9.6 2 19.4 19.2
53	8.89752	95 96	8.89888	96 96	1.10112	9.99864	47	3 29.1 28.8
54	8.89848		8.89984	-	1.10016	9.99864	46	4 38.8 38.4
55	8.89943	95 95	8.90080	96 96	1.09920	9.99863	45	5 48.5 48.0 6 58.2 57.6
56	8.90038	95 95	8.90176	96	1.09824	9.99862	44	7 67.9 67.2 8 77.6 76.8
57	8.90133	95	8.90272	95	1.09728	9.99862	43	8 77.6 76.8
58	8.90228	95	8.90367	95	1.09633	9.99861	42	9 87.3 86.4
59	8.90323	94	8.90462	95	1.09538	9.99860	41	95 94
60	8.90417	94	8.90557	95	1.09443	9.99860	40	I 9.5 9.4 2 19.0 18.8
61	8.90511	94	8.90652	94	1.09348	9.99859	39	3 28.5 28.2
62	8.90605	94	8.90746	95	1.09254	9.99859	38	4 38.0 37.6 5 47.5 47.0
63	8.90699	93	8.90841	94	1.09159	9.99858	37	5 47.5 47.0 6 57.0 56.4
64 65	8.90792	93	8.90935	94	1.09065	9.99857	36	7 66.5 65.8
66	8.90885 8.90978	93	8.91029 8.91122	93	1.08971	9.99857 9.99856	35	8 76.0 75.2 9 85.5 84.6
67	8.91071	93	8.91216	94	1.08784	9.99856	34	
68	8.91164	93	8.91210	93	1.08784	9.99850	33	1 93 92 1 9.3 9.2
69	8.91257	93	8.91402	93	1.08598	9.99854	31	1 9.3 9.2 2 18.6 18.4
70	8.91349	92	8.91495	93	1.08505	9.99854	30	3 27.9 27.6
71	8.91441	92	8.91588	93	1.08412	9.99853	29	4 37.2 36.8 5 46.5 46.0
72	8.91533	92	8.91680	92	1.08320	9.99852	28	6 55.8 55.2
73	8.91625	92	8.91773	93	1.08227	9.99852	27	7 65.1 64.4 8 74.4 73.6
74	8.91716	91	8.91865	92	1.08135	9.99851	26	7 65.I 64.4 8 74.4 73.6 9 83.7 82.8
75	8.91807	91	8.91957	92	1.08043	9.99851	25	
76	8.91898	91	8.92049	92 91	1.07951	9.99850	24	1 91 90 1 9.1 9.0
77	8.91989	91	8.92140	91	1.07860	9.99849	23	I 9.I 9.0 2 18.2 18.0
78	8.92080	91 91	8.92231	92	1.07769	9.99849	22	3 27.3 27.0
79	8.92171	90	8.92323	91	1.07677	9.99848	21	4 36.4 36.0 5 45.5 45.0
80	8.92261	90	8.92414	90	1.07586	9.99847	20	6 54.6 54.0
81	8.92351	90	8.92504	91	1.07496	9.99847	19	7 63.7 63.0
82	8.92441	90	8.92595	90	1.07405	9.99846	18	8 72.8 72.0 9 81.9 81.0
83	8.92531	90	8.92685	91	1.07315	9.99846	17	
84	8.92621	89	8.92776	90	1.07224	9.99845	16	89 1 8.9
85 86	8.92710	89	8.92866	90	1.07134	9.99844	15	2 17.8
	8.92799	89	8.92956	89	1.07044	9.99844	14	3 26.7
87 88	8.92888	89	8.93045	90	1.06955	9.99843	13	4 35.6 5 44.5
89	8.92977 8.93066	89	8.93135 8.93224	89	1.00805	9.99842 9.99842	12 11	6 53.4
90	8.93154	88	8.93313	89	1.06687	9.99841	10	7 62.3
		89		89				8 71.2 9 80.1
91 92	8.93243 8.93331	88	8.93402 8.93491	89	1.06598	9.99840	09 08	
93	8.93419	88 88	8.93580	89	1.00309	9.99839	07	I 88 87 8.8 8.7
94	8.93507		8.93668	88	1.06332	9.99838	06	2 17.6 17.4
95	8.93594	87 88	8.93756	88	1.06244	9.99838	05	3 26.4 26.I
96	8.93682	87	8.93845	89 87	1.06155	9.99837	04	4 35.2 34.8 5 44.0 43.5
97	8.93769	87	8.93932	88	1.06068	9.99836	03	6 52.8 52.2
98	8.93856	87	8.94020	88	1.05980	9.99836	02	7 61.6 60.9
99	8.93943	87	8.94108	87	1.05892	9.99835	10	8 70.4 69.6 9 79.2 78.3
100	8.94030		8.94195		1.05805	9.99834	00	J 175.2 1 175.0
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		_						

94° 85°

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	8.94030	86	8.94195		1.05805	9.99834	100	
or	8.94116		8.94282	87	1.05718	9.99834	99	I 87 86 8.7 8.6
02	8.94203	87 86	8.94369	87	1.05631	9.99833	98	2 17.4 17.2
03	8.94289	86	8.94456	87 87	1.05544	9.99832	97	3 26.1 25.8
04	8.94375	86	8.94543		1.05457	9.99832	96	4 34.8 34.4 5 43.5 43.0 6 52.2 51.6
05	8.94461	85	8.94630	87 86	1.05370	9.99831	95	5 43.5 43.0 6 52.2 51.6
06	8.94546	86	8.94716	86	1.05284	9.99830	94	7 60.9 60.2
07	8.94632	85	8.94802	86	1.05198	9.99830	93	8 69.6 68.8
08	8.94717	85	8.94888	86	1.05112	9.99829	92	9 78.3 77.4
09	8.94802	85	8.94974	86	1.05026	9.99828	9 1	1 85 84 1 8.5 8.4
10	8.94887	85	8.95060	85	1.04940	9.99828	90	2 17.0 16.8
11	8.94972	85	8.95145	86	1.04855	9.99827	89	3 25.5 25.2 4 34.0 33.6
12	8.95057	84	8.95231	85	1.04769	9.99826	88	4 34.0 33.6 5 42.5 42.0
13	8.95141	85	8.95316	85	1.04684	9.99826	87	6 51.0 50.4
14	8.95226	84	8.95401	85	1.04599	9.99825	86	7 59.5 58.8
15	8.95310	84	8.95486	84	1.04514	9.99824	8 ₅	8 68.0 67.2 9 76.5 75.6
	8.95394	84	8.95570	85	1.04430	9.99824		83
17	8.95478 8.95562	84	8.95655	84	1.04345	9.99823	8 ₃ 8 ₂	
19	8.95645	83	8.95739 8.95823	84	1.04261	9.99822 9.99822	81	I 8.3 2 16.6
20	8.95728	83	8.95908	85	1.04092	9.99821	80	3 24.9
		84		83				4 33.2
2 I 2 2	8.95812 8.95895	83	8.95991 8.96075	84	1.04009	9.99820	79 78	5 41.5 6 49.8
23	8.95978	83	8.96159	84	1.03925	9.99820	70 77	7 58.1
_	8.96060	82	8.96242	83			76	7 58.1 8 66.4
24	8.96143	83	8.96325	83	1.03758	9.99818	75	9 74.7
25 26	8.96225	82	8.96409	84	1.03573	9.99817	74	82 81
27	8,96308	83	8.96492	83	1.03508	9.99816	73	I 8.2 8.1 2 16.4 16.2
28	8.96390	82	8.96574	82	1.03300	9.99815	72	2 16.4 16.2 3 24.6 24.3
29	8.96472	82	8.96657	83	1.03343	9.99815	71	4 32.8 32.4
30	8.96553	81	8.96739	82	1.03261	9.99814	70	5 41.0 40.5 6 49.2 48.6
31	8.96635	82	8.96822	83	1.03178	9.99813	69	7 57.4 56.7
32	8.96716	81	8.96904	82	1.03096	9.99813	68	8 65.6 64.8
33	8.96798	82	8.96986	82	1.03014	9.99812	67	9 73.8 72.9
34	8.96879	81	8.97068	82	1.02932	9.99811	66	80
35	8.96960	81 81	8.97150	82 81	1.02850	9.99810	65	I 8.0
36	8.97041	81	8.97231	81	1.02769	9.99810	64	2 16.0 3 24.0
37	8.97122	80	8.97313	81	1.02687	9.99809	63	4 32.0
38	8.97202	81	8.97394	81	1.02606	9.99808	62	5 40.0
39	8.97283	80	8.97475	81	1.02525	9.99808	61	6 48.0 7 56.0
40	8.97363	80	8.97556	81	1.02444	9.99807	60	8 64.0
41	8.97443	80	8.97637	80	1.02363	9.99806	59	9 72.0
42	8.97523	80	8.97717	81	1.02283	9.99805	58	79 78
43	8.97603	79	8.97798	80	1.02202	9.99805	57	1 7.9 7.8 2 15.8 15.6
44	8.97682	80	8.97878	81	1.02122	9.99804	56	3 23.7 23.4
45	8.97762	79	8.97959	80	1.02041	9.99803	55	4 31.6 31.2
46	8.97841	79	8.98039	80		9.99803	54	5 39.5 39.0 6 47.4 46.8
47	8.97920	80	8.98119	80	1.01881	9.99802 9.99801	53 52	
48 49	8.98000 8.98078	78	8.98199 8.98278	79	1.01801	9.99800	52 51	8 63.2 62.4
50		79	8.98358	80	1.01/22	9.99800	50	9 71.1 70.2
80	8.98157							P. P.
	Cos	d.	Cot	d. c.	Tan	Sin	049	

							TIT	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	8.98157	79	8.98358	79	1.01642	9.99800	50	79 78
51	8.98236	78	8.98437	79	1.01563	9.99799	49	I 7.9 7.8
52	8.98314	79	8.98516	79	1.01484	9.99798	48	2 15.8 15.6
53	8.98393	78	8.98595	79	1.01405	9.99797	47	3 23.7 23.4
54	8.98471	78	8.98674	79	1.01326	9.99797	46	4 31.6 31.2 5 39.5 39.0
55	8.98549	78	8.98753	79	1.01247	9.99796	45	5 39.5 39.0 6 47.4 46.8
56	8.98627	78	8.98832	78	1.01168	9.99795	44	7 55.3 54.6
57	8.98705	77	8.98910	79	1.01090	9.99794	43	
58	8.98782	78	8.98989	78	I.OIOII	9.99794	42	9 71.1 70.2
59	8.98860	77	8.99067	78	1.00933	9.99793	41	77
60	8.98937	78	8.99145	78	1.00855	9.99792	40	I 7.7
61	8.99015		8.99223	78	1.00777	9.99791	39	2 15.4 3 23.1
62	8.99092	77 77	8.99301	78	1.00699	9.99791	38	4 30.8
63	8.99169	76	8.99379	77	1.00621	9.99790	37	5 38.5
64	8.99245	77	8.99456	78	1.00544	9.99789	36	
65	8.99322	77	8.99534	77	1.00466	9.99788	35	7 53.9 8 61.6
66	8.99399	76	8.99611	77	1.00389	9.99788	34	9 69.3
67	8.99475	76	8.99688	77	1.00312	9.99787	33	76
68	8.99551	77	8.99765	77	1.00235	9.99786	32	1 7.6
69	8.99628	76	8.99842	77	1.00158	9.99785	31	2 15.2
70	8.99704	75	8.99919	76	1.00081	9.99785	30	3 22.8
71	8.99779	76	8.99995		1.00005	9.99784	29	4 30.4 5 38.0
72	8.99855	76	9.00072	77 76	0.99928	9.99783	28	6 45.6
73	8.99931	75	9.00148	77	0.99852	9.99782	27	7 53.2
74	9.00006	76	9.00225	76	0.99775	9.99782	26	8 60.8 9 68.4
75	9.00082	75	9.00301	76	0.99699	9.99781	25	
76	9.00157	75	9.00377	75	0.99623	9.99780	24	75 74 1 7.5 7.4
77	9.00232	75	9.00452	76	0.99548	9.99779	23	2 15.0 14.8
78	9.00307	75	9.00528	76	0.99472	9.99779	22	3 22.5 22.2
79	9.00382	74	9.00604	75	0.99396	9.99778	21	4 30.0 29.6
80	9.00456	75	9.00679	76	0.99321	9.99777	20	5 37.5 37.0 6 45.0 44.4
81	9.00531		9.00755		0.99245	9.99776	19	7 52.5 51.8
82	9.00605	74 75	9.00830	75 75	0.99170	9.99776	18	
83	9.00680	74	9.00905	75	0.99095	9.99775	17	
84	9.00754	74	9.00980	75	0.99020	9.99774	16	73
85	9.00828	74	9.01055	74	0.98945	9.99773	15	I 7.3 2 I4.6
86	9.00902	74	9.01129	75	0.98871	9.99772	14	3 21.9
87	9.00976	73	9.01204	74	0.98796	9.99772	13	4 29.2
88	9.01049	74	9.01278	75	0.98722	9.99771	12	5 36.5 6 43.8
89	9.01123	73	9.01353	74	0.98647	9.99770	II	
90	9.01196	73	9.01427	74	0.98573	9.99769	10	8 58.4
91	9.01269	74	9.01501	74	0.98499	9.99769	09	9 65.7
92	9.01343	74	9.01575	74	0.98425	9.99768	08	72
93	9.01416	73	9.01649	73	0.98351	9.99767	07	I 7.2
94	9.01489	72	9.01722	74	0.98278	9.99766	06	2 I4.4 3 21.6
95	9.01561	73	9.01796	73	0.98204	9.99765	05	4 28.8
96	9.01634	73	9.01869	74	0.98131	9.99765	04	5 36.0
97	9.01707	72	9.01943	73	0.98057	9.99764	03	
98	9.01779	72	9.02016	73	0.97984	9.99763	02	7 50.4 8 57.6
99	9.01851	72	9.02089	73	0.97911	9.99762	OI	9 64.8
100	9.01923		9.02162		0.97838	9.99761	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

6,							113	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.01923	72	9.02162	77.2	0.97838	9.99761	100	F0
OI	9.01996	73	9.02235	73	0.97765	9.9976τ	99	73
02	9.02067	71 72	9.02308	73 72	0.97692	9.99760	98	I 7.3 2 14.6
03	9.02139	72	9.02380	73	0.97620	9.99759	97	3 21.9
04	9.02211		9.02453		0.97547	9.99758	96	4 29.2
05	9.02283	72 71	9.02525	72 72	0.97475	9.99757	95	5 36.5 6 43.8
06	9.02354	71	9.02597	73	0.97403	9.99757	94	
07	9.02425	72	9.02670	72	0.97330	9.99756	93	8 58.4
o8	9.02497	71	9.02742	71	0.97258	9.99755	92	9 65.7
09	9.02568	71	9.02813	72	0.97187	9.99754	91	72 71
10	9.02639	71	9.02885	72	0.97115	9.99753	90	I 7.2 7.1
11	9.02710		9.02957		0.97043	9.99753	89	2 14.4 14.2 3 21.6 21.3
12	9.02780	70	9.03028	71	0.96972	9.99752	88	4 28.8 28.4
13	9.02851	7I 70	9.03100	72 71	0.96900	9.99751	87	5 36.0 35.5
14	9.02921		9.03171		0.96829	9.99750	86	
15	9.02992	71 70	9.03242	71 72	0.96758	9.99749	85	7 50.4 49.7 8 57.6 56.8
16	9.03062	70	9.03314	71	0.96686	9.99749	84	9 64.8 63.9
17	9.03132	70	9.03385		0.96615	9.99748	83	70
18	9.03202	70	9.03455	70 71	0.96545	9.99747	82	I 7.0
19	9.03272	70	9.03526	71	0.96474	9.99746	81	2 14.0
20	9.03342	70	9.03597	70	0.96403	9.99745	80	3 21.0
21	9.03412		9.03667	, ,	0.96333	9.99744	79	4 28.0 5 35.0
22	9.03481	69 70	9.03738	7I 70	0.96262	9.99744	78	6 42.0
23	9.03551	69	9.03808	70	0.96192	9.99743	77	7 40.0 8 56.0
24	9.03620	1	9.03878		0.96122	9.99742	76	8 50.0 9 63.0
25	9.03690	70 69	9.03948	70 70	0.96052	9.99741	75	69 68
26	9.03759	69	9.04018	70	0.95982	9.99740	74	1 6.9 6.8
27	9.03828	69	9.04088	70	0.95912	9.99739	73	2 13.8 13.6
28	9.03897	69	9.04158	70	0.95842	9.99739	72	3 20.7 20.4
29	9.03966	68	9.04228	69	0.95772	9.99738	71	4 27.6 27.2 5 34.5 34.0
30	9.04034	69	9.04297	70	0.95703	9.99737	70	6 41.4 40.8
31	9.04103	68	9.04367	69	0.95633	9.99736	69	7 48.3 47.6 8 55.2 54.4
32	9.04171	69	9.04436	69	0.95564	9.99735	68	8 55.2 54.4 9 62.1 61.2
33	9.04240	68	9.04505	69	0.95495	9.99734	67	67
34	9.04308	68	9.04574	69	0.95426	9.99734	66	1 6.7
35	9.04376	68	9.04643	69	0.95357	9.99733	65	2 13.4
36	9.04444	68	9.04712	69	0.95288	9.99732	64	3 20.I
37	9.04512	68	9.04781	69	0.95219	9.99731	63	4 26.8
38	9.04580	68	9.04850	68	0.95150	9.99730	62	5 33.5 6 40.2
39	9.04648	67	9.04918	69	0.95082	9.99729	61	7 46.9
40	9.04715	68	9.04987	68	0.95013	9.99728	60	
41	9.04783	67	9.05055	69	0.94945	9.99728	59	9 60.3
42	9.04850	68	9.05124	68	0.94876	9.99727	58	66
43	9.04918	67	9.05192	68	0.94808	9.99726	57	I 6.6 2 13.2
44	9.04985	67	9.05260	68	0.94740	9.99725	56	2 13.2 3 19.8
45	9.05052	67	9.05328	68	0.94672	9.99724	55	4 26.4
46	9.05119	67	9.05396	67	0.94604	9.99723	54	5 33.0 6 39.6
47	9.05186	67	9.05463	68	0.94537	9.99723	53	
48	9.05253	66	9.05531	68	0.94469	9.99722	52 51	8 52.8
49	9.05319	67	9.05599	67	0.94401	9.99721	50	9 59.4
50	9.05386		9.05666		0.94334	9.99720	-00	D. D.
1	Cos	d.	Cot	d. c.	Tan	Sin	I	P. P.

8,							173°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.05386	66	9.05666	67	0.94334	9.99720	50	
51	9.05452	67	9.05733	68	0.94267	9.99719	49	68
52	9.05519	66	9.05801	67	0.94199	9.99718	48	1 6.8 2 13.6
53	9.05585	66	9.05868	67	0.94132	9.99717	47	3 20.4
54	9.05651	66	9.05935	67	0.94065	9.99716	46	4 27.2
55	9.05717	66	9.06002	66	0.93998	9.99716	45	5 34.0 6 40.8
56	9.05783	66	9.06068	67	0.93932	9.99715	44	
57	9.05849	66	9.06135	67	0.93865	9.99714	43	8 54.4
58	9.05915	65	9.06202	66	0.93798	9.99713	42	9 61.2
59	9.05980	66	9.06268	67	0.93732	9.99712	41	67 66
60	9.06046	66	9.06335	66	0.93665	9.99711	40	I 6.7 6.6
61	9.06112	65	9.06401	66	0.93599	9.99710	39	2 13.4 13.2 3 20.1 19.8
62	9.06177	65	9.06467	67	0.93533	9.99709	38	4 26.8 26.4
63	9.06242	65	9.06534	66	0.93466	9.99709	37	5 33.5 33.0
64	9.06307	65	9.06600	66	0.93400	9.99708	36	
65	9.06372	65	9.06666	65	0.93334	9.99707	35	8 53.6 52.8
66	9.06437	65	9.06731	66	0.93269	9.99706	34	9 60.3 59.4
67	9.06502	65	9.06797	66	0.93203	9.99705	33	65
68	9.06567	65	9.06863	65	0.93137	9.99704	32	1 6.5
69	9.06632	64	9.06928	66	0.93072	9.99703	31	2 13.0
70	9.06696	65	9.06994	65	0.93006	9.99702	30	3 19.5
71	9.06761	64	9.07059	65	0.92941	9.99701	29	4 26.0 5 32.5
73	9.06825	64	9.07124	66	0.92876	9.99701	28	6 39.0
73	9.06889	65	9.07190	65	0.92810	9.99700	27	7 45.5 8 52.0
74	9.06954	64	9.07255	65	0.92745	9.99699	26	8 52.0 9 58.5
75	9.07018	64	9.07320	65	0.92680	9.99698	25	
76	9.07082	63	9.07385	64	0.92615	9.99697	24	1 64 63 1 6.4 6.3
77	9.07145	64	9.07449	65	0.92551	9.99696	23	2 12.8 12.6
78	9.07209	64	9.07514	65	0.92486	9.99695	22	3 19.2 18.9
79	9.07273	64	9.07579	64	0.92421	9.99694	31	4 25.6 25.2 5 32.0 31.5
80	9.07337	63	9.07643	65	0.92357	9.99693	20	5 32.0 31.5 6 38.4 37.8
81	9.07400	64	9.07708	64	0.92292	9.99693	19	7 44.8 44.I 8 51.2 50.4
82	9.07464	63	9.07772	64	0.92228	9.99692	18	8 51.2 50.4 9 57.6 56.7
83	9.07527	63	9.07836	64	0.92164	9.99691	17	62
84	9.07590	63	9.07900	64	0.92100	9.99690	16	I 6.2
85 86	9.07653	63	9.07964	64	0.92036	9.99689	15	2 12.4
	9.07716	63	9.08028	64	0.91972	9.99688	14	3 18.6
87 88	9.07779	63	9.08092 9.08156	64	0.91908	9.99687	13	4 24.8 5 31.0
89	9.07842	63	9.08150	64	0.91844	9.99686 9.99685	12 11	6 37.2
90		63	9.08283	63			10	7 43.4
	9.07968	62		64	0.91717	9.99684		8 49.6 9 55.8
91	9.08030	63	9.08347	63	0.91653	9.99683	o9 o8	61
92 93	9.08093	62	9.08474	64	0.91590 0.91526	9.99682 9.99682	08 07	
		62		63				I 6.I 2 12.2
94 95	9.08217	63	9.08537 9.08600	63	0.91463	9.99681 9.99680	o6 . 05	3 18.3
95	9.08342	62	9.08663	63	0.91337	9.99679	04	4 24.4
97	9.08404	62	9.08726	63		9.99678		4 24.4 5 30.5 6 36.6
97 98	9.08466	62	9.08720	63	0.91274	9.99678	03	7 42.7
99	9.08528	62	9.08769	63	0.91211	9.99676	01	8 48.8
100	9.08589	61	9.08914	62	0.91086	9.99675	00	9 54.9
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
	COS	u.	COt	u. c.	Idfi	Sin		r.r.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.08589		9.08914		0.91086	9.99675	100	
01	9.08651	62	9.08977	63	0.91023	9.99674	99	63
02	9.08713	62	9.00977	63	0.90960	9.99673	98	I 6.3 2 12.6
03	9.08774	61	9.09102	62	0.90898	9.99672	97	2 12.6 3 18.9
04	9.08836	62	9.09164	62	0.90836	9.99671	96	4 25.2
05	9.08897	61	9.09227	63	0.90773	9.99670	95	5 31.5
06	9.08958	61 61	9.09289	62 62	0.90711	9.99669	94	
07	9.09019		9.09351		0.90649	9.99669	93	7 44. I 8 50.4
08	9.09080	61 61	9.09413	62 62	0.90587	9.99668	92	9 56.7
09	9.09141	61	9.09475	62	0.90525	9.99667	91	62
10	9.09202	61	9.09537	61	0.90463	9.99666	90	I 6.2
11	9.09263		9.09598		0.90402	9.99665	89	2 12.4 3 18.6
12	9.09324	61	9.09660	62 62	0.90340	9.99664	88	4 24.8
13	9.09385	60	9.09722	61	0.90278	9.99663	87	5 31.0
14	9.09445	61	9.09783	62	0.90217	9.99662	86	6 37.2 7 43.4
15	9.09506	60	9.09845	61	0.90155	9.99661	85	7 43.4 8 49.6
16	9.09566	60	9.09906	61	0.90094	9.99660	84	9 55.8
17	9.09626	60	9.09967	61	0.90033	9.99659	83	61
18	9.09686	61	9.10028	61	0.89972	9.99658	82	1 6.1
19	9.09747	60	9.10089	61	0.89911	9.99657	81	2 12.2
20	9.09807	60	9.10150	61	0.89850	9.99656	80	3 18.3 4 24.4
21	9.09867	1	9.10211	ķ	0.89789	9.99655	79	5 30.5
22	9.09926	59 60	9.10272	61 61	0.89728	9.99654	78	5 30.5 6 36.6
23	9.09986	60	9.10333	61	0.89667	9.99653	77	7 42.7 8 48.8
24	9.10046	60	9.10394		0.89606	9.99652	76	9 54.9
25	9.10106		9.10454	60 61	0.89546	9.99651	75	60
26	9.10165	59 60	9.10515	60	0.89485	9.99650	74	I 6.0
27	9.10225	59	9.10575	60	0.89425	9.99649	73	2 12.0
28	9.10284	59	9.10635	61	0.89365	9.99648	72	3 18.0
29	9.10343	59	9.10696	60	0.89304	9.99648	71	4 24.0 5 30.0
30	9.10402	60	9.10756	60	0.89244	9.99647	70	5 30.0 6 36.0
31	9.10462	59	9.10816	60	0.89184	9.99646	69	7 42.0
32	9.10521	5 9	9.10876	60	0.89124	9.99645	68	
33	9.10580	58 58	9.10936	60	0.89064	9.99644	67	9 54.0
34	9.10638	59	9.10996	60	0.89004	9.99643	66	59
35	9.10697	59	9.11056	59	0.88944	9.99642	65	I 5.9 2 II.8
36	9.10756	59	9.11115	60	0.88885	9.99641	64	3 17.7
37	9.10815	58	9.11175	59	0.88825	9.99640	63	4 23.6
38	9.10873	59	9.11234	60	0.88766	9.99639	62	5 29.5 6 35.4
39	9.10932	58	9.11294	59	0.88706	9.99638	61	
40	9.10990	58	9.11353	60	0.88647	9.99637	60	8 47.2
41	9.11048	59	9.11413	59	0.88587	9.99636	59	9 53.1
42	9.11107	58	9.11472	59	0.88528	9.99635	58	58
43	9.11165	58	9.11531	59	0.88469	9.99634	57	1 5.8 2 11.6
44	9.11223	58	9.11590	59	0.88410	9.99633	56	3 17.4
45	9.11281	58	9.11649	59	0.88351	9.99632	55	4 23.2
46	9.11339	58	9.11708	59		9.99631	54	5 29.0 6 34.8
47	9.11397	57	9.11767	59	0.88233	9.99630	53	
48	9.11454	58	9.11826	58	0.88174	9.99629 9.99628	52 51	8 46.4
49		58		59	0.88057		50	9 52.2
50	9.11570		9.11943	1 -		9.99627	-	D D
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

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_	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
50	9.11570	57	9.11943	58	0.88057	9.99627	50	59
51	9.11627	58	9.12001	59	0.87999	9.99626	49	1 5.9
52	9.11685		9.12060	* 58	0.87940	9.99625	48	1 5.9 2 11.8
53	9.11742	57 57	9.12118	59	0.87882	9.99624	47	3 17.7 4 23.6
54	9.11799	58	9.12177	58	0.87823	9.99623	46	4 23.6 5 29.5
55	9.11857	57	9.12235	58	0.87765	9.99622	45	6 35.4
56	9.11914	57	9.12293	58	0.87707	9.99621	44	7 41.3 8 47.2
57	9.11971	57	9.12351	58	0.87649	9.99620	43	8 47.2 9 53.1
58	9.12028	57	9.12409	58	0.87591	9.99619	42	58
59	9.12085	57	9.12467	58	0.87533	9.99618	41	
60	9.12142	56	9.12525	58	0.87475	9.99617	40	I 5.8 2 II.6
6r	9.12198	57	9.12583	57	0.87417	9.99616	39	3 17.4
62	9.12255	57	9.12640	58	0.87360	9.99615	38	4 23.2
63	9.12312	56	9.12698	58	0.87302	9.99614	37	5 29.0 6 34.8
64	9.12368	57	9.12756	57	0.87244	9.99613	36	7 40.6 8 46.4
65 66	9.12425	56	9.12813	57	0.87187	9.99612	35	
	9.12481	56	9.12870	58	0.87130	9.99611	34	9 52.2
67 68	9.12537	57	9.12928	57	0.87072	9.99610	33	57
69	9.12594 9.12650	56	9.12985	57	0.87015	9.99609	32	I 5.7
70		56	9.13042	57		9.99608	31	2 II.4 3 I7.I
	9.12706	56	9.13099	57	0.86901	9.99607	30	4 22.8
71	9.12762	56	9.13156	57	0.86844	9.99606	29	5 28.5
72	9.12818 9.12874	56	9.13213	57	0.86787	9.99605	28	6 34.2
73		56	9.13270	57	0.86730	9.99604	27	7 39.9 8 45.6
74	9.12930	55	9.13327	57	0.86673	9.99603	26	9 51.3
75 76	9.12985 9.13041	56	9.13384	57	0.86616	9.99601	25	56
		56	9.13441	56	0.86559	9.99600	24	I 5.6
77 78	9.13097 9.13152	55	9.13497	57	o.86503 o.86446	9.99599	23	2 11.2
79	9.13132	56	9.13554 9.13610	56	0.86390	9.99598 9.99597	22 21	3 16.8
80	9.13263	55	9.13667	57	0.86333		20	4 22.4 5 28.0
81		55		56		9.99596		6 33.6
82	9.13318 9.13373	55	9.13723	56	0.86277	9.99595	19 18	7 39.2 8 44.8
83	9.133/3	56	9.13779 9.13835	56	0.86165	9.99594 9.99593	17	8 44.8 9 50.4
84	9.13484	55	9.13892	57	0.86108		16	
85	9.13404	55	9.13092	56	0.86052	9.99592 9.99591	15	55
86	9.13594	55	9.13946	56	0.85996	9.99591	14	I 5.5 2 II.0
87	9.13649	55	9.14060	56	0.85940	9.99590	13	3 16.5
88	9.13049	54	9.14115	55	0.85885	9.99588	13	4 22.0
89	9.13758	55	9.14171	56	0.85829	9.99587	11	5 27.5 6 33.0
90	9.13813	55	9.14227	56	0.85773	9.99586	10	7 38.5 8 44.0
91	9.13867	54	9.14283	56	0.85717	9.99585	09	
92	9.13922	55	9.14203	55	0.85662	9.99584	08	9 49.5
93	9.13976	54 55	9.14394	56 55	0.85606	9.99583	07	54
94	9.14031		9.14449		0.85551	9.99582	06	I 5.4 2 IO.8
95	9.14085	54 54	9.14504	55 56	0.85496	9.99581	05	3 16.2
96	9.14139	54	9.14560	55	0.85440	9.99580	04	4 21.6
97	9.14193	55	9.14615	55	0.85385	9.99578	03	5 27.0 6 32.4
98	9.14248	54	9.14670	55	0.85330	9.99577	02	
99	9.14302	54	9.14725	55	0.85275	9.99576	01	8 43.2
100	9.14356		9.14780		0.85220	9.99575	00	9 48.6
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00		<u>u.</u>	9.14780		0.85220	9.99575	100	1.1.
	9.14356	53		55				
0I 02	9.14409	54	9.14835 9.14890	55	0.85165	9.99574	99 98	55
03	9.14463 9.14517	54	9.14945	55	0.85055	9.99573 9.99572	97	I 5.5
_		54	9.15000	55	0.85000	9.99571	96	2 II.0 3 16.5
04 05	9.14571 9.14624	53	9.15054	54	0.83000	9.99571	95	4 22.0
06	9.14678	54	9.15109	55	0.84891	9.99569	94	5 27.5
07	9.14731	53	9.15164	55	0.84836	9.99568	93	6 33.0 7 38.5
08	9.14785	54	9.15218	54	0.84782	9.99567	92	7 38.5 8 44.0
09	9.14838	53	9.15273	55	0.84727	9.99566	91	9 49.5
10	9.14891	53	9.15327	54	0.84673	9.99565	90	
11	9.14945	54	9.15381	54	0.84619	9.99563	89	54
12	9.14998	53	9.15435	54	0.84565	9.99562	88	
13	9.15051	53 53	9.15490	55 54	0.84510	9.99561	87	I 5.4 2 10.8
14	9.15104	-	9.15544		0.84456	9.99560	86	3 16.2
15	9.15157	53	9.15598	54 54	0.84402	9.99559	85	4 21.6
16	9.15210	53 53	9.15652	54 54	0.84348	9.99558	84	5 27.0 6 32.4
17	9.15263		9.15706	54	0.84294	9.99557	83	7 37.8 8 43.2
18	9.15315	52 53	9.15760	54	0.84240	9.99556	82	8 43.2
19	9.15368	53	9.15813	54	0.84187	9.99555	81	9 48.6
20	9.15421	52	9.15867	54	0.84133	9.99554	80	
21	9.15473		9.15921		0.84079	9.99553	79	53
22	9.15526	53 52	9.15974	53 54	0.84026	9.99552	78	
23	9.15578	52	9.16028	53	0.83972	9.99550	77	2 10.6
24	9.15631	52	9.16081	54	0.83919	9.99549	76	3 15.9
25	9.15683	52	9.16135	53	0.83865	9.99548	75	4 2I.2 5 26.5
26	9.15735	52	9.16188	53	0.83812	9.99547	74	5 26.5 6 31.8
27	9.15787	53	9.16241	54	0.83759	9.99546	73	7 37.1 8 42.4
28	9.15840	52	9.16295	53	0.83705	9.99545	72	8 42.4 9 47.7
29	9.15892	52	9.16348	53	0.83652	9.99544	71	9 41.1
30	9.15944	51	9.16401	53	0.83599	9.99543	70	
31	9.15995	52	9.16454	53	0.83546	9.99542	69	52
32	9.16047	52	9.16507	53	0.83493	9.99540	68	1 5.2
33	9.16099	52	9.16560	53	0.83440	9.99539	67	2 10.4
34	9.16151	52	9.16613	52	0.83387	9.99538	66	3 15.6
35	9.16203	51	9.16665	53	0.83335	9.99537	65	4 20.8 5 26.0 6 31.2
36	9.16254	52	9.16718	53	0.83282	9.99536	64	
37	9.16306	51	9.16771	52	0.83229	9.99535	63	7 36.4 8 41.6
38	9.16357 9.16409	52	9.16823	53	0.83177	9.99534	62 61	9 46.8
39		51		52		9.99533	60	
40	9.16460	51	9.16928	53	0.83072	9.99532		
41	9.16511	52	9.16981	52	0.83019	9.99530	59	51
42	9.16563 9.16614	51	9.17033	52	o.82967 o.82915	9.99529 9.99528	58 57	I 5.I
43		51	9.17085	53				2 IO.2 3 I5.3
44	9.16665 9.16716	51	9.17138	52	0.82862	9.99527	56 55	4 20.4
45 46	9.16767	51	9.17190 9.17242	52	0.82810	9.99526 9.99525	55 54	5 25.5 6 30.6
	9.10707	51		52	0.82756			6 30.6
47 48	9.16869	51	9.17294 9.17346	52	0.82700	9.99524 9.99523	53 52	7 35.7 8 40.8
49	9.16619	50	9.17340	52	0.82602	9.99521	51 51	9 45.9
50	9.16979	51	9.17390	52	0.82550	9.99520	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
000	Cus	u.	COL	а. с.	Idli	OIII	010	1.1.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.16970		9.17450		0.82550	9.99520	50	
51	9.17021	51	9.17502	52	0.82498	9.99519	49	
52	9.17072	51	9.17553	51	0 82447	9.99518	48	52
53	9.17122	50 51°	9.17605	52 52	0.82395	9.99517	47	I 5.2 2 10.4
54	9.17173	-	9.17657	-	0.82343	9.99516	46	3 15.6
55	9.17223	50 50	9.17708	51 52	0.82292	9.99515	45	4 20.8
56	9.17273	51	9.17760	51	0.82240	9.99514	44	5 26.0 6 31.2
57	9.17324	50	9.17811	52	0.82189	9.99512	43	7 36.4 8 41.6
58	9.17374	50	9.17863	51	0.82137	9.99511	42	
59	9.17424	50	9.17914	51	0.82086	9.99510	41	9 46.8
60	9.17474	50	9.17965	52	0.82035	9.99509	40	
61	9.17524	51	9.18017	51	0.81983	9.99508	39	51
62	9.17575	49	9.18068	51	0.81932	9.99507	38	I 5.I
63	9.17624	50	9.18119	51	0.81881	9.99505	37	2 10.2
64	9.17674	50	9.18170	51	0.81830	9.99504	36	3 15.3
65	9.17724	50	9.18221	51	0.81779	9.99503	35	4 20.4 5 25.5
66	9.17774	50	9.18272	51	0.81728	9.99502	34	6 30.6
67	9.17824	49	9.18323	51	0.81677	9.99501	33	7 35·7 8 40.8
68 69	9.17873	50	9.18374	5i	0.81626	9.99500	32 31	9 45.9
70	9.17923	50		50		9.99499	30	3 1 43.9
	9.17973	49	9.18475	51	0.81525	9.99497	-	
71	9.18022	50	9.18526	51	0.81474	9.99496	29	50
72	9.18072	49	9.18577	50	0.81423	9.99495	28	I 5.0
73	9.18121	49	9.18627	51	0.81373	9.99494		2 10.0
74	9.18170	50	9.18678	50	0.81322	9.99493	26	3 I5.0 4 20.0
75 76	9.18220 9.18269	49	9.18728 9.18778	50	0.81272	9.99492	25 24	
		49		51		9.99490		5 25.0 6 30.0
77 78	9.18318 9.18367	49	9.18829	50	0.81171	9.99489	23	7 35.0 8 40.0
79	9.18416	49	9.18929	50	0.81071	9.99488	21	9 45.0
80	9.18465	49	9.18979	50	0.81021	9.99486	20	
81		49		50				
82	9.18514	49	9.19029	51	0.80971	9.99485 9.99483	19	49
83	9.18612	49	9.19030	50	0.80870	9.99483	17	I 4.9
84	9.18661	49	9.19179	49	0.80821	9.99481	16	2 9.8 3 14.7
85	9.18709	48	9.19179	50	0.80771	9.99480	15	4 19.6
86	9.18758	49	9.19279	50	0.80721	9.99479	14	5 24.5 6 29.4
87	9.18806	48	9.19329	50	0.80671	9.99477	13	
88	9.18855	49	9.19379	50	0.80621	9.99476	12	8 39.2
89	9.18904	49 48	9.19428	49 50	0.80572	9.99475	11	9 44.1
90	9.18952	48	9.19478	50	0.80522	9.99474	10	
91	9.19000		9.19528	-	0.80472	9.99473	09	48
92	9.19049	49 48	9.19577	49 50	0.80423	9.99472	08	1 4.8
93	9.19097	48	9.19627	49	0.80373	9.99470	07	2 9.6
94	9.19145	48	9.19676	49	0.80324	9.99469	06	3 14.4 4 19.2
95	9.19193	48	9.19725	50	0.80275	9.99468	05	4 19.2 5 24.0
96	9.19241	48	9.19775	49	0.80225	9.99467	04	6 28.8
97	9.19289	48	9.19824	49	0.80176	9.99466	03	7 33.6 8 38.4
98	9.19337	48	9.19873	49	0.80127	9.99464	02	9 43.2
99	9.19385	48	9.19922	49	0.80078	9.99463	OI	
100	9.19433		9.19971		0.80029	9.99462	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

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	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.19433	48	9.19971	49	0.80029	9.99462	100	
or	9.19481	48	9.20020	1	0.79980	9.99461	99	
02	9.19529	48	9.20069	49 49	0.79931	9.99460	98	49
03	9.19577	47	9.20118	49	0.79882	9.99458	97	I 4.9 2 9.8
04	9.19624	48	9.20167	49	0.79833	9.99457	96	2 9.8
05	9.19672	47	9.20216	49	0.79784	9.99456	95	3 14.7 4 19.6
06	9.19719	48	9.20265	48	0.79735	9.99455	94	5 24.5
07	9.19767	47	9.20313	49	0.79687	9.99454	93	6 29.4
08	9.19814	48	9.20362	49	0.79638	9.99452	92	7 34·3 8 39·2
09	9.19862	47	9.20411	48	0.79589	9.99451	91	9 44.1
10	9.19909	47	9.20459	49	0.79541	9.99450	90	
11	9.19956	48	9.20508	48	0.79492	9.99449	89	48
12	9.20004	47	9.20556	49	0.79444	9.99447	88	1 4.8
13	9.20051	47	9.20605	48	0.79395	9.99446	87	2 9.6
14	9.20098	47	9.20653	48	0.79347	9.99445	86	3 14.4
15 16	9.20145	47	9.20701 9.20750	49	0.79299	9.99444	85 84	4 19.2 5 24.0 6 28.8
17	9.20192	47	9.20798	48	0.79202	9.99443	83	
18	9.20239	47	9.20798	48	0.79202	9.99441	82	7 33.6
19	9.20333	47	9.20894	48	0.79106	9.99440	81	8 38.4 9 43.2
20	9.20380	47	9.20942	48	0.79058	9.99438	80	3 1 43.2
21	9,20427	47	9.20990	48	0.79010	9.99436	79	
22	9.20427	46	9.20990	48	0.78962	9.99430	79	47
23	9.20520	47	9.21086	48	0.78914	9.99433	77	I 4.7
24	9.20567	47	9.21134	48	0.78866	9.99433	76	2 9.4 3 14.1
25	9.20613	46	9.21182	48	0.78818	9.99433	75	4 18.8
26	9.20660	47 46	9.21229	47 48	0.78771	9.99430	74	5 23.5 6 28.2
27	9.20706	46	9.21277	48	0.78723	9.99429	73	
28	9.20752	47	9.21325	47	0.78675	9.99428	72	8 37.6
29	9.20799	46	9.21372	48	0.78628	9.99427	71	9 42.3
30	9.20845	46	9.21420	47	0.78580	9.99425	70	
31	9.20891	47	9.21467	48	0.78533	9.99424	69	46
32	9.20938	46	9.21515	47	0.78485	9.99423	68	1 4.6
33	9.20984	46	9.21562	48	0.78438	9.99422	67	2 9.2
34	9.21030	46	9.21610	47	0.78390	9.99420	66	3 13.8 4 18.4
35	9.21076	46	9.21657	47	0.78343	9.99419	65	5 23.0
36	9.21122	46	9.21704	47	0.78296	9.99418	64	
37	9.21168	46	9.21751	47	0.78249	9.99417	63	7 32.2 8 36.8
38	9.21214	46	9.21798	48	0.78202	9.99415	62	9 41.4
39 40	9.21260	46	9.21846	47	0.78154	9.99414	61	
	9.21306	45	9.21893	47	0.78107	9.99413	60	45
41	9.21351	46	9.21940	47	0.78060	9.99412	59	I 4.5
42 43	9.21397	46	9.21987	47	0.78013	9.99410	58	2 9.0
		45		46		9.99409	57	3 13.5
44 45	9.21488	46	9.22080	47	0.77920	9.99408 9.99407	56 55	4 18.0 5 22.5
46	9.21534	45	9.22174	47	0.77826	9.99407	55 54	6 27.0
47	9.21625	46	9.22221	47	0.77779	9.99404	53	7 31.5
48	9.21625	45	9.22221	46	0.77733	9.99404	52	8 36.0 9 40.5
49	9.21716	46 45	9.22314	47 47	0.77686	9.99403	51	9 40.3
50	9.21761	43	9.22361	47	0.77639	9.99400	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		ч.	000	4. 0.	Lan	OIII		1.1.

	C:-	3	Т	d a	Cot	Cos		P. P.
	Sin	d.	Tan	d. c.				P. P.
50	9.21761	45	9.22361	46	0.77639	9.99400	50	
51	9.21806	45	9.22407	47	0.77593	9.99399	49	47
52	9.21851	46	9.22454	46	0.77546	9.99398	48 47	I 4.7
53		45		47				2 9.4
54	9.21942	45	9.22547	46	0.77453	9.99395	46	3 14.1
55 56	9.21987	45	9.22593 9.22639	46	0.77407	9.99394 9.99393	45 44	4 18.8 5 23.5
		45	9.22685	46	1	9.99393	43	5 23.5 6 28.2
57 58	9.22077	45	9.22085	47	0.77315	9.99391	43	7 32.9
59	9.22122	45	9.22778	46	0.77222	9.99389	41	8 37.6 9 42.3
60	9.22211	44	9.22824	46	0.77176	9.99388	40	9 42.3
61		45	<u> </u>	46		9.99386	39	
62	9.22256 9.22301	45	9.22870 9.22916	46	0.77130	9.99385	38	46
63	9.22346	45	9.22962	46	0.77038	9.99384	37	I 4.6
64	9.22390	44	9.23008	46	0.76992	9.99382	36	2 9.2 3 13.8
65	9.22390	45	9.23054	46	0.76946	9.99381	35	4 18.4
66	9.22480	45	9.23100	46	0.76900	9.99380	34	5 23.0 6 27.6
67	9.22524	44	9.23146		0.76854	9.99379	33	
68	9.22568	44 45	9.23191	45 46	0.76809	9.99377	32	8 36.8
69	9.22613	45	9.23237	46	0.76763	9.99376	31	9 41.4
70	9.22657		9.23283	45	0.76717	9.99375	30	
71	9.22702	45	9.23328	45	0.76672	9.99373	29	45
72	9.22746	44	9.23374	45	0.76626	9.99372	28	I 4.5
73	9.22790	44	9.23419	46	0.76581	9.99371	27	2 9.0
74	9. 22834		9.23465	45	0.76535	9.99369	26	3 13.5
75	9.22878	44 44	9.23510	45	0.76490	9.99368	25	4 18.0 5 22.5
76	9.22922	45	9.23556	45	0.76444	9.99367	24	6 27.0
77	9.22967	44	9.23601	45	0.76399	9.99366	23	7 31.5 8 36.0
78	9.23011	43	9.23646	46	0.76354	9.99364	22	9 40.5
79	9.23054	44	9.23692	45	0.76308	9.99363	21	3 1 4-13
80	9.23098	44	9.23737	45	0.76263	9.99362	20	
81	9.23142	44	9.23782	45	0.76218	9.99360	19	44
82	9.23186	44	9.23827	45	0.76173	9.99359	18	I 4.4 2 8.8
83	9.23230	44	9.23872	45	0.76128	9.99358	17	3 13.2
84	9.23274	43	9.23917	45	0.76083	9.99356	16	4 17.6
85	9.23317	44	9.23962	45	0.76038	9.99355	15	5 22.0 6 26.4
86	9.23361	43	9.24007	45	0.75993	9.99354	14	7 30.8 8 35.2
8 ₇ 88	9.23404	44	9.24052	45	0.75948	9.99352	13	
89	9. 2 3448 9.23491	43	9.24097	45	0.75903	9.99351	11	9 39.6
90		44	9.24142	44	0.75814	9.99348	10	
	9.23535	43		45			09	43
91	9.23578	44	9.24231	45	0.75769	9.99347 9.99346	08	I 4.3 2 8.6
93	9.23622 9.23665	43	9.24276 9.24321	45	0.75724	9.99344	07	2 8.6
		43		44	0.75635	9.99344	06	3 12.9 4 17.2
94 95	9.23708 9.23752	44	9.24365 9.24410	45	0.75035	9.99343	05	5 21.5 6 25.8
95	9.23752	43	9.24454	44	0.75546	9.99342	04	
97	9.23838	43	9.24499	45	0.75501	9.99339	03	7 30.1 8 34.4
98	9.23881	43	9.24543	44	0.75457	9.99339	02	9 38.7
99	9.23924	43	9.24588	45 44	0.75412	9.99336	01	
100	9.23967	43	9.24632	44	0.75368	9.99335	00	
-	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

10							109	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.23967	43	9.24632	44	0.75368	9.99335	100	
01	9.24010		9.24676		0.75324	9.99334	99	
02	9.24053	43 43	9.24720	44 45	0.75280	9.99332	98	
03	9.24096	43	9.24765	45	0.75235	9.99331	97	44
04	9.24139	42	9.24809		0.75191	9.99330	96	I 4.4
05	9.24181	43	9.24853	44 44	0.75147	9.99328	95	2 8.8
06	9.24224	43	9.24897	44	0.75103	9.99327	94	3 13.2
07	9.24267	43	9.24941		0.75059	9.99326	93	4 17.6
08	9.24310	43 42	9.24985	44 44	0.75015	9.99324	92	5 22.0
09	9.24352	43	9.25029	44	0.74971	9.99323	91	6 26.4
10	9.24395	42	9.25073	44	0.74927	9.99322	90	7 30.8 8 35.2
11	9.24437	43	9.25117		0.74883	9.99320	89	8 35.2 9 39.6
12	9.24480	43 42	9.25161	44 44	0.74839	9.99319	88	9 1 39.0
13	9.24522	42	9.25205	44	0.74795	9.99318	87	
14	9.24565	43	9.25248		0.74752	9.99316	86	
15	9.24607	42	9.25292	44 44	0.74708	9.99315	85	43
16	9.24649	43	9.25336	44	0.74664	9.99314	84	I 4.3
17	9.24692	42	9.25379	1	0.74621	9.99312	83	2 8.6
18	9.24734	42	9.25423	44 43	0.74577	9.99311	82	3 12.9
19	9.24776	42	9.25466	43	0.74534	9.99310	81	4 17.2
20	9.24818	42	9.25510	43	0.74490	9.99308	80	5 21.5
21	9.24860	42	9.25553		0.74447	9.99307	79	
22	9.24902	42	9.25597	44 43	0.74403	9.99305	78	7 30.1 8 34.4
23	9.24944	42	9.25640	43	0.74360	9.99304	77	9 38.7
24	9.24986	42	9.25684		0.74316	9.99303	76	9 30.7
25	9.25028	42	9.25727	43 43	0.74273	9.99301	75	
26	9.25070	42	9.25770	43	0.74230	9.99300	74	
27	9.25112	42	9.25813	44	0.74187	9.99299	73	42
28	9.25154	42	9.25857	44	0.74143	9.99297	72	I 4.2
29	9.25196	41	9.25900	43	0.74100	9.99296	71	2 8.4
30	9.25237	42	9.25943	43	0.74057	9.99294	70	3 12.6
31	9.25279	42	9.25986	43	0.74014	9.99293	69	4 16.8
32	9.25321	42	9.26029	43	0.73971	9.99292	68	5 21.0 6 25.2
33	9.25362	42	9.26072	43	0.73928	9.99290	67	6 25.2 7 29.4
34	9.25404	41	9.26115		0.73885	9.99289	66	8 33.6
35	9.25445	41	9.26158	43	0.73842	9.99288	65	9 37.8
36	9.25487	41	9.26201	43	0.73799	9.99286	64	J - 57.0
37	9.25528	42	9.26243	43	0.73757	9.99285	63	
38	9.25570	41	9.26286	43	0.73714	9.99283	62	
39	9.25611	41	9.26329	43	0.73671	9.99282	61	41
40	9.25652	42	9.26372	42	0.73628	9.99281	60	1 4.1
41	9.25694	41	9.26414	43	0.73586	9.99279	5 9	2 8.2
42	9.25735	41	9.26457	43	0.73543	9.99278	58	3 12.3
43	9.25776	41	9.26500	42	0.73500	9.99276	57	4 16.4 5 20.5
44	9.25817	41	9.26542	43	0.73458	9.99275	56	5 20.5 6 24.6
45	9.25858	41	9.26585	43	0.73415	9.99274	55	7 28.7
46	9.25899	41	9.26627	43	0.73373	9.99272	54	8 32.8
47	9.25940	41	9.26670	42	0.73330	9.99271	53	9 36.9
48	9.25981	41	9.26712	42	0.73288	9.99269	52	
49	9.26022	41	9.26754	43	0.73246	9.99268	51	
50	9.26063		9.26797		0.73203	9.99267	50	
	Cos	d.	Cot	d.c.	Tan	Sin	l .	P. P.

							109	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.26063	41	9.26797	42	0.73203	9.99267	50	
51	9.26104	41	9.26839	42	0.73161	9.99265	49	
52	9.26145	41	9.26881	42	0.73119	9.99264	48	
53	9.26186	41	9.26923	43	0.73077	9.99262	47	43
54	9.26227		9.26966		0.73034	9.99261	46	I 4.3
55	9.26267	40 41	9.27008	42 42	0.72992	9.99260	45	2 8.6
56	9.26308	41 4I	9.27050	42	0.72950	9.99258	44	3 12.9
57	9.26349		9.27092		0.72908	9.99257	43	4 17.2
58	9.26389	40 41	9.27134	42 42	0.72866	9.99255	42	5 21.5 6 25.8
59	9.26430	40	9.27176	42	0.72824	9.99254	41	6 25.8 7 30.1
60	9.26470		9.27218		0.72782	9.99252	40	8 34.4
61	9.26511	41	9.27260	42	0.72740	9.99251	39	9 38.7
62	9.26551	40	9.27302	42	0.72698	9.99250	38	3 1 0-11
63	9.26592	41	9.27343	41	0.72657	9.99248	37	
64	9.26632	40	9.27385	42	0.72615	9.99247	36	
65	9.26672	40	9.27427	42	0.72573	9.99245	35	42
66	9.26713	41	9.27469	42	0.72531	9.99244	34	I 4.2
67	9.26753	40	9.27510	41	0.72490	9.99243	33	2 8.2
68	9.26793	40	9.27552	42	0.72448	9.99243	32	3 12.6
69	9.26833	40	9.27594	42	0.72406	9.99240	31	4 16.8
70	9.26873	40	9.27635	41	0.72365	9.99238	30	5 21.0
		40		42			29	6 25.2
71	9.26913	41	9.27677	41	0.72323	9.99237	28	7 29.4
72	9.26954	40	9.27718	42	0.72282	9.99236	27	8 33.6
73	9.26994	40	9.27760	41	0.72240	9.99234	26	9 37.8
74	9.27034	39	9.27801	41	0.72199	9.99233	25	
75	9.27073	40	9.27842	42	0.72158	9.99231	24	
76	9.27113	40	9.27884	41	0.72116	9.99230		41
77	9.27153	40	9.27925	41	0.72075	9.99228	23	I 4.I
78	9.27193	40	9.27966	42	0.72034	9.99227	21	2 8.2
79	9.27233	40	9.28008	41	0.71992	9.99225	20	3 12.3
80	9.27273	39	9.28049	41	0.71951	9.99224		4 16.4
8r	9.27312	40	9.28090	41	0.71910	9.99222	19	5 20.5
82	9.27352	40	9.28131	41	0.71869	9.99221	18	6 24.6
83	9.27392	39	9.28172	41	0.71828	9.99220	17	7 28.7
84	9.27431	40	9.28213	41	0.71787	9.99218	16	8 32.8
85	9.27471	39	9.28254	41	0.71746	9.99217	15	9 36.9
86	9.27510	40	9.28295	41	0.71705	9.99215	14	
87	9.27550	39	9.28336	41	0.71664	9.99214	13	
88	9.27589	40	9.28377	41	0.71623	9.99212	12	40
89	9.27629	39	9.28418	41	0.71582	9.99211	11	
90	9.27668	39	9.28459	41	0.71541	9.99209	10	1 4.0
91	9.27707	40	9.28500	40	0.71500	9.99208	09	3 12.0
92	9.27747	39	9.28540	40 4I	0.71460	9.99206	08	4 16.0
93	9.27786	39	9.28581	41	0.71419	9.99205	07	5 20.0
94	9.27825		9.28622	40	0.71378	9.99203	06	6 24.0
95	9.27864	39 40	9.28662	41	0.71338	9.99202	05	7 28.0
96	9.27904	39	9.28703	41	0.71297	9.99201	04	8 32.0
97	9.27943		9.28744	40	0.71256	9.99199	03	9 36.0
98	9.27982	39 39	9.28784	41	0.71216	9.99198	02	
99	9.28021	39	9.28825	40	0.71175	9.99196	01	
100	9.28060	39	9.28865	40	0.71135	9.99195	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
	-00	4.		~·· ··		~ ***		

O		Sin	d.	Tan	d. c.	Cot	Cos		P. P.
OI	-00							100	P. P.
0.2 9.28138 3.9 9.28946 40 0.71014 9.99190 97 41			39		41				
03									
04 9.28216 38 9.29067 40 0.70973 9.99189 96 1 4.1									41
of 9.28293 39 9.29067 40 0.70933 9.99187 95 2 8.2 of 9.28332 39 9.29188 40 0.70832 9.99184 93 11.3 of 9.28409 39 9.29288 40 0.70822 9.99183 92 5 20.5									
o6 9.28293 39 9.29107 41 0.70893 9.99186 94 3 12.3 o7 9.28332 39 9.29148 40 0.70852 9.99183 93 4 16.4 o8 9.28409 39 9.29268 40 0.70732 9.99181 91 6 24.6 24.6 20.5 20									
07 9.283321 39 9.29148 40 0.70852 9.99184 93 4 16.4 20.5 20.7 20.99188 92.9 20.7 20.99178 89 90.7 28.7 20.7 20.99178 89 90.7 28.7 30.9 20.9428 40 0.70512 9.99178 89 9.99177 88 32.8 32.8 30.92948 40 0.70522 9.99178 85 40 40 40 40 40 40 40 40 40 40 40 40 40 40<									
08	07	9.28332		9.29148		0.70852			4 16.4
10 9.28448 39 9.29368 40 0.70632 9.99178 88 32.8 38 9.29348 40 0.70652 9.99178 88 9 36.	08	9.28371		9.29188		0.70812			
10 9.28487 38 9.29368 40 0.70692 9.99178 88 9 36.9 36.9 36.9 36.9 36.9 36.9 36.9 36	09	9.28409		9.29228		0.70772	9.99181	91	
11	10	9.28448		9.29268		0.70732	9.99180	90	
12	11	9.28487		9.29308		0.70692	9.99178	89	
13	12	9.28525		9.29348			9.99177		3 1 0-13
14	13	9.28564		9.29388		0.70612	9.99175	87	
15									4.0
10 9.28079 39 9.2958 40 0.70492 9.99171 84 1 4.0 17 9.28718 38 9.29588 40 0.70412 9.99168 82 3 12.0 19 9.28794 39 9.29688 40 0.70372 9.99168 82 3 12.0 20 9.28831 38 9.29688 40 0.70372 9.99168 81 4 16.0 21 9.28871 38 9.29688 39 9.29747 40 0.70253 9.99165 80 5 20.0 22 9.28994 38 9.29747 40 0.70253 9.99165 79 7 28.0 23 9.28947 38 9.29867 39 0.70134 9.99157 75 24 9.28985 39 9.29867 40 0.70134 9.99157 75 25 9.29024 38 9.29868 40 0.70034 9.99157 75 26 9.29062 38 9.29945 40 0.70034 9.99157 75 27 9.29100 38 9.29945 40 0.70055 9.99153 72 28 9.29176 38 9.30064 39 0.69976 9.99151 71 2 7.3 30 9.29214 38 9.30064 39 0.69976 9.99157 70 3 11.7 31 9.29252 37 9.30103 40 0.69987 9.99147 68 6 23.4 31 9.29252 37 9.30103 39 0.69857 9.99147 68 6 23.4 32 9.29478 38 9.30339 39 0.69616 9.99138 69 35.1 37 9.29478 38 9.30339 39 0.69661 9.99135 60 1 3.8 38 9.29516 38 9.30339 39 0.69661 9.99133 59 311.4 41 9.29629 37 9.30487 39 0.69624 9.99133 59 311.4 42 9.29667 38 9.30339 39 0.69661 9.99133 59 311.4 41 9.29629 37 9.30487 39 0.69624 9.99133 59 311.4 42 9.29667 38 9.30339 39 0.69661 9.99133 59 311.4 43 9.29774 38 9.30574 39 0.69364 9.99135 57 51 9.0 44 9.29741 38 9.30574 39 0.69367 9.99125 54 8 30.4 45 9.29876 38 9.30537 39 0.69367 9.99125 54 8 30.4 47 9.29854 37 9.30769 38 0.69367 9.99125 54 8 30.4 48 9.29891 37 9.30769 38 0.69379 9.99125 54 8 30.4 49 9.29854 37 9.30769 38 0.69379 9.99125 54 8 30.4 49 9.29876 38 9.30739 39 0.69367 9.99125 54 8									
18 9.28756 38 9.29588 40 0.70412 9.99168 82 3 12.0									
18			38		40				
20 9.28833 38 9.29668 39 9.29668 39 9.29747 40 0.70293 9.99165 80 6 24.0 28.0 29.28999 38 9.29747 40 0.70213 9.99160 77 9.28.0 28.0 24.9.28985 39 9.29866 40 0.70213 9.99160 77 9.28.0 27 9.29100 38 9.29966 40 0.70134 9.99157 75 28.0 2.20 2.20 2.20 2.20 2.20 2.20 2.20					40				
21 9.28871 38 9.29707 40 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99163 79 7 28. 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99160 77 8 32.0 0.70293 9.99159 76 9.99160 77 8 9.99160 70 9.99150 70 9.99160 7	-				40				
22 9.28909 38 9.29747 40 0.70233 9.99160 77 9 36.0 24 9.28985 39 9.29867 40 0.70213 9.99159 76 25 9.29024 38 9.29866 40 0.70134 9.99157 75 26 9.29025 38 9.29985 40 0.70055 9.99156 74 28 9.29138 38 9.29985 40 0.70055 9.99154 73 29 9.29176 38 9.30024 40 0.70055 9.99151 71 22 7.8 30 9.29214 38 9.30024 40 0.69976 9.99151 71 22 7.8 31 9.29252 37 9.30103 40 0.69976 9.99151 71 22 7.8 32 9.29289 38 9.30024 40 0.69976 9.99151 71 22 7.8 33 9.29228 37 9.30103 40 0.69976 9.99148 69 4 15.6 33 9.29289 38 9.30281 40 0.69878 9.99148 66 23.4 34 9.29365 38 9.3021 40 0.69878 9.99145 67 7 27.3 35 9.29441 37 9.30300 39 0.69978 9.99144 66 8 31.2 37 9.29478 38 9.30378 40 0.69779 9.99144 66 37 9.29478 38 9.30378 40 0.69661 9.99139 63 39 9.29554 37 9.30418 39 0.69661 9.99136 61 38 40 9.29591 38 9.30378 40 0.69661 9.99135 60 1 3.8 41 9.29629 37 9.30418 39 0.69661 9.99135 56 0 1 3.8 42 9.29669 37 9.30545 39 0.69662 9.99135 56 0 1 3.8 43 9.29704 37 9.30543 39 0.69465 9.99135 57 5 19.0 44 9.29854 37 9.30563 39 0.69465 9.99135 57 5 19.0 45 9.29719 38 9.30563 39 0.69465 9.99135 57 5 19.0 60 9.29510 38 9.30547 39 0.69465 9.99135 56 6 22.8 47 9.29854 37 9.30769 38 0.69389 9.99125 54 8 30.4 48 9.29891 37 9.30769 38 0.69370 9.99124 53 9 344.2			38		39				
23 9.28947 38 9.29787 40 0.70213 9.99160 77 9 36.0 24 9.28985 39 9.29827 39 9.29866 39 9.29965 38 9.29965 39 9.29955 38 9.29214 38 9.29252 37 9.30103 40 0.69267 9.99151 71 2 7.8 25 9.29244 38 9.29382 37 9.30103 40 0.69367 9.99147 68 62 23.4 26 9.29252 37 9.30103 40 0.69367 9.99147 68 62 23.4 27 9.29252 37 9.30103 40 0.69367 9.99153 72 1 3.9 28 9.29244 38 9.30504 39 0.69968 9.99148 69 5 19.506976 9.99148 69 5 19.506976 9.99144 66 8 31.2 27 9.29252 37 9.30103 40 0.69367 9.99145 67 7 27.3 28 9.29289 38 9.30143 39 0.69368 9.99144 66 8 31.2 29 9.29365 38 9.30221 40 0.69779 9.99144 66 8 31.2 30 9.29365 38 9.30221 40 0.69779 9.99144 66 8 31.2 31 9.29563 38 9.30378 40 0.69700 9.99141 64 9.29516 38 9.30378 40 0.69670 9.99139 63 36 9.29441 37 9.30300 39 0.69661 9.99138 62 9.99138 62 37 9.29554 38 9.30378 39 0.69661 9.99138 62 9.99138 62 38 9.29564 38 9.30574 39 0.69368 9.99135 58 3 11.4 39 9.29554 38 9.30574 39 0.69368 9.99132 58 3 11.4 40 9.29561 38 9.30574 39 0.69368 9.99132 58 3 11.4 40 9.29561 38 9.30537 39 0.69365 9.99133 59 3 11.4 41 9.29629 37 9.30467 39 0.69368 9.99135 57 5 19.0 42 9.29666 38 9.30537 39 0.69368 9.99127 55 7 26.6 43 9.29564 37 9.30769 39 0.69368 9.99127 55 7 26.6 44 9.29741 38 9.30574 39 0.69368 9.99127 55 7 26.6 45 9.29816 38 9.30573 39 0.69368 9.99127 55 7 26.6 47 9.29854 37 9.30769 38 0.69368 9.99125 54 8 30.4 48 9.29891 37 9.30769 38 0.69379 9.99125 54 8 30.4					40				
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26 9.29062 38 9.29966 39 0.70094 9.99156 74 27 9.29100 38 9.29945 40 0.70055 9.99154 73 39 28 9.29138 38 9.29945 40 0.70015 9.99153 72 1 3.9 30 9.29214 38 9.30064 39 0.69976 9.99157 71 2 7.8 31 9.29252 37 9.30103 40 0.69887 9.99147 68 69 5 19.5 32 9.29289 38 9.30123 39 0.69887 9.99144 68 5 19.5 32 9.29252 37 9.30133 39 0.69887 9.99147 68 5 19.5 5 19.5 6 23.4 69 5 19.5 6 23.4 9.99147 68 6 23.4 6 23.4 6 9.99147 68 6 23.4									
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29 9.29176 38 38 31 9.30024 9.30064 49 39 0.69976 0.69936 9.99151 9.99155 71 70 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3									1 3.9
30	29	9.29176		9.30024		0.69976			
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32 9.29289 38 9.30143 39 0.69857 9.99147 68 6 23.4 33 9.29327 38 9.30182 39 0.69858 9.99145 67 7 27.3 34 9.29365 38 9.30221 40 0.69779 9.99144 66 8 31.2 35 9.2943 38 9.30300 39 0.69709 9.99142 65 9 35.1 37 9.29478 38 9.30339 39 0.69620 9.99139 63 38 9.29516 38 9.30378 39 0.69622 9.99138 62 39 9.29554 37 9.3048 39 0.69382 9.99136 61 38 40 9.29560 38 9.30535 39 0.69384 9.99133 59 2 7 41 9.29669 37 9.30535 39 0.69465 9.99133 59 3 11.4	31	9.29252		9.30103		0.69897	9.99148	69	
33 9.29327 38 9.30382 39 0.693818 9.99145 67 7 27.3 34 9.29365 38 9.30221 40 0.69779 9.99144 66 8 31.2 35 9.29443 38 9.30300 39 0.69709 9.99141 64 37 9.29543 38 9.30339 39 0.69661 9.99139 63 39 9.29554 37 9.30448 39 9.99136 61 38 40 9.29551 38 9.30457 39 0.69622 9.99138 62 39 9.29554 37 9.30457 39 0.69584 9.99135 61 38 41 9.29669 38 9.30535 39 0.69584 9.99135 60 1 3.8 41 9.29666 38 9.30535 39 0.69504 9.99133 59 311.4 43 9.29764 37 9.3057		9.29289		9.30143					
34 9.29365 38 9.30221 40 0.69779 9.99144 66 8 31.2 35 9.29443 37 9.30300 39 0.69739 9.99144 64 37 9.29478 38 9.30378 39 0.69661 9.99139 63 38 9.29554 37 9.30418 39 0.69622 9.99138 62 40 9.29591 38 9.30487 39 0.69582 9.99135 60 1 38 41 9.29669 37 9.30547 39 0.69465 9.99133 59 3 11.4 43 9.29704 37 9.30574 39 0.69465 9.99133 59 3 11.4 44 9.29741 38 9.30652 39 0.69465 9.99133 59 3 11.5.2 45 9.29719 38 9.30652 39 0.69387 9.99128 56 622.8 45 </th <th>33</th> <th>9.29327</th> <th></th> <th>9.30182</th> <th></th> <th>0.69818</th> <th>9.99145</th> <th>67</th> <th></th>	33	9.29327		9.30182		0.69818	9.99145	67	
36 9.29441 37 9.30300 39 0.69739 9.99142 64 9.29516 38 9.30318 9.30318 39 0.69661 9.99139 63 38 9.29516 38 9.30318 39 9.29554 37 9.30418 39 0.69661 9.99139 62 9.99136 61 38 9.30418 39 9.29554 37 9.30457 39 0.69661 9.99130 61 38 9.30418 39 0.69621 9.99135 61 38 9.30418 39 0.69543 9.99135 61 38 9.30418 39 0.69543 9.99135 60 1 3.8 9.30418 39 0.69426 9.99135 59 2 7.6 9.30418 39 0.69426 9.99130 57 5 19.0 9.30418 39 0.69426 9.99130 57 5 19.0 9.30418 39 0.69426 9.99130 57 5 19.0 9.30418 43 9.29704 37 9.30574 39 0.69387 9.99128 56 6 22.8 9.99136 61 38 9.30418 39 0.69387 9.99128 56 6 22.8 9.99136 57 5 19.0 9.30418 45 9.29719 37 9.30521 39 0.69387 9.99128 56 6 22.8 9.99136 51 9.30418 45 9.29816 38 9.30591 39 0.69387 9.99125 54 8 30.4 9.29816 38 9.30730 39 0.69379 9.99125 54 8 30.4 9.29891 37 9.30769 38 0.69379 9.99125 54 8 30.4 9.29891 37 9.30769 38 0.69379 9.99125 54 8 30.4 9.29891 37 9.30769 38 0.69379 9.99125 54	34	9.29365	1 -			0.69779	9.99144		
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38									
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41 9.29629 37 9.30496 39 0.69504 9.99133 59 3 11.4 42 9.29666 38 9.30535 39 0.69465 9.99132 58 3 11.4 43 9.29704 37 9.30574 39 0.69426 9.99130 57 5 19.0 44 9.29741 38 9.30613 39 0.69387 9.99128 56 6 22.8 45 9.29779 37 9.30652 39 0.69387 9.99127 55 7 26.6 46 9.29816 38 9.30691 39 0.69309 9.99125 54 8 30.4 47 9.29854 37 9.30730 39 0.69270 9.99124 53 9 34.2 48 9.29891 37 9.30769 38 0.69231 9.99122 52			l .		39				
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43 9.29704 38 9.30513 39 0.69436 9.99132 56 4 15.2 44 9.29741 38 9.30613 39 0.69387 9.99135 57 5 19.0 45 9.29747 38 9.30652 39 0.69387 9.99127 55 7 26.6 46 9.29816 38 9.30691 39 0.69399 9.99127 55 7 26.6 47 9.29854 37 9.30730 39 0.69270 9.99125 54 8 30.4 48 9.29891 37 9.30769 38 0.69231 9.99122 52					39				
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49 9.29928 38 9.30807 39 0.09193 9.99121 51	49	9.29928		9.30807		0.69193	9.99121	51	
50 9.29966 9.30846 0.69154 9.99119 50	50	9.29966	30	9.30846	39	0.69154	9.99119	50	
Cos d. Cot d. c. Tan Sin P. P.			d.		d. c.				P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50		u.	9.30846	u. c.			50	T. F.
	9.29966	37		39	0.69154	9.99119		
21	9.30003	37	9.30885	39	0.69115	9.99118	49	
52	9.30040	37	9.30924	39	0.69076 0.69037	9.99116	48	38
53	9.30077	37	9.30963	38		9.99115	47	
54	9.30114	37	9.31001	39	0.68999	9.99113	46	1 3.8
55	9.30151	37	9.31040	38	0.68960	9.99112	45	2 7.6 3 11.4
56	9.30188	38	9.31078	39		9.99110	44	3 II.4 4 I5.2
57	9.30226	37	9.31117	39	0.68883	9.99108	43	5 19.0
58	9.30263	36	9.31156	38	o.68844 o.68866	9.99107	42 41	6 22.8
59	9.30299	37	9.31194	39		9.99105		7 26.6
60	9.30336	37	9.31233	38	0.68767	9.99104	40	8 30.4
61	9.30373	37	9.31271	39	0.68729	9.99102	39	9 34.2
62	9.30410	37	9.31310	38	0.68690	9.99101	38	
63	9.30447	37	9.31348	38	0.68652	9.99099	37	
64	9.30484	37	9.31386	39	0.68614	9.99098	36	0.77
65	9.30521	36	9.31425	38	0.68575	9.99096	35	37
66	9.30557	37	9.31463	38	0.68537	9.99094	34	I 3.7
67	9.30594	37	9.31501	39	0.68499	9.99093	33	2 7.4
68	9.30631	36	9.31540	38	0.68460	9.99091	32	3 II.I 4 I4.8
69	9.30667	37	9.31578	38	0.68422	9.99090	31	5 18.5
70	9.30704	37	9.31616	38	0.68384	9.99088	30	6 22.2
71	9.30741	36	9.31654	38	0.68346	9.99087	29	7 25.9
72	9.30777	37	9.31692	38	0.68308	9.99085	28	8 29.6
73	9.30814	36	9.31730	38	0.68270	9.99083	27	9 33.3
74	9.30850	37	9.31768	38	0.68232	9.99082	26	
75	9.30887	36	9.31806	38	0.68194	9.99080	25	
76	9.30923	37	9.31844	38	0.68156	9.99079	24	
77	9.30960	36	9.31882	38	0.68118	9.99077	23	36
78	9.30996	36	9.31920	38	0.68080	9.99076	33	I 3.6
79	9.31032	36	9.31958	38	0.68042	9.99074	21	2 7.2
80	9.31068	37	9.31996	38	0.68004	9.99072	20	3 10.8
81	9.31105		9.32034	38	0.67966	9.99071	19	4 14.4 5 18.0
82	9.31141	36 36	9.32072	38	0.67928	9.99069	18	5 18.0 6 21.6
83	9.31177	36	9.32110	37	0.67890	9.99068	17	7 25.2
84	9.31213	_	9.32147		0.67853	9.99066	16	8 28.8
85	9.31250	37	9.32185	38	0.67815	9.99064	15	9 32.4
86	9.31286	36 36	9.32223	38	0.67777	9.99063	14	
87	9.31322	36	9.32260		0.67740	9.99061	13	
88	9.31358	36	9.32298	38 38	0.67702	9.99060	12	
89	9.31394	36	9.32336	37	0.67664	9.99058	II	35
90	9.31430	36	9.32373	38	0.67627	9.99056	10	I 3.5
91	9.31466	"	9.32411	37	0.67589	9.99055	09	2 7.0
92	9.31502	36	9.32448	38	0.67552	9.99053	08	3 10.5
93	9.31538	36	9.32486	37	0.67514	9.99052	07	4 14.0 5 17.5
94	9.31573	1	9.32523		0.67477	9.99050	06	6 21.0
95	9.31609	36	9.32561	38	0.67439	9.99048	05	7 24.5
96	9.31645	36 36	9.32598	37	0.67402	9.99047	04	8 28.0
97	9.31681	-	9.32636	-	0.67364	9.99045	03	9 31.5
98	9.31717	36	9.32673	37	0.67327	9.99044	02	
99	9.31752	35	9.32710	37	0.67290	9.99042	10	
100	9.31788	30	9.32747	31	0.67253	9.99040	00	
-	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
	• 005	. ч.	- 000	u. c.	Tail	OIII		

12							101	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.31788	36	9.32747	38	0.67253	9.99040	100	
10	9.31824	35	9.32785		0.67215	9.99039	99	
02	9.31859	35 36	9.32822	37 37	0.67178	9.99037	98	
03	9.31895	35	9.32859	37	0.67141	9.99036	97	38
04	9.31930	36	9.32896	37	0.67104	9.99034	96	1 3.8
05	9.31966	35	9.32933	38	0.67067	9.99032	95	2 7.6
06	9.32001	36	9.32971	37	0.67029	9.99031	94	3 11.4
07	9.32037	35	9.33008	37	0.66992	9.99029	93	4 15.2
08	9.32072	36	9.33045	37	0.66955	9.99028	92	5 19.0 6 22.8
09	9.32108	35	9.33082	37	0.66918	9.99026	91	7 26.6
10	9.32143	35	9.33119	37	0.66881	9.99024	90	8 30.4
II	9.32178	36	9.33156	37	0.66844	9.99023	89	9 34.2
12	9.32214	35	9.33193	37	0.66807	9.99021	88	
13	9.32249	35	9.33230	36	0.66770	9.99019	87	
14	9.32284	35	9.33266	37	0.66734	9.99018	86	0.7
15	9.32319	36	9.33303	37	0.66697	9.99016	85	37
16	9.32355	35 ·	9.33340	37	0.66660	9.99014	84	I 3.7
17	9.32390	35	9.33377	37	0.66623	9.99013	83	2 7.4
18	9.32425	35	9.33414	36	0.66586	9.99011	82	3 II.I 4 I4.8
19	9.32460	35	9.33450	37	0.66550	9.99010	81	4 14.8 5 18.5
20	9.32495	35	9.33487	37	0.66513	9.99008	80	6 22.2
21	9.32530	35	9.33524	36	0.66476	9.99006	79	7 25.9
22	9.32565	35	9.33560	37	0.66440	9.99005	78	8 29.6
23	9.32600	35	9.33597	37	0.66403	9.99003	77	9 33.3
24	9.32635	35	9.33634	36	0.66366	9.99001	76	
25	9.32670	35	9.33670	37	0.66330	9.99000	75	
26	9.32705	35	9-33707	36	0.66293	9.98998	74	36
27	9.32740	35	9.33743	37	0.66257	9.98996	73	
28	9.32775	34	9.33780	36	0.66220	9.98995	72	I 3.6
29	9.32809	35	9.33816	37	0.66184	9.98993	71	2 7.2 3 10.8
30	9.32844	35	9.33853	36	0.66147	9.98991	70	4 14.4
31	9.32879	35	9.33889	36	0.66111	9.98990	69	5 18.0
32	9.32914	34	9.33925	37	0.66075	9.98988	68	6 21.6
33	9.32948	35	9.33962	36	0.66038	9.98987	67	7 25.2
34	9.32983	35	9.33998	36	0.66002	9.98985	66	8 28.8
35 36	9.33018	34	9.34034	37	0.65966	9.98983 9.98982	65 64	9 32.4
	9.33052	35	9.34071	36				
37	9.33087	34	9.34107	36	0.65893	9.98980 9.98978	63 62	
38 39	9.33121 9.33156	35	9.34I43 9.34I79	36	0.05857	9.98978	61	35
40		34		36		9.98977	60	1 3.5
	9.33190	35	9.34215	37	0.65785			2 7.0
41	9.33225	34	9.34252	36	0.65748	9.98973 9.98972	59 58	3 10.5
42 43	9.33259 9.33294	35	9.34288 9.34324	36	0.65712	9.98972	58	4 14.0
		34	1	36				5 17.5
44 45	9.33328 9.33362	34	9.34360	36	0.65640	9.98968 9.98967	56 55	6 21.0
46	9.33302	35	9.34390	36	0.65568	9.98965	54	7 24.5
		34		36	0.65532	9.98963	53	8 28.0 9 31.5
47 48	9.33431 9.33465	34	9.34468 9.34504	36	0.65532	9.98963	53	9 : 31.3
49	9.33403	34	9.34540	36	0.65460	9.98960	51	
50	9.33534	35	9.34576	36	0.65424	9.98958	50	
	Cos	d.	9.34576 Cot	d. c.	Tan	9.98958 Sin	-00	P. P.
_	COS	ı d.	COT	u.c.	lan	oin		r.r.

12°							167°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.33534	34	9.34576	35	0.65424	9.98958	50	
51	9.33568	34	9.34611	36	0.65389	9.98956	49	
52	9.33602	34	9-34647	36	0.65353	9.98955	48	
53	9.33636	34	9.34683	36	0.65317	9.98953	47	36
54	9.33670	34	9.34719	36	0.65281	9.98951	46	1 3.6
55 56	9.33704 9.33738	34	9.34755	35	0.65245	9.98950 9.98948	45	2 7.2 3 10.8
	0	34	9.34790 9.34826	36	0.65174		44 °	3 IO.8 4 I4.4
57 58	9.33772 9.33806	34	9.34862	36	0.65174	9.98946 9.98945	43 42	5 18.0
59	9.33840	34	9.34897	35	0.65103	9.98943	41	6 21.6
60	9.33874	34	9.34933	36	0.65067	9.98941	40	7 25.2
61	9.33908	34	9.34968	35	0.65032	9.98940	39	8 28.8
63.	9.33942	34	9.35004	36	0.64996	9.98938	38	9 32.4
63	9.33976	34 34	9.35040	36 35	0.64960	9.98936	37	
64	9.34010	33	9.35075	36	0.64925	9.98934	36	
65	9.34043	33	9.35111	35	0.64889	9.98933	35	35
66	9.34077	34	9.35146	35	0.64854	9.98931	34	1 3.5
67	9.34111	34	9.35181	36	0.64819	9.98929	33	2 7.0
68	9.34145	33	9.35217	35	0.64783	9.98928	32	3 10.5
69	9.34178	34	9.35252	36	0.64748	9.98926	31	4 14.0 5 17.5
70	9.34212	34	9.35288	35	0.64712	9.98924	30	6 21.0
71	9.34246	33	9.35323	35	0.64677	9.98923	29	7 24.5
72 73	9.34279 9.34313	34	9.35358 9.35394	36	0.64642 0.64606	9.98921 9. 98919	28 27	8 28.0
	9.34346	33		35	0.64571	9.98917	26	9 31.5
74 75	9.34340	34	9.35429 9.35464	35	0.64536	9.98917	25	
76	9.34413	33	9.35499	35	0.64501	9.98914	24	
77	9.34447	34	9.35534	35	0.64466	9.98912	23	34
78	9.34480	33	9.35570	36 35	0.64430	9.98911	22	I 3.4
79	9.34514	34 33	9.35605	35	0.64395	9.98909	21	2 6.8
80	9.34547	33	9.35640	35	0.64360	9.98907	20	3 10.2
81	9.34580	34	9.35675	35	0.64325	9.98905	19	4 13.6 5 17.0
82	9.34614	33	9.35710	35	0.64290	9.98904	18	5 17.0 6 20.4
83	9.34647	33	9.35745	35	0.64255	9.98902	17	7 23.8
84	9.34680	33	9.35780	35	0.64220	9.98900	16	8 27.2
85 86	9.34713	34	9.35815	35	0.64185	9.98898	15	9 30.6
87	9.34747	33	9.35850	35		9.98897	14	
88	9.34780 9.34813	33	9.35885 9.35920	35	0.64115	9.98895 9.98893	13 12	
89	9.34846	33	9.35955	35	0.64045	9.98892	II	33
90	9.34879	33	9.35989	34	0.64011	9.98890	10	I 3.3
91	9.34912	33	9.36024	35	0.63976	9.98888	09	2 6.6
92	9.34945	33	9.36059	35	0.63941	9.98886	08	3 9.9
93	9.34978	33 33	9.36094	35	0.63906	9.98885	07	4 13.2
94	9.35011		9.36128	34	0.63872	9.98883	06	5 16.5 6 19.8
95	9.35044	33 33	9.36163	35 35	0.63837	9.98881	05	7 23.1
96	9.35077	33	9.36198	35	0.63802	9.98879	04	8 26.4
97	9.35110	33	9.36233	34	0.63767	9.98878	03	9 29.7
98 99	9.35143	33	9.36267 9.36302	35	0.63733	9.98876	02	
100	9.35176	33		34	0.63698	9.98874	00	
100	9.35209		9.36336		0.63664	9.98872	-00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

12							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.35209	22	9.36336	25	0.63664	9.98872	100	
OI	9.35242	33	9.36371	35	0.63629	9.98871	99	
02	9.35274	32	9.36406	35	0.63594	9.98869	98	
03	9.35307	33	9.36440	34	0.63560	9.98867	97	35
04	9.35340	33	9.36475	35	0.63525	9.98865	96	I 3.5
05	9.35373	33	9.36509	34	0.63491	9.98864	95	2 7.0
06	9.35405	32	9.36543	34	0.63457	9.98862	94	3 10.5
07	9.35438	33	9.36578	35	0.63422	9.98860	93	4 14.0
08	9.35471	33	9.36612	34	0.63388	9.98858	93	5 17.5 6 21.0
09	9.35503	32	9.36647	35	0.63353	9.98857	91	6 21.0
10	9.35536	33	9.36681	34	0.63319	9.98855	90	7 24.5
		32		34				8 28.0
11	9.35568 9.35601	33	9.36715	35	0.63285 0.63250	9.98853	89 88	9 31.5
13	9.35633	32	9.36784	34	0.63216	9.98850	87	
		33		34				
14	9.35666	32	9.36818	34	0.63182	9.98848	86	34
15 16	9.35698	33	9.36852	35	0.63148	9.98846	85	
	9.35731	32	9.36887	34	0.63113	9.98844	84	I 3.4 2 6.8
17	9.35763	33	9.36921	34	0.63079	9.98842	83	
18	9.35796	32	9.36955	34	0.63045	9.98841	82	3 10.2 4 13.6
19	9.35828	32	9.36989	34	0.63011	9.98839	81	5 17.0
20	9.35860	33	9.37023	34	0.62977	9.98837	80	6 20.4
21	9.35893	32	9.37057	34	0.62943	9.98835	79	7 23.8
22	9.35925	32	9.37091	34	0.62909	9.98834	78	8 27.2
23	9.35957	32	9.37125	34	0.62875	9.98832	77	9 30.6
24	9.35989	33	9.37159	34	0.62841	9.98830	76	
25	9.36022	32	9.37193	34	0.62807	9.98828	75	
26	9.36054	32	9.37227	34	0.62773	9.98826	74	
27	9.36086	32	9.37261	34	0.62739	9.98825	73	33
28	9.36118	32	9.37295	34	0.62705	9.98823	72	I 3.3
29	9.36150	32	9.37329	34	0.62671	9.98821	71	2 6.6
30	9.36182	32	9.37363	34	0.62637	9.98819	70	3 9.9
31	9.36214	_	9.37397	1	0.62603	9.98817	69	4 13.2
32	9.36246	32	9.37431	34	0.62569	9.98816	68	5 16.5 6 19.8
33	9.36278	32	9.37464	33	0.62536	9.98814	67	7 23.I
34	9.36310	32	9.37498	34	0.62502	9.98812	66	8 26.4
35	9.36342	32	9.37532	34	0.62468	9.98810	65	9 29.7
36	9.36374	32	9.37566	34	0.62434	9.98808	64	3 1 -3.1
37	9.36406	32	9.37599	33	0.62401	9.98807	63	
38	9.36438	32	9.37633	34	0.62367	9.98805	62	
39	9.36470	32	9.37667	34	0.62333	9.98803	61	32
40	9.36502	32	9.37700	33	0.62300	9.98801	60	1 3.2
41	9.36533	31	9.37734	34	0.62266	9.98799	59	2 6.4
42	9.30533	32	9.37768	34	0.62232	9.98799	58	3 9.6
43	9.36597	32	9.37801	33	0.62199	9.98796	57	4 12.8
44	9.36629	32	9.37835	34	0.62165	9.98794	56	5 16.0
44	9.36660	31	9.37868	33	0.02105	9.98794	55	6 19.2
46	9.36692	32	9.37902	34	0.62098	9.98792	55	7 22.4 8 25.6
	9.36724	32		33	0.62065	9.98789		
47 48	9.36724	31	9.37935 9.37969	34	0.62031	9.98789	53 52	9 28.8
49	9.30755	32	9.37909	33	0.62031	9.98785	52	
50		32		33			50	
- 50	9.36819		9.38035		0.61965	9.98783	- 50	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

13°							100	
	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
50	9.36819	31	9.38035	34	0.61965	9.98783	50	
51	9.36850		9.38069		0.61931	9.98781	49	
52	9.36882	32 31	9.38102	33 33	0.61898	9,98780	48	
53	9.36913	32	9.38135	34	0.61865	9.98778	47	33
54	9.36945	-	9.38169	33	0.61831	9.98776	46	I 3.3
55	9.36976	31 32	9.38202	33	0.61798	9.98774	45	2 6.6
56	9.37008	3 ²	9.38235	34	0.61765	9.98772	44	3 9.9
57	9.37039	31	9.38269	33	0.61731	9.98770	43	4 13.2
58	9.37070	32	9.38302	33	0.61698	9.98769	43	5 16.5 6 19.8
59	9.37102	31	9.38335	33	0.61665	9.98767	41	7 23.1
60	9.37133	31	9.38368	33	0.61632	9.98765	40	8 26.4
61	9.37164	32	9.38401	33	0.61599	9.98763	39	9 29.7
62	9.37196	32 31	9.38434	33	0.61566	9.98761	38	7, 7,
63	9.37227	31	9.38468	33	0.61532	9.98759	37	- V
64	9.37258	31	9.38501	33	0.61499	9.98758	36	
65	9.37289	32	9.38534	33	0.61466	9.98756	35	32
66	9.37321	31	9.38567	33	0.61433	9.98754	34	I 3.2
67	9.37352	31	9.38600	33	0.61400	9.98752	33	2 6.4
68	9.37383	31	9.38633	33	0.61367	9.98750	32	3 9.6
69	9.37414	31	9.38666	33	0.61334	9.98748	31	4 12.8 5 16.0
70	9.37445	31	9.38699	33	0.61301	9.98746	30	6 19.2
71	9.37476	31	9.38732	33	0.61268	9.98745	29	7 22.4
72	9.37507	31	9.38765	32	0.61235	9.98743	28	8 25.6
73	9.37538	31	9.38797	33	0.61203	9.98741	27	9 28.8
74	9.37569	31	9.38830	33	0.61170	9.98739	26	
75	9.37600	31	9.38863	33	0.61137	9.98737	25	
76	9.37631	31	9.38896	33	0.61104	9.98735	24	
77	9.37662	31	9.38929	33	0.61071	9.98734	23	31
78	9.37693	31	9.38962	32	0.61038	9.98732	22	I 3.I
79	9.37724	31	9.38994	33	0.61006	9.98730	31	2 6.2
80	9.37755	31	9.39027	. 33	0.60973	9.98728	20	3 9.3
81	9.37786	31	9.39060	32	0.60940	9.98726	19	4 12.4 5 15.5
82	9.37817	30	9.39092	33	0.60908	9.98724	18	6 18.6
83	9.37847	31	9.39125	33	0.60875	9.98722	17	7 21.7
84	9.37878	31	9.39158	32	0.60842	9.98720	16	8 24.8
85	9.37909	31	9.39190	33	0.60810	9.98719	15	9 27.9
86	9.37940	30	9.39223	33	0.60777	9.98717	14	
87	9.37970	31	9.39256	32	0.60744	9.98715	13	
88	9.38001	31	9.39288	33	0.60712	9.98713	12	30
89	9.38032	30	9.39321	. 32	0.60679	9.98711	111	
90	9.38062	31	9.39353	. 33	0.60647	9.98709	10	1 3.0
91	9.38093	31	9.39386	32	0.60614	9.98707	09	2 6.0
92	9.38124	30	9.39418	33	0.60582	9.98705	08	4 12.0
93	9.38154	31	9.39451	32	0.60549	9.98704	07	5 15.0
94	9.38185	30	9.39483	32	0.60517	9.98702	06	6 18.0
95	9.38215	31	9.39515	33	0.60485	9.98700	05	7 21.0
96	9.38246	30	9.39548	32	0.60452	9.98698	04	8 24.0
97	9.38276	31	9.39580	32	0.60420	9.98696	03	9 27.0
98 99	9.38307	30	9.39612	33	0.60388	9.98694	02	
100	9.38337	31	9.39645	32	0.60355		00	
100	9.38368		9.39677	-	0.60323	9.98690	- 00	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.
							700	

14							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.38368	30	9.39677	32	0.60323	9.98690	100	
OI	9.38398	1	9.39709	_	0.60291	9.98689	99	
02	9.38428	30 31	9.39742	33 32	0.60258	9.98687	98	
03	9.38459	30	9.39744	32	0.60226	9.98685	97	33
04	9.38489	30	9.39806	32	0.60194	9.98683	96	I 3.3
05	9.38519	31	9.39838	32	0.60162	9.98681	95	2 6.6
06	9.38550	30	9.39870	33	0.60130	9.98679	94	3 9.9
07	9.38580	30	9.39903	32	0.60097	9.98677	93	4 13.2
08	9.38610	30	9.39935	32	0.60065	9.98675	92	5 16.5 6 19.8
09	9.38640	30	9.39967	32	0.60033	9.98673	91	7 23.1
10	9.38670	31	9.39999	32	0.60001	9.98671	90	8 26.4
11	9.38701	30	9.40031	32	0.59969	9.98670	89	9 29.7
12	9.38731	30	9.40063	32	0.59937	9.98668	88	
13	9.38761	30	9.40095	32	0.59905	9.98666	87	
14	9.38791	30	9.40127	32	0.59873	9.98664	86	
15	9.38821	30	9.40159	32	0.59841	9.98662	85	32
16	9.38851	30	9.40191	32	0.59809	9.98660	84	I 3.2
17	9.38881	30	9.40223	32	0.59777	9.98658	83	2 6.4
18	9.38911	30	9.40255	32	0.59745	9.98656	82	3 9.6 4 12.8
19	9.38941	30	9.40287	32	0.59713	9.98654	81	5 16.0
20	9.38971	30	9.40319	32	0.59681	9.98652	80	6 19.2
21	9.39001	30	9.40351	31	0.59649	9.98650	79	7 22.4
22	9.39031	30	9.40382	32	0.59618	9.98648	78	8 25.6
23	9.39061	30	9.40414	32	0.59586	9.98647	77	9 28.8
24	9.39091	30	9.40446	32	0.59554	9.98645	76	
25	9.39121	29	9.40478	32	0.59522	9.98643	75	
26	9.39150	30	9.40510	31	0.59490	9.98641	74	31
27	9.39180	30	9.40541	32	0.59459	9.98639	73	
28 29	9.39210	30	9.40573	32	0.59427	9.98637 9.98635	72 71	I 3.I 2 6.2
	9.39240	30	9.40605	31	0.59395		70	3 9.3
30	9.39270	29	9.40636	32	0.59364	9.98633		4 12.4
31	9.39299	30	9.40668	32	0.59332	9.98631	69 68	5 15.5
32	9.39329	30	9.40700	31	0.59300	9.98629 9.98627	67	6 18.6
33	9.39359	29	9.40731	32	0.59269			7 21.7
34	9.39388	30	9.40763	32	0.59237	9.98625 9.98623	66 65	8 24.8
35 36	9.39418	30	9.40795 9.40826	31	0.59205	9.98621	64	9 27.9
37	9.39448	29	9.40858	32	0.59144	9.98620	63	
38	9.39477	30	9.40889	31	0.59142	9.98618	62	
39	9.39536	29	9.40009	32 31	0.59079	9.98616	61	30
40	9.39566	30	9.40952		0.59048	9.98614	60	I 3.0
41	9.39595	29	9.40984	32	0.59016	9.98612	59	2 6.0
42	9.39393	30	9.40904	31	0.58985	9.98610	58	3 9.0
43	9.39654	29	9.41046	31 32	0.58954	9.98608	57	4 12.0
44	9.39684	30	9.41078		0.58922	9.98606	56	5 15.0 6 18.0
45	9.39004	29	9.41078	3I 32	0.58891	9.98604	55	0 18.0 7 21.0
46	9.39743	30 29	9.41141	32 31	0.58859	9.98602	54	8 24.0
47	9.39772	29	9.41172	31	0.58828	9.98600	53	9 27.0
48	9.39801	30	9.41203	32	0.58797	9.98598	52	
49	9.39831	29	9.41235	31	0.58765	9.98596	51	
50	9.39860		9.41266		0.58734	9.98594	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

14							165	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.39860	29	9.41266	31	0.58734	9.98594	50	
51	9.39889		9.41297	_	0.58703	9.98592	49	
52	9.39919	30 29	9.41328	31 32	0.58672	9.98590	48	
53	9.39948	29	9.41360	31	0.58640	9.98588	47	31
54	9.39977	29	9.41391	31	0.58609	9.98586	46	1 3.1
55	9.40006	29	9.41422	31	0.58578	9.98584	45	2 6.2
56	9.40035	30	9.41453	31	0.58547	9.98582	44	3 9.3
57	9.40065	29	9.41484	31	0.58516	9.98580	43	4 12.4
58	9.40094	29	9.41515	31	0.58485	9.98578	42	5 15.5 6 18.6
59	9.40123	29	9.41546	32	0.58454	9.98576	41	7 21.7
60	9.40152	29	9.41578	31	0.58422	9.98574	40	8 24.8
61	9.40181	29	9.41609	31	0.58391	9.98573	39	9 27.9
62 63	9.40210	29	9.41640	31	0.58360	9.98571	38	
_	9.40239	29	9.41671	31	0.58329	9.98569	37	
64 65	9.40268	29	9.41702	31	0.58298	9.98567	36	30
66	9.40297	29	9.41733	31	0.58267	9.98565	35	
67	9.40326	29	9.41764	31	0.58236	9.98563	34	I 3.0 2 6.0
68	9.40355 9.40384	29	9.41795 9.41825	30	0.58205	9.98561	33 32	2 6.0
69	9.40304	29	9.41825	31	0.58144	9.98559 9.98557	31	4 12.0
70		29		31	0.58113	9.98555	30	5 15.0
71	9.40442	29	9.41887	31				6 18.0
72	9.40471	29	9.41918	31	0.58082 0.58051	9.98553	29 28	7 21.0
73	9.40529	29	9.41949 9.41980	31	0.58020	9.98551 9.98549	27	8 24.0
74	9.40557	28		31	0.57989	9.98547	26	9 27.0
75	9.40586	29	9.42011 9.42041	30	0.57969	9.98545	25	
76	9.40615	29	9.42041	31	0.57928	9.98543	24	
77	9.40644	29	9.42103	31	0.57897	9.98541	23	29
78	9.40672	28	9.42134	31	0.57866	9.98539	22	I 2.9
79	9.40701	29 29	9.42164	30 31	0.57836	9.98537	21	2 5.8
80	9.40730		9.42195	_	0.57805	9.98535	20	3 8.7
81	9.40759	29 28	9.42226	31	0.57774	9.98533	19	4 11.6
82	9.40787	28 29	9.42256	30	0.57744	9.98531	18	5 14.5
83	9.40816	29 28	9.42287	31 31	0.57713	9.98529	17	6 17.4
84	9.40844	29	9.42318	_	0.57682	9.98527	16	8 23.2
85	9.40873	29	9.42348	30 31	0.57652	9.98525	15	9 26.1
86	9.40902	28	9.42379	31	0.57621	9.98523	14	
87	9.40930	29	9.42410	30	0.57590	9.98521	13	
88	9.40959	28	9.42440	31	0.57560	9.98519	12	00
89	9.40987	29	9.42471	30	0.57529	9.98517	II	28
90	9.41016	28	9.42501	31	0.57499	9.98515	10	1 2.8
91	9.41044	29	9.42532	30	0.57468	9.98513	09	2 5.6
92	9.41073	28	9.42562	31	0.57438	9.98511	08	3 8.4
93	9.41101	29	9 - 42593	30	0.57407	9.98509	07	5 14.0
94	9.41130	28	9.42623	30	0.57377	9.98507	06	6 16.8
95	9.41158	28	9.42653	31	0.57347	9.98505	05	7 19.6
96	9.41186	29	9.42684	30	0.57316	9.98502	04	8 22.4
97 98	9.41215	28	9.42714	31	0.57286	9.98500	03	9 25.2
99	9.41243	28	9.42745	30	0.57255	9.98498	02	
100	9.41271	29	9.42775	30	0.57225	9.98496	00	
100	9.41300		9.42805		0.57195	9.98494		- D. D.
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

	Sin	ı d.	Tan	d. c.	Cot	Cos		P. P.
00	9.41300		9.42805				100	r. r.
		28		31	0.57195	9.98494		
0I 02	9.41328 9.41356	28	9.42836 9.42866	30	0.57164	\$9.98492 9.98490	99 98	
03	9.41384	28	9.42896	30	0.57134	9.98488	97	31
04	9.41413	29	9.42926	30	0.57074	9.98486	96	
05	9.41413	28	9.42920	31	0.57074	9.98484	95	1 3.1 2 6.2
06	9.41469	28 28	9.42987	30	0.57013	9.98482	94	3 9.3
07	9.41497		9.43017	30	0.56983	9.98480	93	4 12.4
08	9.41525	28 28	9.43047	30	0.56953	9.98478	92	5 15.5
09	9.41553	29	9.43077	30	0.56923	9.98476	91	6 18.6
10	9.41582	28	9.43108	30	0.56892	9.98474	90	7 21 7 8 24.8
11	9.41610	ł .	9.43138	1	0.56862	9.98472	89	8 24.8 9 27.9
12	9.41638	28 28	9.43168	30 30	0.56832	9.98470	88	9 1 27.9
13	9.41666	28	9.43198	30	0.56802	9.98468	87	
14	9.41694	28	9.43228	30	0.56772	9.98466	86	
15	9.41722	28	9.43258	30	0.56742	9.98464	85	30
16	9.41750	28	9.43288	30	0.56712	9.98462	84	I 3.0
17	9.41778	28	9.43318	30	0.56682	9.98460	83	2 6.0
18	9.41806	28	9.43348	30	0.56652	9.98458	82	3 9.0
19	9.41834	27	9.43378	30	0.56622	9.98456	81	4 I2.0 5 I5.0
20	9.41861	28	9.43408	30	0.56592	9.98453	80	6 18.0
21	9.41889	28	9.43438	30	0.56562	9.98451	79	7 21.0
22	9.41917.	28	9.43468	30	0.56532	9.98449	78	8 24.0
23	9.41945	28	9.43498	30	0.56502	9.98447	77	9 27.0
24	9.41973	28	9.43528	30	0.56472	9.98445	76	
25 26	9.42001	28	9.43558	29	0.56442	9.98443	75	
	9.42029	27	9.43587	30	0.56413	9.98441	74	29
27 28	9.42056 9.42084	28	9.43617	30	0.56383	9.98439	73	
29	9.42004	28	9.43647 9.43677	30	0.56353	9.98437 9.98435	72 71	1 2.9 2 5.8
30	9.42140	28	9.43707	30			70	3 8.7
		27		29	0.56293	9.98433		4 11.6
3I 32	9.42167	28	9.43736 9.43766	30	0.56264	9.98431 9.98429	69 68	5 14.5 6 17.4
33	9.42193	28	9.43700	30	0.56204	9.98429	67	
34	9.42250	27	9.43826	30	0.56174	9.98427	66	7 20.3
35	9.42278	28	9.43855	29	0.56145	9.98425	65	8 23.2 9 26.1
36	9.42305	27 28	9.43885	30	0.56115	9.98420	64	9 1 20.1
37	9.42333	28	9.43915	30	0.56085	9.98418	63	
38	9.42361	28 27	9.43944	29 30	0.56056	9.98416	62	
39	9.42388	28	9 - 43974	30	0.56026	9.98414	61	28
40	9.42416	27	9.44004	29	0.55996	9.98412	60	1 2.8
41	9.42443	28	9.44033	30	0.55967	9.98410	59	2 5.6
42	9.42471	28 27	9.44063	29	0.55937	9.98408	58	3 8.4
43	9.42498	28	9.44092	30	0.55908	9.98406	57	4 11.2 5 14.0
44	9.42526	27	9.44122	29	0.55878	9.98404	56	5 14.0 6 16.8
45	9.42553	27	9.44151	30	0.55849	9.98402	55	7 19.6
46	9.42580	28	9.44181	29	0.55819	9.98399	54	8 22.4
47	9.42608	27	9.44210	30	0.55790	9.98397	53	9 25.2
48	9.42635	28	9.44240	29	0.55760	9.98395	52	
49	9.42663	27	9.44269	30	0.55731	9.98393	51	
50	9.42690		9.44299		0.55701	9.98391	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

10								
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.42690	27	9.44299	29	0.55701	9.98391	50	
51	9.42717	28	9.44328		0.55672	9.98389	49	
52	9.42745	27	9.44358	नु० 29	0.55642	9.98387	48	
53	9.42772	27	9.44387	29	0.55613	9.98385	47	29
54	9.42799		9.44416		0.55584	9.98383	46	I 2.9
55	9.42826	27 28	9.44446	30 29	0.55554	9.98381	45	2 5.8
56	9.42854	27	9.44475	29	0.55525	9.98378	44	3 8.7
57	9.42881		9.44504		0.55496	9.98376	43	4 11.6
58	9.42908	27	9.44534	30	0.55466	9.98374	42	5 14.5
59	9.42935	27	9.44563	29 29	0.55437	9.98372	41	6 17.4
60	9.42962	27	9.44592		0.55408	9.98370	40	7 20.3
61	9.42989	27	9.44622	30	0.55378	9.98368	39	8 23.2 9 26.1
62	9.42909	28	9.44651	29	0.55349	9.98366	38	9 + 20.1
63	9.43044	27	9.44680	29	0.55320	9.98364	37	
64	9.43044	27	9.44709	29	0.55291	9.98361	36	
65	9.43071	27	9.44709	29	0.55262	9.98359	35	28
66	9.43098	27	9.44768	30	0.55232	9.98357	34	1 2.8
67		27		29	0.55203	9.98355	33	2 5.6
68	9.43152 9.43179	27	9.44797 9.44826	29	0.55174	9.90355	33	3 8.4
69	9.43179	27	9.44855	29	0.55145	9.98351	31	4 11.2
70		27		29	0.55116	9.98349	30	5 14.0 6 16.8
	9.43233	27	9.44884	29				6 16.8
71	9.43260	27	9.44913	29	0.55087	9.98347	29	7 19.6
72	9.43287	27	9.44942	29	0.55058	9.98344	28	8 22.4
73	9.43314	27	9.44971	29	0.55029	9.98342	27	9 25.2
74	9.43341	26	9.45000	29	0.55000	9.98340	26	
75	9.43367	27	9.45029	29	0.54971	9.98338	25	
76	9 · 43394	27	9.45058	29	0.54942	9.98336	24	27
77	9.43421	27	9.45087	29	0.54913	9.98334	23	
78	9.43448	27	9.45116	29	0.54884	9.98332	22	I 2.7
79	9.43475	27	9.45145	29	0.54855	9.98329	21	2 5.4
80	9.43502	26	9.45174	29	0.54826	9.98327	20	3 8.1 4 10.8
81	9.43528	27	9.45203	29	0.54797	9.98325	19	
82	9 - 43555	27	9.45232	29	0.54768	9.98323	18	5 13.5 6 16.2
83	9.43582	27	9.45261	29	0.54739	9.98321	17	7 18.9
84	9.43609	26	9.45290	29	0.54710	9.98319	16	8 21.6
85	9.43635	20	9.45319	29	0.54681	9.98317	15	9 24.3
86	9.43662	27	9.45348	28	0.54652	9.98314	14	
87	9.43689	26	9.45376	29	0.54624	9.98312	13	
88	9.43715	20 27	9.45405	29	0.54595	9.98310	12	
89	9.43742	27	9 - 45434	29	0.54566	9.98308	11	26
90	9.43769	26	9.45463		0.54537	9.98306	10	1 2.6
91	9.43795		9.45492	29	0.54508	9.98304	09	2 5.2
92	9.43793	27	9.45520	28	0.54480	9.98302	08	3 7.8
93	9.43848	26	9.45549	29	0.54451	9.98299	07	4 10.4
94	9.43875	27	9.45578	29	0.54422	9.98297	06	5 13.0 6 15.6
94 95	9.43073	26	9.45606	28	0.54394	9.98297	05	7 18.2
96	9.43928	27	9.45635	29	0.54365	9.98293	04	8 20.8
97	9.43954	26	9.45664	29	0.54336	9.98291	03	9 23.4
98	9.43981	27	9.45692	28	0.54308	9.98289	02	3 . 23.4
99	9.44007	26	9.45721	29	0.54279	9.98286	OI	
100	9.44034	27	9.45750	29	0.54250	9.98284	00	
100				1 -		Sin		P. P.
	Cos	d.	Cot	d.c.	Tan	Sin		P. P.

16°							163°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.44034	26	9.45750	28	0.54250	9.98284	100	
OI	9.44060	27	9.45778	29	0.54222	9.98282	99	
02	9.44087	26	9.45807	28	0.54193	9.98280	98	
03	9.44113	26	9.45835	29	0.54165	9.98278	97	29
04	9.44139	27	9.45864	28	0.54136	9.98275	96	I 2.9
05	9.44166	26	9.45892	29	0.54108	9.98273	95	2 5.8
06	9.44192	26	9.45921	29	0.54079	9.98271	94	3 8.7 4 11.6
07	9.44218	27	9.45950	28	0.54050	9.98269	93	5 14.5
08	9.44245	26	9.45978	28	0.54022	9.98267	92	6 17.4
09	9.44271	26	9.46006	29	0.53994	9.98265	91	7 20.3
10	9.44297	27	9.46035	28	0.53965	9.98262	90	8 23.2
11	9.44324	26	9.46063	29	0.53937	9.98260	89	9 26.1
12	9.44350	26	9.46092	28	0.53908	9.98258	88	
13	9.44376	26	9.46120	29	0.53880	9.98256	87	28
14	9.44402	26	9.46149	28	0.53851	9.98254	86	
15	9.44428	27	9.46177	28	0.53823	9.98251	85	I 2.8
16	9 • 44455	26	9.46205	29	0.53795	9.98249	84	2 5.6 3 8.4
17	9.44481	26	9.46234	28	0.53766	9.98247	83	3 8.4
18	9.44507	26	9.46262	28	0.53738	9.98245	82	5 14.0
19	9.44533	26	9.46290	29	0.53710	9.98243	81	6 16.8
20	9.44559	26	9.46319	28	0.53681	9.98240	80	7 19.6
21	9.44585	26	9.46347	28	0.53653	9.98238	79	8 22.4
22	9.44611	26	9.46375	28	0.53625	9.98236	78	9 25.2
23	9.44637	26	9.46403	29	0.53597	9.98234	77	
24	9.44663	26	9.46432	28	0.53568	9.98232	76	
25	9.44689	26	9.46460	28	0.53540	9.98229	75	
26	9.44715	26	9.46488	28	0.53512	9.98227	74	
27	9.44741	26	9.46516	28	0.53484	9.98225	73	
28	9.44767	26	9.46544	29	0.53456	9.98223	72	27
29	9.44793	26	9.46573	28	0.53427	9.98221	71	I 2.7
30	9.44819	26	9.46601	28	0.53399	9.98218	70	2 5.4
31	9.44845	26	9.46629	28	0.53371	9.98216	69	3 8.1 .
32	9.44871	26	9.46657	28	0.53343	9.98214	68	4 10.8
33	9.44897	26	9.46685	28	0.53315	9.98212	67	5 13.5 6 16.2
34	9.44923	25	9.46713	28	0.53287	9.98209	66	7 18.9
35	9.44948	26	9.46741	28	0.53259	9.98207	65	8 21.6
36	9.44974	26	9.46769	28	0.53231	9.98205	64	9 24.3
37	9.45000	26	9.46797	28	0.53203	9.98203	63	
38	9.45026	26	9.46825	28	0.53175	9.98201	62	
39	9.45052	25	9.46853	28	0.53147	9.98198	61	26
40	9.45077	26	9.46881	28	0.53119	9.98196	60	1 2.6
41	9.45103	26	9.46909	28	0.53091	9.98194	59	2 5.2
42	9.45129	26	9.46937	28	0.53063	9.98192	58	3 7.8
43	9.45155	25	9.46965	28	0.53035	9.98189	57	4 IO.4 5 I3.0
44	9.45180	26	9.46993	28	0.53007	9.98187	56	5 13.0 6 15.6
45	9.45206	26	9.47021	28	0.52979	9.98185	55	7 18.2
46	9.45232	25	9.47049	28	0.52951	9.98183	54	8 20.8
47	9.45257	26	9.47077	28	0.52923	9.98180	53	9 23.4
48	9.45283	26	9.47105	28	0.52895	9.98178	52	
49	9.45309	25	9.47133	27	0.52867	9.98176	51	
50	9.45334		9.47160		0.52840	9.98174	50	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

Section Sect	2.8 5.6 3.4 1.2 5.8 9.6 2.4 5.2
51 9.45360 25 9.47188 28 0.52812 9.98174 49 52 9.45365 25 9.47216 28 0.52784 9.98169 48 53 9.45411 25 9.47242 28 0.52756 9.98167 47 28 54 9.45436 26 9.47272 27 0.5278 9.98167 47 28 55 9.45462 25 9.47272 27 0.5270 9.98165 46 I 2 2 56 9.45487 26 9.47327 28 0.52673 9.98160 44 3 8 57 9.45513 25 9.47383 27 0.52617 9.98186 44 3 4 11 58 9.45538 26 9.47383 27 0.52617 9.98184 43 4 11 59 9.45564 25 9.47440 28 0.52599 9.98153 41 7 16	2.8 5.6 3.4 1.2 4.0 5.8 9.6 2.4 5.2
52 9.45385 26 9.47216 28 0.52784 9.98169 48 53 9.45411 25 9.47214 28 0.52756 9.98167 47 28 54 9.45462 26 9.47279 27 0.52728 9.98165 46 1 2 2 5 55 9.45462 25 9.47299 28 0.52673 9.98165 45 2 2 3 8 4 3 8 56 9.45487 26 9.47337 28 0.52645 9.98165 45 2 2 3 8 4 41 11 3 8 4 41 11 3 8 4 41 13 8 4 4 41 13 8 4 4 41 14 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2.8 5.6 3.4 1.2 4.0 5.8 9.6 2.4 5.2
53 9.4541I 25 9.47244 28 0.52756 9.98167 47 28 54 9.45436 26 9.47272 27 0.52728 9.98165 46 1 2 25 55 9.45462 25 9.47327 28 0.52673 9.98160 44 3 8 57 9.45513 25 9.47337 28 0.52645 9.98156 44 4 11 58 9.45538 26 9.47383 28 0.52617 9.98156 42 6 16 16 60 9.45564 25 9.47438 28 0.525207 9.98153 41 7 15 60 9.45569 26 9.47438 28 0.525267 9.98151 40 8 22 61 9.45615 25 9.47466 27 0.52350 9.98140 39 9 23 62 9.45664 25 9.47521 28	2.8 5.6 3.4 1.2 4.0 5.8 9.6 2.4 5.2
54 9.45436 26 9.47272 27 0.52728 9.98165 46 I 2 55 9.45462 25 9.47299 28 0.52721 9.98165 45 2 2 56 9.45487 26 9.47327 28 0.52673 9.98160 44 3 8 57 9.45538 25 9.47335 28 0.52615 9.98158 43 5 1 59 9.45564 25 9.47410 28 0.52590 9.98153 47 6 1 7 16 60 9.45564 25 9.47440 28 0.52562 9.98153 47 7 16 61 9.45615 25 9.47493 28 0.52562 9.98149 39 9 23 62 9.45664 25 9.47493 28 0.52479 9.98149 39 9 23 63 9.45669 26 9.47521	5.6 3.4 1.2 4.0 5.8 9.6 2.4 5.2
State	3.4 1.2 1.0 5.8 9.6 2.4 5.2
55 9.45487 26 9.47327 28 0.52673 9.98169 44 3 8 57 9.45513 25 9.47335 28 0.52645 9.98158 43 5 1. 58 9.45384 26 9.47383 27 0.52617 9.98156 42 5 1. 6 1. 1. 1. 7 1. 1. 1. 1. 7 1. 1. 1. 1. 1. 1. 7 1.	3.4 1.2 1.0 5.8 9.6 2.4 5.2
57 9.45513 25 9.47355 28 0.52645 9.98158 43 4 11 58 9.45538 26 9.47383 27 0.52617 9.98156 42 6 16 <th>1.0 5.8 9.6 2.4 5.2</th>	1.0 5.8 9.6 2.4 5.2
58 9.45538 26 9.47383 27 0.52617 9.98156 42 6 16 </th <th>5.8 9.6 2.4 5.2</th>	5.8 9.6 2.4 5.2
59 9.45564 9.45589 25 26 9.47410 9.47438 28 28 0.52590 0.52562 9.98153 9.98151 41 41 7 41 7 41 1 41 2 41 2 41 3 41 3 41 <t< th=""><th>9.6 2.4 5.2</th></t<>	9.6 2.4 5.2
60 9.45589 26 9.47438 28 0.52562 9.98151 40 8 22 61 9.45615 25 9.47466 27 0.52534 9.98149 39 9 25 63 9.45605 26 9.47521 28 0.52479 9.98147 38 64 9.45691 26 9.47521 28 0.52479 9.98144 37 65 9.45716 26 9.47576 27 0.52451 9.98142 36 27 66 9.45742 26 9.47576 28 0.52421 9.98140 35 1 2 66 9.45742 26 9.47576 28 0.52424 9.98140 35 1 2 66 9.45742 25 9.47604 28 0.52396 9.98138 34 2 2	2.4
61 9.45615 25 9.47466 27 0.52534 9.98149 39 9 23 663 9.4565 26 9.47521 28 0.52479 9.98144 37 64 9.45691 25 9.47562 27 0.52451 9.98142 36 27 0.52451 9.98144 37 65 9.45716 26 9.47576 27 0.52451 9.98142 36 27 0.52451 9.98142 36 66 9.45742 25 9.47604 28 0.52424 9.98140 35 1 2 6 6 9.45742 25 9.47604 28 0.52424 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 2 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 25 9.47604 28 0.52454 9.98140 35 1 2 5 6 6 9.45742 9.98140 35 1 2 5 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9 6 6 9	2.7
62 9.45640 25 9.47493 28 0.52507 9.98147 38 64 9.45691 25 9.47562 27 0.52451 9.98144 37 64 9.45691 25 9.47562 27 0.52451 9.98142 36 27 65 9.45716 26 9.47576 28 0.52424 9.98140 35 1 2 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 2 5	2.7
63 9.4565 25 9.47521 28 0.52479 9.98144 37 64 9.45691 25 9.47549 27 0.52451 9.98142 36 27 65 9.45716 26 9.47576 28 0.52424 9.98140 35 1 2 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2.7
64 9.45691 25 9.47549 27 0.52451 9.98142 36 27 66 9.45716 26 9.47576 28 0.52451 9.98140 35 1 2 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 5 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 9.45742 25 9.47604 28 0.52396 9.98138 34 2 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2.7
65 9.45716 26 9.47576 28 0.52424 9.98140 35 1 2 6 66 9.45742 25 9.47604 28 0.52496 9.98138 34 2 5	2.7
66 9.45742 25 9.47604 28 0.52396 9.98138 34 2 3	
25 3.11. 1 28 -10-05- 3.5-0-	5.4
	3.I
68 0 45702 25 0 47650 27 0 53341 0 9833 33	5.8
69 9.45817 25 9.47687 28 0.52313 9.98131 31 5 13	3.5
70 0.45843 20 0.47714 2 0.52286 0.08120 30 6 16	5.2
7 18	3.9
72 0 45803 25 0 47760 27 0 53331 0 08134 38	1.6
72 0 45018 25 0 47707 28 0 52202 0 08122 27	1.3
74 0 45014 20 0 47824 27 0 53776 0 08110 36	
75 0 45060 25 0 47850 28 0 50148 0 08117 25	
76 0 45004 25 0 47870 27 0 53131 0 08115 34	
77 0 46010 25 0 47007 28 0 73003 0 08113 23	
78 0 46044 25 0 47034 27 0 73266 0 08470 33	
	2.5
80 0 45005 20 0 47080 20 0 53011 0 08106 20 2 5	5.0
87 0 46120 25 0 48016 27 0 51081 0 08102 TO 3	7.5
82 0 46145 25 0 48044 28 0 51056 0 08101 18 4 10	0.0
82 0 46170 25 0 48071 27 0 51070 0 08000 177 5 12	2.5
24 0 46707 25 0 4808 27 0 77000 0 68007 76	5.0 7.5
85 0.46220 25 0.48126 20 0.51874 0.08004 15 9 00	0.0
86 0 46345 25 0 48353 27 0 57847 0 08003 74	2.5
87 0 46370 23 0 48780 24 0 57800 0 08000 12	
88 0 46305 25 0 48308 20 0 51703 0 08087 13	
89 9.46320 25 9.48235 27 0.51765 9.9885 11 24	
90 0 46245 0 48262 0 67728 0 68682 10	2.4
07 0 46370 25 0 48380 27 0 57777 0 08380 00 2	8
92 9.46395 25 9.48317 28 9.51683 9.98078 98 3	7.2
93 9.46420 25 9.48344 27 0.51656 9.98076 07 4 9).6
04 0 4644 24 0 4877 2/ 0 77670 0 08074 06 5 12	2.0
05 0 46460 25 0 48208 27 0 71603 0 08271 05 6 12	1.4
96 0 46404 25 0 48425 27 0 51575 0 08060 04 7 10	5.8
07 0 46770 0 48470 0 48470 0 08067 00	1.6
98 9.46544 25 9.48480 27 0.51520 9.98064 02	
99 9.46569 25 9.48507 27 0.51493 9.98062 OI	
100 9.46594 9.48534 0.51466 9.98060 00	
Cos d. Cot d. c. Tan Sin P. P.	

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.46594		9.48534		0.51466	9.98060	100	
OI	9.46618	24	9.48561	27	0.51439	9.98057	99	
02	9.46643	25	9.48588	27	0.51412	9.98055	98	
03	9.46668	25	9.48615	27	0.51385	9.98053	97	27
04	9.46693	25	9.48642	27	0.51358	9.98050	96	I 2.7
05	9.46717	24	9.48669	27	0.51331	9.98048	95	2 5.4
06	9.46742	25 25	9.48696	27 27	0.51304	9.98046	94	3 8.1
07	9.46767		9.48723		0.51277	9.98043	93	4 10.8
08	9.46791	24	9.48750	27	0.51250	9.98041	92	5 13.5
09	9.46816	25 25	9.48777	27 27	0.51223	9.98039	91	6 16.2 7 18.9
10	9.46841	24	9.48804		0.51196	9.98036	90	8 21.6
11	9.46865		9.48831	27	0.51169	9.98034	89	9 24.3
12	9.46890	25	9.48858	27	0.51142	9.98032	88	7
13	9.46915	25 24	9.48885	27 27	0.51115	9.98029	87	
14	9.46939		9.48912		0.51088	9.98027	86	26
15	9.46964	25	9.48939	27	0.51061	9.98025	85	I 2.6
16	9.46988	24 25	9.48966	27 27	0.51034	9.98022	84	2 5.2
17	9.47013		9.48993	1	0.51007	9.98020	83	3 7.8
18	9.47037	24 25	9.49020	27 26	0.50980	9.98018	82	4 10.4
19	9.47062	24.	9.49046	27	0.50954	9.98015	81	5 13.0
20	9.47086	25	9.49073	27	0.50927	9.98013	80	6 15.6
21	9.47111	24	9.49100	27	0.50900	9.98011	79	7 18.2 8 20.8
22	9.47135	25	9.49127	27	0.50873	9.98008	78	9 23.4
23	9.47160	24	9.49154	27	0.50846	9.98006	77	3 - 23.4
24	9.47184	25	9.49181	26	0.50819	9.98004	76	
25	9.47209	25	9.49207	27	0.50793	9.98001	75	
26	9.47233	24	9.49234	27	0.50766	9.97999	74	
27	9.47257	25	9.49261	27	0.50739	9.97997	73	
28	9.47282	24	9.49288	26	0.50712	9.97994	72	25
29	9.47306	24	9.49314	27	0.50686	9.97992	71	I 2.5
30	9.47330	25	9.49341	27	0.50659	9.97989	70	2 5.0
31	9 - 47355	24	9.49368	26	0.50632	9.97987	69	3 7.5 4 10.0
32	9.47379	24	9.49394	27	0.50606	9.97985	68	5 12.5
33	9.47403	25	9.49421	27	0.50579	9.97982	67	6 15.0
34	.9.47428	24	9.49448	26	0.50552	9.97980	66	7 17.5
35	9.47452	24	9.49474	27	0.50526	9.97978	65	8 20.0
36	9.47476	24	9.49501	27	0.50499	9.97975	64	9 22.5
37	9.47500	25	9.49528	26	0.50472	9.97973	63	
38	9.47525	24	9.49554	27	0.50446	9.97971	62	
39 40	9.47549	24	9.49581	26	0.50419	9.97968	61	24
	9.47573	24	9.49607	27	0.50393	9.97966	60	I 2.4
41	9.47597	24	9.49634	26	0.50366	9.97963	59	2 4.8
42	9.47621	25	9.49660	27	0.50340	9.97961	58	3 7.2
43	9.47646	24	9.49687	26	0.50313	9.97959	57	4 9.6 5 12.0
44	9.47670	24	9.49713	27	0.50287	9.97956	56	6 14.4
45 46	9.47694 9.47718	24	9.49740	26	0.50260	9.97954	55	7 16.8
		24		27		9.97951	54	8 19.2
47 48	9.47742 9.47766	24	9.49793 9.49819	26	0.50207	9.97949	53	9 21.6
49	9.47790	24	9.49819	27	0.50154	9.97947 9.97944	52 51	
50	9.47814	24		26			50	
	Cos	d.	9.49872 Cat	-1 -	0.50128	9.97942	-00	D. D.
	Cos	a.	Cot	d.c.	Tan	Sin		P. P.

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_	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.47814	24	9.49872	27	0.50128	9.97942	50	
51	9.47838	24	9.49899	26	0.50101	9.97940	49	
52	9.47862	24	9.49925	26	0.50075	9.97937	48	0.7
53	9.47886	24	9.49951	27	0.50049	9-97935	47	27
54	9.47910	24	9.49978	26	0.50022	9.97932	46	I 2.7
55	9.47934	24	9.50004	27	0.49996	9.97930	45	2 5.4 3 8.1
56	9.47958	24	9.50031	26	0.49969	9.97928	44	3 8.1
57	9.47982	24	9.50057	26	0.49943	9.97925	43	5 13.5
58 59	9.48006 9.48030	24	9.50083 9.50110	27	0.49917	9.97923	42	6 16.2
60		24		26	0.49890	9.97920	41	7 18.9
	9.48054	24	9.50136	26	0.49864	9.97918	40	8 21.6
61 62	9.48078	24	9.50162	26	0.49838	9.97916	39	9 24.3
63	9.48102	23	9.50188	27	0.49812	9.97913	38	
	9.48125	24	9.50215	26	0.49785	9.97911	37	
64 65	9.48149 9.48173	24	9.50241	26	0.49759	9.97908	36	26
66	9.48173	24	9.50267 9.50293	26	0.49733	9.97906	35	I 2.6
67	9.48197	24		27	1	9.97904	34	2 5.2
68	9.48221	24	9.50320	26	0.49680	9.97901	33	3 7.8
69	9.48243	23	9.50346 9.50372	26	0.49628	9.97899 9.97896	32 31	5 13.0
70	9.48292	24		26			30	6 15.6
		24	9.50398	26	0.49602	9.97894		7 18.2
7I 72	9.48316	24	9.50424	27	0.49576	9.97891	29 28	8 20.8
73	9.48340 9.48363	23	9.50451	26	0.49549	9.97889 9.97887	28	9 23.4
	1	24	9.50477	26	0.49523			
74 75	9.48387	24	9.50503	26	0.49497	9.97884	26	
76	9.48434	23	9.50529 9.50555	26	0.49471	9.97882 9.97879	25 24	
77	9.48458	24	9.50581	26				
78	9.48482	24	9.50507	26	0.49419	9.97877 9.97874	23 22	24
79	9.48505	23	9.50633	26	0.49393	9.97874	21	I 2.4
80	9.48529	24	9.50659	26	0.49341	9.97870	20	2 4.8
81	9.48552	23		26				3 7.2
82	9.48576	24	9.50685 9.50711	26	0.49315	9.97867 9.97865	19	4 9.6
83	9.48600	24	9.50737	26	0.49263	9.97862	17	5 I2.0 6 I4.4
84	9.48623	23	9.50763	26	0.49237	9.97860	16	
85	9.48647	24	9.50789	26	0.49237	9.97857	15	7 16.8
86	9.48670	23	9.50815	26 26	0.49185	9.97855	14	8 19.2 9 21.6
87	9.48694	24	9.50841		0.49159	9.97853	13	, 22.0
88	9.48717	23	9.50867	26 26	0.49133	9.97850	12	
89	9.48741	24 23	9.50893	26	0.49107	9.97848	11	23
90	9.48764	23	9.50919	26	0.49081	9.97845	10	I 2.3
91	9.48788		9.50945		0.49055	9.97843	09	2 4.6
92	9.48811	23	9.50971	26 26	0.49029	9.97840	08	3 6.9
93	9.48835	24	9.50997	26 26	0.49003	9.97838	07	4 9.2
94	9.48858		9.51023		0.48977	9.97835	06	5 II.5 6 I3.8
95	9.48881	23 24	9.51048	25 26	0.48952	9.97833	05	
96	9.48905	23	9.51074	26	0.48926	9.97830	04	7 16.1 8 18.4
97	9.48928	23	9.51100	26	0.48900	9.97828	03	8 18.4
98	9.48952	23	9.51126	26 26	0.48874	9.97826	02	9 . 20.7
99	9.48975	23	9.51152	26	0.48848	9.97823	OI	
100	9.48998		9.51178		0.48822	9.97821	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

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	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.48998	24	9.51178	25	0.48822	9.97821	100	
01	9.49022	23	9.51203	26	0.48797	9.97818	99	
02	9.49045	23	9.51229	26	0.48771	9.97816	98	26
03	9.49068	23	9.51255	26	0.48745	9.97813	97	
04	9.49091	24	9.51281	25	0.48719	9.97811	96	I 2.6 2 5.2
05	9.49115	23	9.51306	26	0.48694	9.97808	95	2 5.2 3 7.8
06	9.49138	23	9.51332	26	0.48668	9.97806	94	4 10.4
07	9.49161	23	9.51358	26	0.48642	9.97803	93	5 13.0
08	9.49184	24	9.51384	25	0.48616	9.97801	92	6 15.6
09	9.49208	23	9.51409	26	0.48591	9.97798	91	7 18.2
10	9.49231	23	9.51435	26	0.48565	9.97796	90	8 20.8
II	9.49254	23	9.51461	25	0.48539	9.97793	89	9 23.4
12	9.49277	23	9.51486	26	0.48514	9.97791	88	
13	9.49300	23	9.51512	25	0.48488	9.97788	87	25
14	9.49323	24	9.51537	26	0.48463	9.97786	86	
15	9.49347	23	9.51563	26	0.48437	9.97784	85	I 2.5 2 5.0
16	9.49370	23	9.51589	25	0.48411	9.97781	84	3 7.5
17	9 - 49393	23	9.51614	26	0.48386	9.97779	83	4 10.0
18	9.49416	23	9.51640	25	0.48360	9.97776	82	5 12.5
19	9.49439	23	9.51665	26	0.48335	9.97774	81	6 15.0
20	9.49462	23	9.51691	26	0.48309	9.97771	80	7 17.5
21	9.49485	23	9.51717	25	0.48283	9.97769	79	8 20.0
22	9.49508	23	9.51742	26	0.48258	9.97766	78	9 22.5
23	9.49531	23	9.51768	25	0.48232	9.97764	77	
24	9.49554	23	9.51793	26	0.48207	9.97761	76	
25	9 - 49577	23	9.51819	25	0.48181	9.97759	75	
26	9.49600	23	9.51844	26	0.48156	9.97756	74	
27	9.49623	23	9.51870	25	0.48130	9.97754	73	24
28	9.49646	23	9.51895	25	0.48105	9.97751	72	I 2.4
29	9.49669	23	9.51920	26	0.48080	9.97749	71	2 4.8
30	9.49692	23	9.51946	25	0.48054	9.97746	70	3 7.2
31	9.49715	23	9.51971	26	0.48029	9.97744	69	4 9.6
32	9.49738	23	9.51997	25	0.48003	9.97741	68	5 12.0 6 14.4
33	9.49761	22	9.52022	25	0.47978	9.97739	67	
34	9.49783	23	9.52047	26	0.47953	9.97736	66	7 16.8 8 19.2
35	9.49806	23	9.52073	25	0.47927	9.97734	65	8 19.2 9 21.6
36	9.49829	23	9.52098	26	0.47902	9.97731	64	9 21.0
37	9.49852	23	9.52124	25	0.47876	9.97729	63	
38	9.49875	23	9.52149	25	0.47851	9.97726	62 61	23
39	9.49898	22	9.52174	26		9.97723		1 2.3
40	9.49920	23	9.52200	25	0.47800	9.97721	60	2 4.6
41	9.49943	23	9.52225	25	0.47775	9.97718	59	3 6.9
42	9.49966	23	9.52250	25	0.47750	9.97716	58	4 9.2
43	9.49989	22	9.52275	26	0.47725	9.97713	57	5 11.5
44	9.50011	23	9.52301	25	0.47699	9.97711	56	
45 46	9.50034	23	9.52326	25	0.47674	9.97708	55	7 16.1
		23	9.52351	25	1	9.97706	54	8 18.4
47 48	9.50080	22	9.52376	26	0.47624	9.97703	53	9 20.7
49	9.50102	23	9.52402 9.52427	25	0.47598	9.97701	52 51	
50		23		25			50	
-00	9.50148		9.52452	1	0.47548	9.97696	-00	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.50148		9.52452		0.47548	9.97696	50	T. F.
		22		25				
51	9.50170	23	9.52477	25	0.47523	9.97693	49	
52 53	9.50193 9.50216	23	9.52502 9.52528	26	0.47498 0.47472	9.97691 9.97688	48	25
		22		25			47	
54	9.50238	23	9.52553	25	0.47447	9.97686	46	1 2.5
55 56	9.50261 9.50283	22	9.52578 9.52603	25	0.47422	9.97683	45	2 5.0
_		23		25	0.47397	9.97680	44	3 7.5 4 10.0
57	9.50306	22	9.52628	25	0.47372	9.97678	43	4 10.0 5 12.5
58	9.50328	23	9.52653 9.52678	25	0.47347	9.97675	42	6 15.0
59	9.50351	23		25	0.47322	9.97673	41	7 17.5
60	9.50374	22	9.52703	25	0.47297	9.97670	40	8 20.0
6r	9.50396	23	9.52728	25	0.47272	9.97668	39	9 22.5
62	9.50419	22	9.52753	25	0.47247	9.97665	38	
63	9.50441	23	9.52778	26	0.47222	9.97663	37	
64	9.50464	22	9.52804	25	0.47196	9.97660	36	
65	9.50486	22	9.52829	25	0.47171	9.97657	35	24
66	9.50508	23	9.52854	25	0.47146	9.97655	34	I 2.4
67	9.50531	22	9.52879	25	0.47121	9.97652	33	2 4.8
68	9.50553	23	9.52904	25	0.47096	9.97650	32	3 7.2
69	9.50576	22	9.52929	24	0.47071	9.97647	31	4 9.6 5 12.0
70	9.50598	22	9.52953	25	0.47047	9.97645	30	5 I2.0 6 I4.4
71	9.50620	23	9.52978	25	0.47022	9.97642	29	7 16.8
72	9.50643	23	9.53003	25	0.46997	9.97640	28	8 19.2
73	9.50665	23	9.53028	25	0.46972	9.97637	27	9 21.6
74	9.50688	22	9.53053		0.46947	9.97634	26	J
75	9.50710	22	9.53078	25 25	0.46922	9.97632	25	
76	9.50732	23	9.53103	25	0.46897	9.97629	24	
77	9.50755	22	9.53128	25	0.46872	9.97627	23	23
78	9.50777	22	9.53153	25	0.46847	9.97624	22	I 2.3
79	9.50799	22	9.53178	24	0.46822	9.97621	21	2 4.6
80	9.50821	23	9.53202	25	0.46798	9.97619	20	3 6.9
81	9.50844	-	9.53227		0.46773	9.97616	19	4 9.2
82	9.50866	22	9.53252	25	0.46748	9.97614	18	5 11.5
83	9.50888	22	9.53277	25	0.46723	9.97611	17	6 13.8 7 16.1
84	9.50910		9.53302	25	0.46698	9.97609	16	7 16.1 8 18.4
85	9.50933	23	9.53327	25	0.46673	9.97606	15	9 20.7
86	9.50955	22	9.53351	24 25	0.46649	9.97603	14	311
87	9.50977		9.53376	-	0.46624	9.97601	13	
88	9.50999	22 22	9.53401	25	0.46599	9.97598	12	
89	9.51021	22	9.53426	25 24	0.46574	9.97596	11	22
90	9.51043		9.53450		0.46550	9.97593	10	I 2.2
91	9.51066	23	9.53475	25	0.46525	9.97590	09	2 4.4
92	9.51088	22	9.53500	25	0.46500	9.97588	08	3 6.6
93	9.51110		9.53525	25	0.46475	9.97585	07	4 8.8
94	9.51132	22	9.53549	24	0.46451	9.97583	06	5 11.0
95	9.51132	22	9.53549	25	0.46426	9.97580	05	6 13.2
96	9.51134	22	9.53574	25	0.46401	9.97577	04	7 15.4 8 17.6
97	9.51198	22	9.53623	24	0.46377	9.97575	03	9 19.8
98	9.51198	22	9.53648	25	0.46352	9.97573	03	9 19.0
99	9.51242	22	9.53673	25	0.46327	9.97570	01	
100		22		24			00	
100	9.51264		9.53697		0.46303	9.97567		
	Cos	d	Cot	d. c.	Tan	Sin		P. P.

19							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.51264	22	9.53697	25	0.46303	9.97567	100	
OI	9.51286	22	9.53722	24	0.46278	9.97564	99	
02	9.51308	22	9.53746	25	0.46254	9.97562	98	25
03	9.51330	22	9.53771	25	0.46229	9.97559	97	25
04	9.51352	22	9.53796	24	0.46204	9.97557	96	I 2.5
05	9.51374	22	9.53820	25	0.46180	9.97554	95	2 5.0
06	9.51396	22	9.53845	24	0.46155	9.97551	94	3 7.5 4 10.0
07	9.51418	22	9.53869	25	0.46131	9.97549	93	4 IO.0 5 I2.5
08	9.51440	22	9.53894	24	0.46106	9.97546	92	6 15.0
09	9.51462	22	9.53918	25	0.46082	9.97543	91	7 17.5
10	9.51484	22	9.53943	24	0.46057	9.97541	90	8 20.0
11	9.51506		9.53967		0.46033	9.97538	89	9 22.5
12	9.51527	2I 22	9.53992	25 24	0.46008	9.97536	88	
13	9.51549	22	9.54016	25	0.45984	9.97533	87	
14	9.51571		9.54041		0.45959	9.97530	86	24
15	9.51593	22 22	9.54065	24 25	0.45935	9.97528	85	I 2.4
16	9.51615	22	9.54090	25	0.45910	9.97525	84	2 4.8
17	9.51637		9.54114		0.45886	9.97522	83	3 7.2
18	9.51658	2 I 22	9.54139	25 24	0.45861	9.97520	82	4 9.6 5 12.0
19	9.51680	22	9.54163	24	0.45837	9.97517	81	5 12.0 6 14.4
20	9.51702	22	9.54187	25	0.45813	9.97515	80	7 16.8
21	9.51724		9.54212		0.45788	9.97512	79	8 19.2
22	9.51745	21	9.54236	24	0.45764	9.97509	78	9 21.6
23	9.51767	22	9.54261	25 24	0.45739	9.97507	77	
24	9.51789		9.54285	1	0.45715	9.97504	76	
25	9.51811	22	9.54309	24	0.45691	9.97501	75	
26	9.51832	2I 22	9.54334	25 24	0.45666	9.97499	74	
27	9.51854		9.54358		0.45642	9.97496	73	22
28	9.51876	22	9.54382	24	0.45618	9.97493	72	
29	9.51897	2I 22	9.54407	25 24	0.45593	9.97491	71	I 2.2
30	9.51919		9.54431		0.45569	9.97488	70	2 4.4 3 6.6
31	9.51941	22	9.54455	24	0.45545	9.97485	69	4 8.8
32	9.51962	21	9.54480	25	0.45520	9.97483	68	5 11.0
33	9.51984	22 22	9.54504	24	0.45496	9.97480	67	6 13.2
34	9.52006		9.54528		0.45472	9.97477	66	7 15.4
35	9.52027	21	9.54552	24	0.45448	9.97475	65	8 17.6
36	9.52049	22 21	9.54577	25 24	0.45423	9.97472	64	9 19.8
37	9.52070	1	9.54601		0.45399	9.97469	63	
38	9.52092	22 21	9.54625	24 24	0.45375	9.97467	62	
39	9.52113	21 22	9.54649	24	0.45351	9.97464	61	21
40	9.52135	21	9.54673	25	0.45327	9.97461	60	I 2.I
41	9.52156		9.54698	1	0.45302	9.97459	59	2 4.2
42	9.52178	22 21	9.54722	24 24	0.45278	9.97456	58	3 6.3 4 8.4
43	9.52199	22	9.54746	24	0.45254	9.97453	57	4 8.4 5 10.5
44	9.52221	21	9.54770	24	0.45230	9.97451	56	6 12.6
45	9.52242	21	9.54794	24	0.45206	9.97448	55	7 14.7
46	9.52264	21	9.54818	25	0.45182	9.97445	54	8 16.8
47	9.52285	22	9.54843	24	0.45157	9.97443	53	9 18.9
48	9.52307	21	9.54867	24	0.45133	9.97440	52	
49	9.52328	22	9.54891	24	0.45109	9.97437	51	
50	9.52350		9.54915		0.45085	9.97435	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
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19° 160°

19							100	
	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
50	9.52350	21	9.54915	24	0.45085	9.97435	50	
51	9.52371	21	9.54939	24	0.45061	9.97432	49	
52	9.52392	22	9.54963	24	0.45037	9.97429	48	24
53	9.52414	21	9.54987	24	0.45013	9.97427	47	
54	9.52435	21	9.55011	24	0.44989	9.97424	46	I 2.4 2 4.8
55	9.52456	22	9.55035	24	0.44965	9.97421	45	2 4.8 3 7.2
56	9.52478	21	9.55059	24	0.44941	9.97419	44	4 9.6
57	9.52499	21	9.55083	24	0.44917	9.97416	43	5 12.0
58	9.52520	22	9.55107	24	0.44893	9.97413	42	6 14.4
59	9.52542	21	9.55131	24		9.97410	41	7 16.8
60	9.52563	21	9.55155	24	0.44845	9.97408	40	8 19.2
61	9.52584	22	9.55179	24	0.44821	9.97405	39	9 21.6
62	9.52606	21	9.55203	24	0.44797	9.97402	38	
63	9.52627	21	9.55227	2.4	0.44773	9.97400	37	23
64	9.52648	21	9.55251	24	0.44749	9.97397	36	I 2.3
65 66	9.52669	21	9.55275	24	0.44725	9.97394	35 34	2 4.6
	9.52690	22	9.55299	24	0.44701	9.97392		3 6.9
67 68	9.52712	21	9.55323	24	0.44677	9.97389	33 32	4 9.2
69	9.52733 9.52754	21	9.55347	24	0.44653	9.97386 9.97383	31	5 11.5
70		21	9.55371	24			30	6 13.8
	9.52775	21	9.55395	23	0.44605	9.97381		7 16.1
71	9.52796	22	9.55418	24	0.44582	9.97378	29 28	8 18.4
72	9.52818	21	9.55442	24	0.44558	9.97375		9 20.7
73	9.52839	21	9.55466	24	0.44534	9.97373	27	
74	9.52860	21	9.55490	24	0.44510	9.97370	26	
75	9.52881	21	9.55514	24	0.44486	9.97367	25	
76	9.52902	21	9.55538	24	0.44462	9.97364	24	
77	9.52923	21	9.55562	23	0.44438	9.97362	23	21
78	9.52944	21	9.55585	24	0.44415	9.97359	22 21	I 1 2.I
79	9.52965	21	9.55609	24	0.44391	9.97356	20	2 4.2
80	9.52986	21	9.55633	24	0.44367	9.97353		3 6.3
81	9.53007	21	9.55657	23	0.44343	9.97351	19	4 8.4
82	9.53028	21	9.55680	24	0.44320	9.97348	18	5 10.5
83	9.53049	22	9.55704	24	0.44296	9.97345	17	6 12.6
84	9.53071	21	9.55728	24	0.44272	9.97343	16	7 14.7 8 16.8
85 86	9.53092	20	9.55752	23	0.44248	9.97340	15 14	9 18.9
	9.53112	21	9.55775	24	0.44225	9.97337		,,
87 88	9.53133	21	9.55799 9.55823	24	0.44201	9.97334	13	
89	9.53154 9.53175	21	9.55847	24	0.44177	9.97332 9.97329	11	20
90		21		23			10	I , 2.0
	9.53196	21	9.55870	24	0.44130	9.97326		2 4.0
91 92	9.53217	21	9.55894 9.55918	24	0.44106	9.97323 9.97321	o9 o8	3 6.0
92	9.53238	21	9.55918	23	0.44082	9.97321	07	4 8.0
		21		24			06	5 10.0
94	9.53280	21	9.55965	24	0.44035	9.97315	05	6 12.0
95 96	9.5330I 9.53322	21	9.55989 9.56012	23	0.43988	9.97312	04	7 14.0
97		21	9.56036	24		9.97310	0.3	8 16.0 9 18.0
97 98	9.53343 9.53363	20	9.56036	23	0.43964	9.97307	03	9 10.0
99	9.53303	21	9.56083	24	0.43941	9.97304	01	
100		21		24	0.43893		00	
100	9.53405 Con	d.	9.56107	d -		9.97299 Sin		P. P.
	Cos	a.	Cot	d. c.	Tan	SITI		F.F.

20							109	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.53405	21	9.56107	23	0.43893	9.97299	100	
OI	9.53426	21	9.56130	24	0.43870	9.97296	99	
02	9.53447	2I 2I	9.56154	23	0.43846	9.97293	98	24
03	9.53468	20	9.56177	24	0.43823	9.97290	97	24
04	9.53488	21	9.56201	23	0.43799	9.97288	96	I 2.4
05	9.53509	21	9.56224	23	0.43776	9.97285	95	2 4.8
06	9.53530	21	9.56248	23	0.43752	9.97282	94	3 7.2
07	9.53551	20	9.56271	24	0.43729	9.97279	93	4 9.6 5 12.0
08	9.53571	21	9.56295	23	0.43705	9.97276	92	5 12.0 6 14.4
09	9.53592	21	9.56318	24	0.43682	9.97274	91	7 16.8
10	9.53613	21	9.56342	23	0.43658	9.97271	90	8 19.2
11	9.53634	20	9.56365	24	0.43635	9.97268	89	9 21.6
12	9.53654	20 2I	9.56389	23	0.43611	9.97265	88	
13	9.53675	2I 2I	9.56412	24	0.43588	9.97263	87	
14	9.53696	20	9.56436	23	0.43564	9.97260	86	23
15	9.53716	20 2I	9.56459	23	0.43541	9.97257	85	1 2.3
16	9.53737	2I 2I	9.56483	23	0.43517	9.97254	84	2 4.6
17	9.53758	20	9.56506	24	0.43494	9.97251	83	3 6.9
18	9.53778	21	9.56530	23	0.43470	9.97249	82	4 9.2
19	9.53799	20	9.56553	23	0.43447	9.97246	81	5 II.5 6 I3.8
20	9.53819	21	9.56576	24	0.43424	9.97243	80	7 16.1
21	9.53840		9.56600		0.43400	9.97240	79	8 18.4
22	9.53861	2I 20	9.56623	23	0.43377	9.97238	78	9 20.7
23	9.53881	21	9.56646	23 24	0.43354	9.97235	77	
24	9.53902		9.56670		0.43330	9.97232	76	
25	9.53922	20 21	9.56693	. 23	0.43307	9.97229	75	
26	9.53943	20	9.56716	23 24	0.43284	9.97226	74	
27	9.53963	21	9.56740		0.43260	9.97224	73	21
28	9.53984	20	9.56763	23 23	0.43237	9.97221	72	
29	9.54004	21	9.56786	24	0.43214	9.97218	71	I 2.I
30	9.54025	20	9.56810	23	0.43190	9.97215	70	2 4.2 3 6.3
31	9.54045	21	9.56833	_	0.43167	9.97212	69	4 8.4
32	9.54066	20	9.56856	23 24	0.43144	9.97210	68	5 10.5
33	9.54086	21	9.56880	23	0.43120	9.97207	67	6 12.6
34	9.54107	20	9.56903	_	0.43097	9.97204	66	7 14.7
35	9.54127	20	9.56926	23 23	0.43074	9.97201	65	8 16.8
36	9.54148	20	9.56949	24	0.43051	9.97198	64	9 18.9
37	9.54168	20	9.56973	23	0.43027	9.97195	63	
38	9.54188	20	9.56996	23	0.43004	9.97193	62	
39	9.54209	20	9.57019	23	0.42981	9.97190	61	20
40	9.54229	21	9.57042	23	0.42958	9.97187	60	I 2.0
41	9.54250	20	9.57065	24	0.42935	9.97184	59	2 4.0 3 6.0
42	9.54270	20	9.57089	23	0.42911	9.97181	58	
43	9.54290	21	9.57112	23	0.42888	9.97179	57	4 8.0 5 10.0
44	9.54311	20	9.57135	23	0.42865	9.97176	56	6 12.0
45	9.54331	20	9.57158	23	0.42842	9.97173	55	7 14.0
46	9.54351	21	9.57181	23	0.42819	9.97170	54	8 16.0
47	9.54372	20	9.57204	24	0.42796	9.97167	53	9 18.0
48	9.54392	20	9.57228	23	0.42772	9.97164	52	
49	9.54412	21	9.57251	23	0.42749	9.97162	51	
50	9.54433		9.57274		0.42726	9.97159	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.54433	20	9.57274		0.42726	9.97159	50	
51	9.54453		9.57297	23	0.42703	9.97156	49	
52	9.54473	20	9.57320	23	0.42680	9.97153	48	
53	9.54493	20	9.57343	23	0.42657	9.97150	47	23
54	9.54514	21	9.57366	23	0.42634	9.97147	46	I 2.3
5 5	9.54534	20	9.57389	23	0.42611	9.97147	45	2 4.6
56	9.54554	20	9.57412	23	0.42588	9.97142	44	3 6.9
57	9.54574	20	9.57435	23	0.42565	9.97139	43	4 9.2
58	9.54594	20	9.57458	23	0.42542	9.97139	43	5 11.5
59	9.54615	21	9.57481	23	0.42519	9.97133	41	6 13.8
60	9.54635	20		23	0.42496		40	7 16.1
		20	9.57504	23		9.97130		8 18.4
61 6-	9.54655	20	9.57527	23	0.42473	9.97127	39	9 20.7
62	9.54675	20	9.57550	23	0.42450	9.97125	38	
63	9.54695	20	9.57573	23	0.42427	9.97122	37	22
64	9.54715	20	9.57596	23	0.42404	9.97119	36	
65	9.54735	21	9.57619	23	0.42381	9.97116	35	1 2.2
66	9.54756	20	9.57642	23	0.42358	9.97113	34	2 4.4 3 6.6
67	9.54776	20	9.57665	23	0.42335	9.97110	33	4 8.8
68	9.54796	20	9.57688	23	0.42312	9.97108	32	5 11.0
69	9.54816	20	9.57711	23	0.42289	9.97105	31	6 13.2
70	9.54836	20	9.57734	23	0.42266	9.97102	30	7 15.4
71	9.54856	20	9.57757	23	0.42243	9.97099	29	8 17.6
72	9.54876	20	9.57780	23	0.42220	9.97096	28	9 19.8
73	9.54896	20	9.57803	23	0.42197	9.97093	27	
74	9.54916	20	9.57826		0.42174	9.97090	26	
75	9.54936	20	9.57849	23 22	0.42151	9.97087	25	
76	9.54956	20	9.57871	23	0.42129	9.97085	24	
77	9.54976	20	9.57894	-	0.42106	9.97082	23	00
78	9.54996	20	9.57917	23	0.42083	9.97079	22	20
79	9.55016	20	9.57940	23	0.42060	9.97076	21	I 2.0
80	9.55036		9.57963	23	0.42037	9.97073	20	2 4.0
81	9.55056	20	9.57986	23	0.42014	9.97070	19	3 6.0
82	9.55076	20	9.57980	23	0.41991	9.97070	18	, ,
83	9.55096	20	9.58031	22	0.41969	9.97064	17	5 10.0 6 12.0
84	9.55116	20	9.58054	23	0.41946	9.97062	16	7 14.0
85	9.55110	20	9.58054	23	0.41940	9.97002	15	8 16.0
86	9.55155	19	9.58100	23	0.41923	9.97056	14	9 18.0
87		20		22				
88	9.55175	20	9.58122	23	0.41878	9.97053	13 12	
89	9.55195 9.55215	20	9.58145	23	0.41832	9.97050 9.97047	11	19
		20		23			Į.	
90	9.55235	20	9.58191	22	0.41809	9.97044	10	1 1.9 2 3.8
91	9.55255	20	9.58213	23	0.41787	9.97041	09	3 5.7
92	9.55275	19	9.58236	23	0.41764	9.97038	08	4 7.6
93	9.55294	20	9.58259	23	0.41741	9.97036	07	5 9.5
94	9.55314	20	9.58282	22	0.41718	9.97033	06	6 11.4
95	9.55334	20	9.58304	23	0.41696	9.97030	05	7 13.3
96	9.55354	20	9.58327	23	0.41673	9.97027	04	8 15.2
97	9.55374	19	9.58350	22	0.41650	9.97024	03	9 17.1
98	9.55393	20	9.58372	23	0.41628	9.97021	02	
99	9.55413	20	9.58395	23	0.41605	9.97018	01	
100	9.55433		9.58418		0.41582	9.97015	00	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

21								100	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.55433	20	9.58418	22	0.41582	9.97015	3	100	
OI	9.55453		9.58440		0.41560	9.97012	-	99	23
02	9.55472	19 20	9.58463	23 23	0.41537	9.97009	3	98	
03	9.55492	20	9.58486	23	0.41514	9.97006	2	97	2 4.6
04	9.55512	20	9.58508	23	0.41492	9.97004	3	96	3 6.9
05	9.55532	19	9.58531	23	0.41469	9.97001	3	95	4 9.2
06	9.55551	20	9.58554	22	0.41446	9.96998	3	94	5 II.5 6 I3.8
07	9.55571	20	9.58576	23	0.41424	9.96995	3	93	7 16.1
08	9.55591	19	9.58599	22	0.41401	9.96992	3	92	8 18.4
09	9.55610	20	9.58621	23	0.41379	9.96989	3	91	9 20.7
10	9.55630	20	9.58644	22	0.41356	9.96986	3	90	22
II	9.55650	19	9.58666	23	0.41334	9.96983	3	89	
12	9.55669	20	9.58689	23	0.41311	9.96980	3	88	I 2.2 2 4.4
13	9.55689	19	9.58712	22	0.41288	9.96977	3	87	3 6.6
14	9.55708	20	9.58734	23	0.41266	9.96974	3	86	4 8.8
15	9.55728	20	9.58757	22	0.41243	9.96971	3	85 84	5 II.0 6 I3.2
16	9.55748	19	9.58779	23	0.41221	9.96968	3		7 15.4
17	9.55767	20	9.58802	22	0.41198	9.96965	2	83 82	
18	9.55787	19	9.58824	23	0.41176	.9.96963 9.96960	3	81	9 19.8
19	9.55806	20	9.58847	22	0.41153		3	80	
20	9.55826	19	9.58869	23	0.41131	9.96957	3		
21	9.55845	20	9.58892	22	0.41108	9.96954	3	79	20
22	9.55865	19	9.58914	23	0.41086	9.96951	3	78	I 2.0
23	9.55884	20	9.58937	22	0.41063	9.96948	3	77	2 4.0 3 6.0
24	9.55904	19	9.58959	22	0.41041	9.96945	3	76	3 6.0
25	9.55923	20	9.58981	23	0.41019	9.96942 9.96939	3	75	5 10.0
26	9 55943	19	9.59004	22	0.40996		3	74	
27	9.55962	20	9.59026	23	0.40974	9.96936	3	73	7 14.0 8 16.0
28	9.55982	19	9.59049	22	0.40951	9.96933 9.96930	3	71	9 18.0
29	9.56001	20	9.59071	23		9.96927	3	70	
30	9.56021	19	9.59094	22	0.40906		3	69	19
31	9.56040	20	9.59116	22	0.40884	9.96924 9.96921	3	68	1 1.9
32	9.56060	19	9.59138	23	0.40862	9.96921	3	67	2 3.8
33	9.56079	19	9.59161	22			3	66	3 5.7
34	9.56098	20	9.59183	22	0.40817	9.96915	3	65	4 7.6
35 36	9.56118	19	9.59205 9.59228	23	0.40795	9.96909	3	64	6 11.4
	9.56157	20		22	0.40750	9.96906	3	63	7 13.3 8 15.2
37 38	9.50157	19	9.59250 9.59272	22	0.40750	9.96904	2	62	8 15.2 9 17.1
39	9.56195	19	9.59272	23	0.40725	9.96901	3	61	9 1/.2
40	9.56215	20	9.59317	22	0.40683	9.96898	3	60	
	9.56234	19	1	22	0.40661	9.96895	3	59	3
4I 42	9.56253	19	9.59339 9.59362	23	0.40638	9.96892	3	58	
43	9.56273	20	9.59384	22	0.40616	9.96889	3	57	I 0.3 2 0.6
44	9.56292	19	9.59406	22	0.40594	9.96886	3	56	3 0.9
44	9.56311	19	9.59429	23	0.40594	9.96883	3	55	4 1.2
46	9.56330	19	9.59451	22	0.40549	9.96880	3	54	5 I.5 6 I.8
47	9.56350	20	9.59473	22	0.40527	9.96877	3	53	7 2.1
48	9.56369	19	9.59495	22	0.40505	9.96874	3	52	8 2.4
49	9.56388	19	9.59518	23	0.40482	9.96871	3	51	9 2.7
50	9.56498	20	9.59540	22	0.40460	9.96868	3	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	1 003	, u.		. u. c.	1 4411	, DIII		-	

								100	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.56408		9.59540		0.40460	9.96868		50	
51	9.56427	19	9.59562	22	0.40438	9.96865	3	49	22
52	9.56446	19	9.59584	22	0.40416	9.96862	3	48	
53	9.56465	19	9.59606	22	0.40394	9.96859	3	47	I 2.2 2 4.4
54	9.56484	19	9.59629	23	0.40371	9.96856	3	46	3 6.6
55	9.56504	20	9.59651	22	0.40349	9.96853	3	45	4 8.8
56	9.56523	19	9.59673	22 22	0.40327	9.96850	3	44	5 II.0 6 I3.2
57	9.56542	19	9.59695		0.40305	9.96847	3	43	6 13.2 7 15.4
58	9.56561	19	9.59717	22	0.40283	9.96844	3	42	8 17.6
59	9.56580	19	9.59739	22	0.40261	9.96841	3	41	9 19.8
60	9.56599	19	9.59762	23	0.40238	9.96838	3	40	
61	9.56619	20	9.59784	22	0.40216	9.96835	3	39	21
62	9.56638	19	9.59806	22	0.40194	9.96832	3	38	I 2.I
63	9.56657	19	9.59828	22	0.40172	9.96829	3	37	2 4.2
64	9.56676	19	9.59850	22	0.40150	9.96826	3	36	3 6.3
65	9.56695	19	9.59872	22	0.40128	9.96823	3	35	4 8.4
66	9.56714	19	9.59894	22	0.40106	9.96820	3	34	5 10.5 6 12.6
67	9.56733	19	9.59916	22	0.40084	9.96817	3	33	7 14.7 8 16.8
68	9.56752	19	9.59939	23	0.40061	9.96814	3	32	8 16.8 9 18.9
69	9.56771	19	9.59961	22	0.40039	9.96811	3	31	9 10.9
70	9.56790	19	9.59983	22	0.40017	9.96808	3	30	
71	9.56809	19	9.60005	22	0.39995	9.96805	3	29	4.0
72	9.56829	20	9.60027	22	0.39993	9.96802	3	28	19
73	9.56848	19	9.60027	22	0.39973	9.96799	3	27	1 1.9 3.8
	9.56867	19	9.60049	22	0.39931	9.96796	3	26	3 5.7
74 75	9.56886	19	9.60071	22	0.39929	9.96793	3	25	3 5.7 4 7.6
76	9.56905	19	9.60115	22	0.39885	9.96790	3	24	5 9.5
77	9.56924	19	9.60137	22	0.39863	9.96787	3		6 11.4 7 13.3
78	9.56943	19	9.60137	22	0.39841	9.96784	3	23	7 13.3 8 15.2
79	9.56961	18	9.60139	22	0.39819	9.96781	3	21	9 17.1
80	9.56980	19	9.60203	22	0.39797	9.96778	3	20	
81		19		22			4		18
82	9.56999	19	9.60225	22	0.39775	9.96774 9.96771	3	19	1 1.8
83	9.57018 9.57037	19	9.60247	22	0.39753	9.96768	3	17	2 3.6
		19		22			3	16	3 5.4
84	9.57056	19	9.60291	22	0.39709	9.96765 9.96762	3		4 7.2
8 ₅ 86	9.57075 9.57094	19	9.60313 9.60335	22	0.39665	9.96759	3	15 14	5 9.0 6 10.8
87		19	-	22	0.39643	9.96756	3		7 12.6
88	9.57113 9.57132	19	9.60357 9.60379	22	0.39643	9.96753	. 3	13 12	8 14.4 9 16.2
89	9.57132	19	9.60379	21	0.39021	9.96750	3	11	9 / 10.2
90		18	9.60422	22	0.39578	9.96747	3	10	
	9.57169	19		22			3		
91	.9.57188	19	9.60444	22	0.39556	9.96744 9.96741	3	o9 o8	4
92 93	9.57207 9.57226	19	9.60466 9.60488	22	0.39534 0.39512	9.96741	3	07	I 0.4 2 0.8
		19		22			3		
94	9.57245	19	9.60510	22	0.39490	9.96735 9.96732	3	o6 05	4 1.6
95 96	9.57264 9.57282	18	9.60532 9.60554	22	0.39468 0.39446	9.96732	3	05	5 2.0
		19		21			3		
97	9.57301	19	9.60575	22	0.39425	9.96726	3	03 02	7 2.8 8 3.2
98	9.57320	19	9.60597 9.60619	22	0.39403	9.96723	3	02 01	9 3.6
99	9.57339	19		22	0.39381		3		
100	9.57358		9.60641		0.39359	9.96717		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.57358		9.60641	<u>u. c.</u>	0.39359	9.96717	<u>u.</u>	100	
		18	9.60663	22		9.96714	3	99	
0I 02	9.57376 9.57395	19	9.60685	22	0.39337 0.39315	9.96710	4	98	22
03	9.57414	19	9.60706	21	0.39313	9.96707	3	97	I 2.3
		19	9.60728	22	0.39294	9.96704	3	96	3 6.6
04 05	9.57433 9.57451	18	9.60728	22	0.39272	9.96701	3	95	
06	9.57470	19	9.60772	22	0.39238	9.96698	3	94	4 8.8 5 11.0 6 13.2
07	9.57489	19	9.60794	22	0.39206	9.96695	3	93	6 13.2 7 15.4
08	9.57507	18	9.60815	21	0.39185	9.96692	3	92	7 15.4 8 17.6
09	9.57526	19	9.60837	22	0.39163	9.96689	3	91	9 19.8
10	9.57545	19	9.60859	22	0.39141	9.96686	3	90	
11	9.57563	18	9.60881	22	0.39119	9.96683	3	89	21
12	9.57582	19	9.60902	21	0.39119	9.96680	3	88	I 2.I
13	9.57601	19	9.60924	22	0.39076	9.96677	3	87	2 4.2 3 6.3
14	9.57619	18	9.60946	22	0.39054	9.96674	3	86	3 6.3 4 8.4
15	9.57638	19	9.60940	21	0.39033	9.96670	4	85	5 10.5
16	9.57657	19	9.60989	22	0.39011	9.96667	3	84	5 10.5 6 12.6
17	9.57675	18	9.61011	22	0.38989	9.96664	3	83	7 14.7 8 16.8
18	9.57694	19	9.61033	22	0.38967	9.96661	3	82	9 18.9
19	9.57712	18	9.61054	21	0.38946	9.96658	3	81	9 10.9
20	9.57731	19	9.61076	22	0.38924	9.96655	3	80	
21	9.57749	18	9.61098	22	0.38902	9.96652	3	79	19
21	9.57768	19	9.61119	21	0.38881	9.96649	3	78	
23	9.57787	19	9.61141	22	0.38859	9.96646	3	77	I I.9 2 3.8
24	9.57805	18	9.61162	21	0.38838	9.96643	3	76	3 5.7 7.6
25	9.57824	19	9.61184	22	0.38816	9.96640	3	75	4 7.6
26	9.57842	18	9.61206	22	0.38794	9.96636	4	74	5 9.5 6 11.4
27	9.57861	19	9.61227	21	0.38773	9.96633	3	73	7 13.3 8 15.2
28	9.57879	18	9.61249	22	0.38751	9.96630	3	72	
29	9.57898	19	9.61271	22	0.38729	9.96627	3	71	9 17.1
30	9.57916	18	9.61292	21	0.38708	9.96624	3	70	
31	9.57935	19	9.61314	22	0.38686	9.96621	3	69	18
32	9.57953	18	9.61335	21	0.38665	9.96618	3	68	1 1.8
33	9.57972	19	9.61357	22	0.38643	9.96615	3	67	2 3.6
34	9.57990	18	9.61378	21	0.38622	9.96612	3	66	3 5.4 7.2
35	9.58008	18	9.61400	22	0.38600	9.96608	4	65	5 9.0
36	9.58027	19	9.61422	22 2I	0.38578	9.96605	3	64	
37	9.58045	1	9.61443	1	0.38557	9.96602	3	63	7 12.6 8 14.4
38	9.58064	19	9.61465	22 21	0.38535	9.96599	3	62	9 16.2
39	9.58082	19	9.61486	21	0.38514	9.96596	3	61	
40	9.58101	18	9.61508		0.38492	9.96593	1	60	
41	9.58119		9.61529	21	0.38471	9.96590	3	59	3
42	9.58137	18	9.61551	22	0.38449	9.96587	3	58	
43	9.58156	19	9.61572	2I 22	0.38428	9.96583	4	57	2 0.6
44	9.58174		9.61594	1	0.38406	9.96580	3	56	3 0.9
45	9.58192	18	9.61615	2I 22	0.38385	9.96577	3	55	4 1.2 5 1.5
46	9.58211	19	9.61637	22 2I	0.38363	9.96574	3	54	5 I.5 6 I.8
47	9.58229	18	9.61658	22	0.38342	9.96571	1	53	7 2.I 8 2.4
48	9.58247	19	9.61680	22 2I	0.38320	9.96568	3	52	8 2.4 9 2.7
49	9.58266	18	9.61701	21	0.38299	9.96565	3	51	9,,
50	9.58284		9.61722		0.38278	9.96562		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.
112°								67°	

Social Color	44								101	
51 9.58302 19 9.61744 21 0.38256 9.96558 3 48 1 2.2 53 9.583391 18 9.61765 21 0.38285 9.96558 3 48 1 2.2 54 9.58357 18 9.61808 22 0.38179 9.96549 3 46 3 6.6 55 9.58375 19 9.61830 21 0.38149 9.96546 3 45 4 8.8 57 9.58412 18 9.61872 21 0.38149 9.96540 3 44 51 11 57 9.58448 18 9.61894 21 0.38169 9.96530 3 44 42 3 71 15.2 58 9.58436 18 9.61936 22 0.38042 9.96530 3 41 3 71 16.4 9.58485 18 9.61936 22 0.38021 9.96530 3 3		Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
St	50	9.58284	+Q	9.61722	22	0.38278	9.96562		50	
52 0.58321 19 9.61765 21 0.38265 9.96555 3 48 1 2 1 2 0.38243 9.96555 3 47 2 4 2 4 3 46 3 6 6 3 6 3 46 3 6 3 4 8 8 8 6 3 46 3 46 3 46 3 6 6 3 6 6 3 45 4 8 8 6 3 46 3 46 3 6 6 3 46 3 4 4 8 8 6 3 4 4 8 8 6 3 4 4 4 8 8 8 6 18 9.61873 2 0.38169 9.96534 3 4 4 2 4 4 2 4 4 2 4 4 4 <	51			9.61744		0.38256	9.96558		49	00
53 9.58339 18 9.61787 22 0.38213 9.96552 3 47 1 2 4.6 3 46 3 46 3 46 3 46 3 46 3 46 3 4 8.8 8 55 9.58394 18 9.61830 22 0.38179 9.96549 3 45 5 511.6 3 4 8.8 8 56 9.58412 18 9.61872 21 0.38128 9.96540 3 44 3 7 15.2 58 9.58438 19 9.61915 21 0.38086 9.96533 3 41 3 7 15.2 4 43 7 15.2 4 43 7 15.2 4 43 7 15.2 4 43 4 43 7 15.2 4 43 4 43 7 15.2 4 43 4 43 7 15.2 4									48	
S5		9.58339		9.61787		0.38213	9.96552		47	
S5	54	9.58357		9.61808		0.38192	9.96549		46	3 6.6
S7				9.61830						4 8.8
S7	56	9.58394		9.61851		0.38149	9.96543		44	5 11.0
Section Sect	57	9.58412		9.61872		0.38128	9.96540		43	7 15.4
59 9.58448 19 9.61915 21 0.38064 9.96533 3 41 9 1.91 61 9.58485 18 9.61958 21 0.38064 9.96530 3 39 21 62 9.58503 18 9.61979 22 0.38021 9.96524 3 38 1 2.1 64 9.58539 18 9.62021 21 0.379978 9.96524 3 36 4 8 65 9.58557 19 9.62022 21 0.37978 9.96517 3 36 4 8 6 4 8 6 12 0.37937 9.96517 3 36 4 8 6 12 0.37937 9.96517 3 36 4 8 12 0.37937 9.96517 3 36 4 8 12 0.37937 9.96511 3 35 10 34 12 0.37937 9.96511 3 33 <	58	9.58430		9.61894		0.38106	9.96536			
60 9.58467 18 9.61936 22 0.38064 9.965320 3 40 61 9.58485 18 9.61938 21 0.38042 9.96527 3 38 1 2.1 63 9.58531 18 9.62001 21 0.38021 9.96524 3 38 1 2.1 64 9.58539 18 9.62022 21 0.37999 9.96524 3 36 4 8.8 65 9.58537 19 9.62043 21 0.37937 9.96514 3 36 4 8.8 67 9.58594 18 9.62065 21 0.37937 9.96514 3 35 5 10.1 67 9.58630 18 9.62108 21 0.37937 9.96514 3 33 3 16.12.0 69 9.58630 18 9.62178 21 0.37839 9.96508 3 32 9 18.16.1	59	9.58448		9.61915		0.38085	9.96533		41	9 19.8
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63 0.58521 18 9.62001 22 0.37999 9.96521 3 37 2 4.2 36 4 8.7 3 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 4 8.8 3.6 1.8 9.62065 21 0.37937 9.96511 3 3.5 5 10.1 12.0 1.8 9.62128 21 0.37893 9.96508 3 3.3 3 16.1 12.0 1.8 16.2 1.8 9.62178 21 0.37893 9.96508 3 3.2 9										
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65 9.58557 18 9.62043 21 0.37957 9.96514 3 35 5 10 12 22 0.37957 9.96514 3 35 5 10 12 12 0.37957 9.96514 3 35 5 10 12 12 0.37957 9.96508 3 33 34 6 12 12 0.37914 9.96508 3 33 3 8 16 12 16 9.95863 3 33 3 8 16 12 16 9.96508 3 33 3 8 16 12 16 9.96508 3 33 3 8 16 16 16 16 16 18 9.62150 21 0.37829 9.96508 3 33 3 18 16 3 9.96498 3 30 30 18 9.62192 22 0.37850 9.96498 3 30 29 18 9.58721	64	9.58539		9.62022		0.37978	9.96517		36	4 8.4
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68 9 58612 18 9 62128 21 0.37893 9.96505 3 32 9 18.4 70 9.58648 18 9.62150 21 0.37892 9.96502 4 31 31 71 9.58666 18 9.62171 21 0.37850 9.96498 3 29 18 73 9.58702 19 9.62214 21 0.37850 9.96492 3 28 1 1.1 75 9.58721 18 9.62235 21 0.37765 9.96489 3 26 4 7 76 9.58757 18 9.62274 21 0.37734 9.96479 3 24 6 10.2 77 9.58757 18 9.62297 21 0.37733 9.96479 3 24 6 10.2 78 9.58793 18 9.62290 21 0.37630 9.96479 3 24 6 10.2 79	67	9.58594		9.62086		0.37914	9.96508		33	7 14.7
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72	71			0.62171					20	18
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86 9.58937 18 9.02489 22 0.37511 9.96447 3 14 7 11.0 87 9.58955 29 9.62511 07 0.37489 9.96444 3 13 8 13.0									1	5 8.5
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0.5063 18 0.63637 21 0.37363 0.06437 3 07 2 0.8										2 0.8
04 0 50081 10 0 62650 22 0 37341 0 06433 3 1.2		1	18		22					3 1.2
96 9.50116 18 9.62701 21 9.37209 9.96415 4 94 6 2.4										6 2.4
95 9.3910 18 9.62701 21 0.37299 9.90413 3 04 7 2.8				1	1	}			1 '	7 2.8
08 0 50752 10 0 63742 21 0 37357 0 06400 3 03 6					1					
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10 21 3			18	-	21			3		
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Cos d. Cot d. c. Tan Sin d. P. P.		Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.59188		9.62785		0.37215	9.96403		100	
		18	9.62806	21	0.37194	9.96399	4	99	
0I 02	9.59206 9.59223	17	9.62827	21	0.37194	9.96396	3	98	21
03	9.59223	18	9.62848	21	0.37152	9.96393	3	97	I 2.I
		18	9.62869	21	0.37131	9.96390	3	96	2 4.2 3 6.3
04	9.59259	18	9.62890	21	0.37131	9.96390	3	95	4 8.4
o5 o6	9.59277 9.59295	18	9.62912	22	0.37088	9.96383	4	94	4 8.4 5 10.5 6 12.6
		18	9.62933	21	0.37067	9.96380	3	93	6 12.6
07 08	9.59313 9.59330	17	9.62954	21	0.37046	9.96377	3	93	7 14.7 8 16.8
09	9.59330	18	9.62934	21	0.37025	9.96374	3	91	9 18.9
10	9.59366	18	9.62996	21	0.37004	9.96370	4	90	
		18	9.63017	21	0.36983	9.96367	3	89	20
11	9.59384	17	9.63017	21	0.36962	9.96364	3	88	I 2.0
13	9.59401 9.59419	18	9.63059	21	0.36941	9.96361	3	87	2 4.0 3 6.0
-		18	9.63080	21	0.36920	9.96357	4	86	
14	9.59437	18	9.63101	21	0.36899	9.96354	3	85	4 8.0 5 10.0
15 16	9.59455 9.59472	17	9.63121	20	0.36879	9.96351	3	84	5 IO.0 6 I2.0
		18	9.63142	21	0.36858	9.96348	3	83	7 14.0
17	9.59490 9.59508	18	9.63142	21	0.30050	9.96344	4	82	8 16.0 9 18.0
19	9.59526	18	9.63184	21	0.36816	9.96341	3	81	9 18.0
20		17	9.63205	21	0.36795	9.96338	3	80	
	9.59543	18		21			3		40
21	9.59561	18	9.63226	21	0.36774	9.96335	4	79 78	18
22	9.59579	17	9.63247 9.63268	21	0.36753	9.96331 9.96328	3	70 77	1 1.8 2 3.6
23	9.59596	18		21			3		3 5.4
24	9.59614	18	9.63289	21	0.36711	9.96325 9.96322	3	76	4 7.2
25 26	9.59632	17	9.63310 9.63331	21	0.36690	9.96318	4	75 74	4 7.2 5 9.0 6 10.8
	9.59649	18		21			3		7 12.6
27	9.59667	17	9.63352	21	0.36648	9.96315 9.96312	3	73	8 14.4
28 29	9.59684	18	9.63373 9.63393	20	0.36607	9.96312	3	72 71	9 16.2
	9.59702	18		21			4	70	
30	9.59720	17	9.63414	21	0.36586	9.96305	3		17
31	9.59737	18	9.63435	21	0.36565	9.96302	3	69	1 1.7
32	9.59755	17	9.63456	21	0.36544	9.96299	-	68 67	2 3.4
33	9.59772	18	9.63477	21	0.36523	9.96296	4		3 5.1 4 6.8 5 8.5 6 10.2
34	9.59790	18	9.63498	21	0.36502	9.96292	3	66	5 8.5
35	9.59808	17	9.63519	20	0.36481	9.96289 9.96286	3	65 64	
36	9.59825	18	9.63539	21	0.36461		4		7 11.9 8 13.6
37	9.59843	17	9.63560	21	0.36440	9.96282	3	63 62	8 13.6 9 15.3
38 39	9.59860	18	9.63581 9.63602	21	0.36419	9.96279 9.96276	3	61	9 [25.5
	9.59878	17		21			3	60	
40	9.59895	18	9.63623	20	0.36377	9.96273	4		3
41	9.59913	17	9.63643	21	0.36357	9.96269	3	59	_
42	9.59930	18	9.63664	21	0.36336	9.96266	3	58	I 0.3 2 0.6
43	9.59948	17	9.63685	21	0.36315	9.96263	3	57	3 0.9
44	9.59965	18	9.63706	20	0.36294	9.96260	4	56	4 1.2
45	9.59983	17	9.63726	21	0.36274	9.96256	3	55	5 I.5 6 I.8
46	9.60000	18	9.63747	21	0.36253	9.96253	3	54	7 2.1
47	9.60018	17	9.63768	21	0.36232	9.96250	4	53	
48	9.60035	18	9.63789	20	0.36211	9.96246	3	52	9 2.7
49	9.60053	17	9.63809	21		9.96243	3	51	
50	9.60070		9.63830		0.36170	9.96240		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

Sin d. Tan d.c. Cot Cos d. P. P.	23°								156°	
Section Sect		Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
ST 9.60887 18 9.63851 2 0.36149 9.96230 3 48 34 35 48 34 35 34 35 34 35 34 35 34 35 34 34	50	9.60070	7.7	9.63830	OT	0.36170	9.96240		50	
52 9.60105 17 9.63872 20 0.36128 9.96233 3 47 2 1 2.1 2.1 2.3 2.0 0.36108 9.96233 3 47 2 4.2 <t< th=""><th>51</th><th>9.60087</th><th></th><th>9.63851</th><th></th><th>0.36149</th><th>9.96236</th><th></th><th>49</th><th>21,</th></t<>	51	9.60087		9.63851		0.36149	9.96236		49	21,
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00	9.60931	17	9.64858	21	0.35142	9.96073		100	
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02	9.60965	17 17	9.64899	20	0.35101	9.96066	4	98	I 2.I
03	9.60982	17	9.64919	21	0.35081	9.96063	3	97	2 4.2
04	9.60999	17	9.64940	20	0.35060	9.96060	4	96	3 6.3 4 8.4
05	9.61016	17	9.64960	21	0.35040	9.96056	3	95	4 8.4 5 10.5
06	9.61033	17	9.64981	20	0.35019	9.96053	4	94	5 10.5 6 12.6
07 08	9.61050 9.61067	17	9.65001 9.65021	20	0.34999	9.96049 9.96046	3	93 92	7 14.7 8 16.8
09	9.61084	17	9.65042	21	0.34979	9.96043	3	91	9 18.9
10	9.61101	17	9.65062	20	0.34938	9.96039	4	90	
	9.61118	17	9.65082	20	0.34918	9.96036	3	89	20
11	9.61135	17	9.65103	21	0.34918	9.96030	4	88	I 2.0
13	9.61152	17	9.65123	20	0.34877	9.96029	3	87	2 4.0
14	9.61169	17	9.65143	20	0.34857	9.96026	3	86	
15	9.61186	17	9.65164	21	0.34836	9.96022	4	85	5 10.0
16	9.61203	17	9.65184	20 20	0.34816	9.96019	3	84	6 12.0
17	9.61220	17	9.65204		0.34796	9.96015	4	83	7 14.0 8 16.0
18	9.61236	16 17	9.65224	20 2I	0.34776	9.96012	3	82	9 18.0
19	9.61253	17	9.65245	20	0.34755	9.96009	4	81	
20	9.61270	17	9.65265	20	0.34735	9.96005	3	80	
21	9.61287	17	9.65285	21	0.34715	9.96002		79	17
22	9.61304	17	9.65306	20	0.34694	9.95998	4	78	I I.7
23	9.61321	17	9.65326	20	0.34674	9.95995	3	77	2 3.4
24	9.61338	16	9.65346	20	0.34654	9.95992	4	76	3 5.I 4 6.8
25 26	9.61354	17	9.65366	21	0.34634	9.95988	3	75	5 8.5
	9.61371	17	9.65387	20	0.34613	9.95985	4	74	6 IO.2 7 II.9
27 28	9.61388	17	9.65407	20	0.34593 0.34573	9.95981 9.95978	3	73 72	7 II.9 8 I3.6
29	9.61405	17	9.65447	20	0.34553	9.95978	4	71	9 15.3
30	9.61438	16	9.65467	20	0.34533	9.95971	3	70	
	9.61455	17	9.65488	21	0.34512	9.95968	3	69	16
31 32	9.61455	17	9.65508	20	0.34512	9.95964	4	68	1 1.6
33	9.61489	17	9.65528	20	0.34472	9.95961	3	67	2 3.2
34	9.61506	17	9.65548	20	0.34452	9.95957	4	66	3 4.8 4 6.4
35	9.61522	16	9.65568	20	0.34432	9.95954	3	65	5 8.0
36	9.61539	17 17	9.65589	2I 20	0.34411	9.95950	4	64	6 9.6 7 II.2
37	9.61556	ł	9.65609	20	0.34391	9.95947	3	63	8 12.8
38	9.61573	17	9.65629	20	0.34371	9.95944	3	62	9 14.4
39	9.61589	17	9.65649	20	0.34351	9.95940	3	61	
40	9.61606	17	9.65669	20	0.34331	9.95937	4	60	
41	9.61623	16	9.65689	21	0.34311	9.95933	3	59	3
42	9.61639	17	9.65710	20	0.34290	9.95930	4	58	I 0.3
43	9.61656	17	9.65730	20	0.34270	9.95926	3	57	2 0.6 3 0.9
44	9.61673 9.61689	16	9.65750	20	0.34250	9.95923 9.95920	3	56 55	4 1.2
45 46	9.61706	17	9.65770	20	0.34230	9.95926	4	55	5 I.5 6 I.8
47	9.61723	17	9.65810	20	0.34190	9.95913	3	53	
48	9.61739	16	9.65830	20	0.34170	9.95909	4	52	8 2.4
49	9.61756	17	9.65850	20	0.34150	9.95906	3	51	9 2.7
50	9.61773	17	9.65870	20	0.34130	9.95902	4	50	
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90 9.62432 16 9.66669 20 0.33331 9.95753 3 10 9.95763 3 08 9.95248 16 9.66729 20 0.33291 9.95755 3 08 1 9.95755 4 07 2	-4.4
91 9.62448 9 9.66689 20 0.33311 9.95759 4 09 9.62465 17 9.66709 20 0.33291 9.95756 3 08 1 9.95759 4 07 2	
92 9.62465 17 0.66709 20 0.33291 9.95756 3 08 1 93 9.62481 16 9.66729 20 0.33271 9.95752 4 07 2	4
93 9.62481 16 9.66729 20 0.33271 9.95752 4 07 2	
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04 0.62407 0.66748 0.22252 0.05740 06 3	1.2
05 0 62512 16 0 66768 20 0 22222 0 05745 4 05 4	1.6
96 9.62530 17 9.66788 20 0.33212 9.95742 3 04 5	2.0
97 9.62546 16 9.66808 20 0.33192 9.95738 4 03 7	2.4
98 9.62562 10 9.66828 20 9.33172 9.95735 3 92 8	3.2
99 9,62579 17 9,66847 19 9,33153 9,95731 4 91 9	3.6
100 9.62595 16 9.66867 20 0.33133 9.95728 3 00	
Cos d. Cot d. c. Tan Sin d. P.	P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
-00		<u>u.</u>	9.66867	<u>u. c.</u>	0.33133	9.95728		100	
00	9.62595	16	9.66887	20			4		
OI	9.62611	16	9.66907	20	0.33113	9.95724 9.95720	4	99 98	20
02	9.62627	17	9.66927	20	0.33093	9.95717	3	98	I 2.0
03	9.62644	16		19			4	96	2 4.0 3 6.0
04	9.62660	16	9.66946 9.66966	20	0.33054	9.95713	3	96 95	4 8.0
05 06	9.62676 9.62692	16	9.66986	20	0.33034	9.95710 9.95706	4	95	5 10.0
		16		20			3		
07	9.62708	17	9.67006 9.67025	19	0.32994	9.95703 9.95699	4	93 92	7 14.0 8 16.0
08	9.62725 9.62741	16	9.67025	20	0.32975	9.95696	3	92 91	9 18.0
09		16		20			4	90	
10	9.62757	16	9.67065	20	0.32935	9.95692	3		19
11	9.62773	16	9.67085	19	0.32915	9.95689	4	89 88	
12	9.62789	17	9.67104	20	0.32896 0.32876	9.95685 9.95681	4	87	I I.9 2 3.8
13	9.62806	16	9.67124	20			3		3 5.7
14	9.62822	16	9.67144	19	0.32856	9.95678	4	86 85	4 7.6
15	9.62838	16	9.67163	20	0.32837 0.32817	9.95674 9.95671	3	84	4 7.6 5 9.5 6 11.4
16	9.62854	16	9.67183	20			4		7 I3.3 8 I5.2
17	9.62870	16	9.67203	20	0.32797	9.95667 9.95664	3	83 82	
18	9.62886	16	9.67223 9.67242	19	0.32777	9.95660	4	81	9 17.1
19	9.62902	16		20			3	80	
20	9.62918	17	9.67262	20	0.32738	9.95657	4		
21	9.62935	16	9.67282	19	0.32718	9.95653	4	79	17
22	9.62951	16	9.67301	20	0.32699	9.95649	3	78	I I.7
23	9.62967	16	9.67321	20	0.32679	9.95646	4	77	2 3.4 3 5.1
24	9.62983	16	9.67341	19	0.32659	9.95642	3	76	3 5.I 4 6.8
25	9.62999	16	9.67360	20	0.32640	9.95639	4	75	5 8.5
26	9.63015	16	9.67380	19	0.32620	9.95635	3	74	4 6.8 5 8.5 6 10.2 7 11.9 8 13.6
27	9.63031	16	9.67399	20	0.32601	9.95632	4	73	7 II.9 8 I3.6
28	9.63047	16	9.67419	20	0.32581	9.95628	4	72 71	9 15.3
29	9.63063	16	9.67439	19	0.32561	9.95624	3	70	
30	9.63079	16	9.67458	20	0.32542	9.95621	4		16
31	9.63095	16	9.67478	20	0.32522	9.95617	3	69	1 1.6
32	9.63111	16	9.67498	19	0.32502	9.95614	4	68 67	2 3.2
33	9.63127	16	9.67517	20	0.32483	9.95610	4		3 4.8
34	9.63143	16	9.67537	19	0.32463	9.95606	3	66	
35	9.63159	16	9.67556	20	0.32444	9.95603	4	65 64	5 8.0 6 9.6
36	9.63175	16	9.67576	20	0.32424	9.95599	3		7 11.2
37	9.63191	16	9.67596	19	0.32404	9.95596	4	63 62	
38	9.63207	16	9.67615 9.67635	20	0.32385	9.95592 9.95588	4	61	9 14.4
39	9.63223	16		19			3	60	
40	9.63239	16	9.67654	20	0.32346	9.95585	4		
41	9.63255	16	9.67674	19	0.32326	9.95581	3	59	3
42	9.63271	16	9.67693	20	0.32307	9.95578	4	58	I 0.3 2 0.6
43	9.63287	16	9.67713	19		9.95574	4	57	2 0.6
44	9.63303	16	9.67732	20	0.32268	9.95570	3	56	4 1.2
45	9.63319	16	9.67752 9.67772	20	0.32248	9.95567 9.95563	4	55 54	5 I.5 6 I.8
46	9.63335	16		19	1		3		3 0.9 4 1.2 5 1.5 6 1.8 7 2.1 8 2.4
47	9.63351	16	9.67791	20	0.32209	9.95560	4	53 52	8 2.4
48	9.63367 9.63383	16	9.67830	19	0.32109	9.95550	4	52	9 2.7
49		15		20		1	3	50	
50	9.63398		9.67850	1	0.32150	9.95549		- 00	D. D.
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

								104	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.63398	16	9.67850	19	0.32150	9.95549		50	
51	9.63414	16	9.67869		0.32131	9.95545	4	49	20
52	9.63430	16	9.67889	20 19	0.32111	9.95542	3	48	1 2.0
53	9.63446	16	9.67908	20	0.32092	9.95538	4	47	2 4.0
54	9.63462	16	9.67928]	0.32072	9.95534	4	46	3 6.0
55	9.63478	16	9.67947	19 20	0.32053	9.95531	3	45	4 8.0
56	9.63494	16	9.67967	19	0.32033	9.95527	4	44	5 IO.0 6 I2.0
57	9.63510	15	9.67986		0.32014	9.95523		43	7 14.0
58	9.63525	16	9.68005	19 20	0.31995	9.95520	3	42	
59	9.63541	16	9.68025	19	0.31975	9.95516	4 3	41	9 18.0
60	9.63557	16	9.68044	20	0.31956	9.95513	4	40	
61	9.63573	16	9.68064)	0.31936	9.95509		39	19
62	9.63589	15	9.68083	19 20	0.31917	9.95505	4	38	I I.9
63	9.63604	16	9.68103	19	0.31897	9.95502	3 4	37	2 3.8 3 5.7
64	9.63620	16	9.68122		0.31878	9.95498		36	3 5.7
65	9.63636	16	9.68142	20 19	0.31858	9.95494	4	35	5 9.5
66	9.63652	16	9.68161	19	0.31839	9.95491	3 4	34	
67	9.63668	15	9.68180	20	0.31820	9.95487		33	7 13.3 8 15.2
68	9.63683	16	9.68200	19	0.31800	9.95483	4	32	9 17.1
69	9.63699	16	9.68219	20	0.31781	9.95480	3 4	31	
70	9.63715	16	9.68239	19	0.31761	9.95476	3	30	
71	9.63731		9.68258	1	0.31742	9.95473		29	16
72	9.63746	15 16	9.68277	19 20	0.31723	9.95469	4	28	1 1.6
73	9.63762	16	9.68297	19	0.31703	9.95465	4 3	27	2 3.2
74	9.63778	16	9.68316		0.31684	9.95462	1	26	3 4.8
75	9.63794	15	9.68336	20 19	0.31664	9.95458	4	25	4 6.4 5 8.0
76	9.63809	16	9.68355	19	0.31645	9.95454	4 3	24	5 8.0 6 9.6
77	9.63825	16	9.68374		0.31626	9.95451		23	7 11.2
78	9.63841	15	9.68394	20 19	0.31606	9.95447	4	22	
79	9.63856	16	9.68413	19	0.31587	9.95443	3	21	9 14.4
80	9.63872	16	9.68432	20	0.31568	9.95440	4	20	
81	9.63888		9.68452		0.31548	9.95436		19	15
82	9.63903	15 16	9.68471	19	0.31529	9.95432	4	18	I 1.5
83	9.63919	16	9.68490	19 20	0.31510	9.95429	3 4	17	2 3.0 3 4.5
84	9.63935		9.68510		0.31490	9.95425	1	16	4 6.0
85	9.63950	15 16	9.68529	19	0.31471	9.95421	4 3	15	5 7.5
86	9.63966	16	9.68548	20	0.31452	9.95418	4	14	
87	9.63982	15	9.68568	19	0.31432	9.95414	4	13	7 IO.5 8 I2.0
88	9.63997	16	9.68587	19	0.31413	9.95410	3	12	9 13.5
89	9.64013	15	9.68606	20	0.31394	9.95407	4	II	
90	9.64028	16	9.68626	19	0.31374	9.95403	4	10	
91	9.64044	16	9.68645	19	0.31355	9.95399	3	09	4
92	9.64060	15.	9.68664	19	0.31336	9.95396	4	о8	I 0.4
93	9.64075	16	9.68683	20	0.31317	9.95392	4	07	2 0.8
94	9.64091	15	9.68703	19	0.31297	9.95388	4	06	3 I.2 4 I.6
95	9.64106	16	9.68722	19	0.31278	9.95384	3	05	
96	9.64122	16	9.68741	19	0.31259	9.95381	4	04	5 2.0 6 2.4
97	9.64138	15	9.68760	20	0.31240	9 95377	4	03	7 2.8 8 3.2
98	9.64153	16	9.68780	19	0.31220	9.95373	4	02	8 3.2 9 3.6
99	9.64169	15	9.68799	19	0.31201	9.95369	3	10	7 , 0
100	9.64184		9.68818	-	0.31182	9.95366		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.64184	16	9.68818	19	0.31182	9.95366		100	
OI	9.64200		9.68837	1	0.31163	9.95362	4	99	20
02	9.64215	15	9.68857	20	0.31143	9.95359	3	98	1 2.0
03	9.64231	16	9.68876	19	0.31124	9.95355	4	97	2 4.0
04	9.64246	1	9.68895		0.31105	9.95351	4	96	3 6.0
05	9.64262	16	9.68914	19	0.31086	9.95348	3	95	4 8.0
06	9.64277	15	9.68934	20 19	0.31066	9.95344	4 4	94	5 10.0 6 12.0
07	9.64293	ł	9.68953		0.31047	9.95340	1	93	7 14.0
о8	9.64308	15	9.68972	19	0.31028	9.95336	4	92	
09	9.64324	15	9.68991	19 19	0.31009	9.95333	3	91	9 18.0
10	9.64339	16	9.69010	19	0.30990	9.95329	4	90	
11	9.64355	15	9.69029		0.30971	9.95325		89	19
12	9.64370	16	9.69049	20 19	0.30951	9.95322	3	88	1 1.9 3.8
13	9.64386	15	9.69068	19	0.30932	9.95318	4	87	3 3.8
14	9.64401	16	9.69087		0.30913	9.95314	1	86	4 7.6
15	9.64417	15	9.69106	19 19	0.30894	9.95310	3	85	5 9.5
16	9.64432	15	9.69125	19	0.30875	9.95307	4	84	6 11.4
17	9.64447	16	9.69144	20	0.30856	9.95303	1	83	7 13.3 8 15.2
18	9.64463	15	9.69164	19	0.30836	9.95299	4 4	82	9 17.1
19	9.64478	16	9.69183	19	0.30817	9.95295	3	81	
20	9.64494	15	9.69202	19	0.30798	9.95292	4	80	
21	9.64509	15	9.69221	19	0.30779	9.95288	4	79	16
22	9.64524	16	9.69240	19	0.30760	9.95284	3	78	1 1.6
23	9.64540	15	9.69259	19	0.30741	9.95281	4	77	2 3.2
24	9.64555	16	9.69278	20	0.30722	9.95277	4	76	3 4.8
25	9.64571	15	9.69298	19	0.30702	9.95273	4	75	
26	9.64586	15	9.69317	19	0.30683	9.95269	3	74	6 9.6
27	9.64601	16	9.69336	19	0.30664	9.95266	4	73	7 II.2 8 I2.8
28	9.64617	15	9.69355	19	0.30645	9.95262	4	72	9 14.4
29	9.64632	15	9.69374	19	0.30626	9.95258	4	71	31 -4.4
30	9.64647	16	9.69393	19	0.30607	9.95254	3	70	15
31	9.64663	15	9.69412	19	0.30588	9.95251	4	69	
32	9.64678	15	9.69431	19	0.30569	9.95247	4	68	I I.5 2 3.0
33	9.64693	16	9.69450	19	0.30550	9.95243	4	67	3 4.5
34	9.64709	15	9.69469	19	0.30531	9.95239	3	66	4 6.0
35 36	9.64724 9.64739	15	9.69488 9.69507	19	0.30512	9.95236	4	65 64	5 7.5 6 9.0
		16		19		9.95232	4		7 10.5
37 38	9.64755 9.64770	15	9.69526	19	0.30474 0.30455	9.95228	4	63 62	
39	9.64776	15	9.69545 9.69565	20	0.30455	9.95224 9.95221	3	61	9 13.5
40	9.64800	15	9.69584	19	0.30435	9.95217	4	60	
41	9.64816	16	9.69603	19	0.30397	9.95217	4	59	
42	9.64831	15	9.69622	19	0.30397	9.95213	4	59 58	3
43	9.64846	15	9.69641	19	0.30359	9.95206	3	57	I 0.3 2 0.6
44	9.64861	15	9.69660	19	0.30340	9.95202	4	56	3 0.9
45	9.64877	16	9.69679	19	0.30321	9.93202	4	55	4 I.2
46	9.64892	15	9.69698	19	0.30302	9.95194	4	54	5 I.5 6 I.8
47	9.64907	15	9.69717	19	0.30283	9.95190	4	53	7 2.1
48	9.64922	15	9.69736	19	0.30264	9.95187	3	52	7 2.1 8 2.4
49	9.64938	16 15	9.69755	19	0.30245	9.95183	4	51	9 2.7
50	9.64953	13	9.69774	19	0.30226	9.95179	4	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

26								103	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.64953	15	9.69774	19	0.30226	9.95179		50	
51	9.64968		9.69793	· 1	0.30207	9.95175	4	49	19
52	9.64983	15 15	9.69812	19	0.30188	9-95172	3	48	1 1.9
53	9.64998	16	9.69831	19	0.30169	9.95168	4	47	2 3.8
54	9.65014		9.69850	18	0.30150	9.95164		46	3 5.7 7.6
55	9.65029	15 15	9.69868	19	0.30132	9.95160	4	45	4 7.6 5 9.5
56	9.65044	15	9.69887	19	0.30113	9.95156	4 3	44	6 11.4
57	9.65059	-	9.69906	-	0.30094	9.95153		43	7 13.3
58	9.65074	15 15	9.69925	19 19	0.30075	9.95149	4	42	
59	9.65089	15	9.69944	19	0.30056	9.95145	4	41	9 17.1
60	9.65104	16	9.69963	19	0.30037	9.95141	4	40	
61	9.65120		9.69982	-	0.30018	9.95137		39	18
62	9.65135	15	9.70001	19	0.29999	9.95134	3	38	1 1.8
63	9.65150	15	9.70020	19 19	0.29980	9.95130	4	37	2 3.6 3 5.4
64	9.65165	1	9.70039		0.29961	9.95126		36	4 7.2
65	9.65180	15 15	9.70058	19 19	0.29942	9.95122	4	35	5 9.0
66	9.65195	15	9.70077	19	0.29923	9.95118	3	34	6 10.8
67	9.65210	1	9.70096	18	0.29904	9.95115		33	7 12.6 8 14.4
68	9.65225	15	9.70114	19	0.29886	9.95111	4	32	9 16.2
69	9.65240	15	9.70133	19	0.29867	9.95107	4	31	
70	9.65255	16	9.70152	19	0.29848	9.95103	4	30	
71	9.65271		9.70171		0.29829	9.95099		29	15
72	9.65286	15	9.70190	19	0.29810	9.95096	3	28	1 1.5
73	9.65301	15	9.70209	19	0.29791	9.95092	4	27	2 3.0
74	9.65316	1	9.70228	1	0.29772	9.95088		26	3 4.5 4 6.0
75	9.65331	15	9.70247	19	0.29753	9.95084	4	25	
76	9.65346	15	9.70265	19	0.29735	9.95080	4	24	6 9.0
77	9.65361		9.70284		0.29716	9.95076		23	7 10.5 8 12.0
78	9.65376	15	9.70303	19	0.29697	9.95073	3	22	8 12.0 9 13.5
79	9.65391	15	9.70322	19	0.29678	9.95069	4	21	9 13.3
80	9.65406	15	9.70341	19	0.29659	9.95065	4	20	
81	9.65421	1	9.70360	19	0.29640	9.95061	4	19	14
82	9.65436	15	9.70379	18	0.29621	9.95057	3	18	1 1.4
83	9.65451	15	9.70397	19	0.29603	9.95054	4	17	3 4.2
84	9.65466	15	9.70416	19	0.29584	9.95050	4	16	4 5.6
85	9.65481	15	9.70435	19	0.29565	9.95046	4	15	5 7.0 6 8.4
86	9.65496	15	9.70454	19	0.29546	9.95042	4	14	
87	9.65511	15	9.70473	18	0.29527	9.95038	4	13	8 11.2
88	9.65526	15	9.70491	19	0.29509	9.95034	4	12 11	9 12.6
89	9.65541	- 15	9.70510	19	0.29490	9.95030	3		
90	9.65556	- 15	9.70529	19	0.29471	9.95027	4	10	
91	9.65571	14	9.70548	19	0.29452	9.95023	4	09	4
92	9.65585	15	9.70567	18	0.29433	9.95019	4	08	1 0.4
93	9.65600	15	9.70585	19	0.29415	9.95015	4	07	2 0.8 3 1.2
94	9.65615	15	9.70604	19	0.29396	9.95011	4	06	
95	9.65630	15	9.70623	19	0.29377	9.95007	3	05	5 2.0
96	9.65645	15	9.70642	18	0.29358	9.95004	4	04	
97	9.65660	15	9.70660	19	0.29340	9.95000	4	03	8 3.2
98	9.65675	15	9.70679 9.70698	19	0.29321	9.94996 9.94992	4	01	9 3.6
99	9.65690	- 15		- 19			4	00	
100	9.65705	-	9.70717	1	0.29283	9.94988	d.	-00	P. P.
	Cos	d.	Cot	1 d. c.	Tan	Sin	. d.	1	P. P.

	Sin	l d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.65705		9.70717		0.29283	9.94988		100	
OI	9.65720	15	9.70735	18	0.29265		4		
02	9.65720	14	9.70735	19	0.29205	9.94984 9.94980	4	99 98	19
03	9.65749	15	9.70773	19	0.29240	9.94986	4	97	1 1.9
		15		19			3		2 3.8
04 05	9.65764 9.65779	15	9.70792	18	0.29208	9.94973	4	96	3 5.7 4 7.6
06	9.65779	15	9.70810	19	0.29190	9.94969	4	95	5 9.5
		15		19		9.94965	4	94	6 11.4
07	9.65809	14	9.70848	18	0.29152	9.94961	4	93	7 13.3 8 15.2
o8 o9	9.65823	15	9.70866	19	0.29134	9.94957	4	92	8 15.2 9 17.1
	9.65838	15	9.70885	19	0.29115	9.94953	4	91	9 17.1
10	9.65853	15	9.70904	18	0.29096	9.94949	3	90	
II	9.65868	15	9.70922	19	0.29078	9.94946	4	89	18
12	9.65883	15	9.70941	19	0.29059	9.94942	4	88	1 1.8
13	9.65898	14	9.70960	18	0.29040	9.94938	4	87	2 3.6 3 5.4
14	9.65912		9.70978		0.29022	9.94934		86	3 5.4
15	9.65927	15 15	9.70997	19	0.29003	9.94930	4	85	5 9.0
16	9.65942	15	9.71016	18	0.28984	9.94926	4	84	
17	9.65957		9.71034		0.28966	9.94922		83	7 12.6 8 14.4
18	9.65971	14	9.71053	19	0.28947	9.94918	4	82	8 I4.4 9 I6.2
19	9.65986	15	9.71072	19 18	0.28928	9.94914	4	81	3 1 20.2
20	9.66001	15	9.71090		0.28910	9.94911	3	80	
21	9.66016	15	9.71109	19	0.28891	9.94907	4	79	15
22	9.66030	14	9.71128	19	0.28872	9.94903	4	78	
23	9.66045	15	9.71146	18	0.28854	9.94899	4	77	I I.5 2 3.0
24	9.66060	15	9.71165	19	0.28835	9.94895	4	76	
25	9.66075	15	9.71184	19	0.28816	9.94891	4	75	4 6.0
26	9.66089	14	9.71202	18	0.28798	9.94887	4	74	5 7.5
27	9.66104	15		19	0.28779		4		6 9.0
28	9.66119	15	9.71221 9.71239	18	0.287/9	9.94883 9.94879	4	73 72	7 10.5 8 12.0
29	9.66133	14	9.71258	19	0.28742	9.94875	4	71	9 13.5
30	9.66148	15		19			4	70	
		15	9.71277	18	0.28723	9.94871	3		14
31	9.66163	14	9.71295	19	0.28705	9.94868	4	69	
32	9.66177	15	9.71314	18	0.28686	9.94864	4	68	I 1.4 2 2.8
33	9.66192	15	9.71332	19	0.28668	9.94860	4	67	3 4.2
34	9.66207	14	9.71351	19	0.28649	9.94856	4	66	4 5.6
35	9.66221	15	9.71370	18	0.28630	9.94852	4	65	4 5.6 5 7.0 6 8.4
36	9.66236	15	9.71388	19	0.28612	9.94848	4	64	
37	9.66251	14	9.71407	18	0.28593	9.94844	4	63	8 11.2
38	9.66265	15	9.71425	19	0.28575	9.94840	4	62	9 12.6
39	9.66280	15	9.71444	18	0.28556	9.94836	4	61	
40	9.66295	14	9.71462	19	0.28538	9.94832		60	
41	9.66309		9.71481		0.28519	9.94828	4	59	3
42	9.66324	15	9.71499	18	0.28501	9.94824	4	58	
43	9.66338	14	9.71518	19	0.28482	9.94820	4	57	2 0.6
44	9.66353	15	9.71537	19	0.28463	9.94817	3	56	3 0.9
45	9.66368	15	9.71555	18	0.28445	9.94813	4	55	4 1.2
46	9.66382	14	9.71574	19	0.28426	9.94809	4	54	4 1.2 5 1.5 6 1.8
47	9.66397	15	9.71592	18	0.28408	9.94805	4	53	7 2.1
48	9.66411	14	9.71611	19	0.28389	9.94801	4	52	7 2.I 8 2.4
49	9.66426	15	9.71629	18	0.28371	9.94797	4	51	9 2.7
50	9.66441	15	9.71648	19	0.28352	9.94793	4	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
		u.		ч. с.	Lan	- DIII	u.		

27								152	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.66441	14	9.71648	18	0.28352	9.94793	4	50	
51	9.66455	15	9.71666	19	0.28334	9.94789		49	19
52	9.66470	14	9.71685	18	0.28315	9.94785	4	48	
53	9.66484	15	9.71703	19	0.28297	9.94781	4	47	2 3.8
54	9.66499	14	9.71722	18	0.28278	9.94777		46	3 5.7
55	9.66513	15	9.71740	19	0.28260	9.94773	4	45	4 7.6 5 9.5
56	9.66528	14	9.71759	18	0.28241	9.94769	4	44	5 9.5 6 II.4
57	9.66542	15	9.71777	19	0.28223	9.94765	4	43	7 13.3
58	9.66557	14	9.71796	18	0.28204	9.94761	4	42	
59	9.66571	15	9.71814	19	0.28186	9.94757	4	41	9 17.1
60	9.66586	14	9.71833	18	0.28167	9.94753	4	40	
61	9.66600	15	9.71851	18	0.28149	9.94749	4	39	18
62	9.66615	14	9.71869	19	0.28131	9.94745	4	38	I I.8
63	9.66629	15	9.71888	18	0.28112	9.94741	4	37	2 3.6 3 5.4
64	9.66644	14	9.71906	19	0.28094	9.94737	3	36	4 7.2
65	9.66658	15	9.71925	18	0.28075	9.94734	4	35	5 9.0
66	9.66673	14	9.71943	19	0.28057	9.94730	4	34	
67	9.66687	15	9.71962	18	0.28038	9.94726	4	33	7 12.6 8 14.4
68	9.66702	14	9.71980	18	0.28020	9.94722	4	32	9 16.2
69	9.66716	15	9.71998	19	0.28002	9.94718	4	31	
70	9.66731	14	9.72017	18	0.27983	9.94714	4	30	•
71	9.66745	14	9.72035	19	0.27965	9.94710	4	29	15
72	9.66759	15	9.72054	18	0.27946	9.94706	4	28	1 1.5
73	9.66774	14	9.72072	19	0.27928	9.94702	4	27	2 3.0
74	9.66788	15	9.72091	18	0.27909	9.94698	4	26	3 4.5 4 6.0
75	9.66803	14	9.72109	18	0.27891	9.94694	4	25	4 6.0 5 7.5
76	9.66817	14	9.72127	19	0.27873	9.94690	4	24	6 9.0
77	9.66831	15	9.72146	18	0.27854	9.94686	4	23	7 10.5 8 12.0
78	9.66846	14	9.72164	18	0.27836	9.94682	4	22	8 12.0 9 13.5
79	9.66860	15	9.72182	19	0.27818	9.94678	4	21	9 23.3
80	9.66875	14	9.72201	18	0.27799	9.94674	4	20	44
81	9.66889	14	9.72219	19	0.27781	9.94670	4	19	14
82	9.66903	15	9.72238	18	0.27762	9.94666	4	18	I I.4 2 2.8
83	9.66918	14	9.72256	18	0.27744	9.94662	4	17	3 4.2
84	9.66932	14	9.72274	19	0.27726	9.94658	4	16	4 5.6
85	9.66946	15	9.72293	18	0.27707	9.94654	4	15	4 5.6 5 7.0 6 8.4
86	9.66961	14	9.72311	18	0.27689	9.94650	4	14	7 9.8
87	9.66975	14	9.72329	19	0.27671	9.94646	4	13	8 11.2
88 89	9.66989	15	9.72348	18	0.27652	9.94642	4	12	9 12.6
	9.67004	14	9.72366	18	0.27634	9.94638	4	II	
90	9.67018	14	9.72384	19	0.27616	9.94634	4	10	
91	9.67032	15	9.72403	18	0.27597	9.94630	4	09	4
92	9.67047	14	9.72421	18	0.27579	9.94626	4	08	I 0.4 2 0.8
93	9.67061	14	9.72439	19	0.27561	9.94622	4	07	2 0.8 3 1.2
94	9.67075	15	9.72458	18	0.27542	9.94618	4	06	4 1.6
95 96	9.67090 9.67104	14	9.72476	18	0.27524	9.94614	4	05	5 2.0
		14	9.72494	19	0.27506	9.94610	4	04	6 2.4 7 2.8
97 98	9.67118 9.67132	14	9.72513	18	0.27487	9.94606	4	03	7 2.8 8 3.2
99	9.67132	15	9.7253I 9.72549	18	0.27469	9.94598	4	01	9 3.6
100	9.67161	14	9.72567	18	0.27433	9.94593	5	00	
200	Cos	d.	Cot	d. c.	Tan	9.94593 Sin	d.		P. P.
	COS	u.	COL	u. c.	ian	5111	(1.	•	1.F.

	01							101	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.67161	14	9.72567	19	0.27433	9.94593	4	100	
OI	9.67175	14	9.72586	18	0.27414	9.94589		99	19
02	9.67189	15	9.72604	18	0.27396	9.94585	4	98	
03	9.67204	14	9.72622	19	0.27378	9.94581	4	97	I 1.9 2 3.8
04	9.67218	14	9.72641	18	0.27359	9.94577		96	3 5.7
05	9.67232	14	9.72659	18	0.27341	9.94573	4	95	4 7.6
06	9.67246	15	9.72677	18	0.27323	9.94569	4	94	5 9.5 6 11.4
07	9.67261	-	9.72695		0.27305	9.94565		93	6 II.4 7 I3.3
08	9.67275	14	9.72714	19	0.27286	9.94561	4	92	7 13.3 8 15.2
09	9.67289	14	9.72732	18	0.27268	9.94557	4	91	9 17.1
10	9.67303		9.72750	18	0.27250	9.94553	4	90	
11	9.67317	14	9.72768		0,27232	9.94549	4	89	18
12	9.67332	15	9.72787	19	0.27213	9.94545	4	88	1 1.8
13	9.67346	14	9.72805	18	0.27195	9.94541	4	87	2 3.6
14	9.67360	14	9.72823	18	0.27177	9.94537	. 4	86	3 5.4
15	9.67374	14	9.72841	18	0.27159	9.94533	4	85	4 7.2
16	9.67388	14	9.72859	18	0.27141	9.94529	4	84	5 9.0 6 10.8
17	9.67402	14	9.72878	19	0.27122	9.94525	4	83	7 12.6 8 14.4
18	9.67417	15	9.72896	18	0.27104	9.94521	4	82	8 14.4
19	9.67431	14	9.72914	18	0.27086	9.94517	4	81	9 16.2
20	9.67445	14	9.72932	18	0.27068	9.94513	4	80	
21		14		18			5		
21	9.67459	14	9.72950	19	0.27050	9.94508	4	79	15
23	9.67473 9.67487	14	9.72969 9.72987	18	0.27031	9.94504	4	78	I I.5
_		14		18	0.27013	9.94500	4	77	2 3.0
24	9.67501	14	9.73005	18	0.26995	9.94496	4	76	3 4.5 4 6.0
25 26	9.67515	15	9.73023	18	0.26977	9.94492	4	75	
	9.67530	14	9.73041	19	0.26959	9.94488	4	74	5 7.5 6 9.0 7 10.5 8 12.0
27	9.67544	14	9.73060	18	0.26940	9.94484	4	73	7 10.5
28 29	9.67558	14	9.73078	18	0.26922	9.94480	4	72	8 12.0 9 13.5
	9.67572	14	9.73096	18	0.26904	9.94476	4	71	9 13.3
30	9.67586	14	9.73114	18	0.26886	9.94472	4	70	
31	9.67600	14	9.73132	18	0.26868	9.94468		69	14
32	9.67614	14	9.73150	19	0.26850	9.94464	4	68	I I.4
33	9.67628	14	9.73169	18	0.26831	9.94460	4 5	67	2 2.8 3 4.2
34	9.67642		9.73187	18	0.26813	9.94455		66	
35	9.67656	14	9.73205	18	0.26795	9.94451	4	65	5 7.0
36	9.67670	14	9.73223	18	0.26777	9.94447	4	64	6 8.4
37	9.67684		9.73241	18	0.26759	9.94443	4	63	7 9.8 8 11.2
38	9.67698	14	9.73259	18	0.26741	9.94439	4	62	9 12.6
39	9.67712	14	9.73277	18	0.26723	9.94435	4	61	
40	9.67726		9.73295		0.26705	9.94431	4	60	
41	9.67740	14	9.73314	19	0.26686	9.94427	4	59	4
42	9.67754	14	9.73332	18	0.26668	9.94423	4	58	
43	9.67768	14	9.73350	18	0.26650	9.94419	4	57	I 0.4 2 0.8
44	9.67782	14	9.73368	18	0.26632	9.94415	4	56	3 1.2
45	9.67796	14	9.73386	18	0.26614	9.94410	5	55	4 1.6
46	9.67810	14	9.73404	18	0.26596	9.94406	4	54	5 2.0
47	9.67824	14	9.73422	18	0.26578	9.94402	4	53	3 1.2 4 1.6 5 2.0 6 2.4 7 2.8 8 3.2
48	9.67838	14	9.73440	18	0.26560	9.94402	4	53	8 3.2
49	9.67852	14	9.73458	18	0.26542	9.94394	4	51	9 3.6
50	9.67866	14	9.73476	18	0.26524	9.94390	4	50	
	Cos	d.	Cot	4.0	Tan			-00	D D
	Cos	a.	Cot	d. c.	lan	Sin	d.		P. P.

28°								151°	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.67866	14	9.73476	19	0.26524	9.94390	4	50	
51	9.67880	14	9.73495	18	0.26505	9.94386		49	18
52	9.67894	14	9.73513	18	0.26487	9.94382	4 5	48	1 1.8
53	9.67908	14	9.73531	18	0.26469	9.94377	4	47	2 3.6
54	9.67922	14	9.73549	18	0.26451	9.94373	4	46	3 5.4
55	9.67936	14	9.73567	18	0.26433	9.94369	4	45	
56	9.67950	14	9.73585	18	0.26415	9.94365	4	44	5 9.0 6 10.8 7 12.6 8 14.4
57 58	9.67964 9.67978	14	9.73603 9.73621	13	0.26397	9.94361 9.94357	4	43 42	7 12.6 8 14.4
59	9.67992	14	9.73639	18	0.26361	9.94357	4	41	9 16.2
60	9.68006	14	9.73657	18	0.26343	9.94349	4	40	
61	9.68020	14	9.73675	18	0.26325	9.94344	5	39	17
62	9.68033	13	9.73693	18	0.26307	9.94344	4	38	1 1.7
63	9.68047	14	9.73711	18	0.26289	9.94336	4	37	2 3.4
64	9.68061	14	9.73729	18	0.26271	9.94332	4	36	3 5.I 4 6.8
65	9.68075	14	9.73747	18	0.26253	9.94328	4	35	
66	9.68089	14	9.73765	18	0.26235	9.94324	4	34	6 10.2
67	9.68103		9.73783	18	0.26217	9.94320		33	7 II.9 8 I3.6
68	9.68117	14 13	9.73801	18	0.26199	9.94315	5 4	32	9 15.3
69	9.68130	14	9.73819	18	0.26181	9.94311	4	31	
70	9.68144	14	9.73837	18	0.26163	9.94307	4	30	
71	9.68158	14	9.73855	т8	0.26145	9.94303	4	29	14
72	9.68172	14	9.73873	18	0.26127	9.94299	4	28	I 1.4
73	9.68186	14	9.73891	18	0.26109	9.94295	4	27	2 2.8 3 4.2
74	9.68200	13	9.73909	18	0.26091	9.94291	5	26	4 5.6
75 76	9.68213 9.68227	14	9.73927	18	0.26073	9.94286	4	25 24	5 7.0 6 8.4
		14	9.73945	18		9.94282	4		7 9.8
77 78	9.68241 9.68255	14	9.73963 9.73981	18	0.26037	9.94278 9.94274	4	23	8 11.2
79	9.08255	14	9.73999	18	0.26001	9.94274	4	21	9 12.6
80	9.68283	14	9.74017	18	0.25983	9.94266	4	20	
81	9.68296	13	9.74035	18	0.25965	9.94261	5	19	13
82	9.68310	14	9.74053	18	0.25947	9.94257	4	18	I I.3 2 2.6
83	9.68324	14	9.74071	18	0.25929	9.94253	4	17	2 2.6 3.9
84	9.68338	14	9.74089	18	0.25911	9.94249	4	16	4 5.2
85	9.68351	13	9.74107	18	0.25893	9.94245	4	15	4 5.2 5 6.5 6 7.8
86	9.68365	14 14	9.74125	17	0.25875	9.94241	5	14	7 9.1
87	9.68379	14	9.74142	18	0.25858	9.94236	4	13	8 10.4
88	9.68393	13	9.74160	18	0.25840	9.94232	4	12	9 11.7
89	9.68406	14	9.74178	18	0.25822	9.94228	4	II	
90	9.68420	14	9.74196	18	0.25804	9.94224	4	10	
91	9.68434	14	9.74214	18	0.25786	9.94220	5	09	5
92	9.68448	13	9.74232	18	0.25768	9.94215	4	08	1 0.5
93	9.68461	14	9.74250	18	0.25750	9.94211	4	07	2 I.0 3 I.5
94	9.68475	14	9.74268	18	0.25732	9.94207	4	06	4 2.0
95 96	9.68489 9.68502	13	9.74286 9.74304	18	0.25714	9.94203	4	05 04	5 2.5
97		14		18			4		
97 98	9.68516 9.68530	14	9.74322 9.74339	17	0.25678	9.94195 9.94190	5	03	8 4.0
99	9.68543	13	9.74339	18	0.25643	9.94190	4	01	9 4.5
100	9.68557	14	9.74375	18	0.25625	9.94182	4	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	COS	u.	COL	а. с.	Ian	- Dili	u.		1.1.

_	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.68557	_u.		<u>u. c.</u>			_u.	100	F. F.
		14	9.74375	18	0.25625	9.94182	4		
0I 02	9.68571	13	9.74393	18	0.25607	9.94178	4	99 98	18
03	9.68598	14	9.74411	18	0.25589	9.94174 9.94169	5	90	I 1.8
_		14		18	l .		4		2 3.6
04	9.68612	13	9.74447	18	0.25553	9.94165	4	96	3 5.4 4 7.2
o5 o6	9.68639	14	9.74465 9.74482	17	0.25535	9.94161	4	95 94	
		14		18		9.94157	5		6 10.8
o7 o8	9.68653 9.68666	13	9.74500	18	0.25500	9.94152	4	93	7 12.6 8 14.4
09	9.68680	14	9.74518	18	0.25482	9.94148	4	92 91	8 14.4 9 16.2
		14	9.74536	18		9.94144	4		7
10	9.68694	13	9.74554	18	0.25446	9.94140	4	90	477
II	9.68707	14	9.74572	17	0.25428	9.94136	5	89	. 17
12	9.68721	13	9.74589	18	0.25411	9.94131	4	88	I I.7 2 3.4
13	9.68734	14	9.74607	18	0.25393	9.94127	4	87	
14	9.68748	14	9.74625	18	0.25375	9.94123	4	86	4 6.8
15	9.68762	13	9.74643	18	0.25357	9.94119	5	85	5 8.5 6 10.2
16	9.68775	14	9.74661	18	0.25339	9.94114	4	84	6 10.2
17	9.68789	13	9.74679	17	0.25321	9.94110	4	83	7 II.9 8 I3.6
18	9.68802	14	9.74696	18	0.25304	9.94106	4	82	9 15.3
19	9.68816	13	9.74714	18	0.25286	9.94102	4	81	
20	9.68829	14	9.74732	18	0.25268	9.94098	5	80	
21	9.68843		9.74750	18	0.25250	9.94093		79	14
22	9.68857	14	9.74768	17	0.25232	9.94089	4	78	I I.4
23	9.68870	14	9.74785	18	0.25215	9.94085	4	77	2 2.8
24	9.68884		9.74803	18	0.25197	9.94081		76	3 4.2
25	9.68897	13 14	9.74821	18	0.25179	9.94076	5	75	4 5.6
26	9.68911	13	9.74839	17	0.25161	9.94072	4	74	5 7.0 6 8.4 7 9.8
27	9.68924		9.74856	18	0.25144	9.94068		73	7 9.8 8 II.2
28	9.68938	14 13	9.74874	18	0.25126	9.94064	4	72	8 II.2 9 I2.6
29	9.68951	14	9.74892	18	0.25108	9.94059	5 4	71	9 12.0
30	9.68965	13	9.74910	17	0.25090	9.94055		70	
31	9.68978		9.74927		0.25073	9.94051	4	69	13
32	9.68992	14	9.74945	18 18	0.25055	9.94047	4	68	I I.3 2 2.6
33	9.69005	13 14	9.74963	18	0.25037	9.94042	5	67	2 2.6 3.9
34	9.69019		9.74981	1	0.25019	9.94038	4	66	4 5.2
35	9.69032	13	9.74998	17	0.25002	9.94034	4	65	4 5.2 5 6.5 6 7.8
36	9.69046	14	9.75016	18 18	0.24984	9.94030	4	64	6 7.8 7 9.1
37	9.69059	13	9.75034	18	0.24966	9.94025	5	63	7 9.1 8 10.4
38	9.69073	14	9.75052	18	0.24948	9.94021	4	62	9 11.7
39	9.69086	13 14	9.75069	18	0.24931	9.94017	4	61	
40	9.69100		9.75087	18	0.24913	9.94012	5	60	
41	9.69113	13	9.75105		0.24895	9.94008	4	59	4
42	9.69113	14	9.75123	18	0.24877	9.94004	4	58	_
43	9.69140	13	9.75140	17	0.24860	9.94000	4	57	1 0.4 2 0.8
44	9.69153	13	9.75158		0.24842	9.93995	5	56	
45	9.69167	14	9.75176	18	0.24824	9.93991	4	55	4 I.6 5 2.0
46	9.69180	13	9.75193	17	0.24807	9.93987	4	54	6 2.4
47	9.69194	14	9.75211		0.24789	9.93983	4	53	7 2.8
48	9.69207	13	9.75229	18	0.24771	9.93978	5	52	8 3.2 9 3.6
49	9.69220	13	9.75247	18	0.24753	9.93974	4	51	9 3.6
50	9.69234	14	9.75264	17	0.24736	9.93970	4	50	
_	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	. 0:	. 1	(D)	. 1	0.1				
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.69234	13	9.75264	18	0.24736	9.93970	5	50	
51	9.69247	14	9.75282	18	0.24718	9.93965	-	49	18
52	9.69261	13	9.75300	17	0.24700	9.93961	4	48	- I I.8
53	9.69274	13	9.75317	18	0.24683	9.93957	4	47	2 3.6
54	9.69287	14	9.75335	18	0.24665	9.93953		46	3 5.4
55	9.69301	13	9.75353	17	0.24647	9.93948	5	45	4 7.2
56	9.69314	14	9.75370	18	0.24630	9.93944	4	44	5 9.0 6 10.8
57	9.69328	13	9.75388	18	0.24612	9.93940		43	7 12.6 8 14.4
58	9.69341	13	9.75406	17	0.24594	9.93935	5	42	
59	9.69354	14	9.75423	18	0.24577	9.93931	4	41	9 16.2
60	9.69368	13	9.75441	18	0.24559	9.93927	5	40	
61	9.69381		9.75459		0.24541	9.93922	4	39	17
62	9.69394	13	9.75476	17	0.24524	9.93918	4	38	I 1.7
63	9.69408		9.75494	17	0.24506	9.93914		37	2 3.4
64	9.69421	13	9.75511	18	0.24489	9.93909	5	36	3 5.I 4 6.8
65	9.69434	13	9.75529	18	0.24471	9.93905	4	35	5 8.5
66	9.69448	13	9.75547	17	0.24453	9.93901	4	34	6 10.2
67	9.69461		9.75564	18	0.24436	9.93897		33	7 II.9 8 I3.6
68	9.69474	13 13	9.75582	18	0.24418	9.93892	5	32	9 15.3
69	9.69487	13	9.75600	17	0.24400	9.93888	4	31	01.0.0
70	9.69501		9.75617	18	0.24383	9.93884		30	
71	9.69514	13	9.75635		0.24365	9.93879	5	29	14
72	9.69527	13	9.75652	17	0.24348	9.93875	4	28	1 1.4
73	9.69541	14	9.75670	18	0.24330	9.93871	4	27	2 2.8
74	9.69554	13	9.75688	18	0.24312	9.93866	5	26	3 4.2
75	9.69567	13	9.75705	17	0.24295	9.93862	4	25	4 5.6
76	9.69580	13	9.75723	18	0.24277	9.93858	4	24	5 7.0 6 8.4
77	9.69594	14	9.75740	17	0.24260	9.93853	5	23	7 9.8 8 11.2
78	9.69607	13	9.75758	18	0.24242	9.93849	4	22	
79	9.69620	13	9.75776	18	0.24224	9.93845	4	21	9 12.6
80	9.69633	13	9.75793	17	0.24207	9.93840	5	20	
81	9.69647	14	9.75811	18	0.24189	9.93836	4	19	13
82	9.69660	13	9.75828	17	0.24172	9.93832	4	18	I I.3 2 2.6
83	9.69673	13	9.75846	18	0.24154	9.93827	5	17	2 2.6
84	9.69686	13	9.75863	17	0.24137	9.93823	4	16	3 3.9 4 5.2
85	9.69699	13	9.75881	18	0.24137	9.93819	4	15	4 5.2 5 6.5 6 7.8
86	9.69713	14	9.75899	18	0.24101	9.93814	5	14	6 7.8
87	9.69726	13	9.75916	17	0.24084	9.93810	4	13	7 9.1 8 10.4
88	9.69739	13	9.75934	18	0.24066	9.93805	5	12	9 11.7
89	9.69752	13	9.75951	17	0.24049	9.93801	4	II	
90	9.69765	13	9.75969	18	0.24031	9.93797	4	10	
91	9.69779	14	9.75986	17	0.24014	9.93792	5	09	5
92	9.69779	13	9.75900	18	0.23996	9.93792	4	08	_
93	9.69805	13	9.76021	17	0.23990	9.93784	4	07	I 0.5 2 I.0
94	9.69818	13	9.76039	18	0.23961	9.93779	5	06	3 1.5
94 95	9.69831	13	9.76039	17	0.23944	9.93779	4	05	4 2.0
96	9.69844	13	9.76074	18	0.23944	9.93771	4	04	4 2.0 5 2.5 6 3.0
97	9.69858	14	9.76091	17	0.23909	9.93766	5	03	
98	9.69871	13	9.76109	18	0.23909	9.93762	4	03	8 4.0
99	9.69884	13	9.76126	17	0.23874	9.93757	5	OI	9 4.5
100	9.69897	13	9.76144	18	0.23856	9.93753	4	00	
-	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	COS	u,	Cot	u. c.	ran	OIII I	u.		r. r.

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	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.69897	13	9.76144	17	0.23856	9.93753	4	100	
OI	9.69910	13	9.76161	18	0.23839	9.93749	5	99	18
02	9.69923	13	9.76179	17	0.23821	9.93744	4	98	1 1.8
03	9.69936	13	9.76196	18	0.23804	9.93740	4	97	2 3.6
04	9.69949	14	9.76214	17	0.23786	9.93736	5	96	3 5.4
05	9.69963	13	9.76231	18	0.23769	9.93731	4	95	4 7.2 5 9.0
06	9.69976	13	9.76249	17	0.23751	9.93727	5	94	5 9.0 6 10.8
07	9.69989	13	9.76266	18	0.23734	9.93722	4	93	7 12.6
08	9.70002	13	9.76284	17	0.23716	9.93718	4	92	8 14.4
09	9.70015	13	9.76301	18	0.23699	9.93714	5	91	9 16.2
10	9.70028	13	9.76319	17	0.23681	9.93709	4	90	
11	9.70041		9.76336	18	0.23664	9.93705		89	17
12	9.70054	13	9.76354	17	0.23646	9.93700	5	88	I I.7
13	9.70067	13 13	9.76371	18	0.23629	9.93696	4	87	2 3.4 3 5.1
14	9.70080	_	9.76389		0.23611	9.93692		86	3 5.I 4 6.8
15	9.70093	13 13	9.76406	17 18	0.23594	9.93687	5 4	85	5 8.5
16	9.70106	13	9.76424	17	0.23576	9.93683	5	84	6 10.2
17	9.70119	-	9.76441		0.23559	9.93678		83	7 II.9 8 I3.6
18	9.70132	13 13	9.76458	17 18	0.23542	9.93674	4	82	9 15.3
19	9.70145	13	9.76476	17	0.23524	9.93670	4 5	81	
20	9.70159		9.76493	18	0.23507	9.93665		80	
21	9.70172	13	9.76511		0.23489	9.93661	4	79	14
22	9.70185	13	9.76528	17 18	0.23472	9.93656	5	78	1 1.4
23	9.70198	13	9.76546	17	0.23454	9.93652	4	77	2 2.8
24	9.70211	13	9.76563		0.23437	9.93648	4	76	3 4.2
25	9.70224	13	9.76580	17 18	0.23420	9.93643	5	75	4 5.6
26	9.70237	13	9.76598	17	0.23402	9.93639	4	74	5 7.0 6 8.4
27	9.70250	13	9.76615		0.23385	9.93634	5	73	7 9.8
28	9.70263	13	9.76633	18	0.23367	9.93630	4	72	8 11.2
29	9.70276	13 12	9.76650	17 18	0.23350	9.93625	5	71	9 12.6
30	9.70288		9.76668		0.23332	9.93621	4	70	
31	9.70301	13	9.76685	17	0.23315	9.93617	4	69	13
32	9.70314	13	9.76702	17	0.23298	9.93612	5	68	I I.3 2 2.6
33	9.70327	13	9.76720	18 17	0.23280	9.936c8	4	67	2 2.6 3 3.9
34	9.70340	13	9.76737		0.23263	9.93603	5	66	3 3.9 4 5.2 5 6.5 6 7.8
35	9.70353	13	9.76754	17	0.23246	9.93599	4	65	4 5.2 5 6.5 6 7.8
36	9.70366	13	9.76772	18 17	0.23228	9.93594	5	64	6 7.8
37	9.70379	13	9.76789		0.23211	9.93590	4	63	7 9.1 8 10.4
38	9.70392	13	9.76807	18	0.23193	9.93585	5	62	9 11.7
39	9.70405	13 13	9.76824	17 17	0.23176	9.93581	4	61	
40	9.70418	_	9.76841	17	0.23159	9.93577		60	
41	9.70431	13	9.76859		0.23141	9.93572	5	59	4
42	9.70444	13	9.76876	17	0.23124	9.93568	4	58	1 0.4
43	9.70457	13	9.76893	17 18	0.23107	9.93563	5	57	2 0.8
44	9.70470	13	9.76911		0.23089	9.93559	4	56	3 1.2
45	9.70482	12	9.76928	17	0.23072	9.93554	5	55	4 I.6 5 2.0
46	9.70495	13	9.76945	17	0.23055	9.93550	. 5	54	4 I.6 5 2.0 6 2.4
47	9.70508	13	9.76963		0.23037	9.93545		53	7 2.8
48	9.70521	13	9.76980	17	0.23020	9.93541	4	52	
49	9.70534	13 13	9.76998	18 17	0.23002	9.93537	5	51	9 3.6
50	9.70547	13	9.77015	- 1	0.22985	9.93532	3	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

30°								149°	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.70547	13	9.77015	17	0.22985	9.93532	4	50	
51	9.70560	-	9.77032	18	0.22968	9.93528	- 1	49	18
52	9.70573	13 12	9.77050	17	0.22950	9.93523	5 4	48	1 1.8
53	9.70585	13	9.77067	17	0.22933	9.93519	5	47	2 3.6
54	9.70598	13	9.77084	17	0.22916	9.93514		46	2 3.6 3 5.4
55	9.70611	13	9.77101	18	0.22899	9.93510	4 5	45	4 7.2 5 9.0
56	9.70624	13	9.77119	17	0.22881	9.93505	4	44	5 9.0 6 10.8
57	9.70637	13	9.77136	17	0.22864	9.93501		43	7 12.6
58	9.70650	12	9.77153	18	0.22847	9.93496	5 4	42	8 14.4 9 16.2
59	9.70662	13	9.77171	17	0.22829	9.93492	5	41	9 10.2
60	9.70675	13	9.77188	17	0.22812	9.93487	4	40	
61	9.70688	13	9.77205	18	0.22795	9.93483		39	17
62	9.70701	13	9.77223	17	0.22777	9.93478	5 4	38	I I.7
63	9.70714	13	9.77240	17	0.22760	9.93474	5	37	2 3.4 3 5.1
64	9.70727	12	9.77257	17	0.22743	9.93469	4	36	
65	9.70739	13	9.77274	18	0.22726	9.93465	5	35	5 8.5
66	9.70752	13	9.77292	17	0.22708	9.93460	4	34	6 10.2
67	9.70765	13	9.77309	17	0.22691	9.93456	5	33	7 II.9 8 I3.6
68	9.70778	12	9.77326	18	0.22674	9.93451	4	32	9 15.3
69	9.70790	13	9.77344	17	0.22656	9.93447	5	31	
70	9.70803	13	9.77361	17	0.22639	9.93442	4	30	
71	9.70816	13	9.77378	17	0.22622	9.93438	5	29	13
72	9.70829	13 13	9.77395	18	0.22605	9.93433	5	28	1 1.3
73	9.70842	12	9.77413	17	0.22587	9.93429	5	27	I I.3 2 2.6
74	9.70854	13	9.77430	17	0.22570	9.93424	4	26	3 3.9 4 5.2 5 6.5 6 7.8
75	9.70867	13	9.77447	17	0.22553	9.93420	5	25	4 5.2 5 6.5 6 7.8
76	9.70880	12	9.77464	18	0.22536	9.93415	4	24	6 7.8
77	9.70892	13	9.77482	17	0.22518	9.93411	5	23	7 9.1
78	9.70905	13	9.77499	17	0.22501	9.93406	4	22	8 10.4 9 11.7
79	9.70918	13	9.77516	17	0.22484	9.93402	5	21	3 33.1
80	9.70931	12	9.77533	18	0.22467	9.93397	4	20	12
81	9.70943	13	9.77551	17	0.22449	9.93393	5	19	
82	9.70956	13	9.77568	17	0.22432	9.93388	4	18	I I.2 2 2.4
83	9.70969	12	9.77585	17	0.22415	9.93384	5	17	3 3.6
84	9.70981	13	9.77602	17	0.22398	9.93379	4	16	4 4.8 5 6.0
85 86	9.70994	13	9.77619	18	0.22381	9.93375	5	15	4 4.8 5 6.0 6 7.2
	9.71007	13	9.77637	17	0.22363	9.93370	4	14	7 8.4
87 88	9.71020	12	9.77654	17	0.22346	9.93366	5	13	8 9.6
89	9.71032	13	9.77671	17	0.22329	9.93361	4	12	9 10.8
	9.71045	13	9.77688	18	0.22312	9.93357	5		
90	9.71058	12	9.77706	17	0.22294	9.93352	5	10	
91	9.71070	13	9.77723	17	0.22277	9.93347	4	09	5
92	9.71083	13	9.77740	17	0.22260	9.93343	5	08	I 0.5
93	9.71096	12	9-77757	17	0.22243	9.93338	4	07	2 I.0 3 I.5
94	9.71108	13	9-77774	17	0.22226	9.93334	5	06	4 2.0
95 96	9.71121	12	9.77791	18	0.22209	9.93329	4	05	5 2.5
	9.71133	13	9.77809	17			5		6 3.0
97	9.71146	13	9.77826	17	0.22174	9.93320	4	03	7 3.5
98 99	9.71159	12	9.77843	17	0.22157	9.93316	5	02 01	9 4.5
100	9.71171	13		17	_	1	4	00	
100	9.71184	-	9.77877		0.22123	9.93307	-		P. P.
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

31°								148°	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
00	9.71184		9.77877	18	0.22123	9.93307		100	
OI	9.71197	13	9.77895		0.22105	9.93302	5	99	18
02	9.71209	12	9.77912	17	0.22088	9.93297	5	98	1 1.8
03	9.71222	13 12	9.77929	17	0.22071	9.93293	4 5	97	2 3.6
04	9.71234		9.77946		0.22054	9.93288		96	3 5.4
05	9.71247	13 13	9.77963	17 17	0.22037	9.93284	4 5	95	4 7.2 5 9.0
06	9.71260	12	9.77980	17	0.22020	9.93279	4	94	5 9.0 6 10.8 7 12.6 8 14.4
07	9.71272	13	9.77997	18	0.22003	9.93275	5	93	7 12.6
08	9.71285	13	9.78015	17	0.21985	9.93270	5	92	8 14.4
09	9.71297	13	9.78032	17	0.21968	9.93265	4	91	9 10.2
10	9.71310	12	9.78049	17	0.21951	9.93261	5	-90	
11	9.71322		9.78066		0.21934	9.93256		89	17
12	9.71335	13 13	9.78083	17	0.21917	9.93252	4 5	88	1 1.7
13	9.71348	13	9.78100	17	0.21900	9.93247	4	87	2 3.4 3 5.1
14	9.71360	13	9.78117	18	0.21883	9.93243	5	86	3 5.I 4 6.8
15	9.71373	13	9.78135	17	0.21865	9.93238	5	85	4 6.8 5 8.5 6 10.2
16	9.71385	13	9.78152	17	0.21848	9.93233	4	84	
17	9.71398	12	9.78169	17	0.21831	9.93229	5	83	7 II.9 8 I3.6
18	9.71410	13	9.78186	17	0.21814	9.93224	4	82	9 15.3
19	9.71423	12	9.78203	17	0.21797	9.93220	5	81	
20	9.71435	13	9.78220	17	0.21780	9.93215	4	80	
21	9.71448	12	9.78237		0.21763	9.93211		79	13
22	9.71460	13	9.78254	17 17	0.21746	9.93206	5 5	78	I I.3 2 2.6
23	9.71473	12	9.78271	18	0.21729	9.93201	4	77	
24	9.71485	13	9.78289	17	0.21711	9.93197	5	76	3 3.9 4 5.2
25	9.71498	13	9.78306	17	0.21694	9.93192	4	75	4 5.2 5 6.5 6 7.8
26	9.71510	13	9.78323	17	0.21677	9.93188	5	74	5 6.5 6 7.8
27	9.71523	12	9.78340	17	0.21660	9.93183	5	73	7 9.1 8 10.4
28	9.71535	13	9.78357	17	0.21643	9.93178	4	72	9 11.7
29	9.71548	12	9.78374	17	0.21626	9.93174	5	71	, ,,
30	9.71560	13	9.78391	17	0.21609	9.93169	4	70	12
31	9.71573	12	9.78408	17	0.21592	9.93165	5	69	1 1.2
32	9.71585	13	9.78425	17	0.21575	9.93160	5	68 67	
33	9.71598	12	9.78442	17	0.21558	9.93155	4		3 3.6
34	9.71610	12	9.78459	17	0.21541	9.93151	5	66	4 4.8 5 6.0
35	9.71622	13	9.78476	17	0.21524	9.93146	5	65 64	4 4.8 5 6.0 6 7.2
36	9.71635	12	9.78493	17	0.21507	9.93141	4		7 8.4
37	9.71647	13	9.78510	18	0.21490	9.93137	5	63 62	8 9.6
38 39	9.71660 9.71672	12	9.78528 9.78545	17	0.21472	9.93132 9.93128	4	61	9 10.8
40		13		17			5	60	
	9.71685	12	9.78562	17	0.21438	9.93123	5		
41	9.71697	12	9.78579	17	0.21421	9.93118	4	59	4
42	9.71709 9.71722	13	9.78596 9.78613	17	0.21404	9.93114	5	58 57	1 0.4
43		12		17			5	56	2 0.8 3 1.2
44	9.71734	13	9.78630	17	0.21370	9.93104	4	55	4 1.6
45 46	9.71747 9.71759	12	9.78664	17	0.21336	9.93100	5	54	4 1.6 5 2.0 6 2.4
		12	9.78681	17	0.21319	9.93093	4	53	6 2.4 7 2.8
47 48	9.71771	13	9.78698	17	0.21319	9.93091	5	53	8 3.2
49	9.71704	12	9.78715	17	0.21302	9.93081	5	51	9 3.6
50	9.71790	13	9.78732	17	0.21268	9.93077	4	50	
- 00	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	Cos	u.	COL	d. C.	1411	OIII	. ц.	-	1.1.

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-	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.71809	12	9.78732	17	0.21268	9.93077	5	50	
51	9.71821	12	9.78749	17	0.21251	9.93072	5	49	17
52	9.71833	13	9.78766	17	0.21234	9.93067	4	48	17 1.7
53	9.71846	12	9.78783	17	0.21217	9.93063	5	47	2 3.4
54	9.71858	12	9.78800	17	0.21200	9.93058	5	46	3 5.I
55	9.71870	13	9.78817	17	0.21183	9.93053	4	45	4 6.8 5 8.5
56	9.71883	12	9.78834	17	0.21166	9.93049	5	44	4 6.8 5 8.5 6 10.2
57	9.71895	12	9.78851	17	0.21149	9.93044	5	43	7 II.9 8 I3.6
58	9.71907	13	9.78868	17	0.21132	9.93039	3	42	
59	9.71920	12	9.78885	17	0.21115	9.93035	5	41	9 15.3
60	9.71932	12	9.78902	17	0.21098	9.93030	5	40	
61	9.71944		9.78919		0.21081	9.93025	ì	39	16
62	9.71957	13	9.78936	17	0.21064	9.93021	4	38	1 1.6
63	9.71969	12	9.78953	17	0.21047	9.93016	5	37	2 3.2
64	9.71981		9.78970	1	0.21030	9.93011	5	36	3 4.8 4 6.4
65	9.71994	13	9.78987	17	0.21013	9.93007	4	35	5 8.0
66	9.72006	12	9.79004	17	0.20996	9.93002	5	34	
67	9.72018		9.79021		0.20979	9.92997	5	33	7 11.2 8 12.8
68	9.72030	12	9.79038	17	0.20962	9.92993	4	32	9 14.4
69	9.72043	13	9.79055	17	0.20945	9.92988	5	31	3 1 - 1.4
70	9.72055		9.79072		0.20928	9.92983	5	30	
71	9.72067	12	9.79089	17	0.20911	9.92979	4	29	13
72	9.72079	12	9.79009	17	0.20894	9.92974	5	28	
73	9.72092	13	9.79122	16	0.20878	9.92969	5	27	I I.3 2 2.6
74	9.72104	12	9.79139	17	0.20861	9.92965	4	26	3 3.9
75	9.72116	12	9.79139	17	0.20844	9.92960	5	25	4 5.2
76	9.72128	12	9.79173	17	0.20827	9.92955	5	24	3 3.9 4 5.2 5 6.5 6 7.8
77	9.72141	13	9.79190	17	0.20810	9.92951	4	23	7 9.1
78	9.72141	12	9.79190	17	0.20793	9.92931	5	22	7 9.1 8 10.4
79	9.72165	12	9.79224	17	0.20776	9.92941	5	21	9 11.7
80	9.72177	12	9.79241	17	0.20759	9.92936	5	20	
81		13		17			4		12
81	9.72190	12	9.79258	17	0.20742	9.92932	5	19	I I.2
83	9.72202	12	9.79275	17	0.20725	9.92927	5	17	2 2.4
	9.72214	12	9.79292	17		9.92922	4		3 3.6
84	9.72226	12	9.79309	17	0.20691	9.92918	5	16	4 4.8 5 6.0
85 86	9.72238 9.72251	13	9.79326 9.79343	17	0.20674	9.92913 9.92908	5	15 14	6 7.2
		12		16			5		7 8.4
87 88	9.72263	12	9.79359	17	0.20641	9.92903	4	13 12	8 9.6
89	9.72275 9.72287	12	9.79376	17	0.20024	9.92899 9.92894	5	II	9 10.8
90		12	9.79393	17			5	10	
	9.72299	13	9.79410	17	0.20590	9.92889	4		
91	9.72312	12	9.79427	17	0.20573	9.92885	5	09	5
92	9.72324	12	9.79444	17	0.20556	9.92880	5	08	I 0.5
93	9.72336	12	9.79461	17	0.20539	9.92875	5	07	2 I.0 3 I.5
94	9.72348	12	9.79478	17	0.20522	9.92870	4	06	3 I.5 4 2.0
95	9.72360	12	9.79495	16	0.20505	9.92866	5	05	5 2.5
96	9.72372	13	9.79511	17	0.20489	9.92861	5	04	
97	9.72385	12	9.79528	17	0.20472	9.92856	4	03	7 3.5 8 4.0
98	9.72397	12	9.79545	17	0.20455	9.92852	5	02	9 4.5
99	9.72409	12	9.79562	17	0.20438	9.92847	5	OI	. , , ,
100	9.72421		9 - 79579		0.2042I	9.92842		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

32°								141	
77	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.72421	12	9.79579	17	0.20421	9.92842	5	100	1
OI	9 72433	-	9.79596		0.20404	9.92837	- 1	99	17
02	9.72445	12 12	9.79613	17	0.20387	9.92833	5	98	1 1.7
03	9.72457	12	9.79630	16	0.20370	9.92828	5	97	2 3.4
04	9.72469		9.79646		0.20354	9.92823	5	96	3 5.I 4 6.8
05	9.72482	13 12	9.79663	17 17	0.20337	9.92818	4	95	
06	9.72494	12	9.79680	17	0.20320	9.92814	5	94	5 8.5 6 10.2
07	9.72506		9.79697		0.20303	9.92809	5	93	7 II.9 8 I3.6
08	9.72518	12	9.79714	17	0.20286	9.92804	5	92	
09	9.72530	12	9.79731	16	0.20269	9.92799	4	91	9 15.3
10	9.72542	12	9.79747	17	0.20253	9.92795	5	90	
11	9.72554		9.79764		0.20236	9.92790	5	89	16
12	9.72566	12 12	9.79781	17 17	0.20219	9.92785	5	88	1 1.6
13	9.72578	12	9.79798	17	0.20202	9.92780	4	87	3 3.2 4.8
14	9.72590	12	9.79815	17	0.20185	9.92776	5	86	4 6.4
15	9.72602	12	9.79832	16	0.20168	9.92771	5	85	5 8.0
16	9.72614	13	9.79848	17	0.20152	9.92766	5	84	6 9.6 7 II.2
17	9.72627	12	9.79865	17	0.20135	9.92761	5	83	7 II.2 8 I2.8
18	9.72639	12	9.79882	17	0.20118	9.92756	4	82	9 14.4
19	9.72651	12	9.79899	17	0.20101	9.92752	5	81	
20	9.72663	12	9.79916	16	0.20084	9.92747	5	80	
21	9.72675	12	9.79932		0.20068	9.92742	5	79	13
22	9.72687	12	9.79949	17	0.20051	9.92737	4	78	1 1.3
23	9.72699	12	9.79966	17	0.20034	9.92733	5	77	2 2.6
24	9.72711	1	9.79983		0.20017	9.92728	5	76	3 3.9
25	9.72723	12	9.80000	17	0.20000	9.92723	5	75	4 5.2
26	9.72735	12	9.80016	17	0.19984	9.92718	5	74	4 5.2 5 6.5 6 7.8
27	9.72747	12	9.80033	17	0.19967	9.92713	4	73	7 9.1
28	9.72759	12	9.80050	17	0.19950	9.92709	5	72	8 IO.4 9 II.7
29	9.72771	12	9.80067	17	0.19933	9.92704	5	71	9 11.7
30	9.72783	12	9.80084	16	0.19916	9.92699	5	70	12
31	9.72795	12	9.80100	17	0.19900	9.92694	4	69	
32	9.72807	12	9.80117	17	0.19883	9.92690	5	68	I 1.2 2 2.4
33	9.72819	12	9.80134	17	0.19866	9.92685	5	67	3 3.6
34	9.72831	12	9.80151	17	0.19849	9.92680	5	66	4 4.8
35	9.72843	12	9.80168	16	0.19832	9.92675	5	65	5 6.0
36	9.72855	12	9.80184	17	0.19816	9.92670	4	64	7 8.4
37	9.72867	12	9.80201	17	0.19799	9.92666	5	63	8 9.6
38	9.72879	II	9.80218	17	0.19782	9.92661	5	62	9 10.8
39	9.72890	12	9.80235	16	0.19765	9.92656	5	61	
40	9.72902	. 12	9.80251	17	0.19749	9.92651	5	60	
41	9.72914	12	9.80268	17	0.19732	9.92646	5	59	4
42	9.72926	12	9.80285	17	0.19715	9.92641	4	58	I 0.4 2 0.8
43	9.72938	12	9.80302	16	0.19698	9.92637	5	57	2 0.8
44	9.72950	12	9.80318	17	0.19682	9.92632	5	56	3 I.2 4 I.6
45	9.72962	12	9.80335	17	0.19665	9.92627	5	55	5 2.0
46	9.72974	12	9.80352	17	0.19648	9.92622	5	54	
47	9.72986	12	9.80369	16	0.19631	9.92617	4	53	
48	9.72998	12	9.80385	17	0.19615	9.92613	5	52 51	8 3.2 9 3.6
49	9.73010	12		17	0.19598		- 5	50	
50	9.73022		9.80419		0.19581	9.92603	- 1	- 30	P. P.
	Cos	d.	Cot	d. c.	Tan	Sin	d.		r. r.

	Sin	d.	Tan	d. c.	Cot	Con	a		D.D.
		d.		d. c.	Cot	Cos	d.		P. P.
50	9.73022	12	9.80419	16	0.19581	9.92603	5	50	
51	9.73034	11	9.80435	17	0.19565	9.92598	5	49	17
52	9.73045	12	9.80452	17	0.19548	9.92593	5	48	1 177
53	9.73057	12	9.80469	17	0.19531	9.92588	4	47	2 3.4
54	9.73069	12	9.80486	16	0.19514	9.92584	5	46	3 5.I 4 6.8
55	9.73081	12	9.80502	17	0.19498	9.92579	5	45	
56	9.73093	12	9.80519	17	0.19481	9.92574	5	44	6 10.2
57	9.73105	12	9.80536	16	0.19464	9.92569	5	43	7 II.9 8 I3.6
58	9.73117	12	9.80552 9.80569	17	0.19448	9.92564	5	42 41	9 15.3
59	9.73129	II		17	0.19431	9.92559	4		9 -3.5
60	9.73140	12	9.80586	17	0.19414	9.92555	5	40	10
61	9.73152	12	9.80603	16	0.19397	9.92550	5	39	16
62	9.73164	12	9.80619	17	0.19381	9.92545	5	38	I 1.6 2 3.2
63	9.73176	12	9.80636	17	0.19364	9.92540	5	37	3 4.8
64	9.73188	12	9.80653	16	0.19347	9.92535	5	36	4 6.4
65	9.73200	II	9.80669	17	0.19331	9.92530	5	35	5 8.0
66	9.73211	12	9.80686	17	0.19314	9.92525	4	34	6 9.6 7 II.2
67	9.73223	12	9.80703	16	0.19297	9.92521	5	33	8 12.8
68	9.73235	12	9.80719	17	0.19281	9.92516	5	32	9 14.4
69	9.73247	12	9.80736	17	0.19264	9.92511	5	31	
70	9.73259	12	9.80753	16	0.19247	9.92506	5	30	
71	9.73271	11	9.80769	17	0.19231	9.92501	5	29	12
72	9.73282	12	9.80786	17	0.19214	9.92496	5	28	I I.2
73	9.73294	12	9.80803	16	0.19197	9.92491	5	27	2 2.4 3 3.6
74	9.73306	12	9.80819	17	0.19181	9.92486	4	26	3 3.6
75	9.73318	II	9.80836	17	0.19164	9.92482	5	25	4 4.8 5 6.0 6 7.2
76	9.73329	12	9.80853	16	0.19147	9.92477	5	24	6 7.2
77	9.73341	12	9.80869	17	0.19131	9.92472	5	23	7 8.4 8 9.6
78	9.73353	12	9.80886	17	0.19114	9.92467	5	22 2I	9 10.8
79	9.73365	12	9.80903	16	0.19097	9.92462	5		
80	9.73377	11	9.80919	17	0.19081	9.92457	5	20	11
81	9.73388	12	9.80936	17	0.19064	9.92452	5	19	1 1.1
82	9.73400	12	9.80953	16	0.19047	9.92447	4	18	2 2.2
83	9.73412	12	9.80969	17	0.19031	9.92443	5	17	3 3.3
84	9.73424	11	9.80986	17	0.19014	9.92438	5	16	4 4.4
85 86	9.73435	12	9.81003	16	0.18997	9.92433	5	15 14	5 5.5 6 6.6
	9.73447	12		17	1		5		7 7.7 8 8.8
87 88	9.73459	II	9.81036 9.81052	16	0.18964	9.92423 9.92418	5	13	
89	9.73470 9.73482	12	9.81052	17	0.18931	9.92418	5	11	9 9.9
		12		17			5	10	
90	9.73494	12	9.81086	16	0.18914	9.92408	5		
91	9.73506	11	9.81102	17	0.18898	9.92403	5	09 08	5
92	9.73517	12	9.81119 9.81136	17	0.18864	9.92398 9.92394	4	07	I 0.5 2 1.0
93	9.73529	12		16			5	06	3 1.5
94	9.73541	11	9.81152	17	0.18848	9.92389 9.92384	5	05	4 2.0
95 96	9.73552	12	9.81185	16	0.18815	9.92304	5	04	5 2.5
_	9.73564	12		17			5		
97 98	9.73576	12	9.81202	17	0.18798	9.92374 9.92369	5	03	7 3.5 8 4.0
98	9.73588 9.73599	· II	9.81219	16	0.18765	9.92364	5	01	9 4.5
100		12	9.81252	17	0.18748	9.92359	5	00	
100	9.73611	-	Cot	d. c.	Tan	Sin	d.	-	P. P.
	Cos	d.	· Cot	. d. c.	lan	, 0111	. ц.		F.F.

33								140	
N.	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.73611	12	9.81252	16	0.18748	9.92359	5	100	
10	9.73623	-	9.81268		0.18732	9.92354		99	17
02	9.73634	11 12	9.81285	17 17	0.18715	9.92349	5 5	98	I 1.7
03	9.73646	12	9.81302	16	0.18698	9.92344	5	97	2 3.4
04	9.73658		9.81318		0.18682	9.92339		96	3 5.1
05	9.73669	11	9.81335	17 16	0.18665	9.92335	4	95	4 6.8
06	9.73681	II	9.81351	17	0.18649	9.92330	5	94	5 8.5 6 10.2
07	9.73692		9.81368		0.18632	9.92325		93	7 11.9 8 13.6
08	9.73704	12 12	9.81384	16 17	0.18616	9.92320	5 5	92	
09	9.73716	II	9.81401	17	0.18599	9.92315	5	91	9 15.3
10	9.73727	12	9.81418	16	0.18582	9.92310		90	
11	9.73739		9.81434	}	0.18566	9.92305	5	89	16
12	9.73751	12	9.81451	17 16	0.18549	9.92300	5	88	1 1.6
13	9.73762	11 12	9.81467	17	0.18533	9.92295	5	87	2 3.2
14	9.73774		9.81484		0.18516	9.92290	5	86	3 4.8 4 6.4
15	9.73785	11	9.81500	16	0.18500	9.92285	5	85	5 8.0
16	9.73797	12	9.81517	17 16	0.18483	9.92280	5 5	84	5 8.0 6 9.6
17	9.73809		9.81533		0.18467	9.92275		83	7 11.2 8 12.8
18	9.73820	11	9.81550	17 17	0.18450	9.92270	5 5	82	9 14.4
19	9.73832	II	9.81567	16	0.18433	9.92265	5	81	
20	9.73843	12	9.81583	17	0.18417	9.92260	5	80	
21	9.73855		9.81600		0.18400	9.92255		79	12
22	9.73867	12	9.81616	16	0.18384	9.92250	5	78	1 1.2
23	9.73878	11 12	9.81633	17 16	0.18367	9.92245	5	77	2 2.4
24	9.73890	1	9.81649	1	0.18351	9.92240	5	76	3 3.6
25	9.73901	II	9.81666	17 16	0.18334	9.92235	5	75	4 4.8 5 6.0
26	9.73913	12 11	9.81682	17	0.18318	9.92231	4	74	5 6.0 6 7.2
27	9.73924	1	9.81699	16	0.18301	9.92226	5	73	7 8.4
28	9.73936	12 11	9.81715	17	0.18285	9.92221	5	72	8 9.6
29	9.73947	12	9.81732	16	0.18268	9.92216	5 5	71	9 10.8
30	9.73959	12	9.81748	17	0.18252	9.92211	5	70	
31	9.73971		9.81765		0.18235	9.92206		69	11
32	9.73982	11	9.81781	16 17	0.18219	9.92201	5 5	68	I I.I
33	9.73994	II	9.81798	16	0.18202	9.92196	5	67	2 2.2 3 3.3
34	9.74005		9.81814	1	0.18186	9.92191		66	4 4.4
35	9.74017	12 11	9.81831	17 16	0.18169	9.92186	5 5	65	4 4.4 5 5.5 6 6.6
36	9.74028	12	9.81847	17	0.18153	9.92181	5	64	
37	9.74040	11	9.81864	16	0.18136	9.92176	5	63	7 7.7 8 8.8
38	9.74051	12	9.81880	17	0.18120	9.92171	5	62	9 9.9
39	9.74063	11	9.81897	16	0.18103	9.92166	5	61	
40	9.74074	12	9.81913	17	0.18087	9.92161	5	60	
41	9.74086	111	9.81930	16	0.18070	9.92156	5	59	5
42	9.74097	12	9.81946	17	0.18054	9.92151	5	58	1 0.5
43	9.74109	II	9.81963	16	0.18037	9.92146	5	57	2 I.O
44	9.74120	12	9.81979	17	0.18021	9.92141	5	56	3 I.5 4 2.0
45	9.74132	II	9.81996	16	0.18004	9.92136	5	55	5 2.5
46	9.74143	12	9.82012	17	0.17988	9.92131	5	54	6 3.0
47	9.74155	11	9.82029	16	0.17971	9.92126	5	53	7 3.5 8 4.0
48	9.74166	11	9.82045	17	0.17955	9.92121	5	52	9 4.5
49	9.74177	12	9.82062	16	0.17938	9.92116	5	51	, , , ,
50	9.74189		9.82078		0.17922	9.92111		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.74189		9.82078	<u>a. c.</u>	0.17922	9.92111	<u>u.</u>	50	
		11		17			5		
51 52	9.74200 9.74212	12	9.82095 9.82111	16	0.17905	9.92106 9.92101	5	49 48	17_
53	9.74212	II	9.82111	17	0.17872	9.92101	5	47	I I.7
		12		16			5		2 3.4
54	9.74235 9.74246	II	9.82144	17	0.17856	9.92091 9.92086	5	46	3 5.I 4 6.8
55 56	9.74240	12	9.82177	16	0.17823	9.92081	5 6	45 44	5 8.5
		II	9.82194	17			6		6 10.2
57 58	9.74269 9.74280	11	9.82210	16	0.17806 0.17790	9.92075 9.92070	5	43 42	7 II.9 8 I3.6
59	9.74292	12	9.82216	16	0.17790	9.92070	5	42 4I	9 15.3
60	9.74303	II	9.82243	17	0.17757	9.92060	5	40	
		12		16			5		16
61 62	9.74315	11	9.82259	17	0.17741	9.92055	5	39	1 1.6
63	9.74326	II	9.82276 9.82292	16	0.17724 0.17708	9.92050	5	38 37	2 3.2
	9.74337	12	-	17			5		3 4.8
64 65	9.74349	11	9.82309 9.82325	16	0.17691 0.17675	9.92040	5	36	
66	9.74360 9.74372	12	9.82325	16	0.17675	9.92035	5	35 34	4 0.4 5 8.0 6 9.6
		II		17			5		7 11.2
67 68	9.74383 9.74394	11	9.82358 9.82374	16	0.17642 0.17626	9.92025 9.92020	5	33 32	
69	9.74394	12	9.82374	17	0.17620	9.92020	5	32 31	9 14.4
70		11	9.82407	16		9.92010	5	30	
	9.74417	II	-	17	0.17593		5		
71	9.74428	12	9.82424	16	0.17576	9.92005	5	29 28	12
72	9.74440	11	9.82440 9.82456	16	0.17560	9.92000	5	28	I I.2
73	9.74451	12		17	0.17544	9.91995	5		2 2.4 3 3.6
74	9.74463	11	9.82473	16	0.17527	9.91990	5	26	3 3.6
75 76	9.74474	11	9.82489 9.82506	17	0.17511	9.91985 9.91980	5	25	5 6.0
	9.74485	12		16	0.17494		5	24	
77 78	9.74497	11	9.82522 9.82538	16	0.17478 0.17462	9.91975 9.91969	6	23	7 8.4 8 9.6
76 79	9.74508 9.74519	II	9.82555	17	0.17402	9.91964	5	21	9 10.8
80		12		16			5	20	
	9.74531	II	9.82571	17	0.17429	9.91959	5		11
81	9.74542	11	9.82588	16	0.17412	9.91954	5	19	1 1.1
82 83	9.74553	12	9.82604	16	0.17396	9.91949 9.91944	5	17	2 2.2
_	9.74565	11		17	0.17380		5		3 3.3
84	9.74576	11	9.82637	16	0.17363	9.91939	5	16	4 4.4
85 86	9.74587	11	9.82653 9.82670	17	0.17347 0.17330	9.91934 9.91929	5	15	5 5.5 6 6.6
	9.74598	12		16			5		7 7.7 8 8.8
87 88	9.74610	11	9.82686	16	0.17314	9.91924	5	13	
88	9.74621 9.74632	II	9.82702	17	0.17298 0.17281	9.91919	5	11	9 9.9
90		12		16			6	10	
	9.74644	11	9.82735	16	0.17265	9.91908	5		
91	9.74655	11	9.82751	17	0.17249	9.91903	5	o9 o8	6
92	9.74666	II	9.82768	16	0.17232	9.91898 9.91893	5	08	1 0.6
93	9.74677	12	9.82784	17	0.17216		5		2 I.2 3 I.8
94	9.74689	11	9.82801	16	0.17199	9.91888	5	06	
95	9.74700	11	9.82817 9.82833	16	0.17163	9.91883	5	05 04	5 3.0
96	9.74711	11		17			5		
97	9.74722	12	9.82850 9.82866	16	0.17150	9.91873	5	03	7 4.2 8 4.8
98 99	9.74734	11	9.82882	16	0.17134	9.91863	5	01	9 5.4
	9.74745	11		17			6	00	
100	9.74756		9.82899		0.17101	9.91857	-	-00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.74756	11	9.82899	16	0.17101	9.91857	5	100	
01	9.74767	12	9.82915	16	0.17085	9.91852	5	99	17
02	9.74779	11	9.82931	17	0.17069	9.91847	5	98	I I.7
03	9.74790	II	9.82948	16	0.17052	9.91842	5	97	2 3.4
04	9.74801	11	9.82964	16	0.17036	9.91837	5	96	3 5.I 4 6.8
05	9.74812	11	9.82980	17	0.17020	9.91832	5	95	4 6.8 5 8.5
06	9.74824	11	9.82997	16	0.17003	9.91827	5	94	4 6.8 5 8.5 6 10.2
07	9.74835		9.83013		0.16987	9.91822	6	93	7 II.9 8 I3.6
08	9.74846	II II	9.83029	16 17	0.16971	9.91816		92	
09	9.74857	II	9.83046	16	0.16954	9.91811	5	91	9 15.3
10	9.74868		9.83062	16	0.16938	9.91806		90	
11	9.74880	12	9.83078		0.16922	9.91801	5	89	16
12	9.74891	11	9.83095	17	0.16905	9.91796	5	88	1 1.6
13	9.74902	11	9.83111	16	0.16889	9.91791	5	87	2 3.2
14	9.74913	II	9.83127	16	0.16873	9.91786	5	86	3 4.8 4 6.4
15	9.74924	11	9.83144	17	0.16856	9.91781	5	85	5 8.0
16	9.74935	11	9.83160	16	0.16840	9.91775	6	84	6 9.6
17	9.74947	12	9.83176	16	0.16824	9.91770	5	83	7 II.2 8 I2.8
18	9.74958	11	9.83193	17	0.16807	9.91765	5	82	8 12.8 9 14.4
19	9.74969	11	9.83209	16	0.16791	9.91760	5	81	9 14.4
20	9.74980	II	9.83225	16	0.16775	9.91755	5	80	
		II	9.83242	17	0.16758	9.91750	5	79	40
2I 22	9.74991	11	9.83242	16	0.16742	9.91750	6	79	12
23	9.75002 9.75014	12	9.83274	16	0.16726	9.91744	5	77	I I.2
_		11		16	0.16710		5	76	2 2.4 3 3.6
24	9.75025	11	9.83290	17	0.16693	9.91734	5		
25 26	9.75036	11	9.83307	16	0.16677	9.91729	5	75 74	4 4.8 5 6.0 6 7.2
	9.75047	11	9.83323	16		9.91724	5		
27	9.75058	11	9.83339	17	0.16661	9.91719	5	73	7 8.4 8 9.6
28	9.75069	11	9.83356	16	0.16644	9.91714	6	72	9 10.8
29	9.75080	11	9.83372	16		9.91708	5	71	* '
30	9.75091	12	9.83388	17	0.16612	9.91703	5	70	11
31	9.75103	II	9.83405	16	0.16595	9.91698	5	69	
32	9.75114	11	9.83421	16	0.16579	9.91693		68	I I.I 2 2.2
33	9.75125	11	9.83437	16	0.16563	9.91688	5 6	67	3 3.3
34	9.75136	11	9.83453	17	0.16547	9.91682	5	66	4 4.4
35	9.75147	II	9.83470	16	0.16530	9.91677	5	65	4 4.4 5 5.5 6 6.6
36	9.75158	II	9.83486	16	0.16514	9.91672	5	64	
37	9.75169	111	9.83502	16	0.16498	9.91667	5	63	7 7.7 8 8.8
38	9.75180	11	9.83518	17	0.16482	9.91662	5	62	9 9.9
39	9.75191	11	9.83535	16	0.16465	9.91657	6	61	
40	9.75202	II	9.83551	16	0.16449	9.91651	5	60	
41	9.75213		9.83567	1	0.16433	9.91646		59	5
42	9.75224	II	9.83583	16	0.16417	9.91641	5 5	58	1 0.5
43	9.75236	12 11	9.83600	17	0.16400	9.91636	5	57	2 1.0
44	9.75247	1	9.83616		0.16384	9.91631	6	56	3 I.5 4 2.0
45	9.75258	II	9.83632	16	0.16368	9.91625	5	55	5 2.5
46	9.75269	II	9.83648	3	0.16352	9.91620	5	54	6 3.0
47	9.75280	1	9.83665	17	0.16335	9.91615		53	7 3.5
48	9.75291	II	9.83681	16	0.16319	9.91610	5	52	
49	9.75302	11	9.83697	16	0.16303	9.91605	5	51	9 4.5
50	9.75313	11	9.83713	10	0.16287	9.91599		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
L	COS	и,	· COL	u. c.	I an	DIII	, u.		1

	Sin	d.	Tan	d. c.	Cot	1 Cos	d.		1 P. P.
50	9.75313		9.83713		0.16287	9.91599	<u>u.</u>	50	T.F.
51		II	9.83730	17	0.16270		5		
52	9.75324 9.75335	II	9.83746	16	0.16254	9.91594 9.91589	5	49 48	17
53	9.75346	11	9.83740	16	0.16238	9.91584	5	47	I I.71
54	9.75357	11	9.83778	16	0.16222		5		2 3.4
55	9.75368	II	9.83778	17	0.16205	9.91579 9.91573	6	46 45	3 5.1 4 6.8
56	9.75379	11	9.83811	16	0.16189	9.91568	5	45	5 8.5
57	9.75390	II	9.83827	16	0.16173	9.91563	5	43	6 10.2
58	9.75401	II	9.83843	16	0.16157	9.91558	5	43	7 II.9 8 I3.6
59	9.75412	11	9.83859	16	0.16141	9.91552	6	41	9 15.3
60	9.75423	II	9.83876	17	0.16124	9.91547	5	40	
61	9.75434	1	9.83892	16	0.16108	9.91542	5	39	16
62	9.75445	II	9.83908	16	0.16092	9.91537	5	38	1 1.6
63	9.75456	11	9.83924	16	0.16076	9.91531	6	37	2 3.2
64	9.75467		9.83941		0.16059	9.91526	5	36	3 4.8
65	9.75478	11	9.83957	16 16	0.16043	9.91521	5	35	4 6.4 5 8.0
66	9.75489	II	9.83973	16	0.16027	9.91516	5	34	6 9.6
67	9.75500	II	9.83989	16	0.16011	9.91511	6	33	7 II.2 8 I2.8
68	9.75511	II	9.84005	17	0.15995	9.91505	5	32	9 14.4
69	9.75522	II	9.84022	16	0.15978	9.91500	5	31	
70	9.75533	11	9.84038	16	0.15962	9.91495	5	30	
71	9.75544	10	9.84054	16	0.15946	9.91490	6	29	11
72	9.75554	II	9.84070	16	0.15930	9.91484	5	28	I I.I
73	9.75565	11	9.84086	17	0.15914	9.91479	5	27	2 2.2
74	9.75576	11	9.84103	16	0.15897	9.91474	5	26	3 3.3 4.4
75 76	9.75587	II	9.84119	16	0.15881	9.91469	6	25	5 5.5
77	9.75598	II	9.84135	16		9.91463	5	24	5 5.5 6 6.6
77	9.75609 9.75620	11	9.84151 9.84167	16	0.15849	9.91458	5	23	7 7.7 8 8.8
79	9.75631	11	9.84183	16	0.15817	9.91453 9.91447	6	22 21	9 9.9
80	9.75642	II	9.84200	17	0.15800	9.91442	5	20	
81	9.75653	11	9.84216	16	0.15784	9.91437	5	19	10
82	9.75664	11	9.84232	16	0.15768	9.91437	5	18	1 1 1.0
83	9.75675	II	9.84248	16	0.15752	9.91426	6	17	2 2.0
84	9.75685	10	9.84264	16	0.15736	9.91421	5	16	3 3.0
85	9.75696	II	9.84280	16	0.15720	9.91416	5	15	
86	9.75707	II II	9.84297	17 16	0.15703	9.91411	5 6	14	5 5.0 6 6.0
87	9.75718		9.84313	16	0.15687	9.91405		13	7 7.0 8 8.0
88	9.75729	II	9.84329	16	0.15671	9.91400	5	12	9 9.0
89	9.75740	II	9.84345	16	0.15655	9.91395	6	11	
90	9.75751	11	9.84361	16	0.15639	9.91389	5	10	
91	9.75762	IO	9.84377	17	0.15623	9.91384	5	09	6
92	9.75772	II	9.84394	16	0.15606	9.91379	5	08	I 0.6
93	9.75783	11	9.84410	16	0.15590	9.91374	6	07	2 I.2 3 I.8
94	9.75794	II	9.84426	16	0.15574	9.91368	5	06	4 2.4
95 96	9.75805 9.75816	11	9.84442 9.84458	16	0.15558 0.15542	9.91363 9.91358	5	05 04	5 3.0
97	9.75827	II	9.84474	16	0.15526	9.91352	6		6 3.6 7 4.2
97 98	9.75837	10	9.84490	16	0.15520	9.91352	5	03	7 4.2 8 4.8
99	9.75848	II	9.84507	17	0.15493	9.91342	5	OI	9 5.4
100	9.75859	II	9.84523	16	0.15477	9.91336	6	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
1049							1000		

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	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.75859	II	9.84523	16	0.15477	9.91336	_	100	
OI	9.75870		9.84539		0.15461	9.91331	5	99	17
02	9.75881	11	9.84555	16 16	0.15445	9.91326	5	98	1 1.7
03	9.75892	II	9.84571	16	0.15429	9.91321	5	97	2 3.4
04	9.75902	II	9.84587		0.15413	9.91315		96	3 5.I 4 6.8
05	9.75913		9.84603	16 16	0.15397	9.91310	5	95	4 6.8
06	9.75924	II	9.84619	17	0.15381	9.91305	5	94	5 8.5 6 10.2
07	9.75935		9.84636		0.15364	9.91299		93	7 11.9
08	9.75946	II	9.84652	16	0.15348	9.91294	5	92	8 13.6
09	9.75956	10	9.84668	16 16	0.15332	9.91289	5	91	9 15.3
10	9.75967	II	9.84684		0.15316	9.91283		90	
II	9.75978	II	9.84700	16	0.15300	9.91278	5	89	16
12	9.75989	II	9.84716	16	0.15284	9.91273	5	88	1 1.6
13	9.76000	II	9.84732	16	0.15268	9.91267	6	87	2 3.2
	9.76010	10	9.84748	16	0.15252	9.91262	5	86	3 4.8 4.6.4
14 15	9.76021	11	9.84764	16	0.15236	9.91202	5	85	4 6.4 5 8.0
16	9.76032	II	9.84781	17	0.15219	9.91251	6	84	5 8.0 6 9.6
		II		16	0.15219	9.91231	5	83	7 11.2
17 18	9.76043	10	9.84797	16	0.15203		5	82	
19	9.76053 9.76064	II	9.84813 9.84829	16	0.15167	9.91241	6	81	9 14.4
		11		16		9.91235	5		
20	9.76075	11	9.84845	16	0.15155	9.91230	5	80	
21	9.76086	10	9.84861	16	0.15139	9.91225	6	79	11
22	9.76096	II	9.84877	16	0.15123	9.91219	5	78	1 1.1
23	9.76107	II	9.84893	16	0.15107	9.91214	5	77	2 2.2
24	9.76118	II	9.84909	16	0.15091	9.91209	6	76	3 3.3 4 4.4 5 5.5 6 6.6
25	9.76129	10	9.84925	16	0.15075	9.91203	5	75	4 4.4
26	9.76139	II	9.84941	17	0.15059	9.91198	6	74	5 5.5 6 6.6
27	9.76150	II	9.84958	16	0.15042	9.91192		73	7 7.7 8 8.8
28	9.76161	10	9.84974	16	0.15026	9.91187	5	72	
29	9.76171	II	9.84990	16	0.15010	9.91182	5 6	71	9 9.9
30	9.76182		9.85006		0.14994	9.91176		70	
31	9.76193	II	9.85022	16	0.14978	9.91171	5	69	10
32	9.76203	10	9.85038	16	0.14962	9.91166	5	68	I I.O
33	9.76214	II .	9.85054	16	0.14946	9.91160	6	67	2 2.0
34	9.76225	11	9.85070	16	0.14930	9.91155	5	66	3 3.0
35	9.76236	II	9.85086	16	0.14914	9.91149	6	65	5 5.0
36	9.76246	10	9.85102	16	0.14898	9.91144	5	64	3 3.0 4 4.0 5 5.0 6 6.0 7 7.0 8 8.0
37	9.76257	11	9.85118	16	0.14882	9.91139	5	63	7 7.0 8 8.0
38	9.76268	II	9.85134	16	0.14866	9.91139	6	62	8 8.0
39	9.76278	10	9.85150	16	0.14850	9.91128	5	61	9 9.0
40	9.76289	11	9.85166	16	0.14834	9.91123	5	60	
		II		16			6		
41	9.76300	10	9.85182 9.85198	16	0.14818	9.91117	5	59	5
42	9.76310 9.76321	11	9.85215	17	0.14802	9.91112	6	58 57	I 0.5
		II		16		9.91106	5		2 1.0
44	9.76332	IO	9.85231	16	0.14769	9.91101	5	56	3 I.5 4 2.0
45	9.76342	II	9.85247	16	0.14753	9.91096	6	55	5 2.5
46	9.76353	II	9.85263	16	0.14737	9.91090	5	54	6 3.0
47	9.76364	10	9.85279	16	0.14721	9.91085	6	53	7 3.5 8 4.0
48	9.76374	II	9.85295	16	0.14705	9.91079	5	52	8 4.0 9 4.5
49	9.76385	10	9.85311	16	0.14689	9.91074	5	51	314.3
50	9.76395		9.85327		0.14673	9.91069		50	
	Cos	đ.	Cot	d. c.	Tan	Sin	đ.		P. P.

35								144	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.76395	11	9.85327	16	0.14673	9.91069	6	50	
51	9.76406		9.85343		0.14657	9.91063		49	16
52	9.76417	II	9.85359	16 16	0.14641	9.91058	5 6	48	1 1.6
53	9.76427	II	9.85375	16	0.14625	9.91052	5	47	2 3.2
54	9.76438		9.85391	16	0.14609	9.91047		46	3 4.8
55	9.76448	10	9.85407	16	0.14593	9.91042	5 6	45	4 6.4
56	9.76459	II	9.85423	16	0.14577	9.91036	5	44	5 8.0 6 9.6
57	9.76470		9.85439		0.14561	9.91031		43	
58	9.76480	10	9.85455	16	0.14545	9.91025	6	42	7 II.2 8 I2.8
59	9.76491	II	9.85471	16 16	0.14529	9.91020	5 6	41	9 14.4
60	9.76501		9.85487		0.14513	9.91014		40	
61	9.76512	II	9.85503	16	0.14497	9.91009	5	39	15
62	9.76523	II	9.85519	16	0.14481	9.91004	5	38	I I.5
63	9.76533	10	9.85535	16	0.14465	9.90998	6	37	2 3.0
64	9.76544	11	9.85551	16	0.14449	9.90993	5	36	3 4.5 4 6.0
65	9.76554	10	9.85567	16	0.14433	9.90987	6	35	4 6.0 5 7.5
66	9.76565	11	9.85583	16	0.14417	9.90982	5	34	6 9.0
67	9.76575	10	9.85599	16	0.14401	9.90976	6	33	7 IO.5 8 I2.0
68	9.76586	II	9.85615	16	0.14385	9.90970	5	32	8 12.0 9 13.5
69	9.76597	II	9.85631	16	0.14369	9.90966	5 6	31	9 13.3
70	9.76607	10	9.85647	16	0.14353	9.90960	6	30	
		11		16			5		
71	9.76618	10	9.85663	16	0.14337	9.90955	6	29 28	11
72	9.76628 9.76639	11	9.85679 9.85695	16	0.14321	9.90949 9.90944	5	27	I.I I.I
73		10		16			6		2 2.2 3 3.3
74	9.76649	11	9.85711	16	0.14289	9.90938	5	26	4 4.4
75 -6	9.76660	10	9.85727	16	0.14273	9.90933	6	25	5 5.5 6 6.6
76	9.76670	11	9.85743	16	0.14257	9.90927	5	24	6 6.6
77	9.76681	10	9.85759	16	0.14241	9.90922	6	23	7 7.7 8 8.8
78	9.76691	II	9.85775	16	0,14225	9.90916	5	22	9 9.9
79	9.76702	10	9.85791	16	0.14209	9.90911	5	21	
80	9.76712	11	9.85807	16	0.14193	9.90906	6	20	10
81	9.76723	10	9.85823	16	0.14177	9.90900	5	19	
82	9.76733	11	9.85839	16	0.14161	9.90895	6	18	I I.0 2 2.0
83	9.76744	10	9.85855	16	0.14145	9.90889	5	17	3 3.0
84	9.76754	II	9.85871	16	0.14129	9.90884	6	16	4 4.0
85	9.76765	10	9.85887	16	0.14113	9.90878	5	15	4 4.0 5 5.0 6 6.0
86	9.76775	II	9.85903	16	0.14097	9.90873	6	14	
87	9.76786	10	9.85919	16	0.14081	9.90867	5	13	7 7.0 8 8.0
88	9.76796	10	9.85935	16	0.14065	9.90862	6	12	9 9.0
89	9.76807	10	9.85951	16	0.14049	9.90856	5	11	
90	9.76817		9.85967	16	0.14033	9.90851	6	10	
91	9.76828	II	9.85983		0.14017	9.90845		09	6
92	9.76838	10	9.85999	16	0.14001	9.90840	5	08	1 0.6
93	9.76849	II	9.86014	15	0.13986	9.90834	6	07	
94	9.76859	10	9.86030	16	0.13970	9.90829	5	06	3 1.8
95	9.76870	11	9.86046	16	0.13954	9.90823	6	05	4 2.4
96	9.76880	10	9.86062	16	0.13938	9.90818	5 6	04	4 2.4 5 3.0 6 3.6
97	9.76891	II	9.86078	16	0.13922	9.90812		03	7 4.2
98	9.76901	10	9.86094	16	0.13906	9.90807	5	02	8 4.8
99	9.76911	10	9.86110	16	0.13890	9.90801	6	OI	9 5.4
100	9.76922	II	9.86126	16	0.13874	9.90796	5	00	
200	Cos	<i>a</i>	-	d 0	Tan	Sin	d.		P. P.
	Cos	d.	Cot	d. c.	lan	Sin	a.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.76922	10	9.86126	16	0.13874	9.90796	6	100	
OI	9.76932		9.86142	16	0.13858	9.90790		99	16
02	9.76943	II IO	9.86158	16	0.13842	9.90785	5	98	
03	9.76953	II	9.86174	16	0.13826	9.90779	5	97	2 3.2
04	9.76964	10	9.86190	16	0.13810	9.90774	6	96	3 4.8
05	9.76974	10	9.86206	16	0.13794	9.90768		95	4 6.4 5 8.0
06	9.76984	II	9.86222	16	0.13778	9.90763	5 6	94	6 9.6
07	9.76995	10	9.86238	16	0.13762	9.90757	5	93	7 11.2
08	9.77005	II	9.86254	15	0.13746	9.90752	6	92	
09	9.77016	10	9.86269	16	0.13731	9.90746	5	91	9 14.4
10	9.77026	10	9.86285	16	0.13715	9.90741	6	90	
II	9.77036	11	9.86301	16	0.13699	9.90735	5	89	15
12	9.77047	10	9.86317	16	0.13683	9.90730	6	88 87	I I.5 2 3.0
13	9.77057	II	9.86333	16	0.13667	9.90724	6		
14	9.77068	10	9.86349	16	0.13651	9.90718	5	86	3 4.5 4 6.0
15 16	9.77078	10	9.86365 9.86381	16	0.13635	9.90713	6	85 84	5 7.5 6 9.0
	9.77088	II		16	1		5	83	3 4.5 4 6.0 5 7.5 6 9.0 7 10.5 8 12.0
17 18	9.77099	10	9.86397 9.86413	16	0.13603	9.90702 9.90696	6	82	
19	9.77109 9.77119	10	9.86429	16	0.13571	9.90691	5 6	81	9 13.5
20	9.77130	II	9.86445	16	0.13555	9.90685	ŧ	80	
		10	<u> </u>	15			5		
2I 22	9.77140	10	9.86460	16	0.13540	9.90680	6	79 78	11
23	9.77161	11	9.86492	16	0.13524	9.90669	5	77	I I.I 2 2.2
		10	9.86508	16	0.13492	9.90663	6	76	3 3.3
24 25	9.77171 9.77181	10	9.86524	16	0.13492	9.90003	6	75	4 4.4
26	9.77192	11	9.86540	16	0.13460	9.90652	5	74	4 4.4 5 5.5 6 6.6
27	9.77202	10	9.86556	16	0.13444	9.90646	6	73	
28	9.77212	10	9.86572	16	0.13444	9.90641	5	72	7 7.7 8 8.8
29	9.77223	II	9.86588	16	0.13412	9.90635	6	71	9 9.9
80	9.77233	10	9.86603	15	0.13397	9.90630	5	70	
31	9.77243	10	9.86619	16	0.13381	9.90624	6	69	10
32	9.77254	11	9.86635	16	0.13365	9.90618	6	68	1 1.0
33	9.77264	10	9.86651	16	0.13349	9.90613	5	67	2 2.0 3.0
34	9.77274	10	9.86667		0.13333	9.90607	1	66	
35	9.77285	II	9.86683	16	0.13317	9.90602	5	65	4 4.0 5 5.0 6 6.0
36	9.77295	10	9.86699	16	0.13301	9.90596	5	64	
37	9.77305	1	9.86715	16	0.13285	9.90591	6	63	7 7.0 8 8.0
38	9.77316	II	9.86731	15	0.13269	9.90585	6	62	9 9.0
39	9.77326	10	9.86746	16	0.13254	9.90579	5	61	
40	9.77336	10	9.86762	16	0.13238	9.90574	6	60	
41	9.77346	111	9.86778	16	0.13222	9.90568	l	59	5
42	9.77357	10	9.86794	16	0.13206	9.90563	5	58	1 0.5
43	9.77367	10	9.86810	16	0.13190	9.90557	6	57	2 I.0 3 I.5
44	9.77377	IO	9.86826	16	0.13174	9.90551	5	56	4 2.0
45	9.77387	11	9.86842	15	0.13158	9.90546	6	55	5 2.5
46	9.77398	IO	9.86857	16	0.13143	9.90540	5	54	
47	9.77408	10	9.86873	16	0.13127	9.90535	6	53	8 4.0
48	9.77418	II	9.86889 9.86905	16	0.13111	9.90529	6	52 51	9 4.5
49 50	9.77429	10		16	0.13095	9.90523	- 5	50	
90	9·77439		9.86921	1 .	0.13079	9.90518	-	- 50	P. P.
	Cos	d.	Cot	d. c.	Tan	Sin	d.		r.r.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.77439		9.86921		0.13079	9.90518	_	50	
51	9.77449	10	9.86937	16	0.13063	9.90512	6	49	
52	9.77459	10	9.86953	16	0.13047	9.90507	5	48	16
53	9.77469	10	9.86968	15	0.13032	9.90501	6	47	1 1.6
54	9.77480	II	9.86984	16	0.13016	9.90495	6	46	3 4.8
55	9.77490	10	9.87000	16	0.13000	9.90490	5	45	4 6.4
56	9.77500	10	9.87016	16 16	0.12984	9.90484	6	44	5 8.0
57	9.77510	10	9.87032		0.12968	9.90479	5	43	6 9.6 7 II.2
58	9.77521	II	9.87048	16	0.12952	9.90473	6	42	7 II.2 8 I2.8
59	9.77531	10	9.87063	15 16	0.12937	9.90467	6	41	9 14.4
60	9.77541	10	9 87079	16	0.12921	9.90462	5	40	
61	9.77551	10	9.87095	16	0.12905	9.90456	6	39	15
62	9.77561	II	9.87111	16	0.12889	9.90450	5	38	1 1.5
63	9.77572	IO	9.87127	16	0.12873	9.90445	6	37	2 3.0
64	9.77582	10	9.87143	15	0.12857	9.90439	5	36	3 4.5 4 6.0
65	9.77592	10	9.87158	16	0.12842	9.90434	6	35	5 7.5
66	9.77602	10	9.87174	16	0.12826	9.90428	6	34	
67	9.77612	II	9.87190	16	0.12810	9.90422	5	33	7 10.5 8 12.0
68	9.77623	IO	9.87206	16	0.12794	9.90417	6	32	9 13.5
69	9.77633	10	9.87222	16	0.12778	9.90411	6	31	
70	9.77643	10	9.87238	15	0.12762	9.90405	5	30	
71	9.77653	10	9.87253	16	0.12747	9.90400	6	29	11
72	9.77663	10	9.87269	16	0.12731	9.90394	6	28	I I.I
73	9.77673	11	9.87285	16	0.12715	9.90388	5	27	2 2.2 3.3
74	9.77684	10	9.87301	16	0.12699	9.90383	6	26	4 4.4
75 76	9.77694	10	9.87317 9.87332	15	0.12668	9.90377 9.90371	6	25 24	3 3.3 4 4.4 5 5.5 6 6.6
77		10	9.87348	16	0.12652	9.90366	5	23	0 0.0
77	9.77714	IO	9.87364	16	0.12636	9.90360	6	23	7 7.7 8 8.8
79	9.77734	10	9.87380	16	0.12620	9.90354	6	21	9 9.9
80	9.77744	10	9.87396	16	0.12604	9.90349	5	20	
8r	9.77755	II	9.87412	16	0.12588	9.90343	6	19	10
82	9.77765	10	9.87427	15	0.12573	9.90337	6	18	I I.O
83	9.77775	10	9.87443	16	0.12557	9.90332	5	17	2 2.0 3.0
84	9.77785	10	9.87459	16	0.12541	9.90326		16	4 4.0
85	9.77795	10	9.87475	16	0.12525	9.90320	6	15	4 4.0 5 5.0 6 6.0
86	9.77805	10	9.87490	15 16	0.12510	9.90315	5	14	
.87	9.77815	10	9.87506	16	0.12494	9.90309	6	13	7 7.0 8 8.0
88	9.77825	10	9.87522	16	0.12478	9.90303	5	12	9 9.0
89	9.77835	II	9.87538	16	0.12462	9.90298	6	II	
90	9.77846	10	9.87554	15	0.12446	9.90292	6	10	
91	9.77856	10	9.87569	16	0.12431	9.90286	6	09	6
92	9.77866	10	9.87585	16	0.12415	9.90280	5	08	1 0.6
93	9.77876	10	9.87601	16	0.12399	9.90275	6	07	3 1.8
94	9.77886	10	9.87617	16	0.12383	9.90269	6	06	4 2.4
95 96	9.77896 9.77906	10	9.87633 9.87648	15	0.12367	9.90263 9.90258	5	05 04	5 3.0
97	9.77916	10	9.87664	16	0.12336	9.90258	6	03	7 4.2
98	9.77916	10	9.87680	16	0.12330	9.90252	6	02	
99	9.77936	10	9.87696	16	0.12304	9.90241	5	OI	9 5.4
100	9.77946	10	9.87711	15	0.12289	9.90235	6	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
-				-			-		

	0: 1	-	(D.)	1	Cat	C 1	d I		P. P.
	Sin	d.	Tan	d. c.	Cot	Cos	<u>d.</u>		P. P.
00	9.77946	10	9.87711	16	0.12289	9.90235	6	100	
10	9.77956	10	9.87727	16	0.12273	9.90229	6	99	16
02	9.77966	10	9.87743	16	0.12257	9.90223	5	98	1 1.6
03	9.77976	II	9.87759	16	0.12241	9.90218	6	97	2 3.2
04	9.77987	10	9.87775	15	0.12225	9.90212	6	96	3 4.8
05	9.77997	10	9.87790	16	0.12210	9.90206	5	95	4 6.4
06	9.78007	10	9.87806	16	0.12194	9.90201	6	94	5 8.0
07	9.78017	10	9.87822	16	0.12178	9.90195	6	93	7 11.2
о8	9.78027	10	9.87838	15	0.12162	9.90189	6	92	
09	9.78037	10	9.87853	16	0.12147	9.90183	5	91	9 14.4
10	9.78047	10	9.87869	16	0.12131	9.90178	6	90	
11	9.78057	10	9.87885	16	0.12115	9.90172	6	89	15
12	9.78067	10	9.87901	15	0.12099	9.90166	6	88	1 1.5
13	9.78077	10	9.87916	16	0.12084	9.90160	5	87	2 3.0
14	9.78087	10	9.87932	16	0.12068	9.90155	6	86	3 4.5 4 6.0
15	9.78097	10	9.87948	16	0.12052	9.90149	6	85	5 7.5
16	9.78107	10	9.87964	15	0.12036	9.90143	6	84	
17	9.78117	10	9.87979	16	0.12021	9.90137	5	83	7 10.5 8 12.0
18	9.78127	10	9.87995	16	0.12005	9.90132	6	82	9 13.5
19	9.78137	10	9.88011	16	0.11989	9.90126	6	81	
20	9.78147	10	9.88027	15	0.11973	9.90120	6	80	
21	9.78157	10	9.88042	16	0.11958	9.90114	5	79	11
22	9.78167	10	9.88058	16	0.11942	9.90109	6	78	1 1.1
23	9.78177	10	9.88074	15	0.11926	9.90103	6	77	2 2.2
24	9.78187	10	9.88089	16	0.11911	9.90097	6	76	3 3.3
25	9.78197	10	9.88105	16	0.11895	9.90091	5	75	4 4.4
26	9.78207	10	9.88121	16	0.11879	9.90086	6	74	5 5.5 6 6.6
27	9.78217	10	9.88137	15	0.11863	9.90980	6	73	7 7.7 8 8.8
28	9.78227	9	9.88152	16	0.11848	9.90074	6	72	8 8.8 9 9.9
29	9.78236	10	9.88168	16	0.11832	9.90068	5	71	9 9.9
30	9.78246	10	9.88184	16	0.11816	9.90063	6	70	
31	9.78256	10	9.88200	15	0.11800	9.90057	6	69	9
32	9.78266	10	9.88215	16	0.11785	9.90051	6	68	1 0.9 2 1.8
33	9.78276	10	9.88231	16	0.11769	9.90045	6	67	3 2.7
34	9.78286	10	9.88247	15	0.11753	9.90039	5	66	4 3.6
35	9.78296	10	9.88262	16	0.11738	9.90034	6	65	5 4.5
36	9.78306	10	9.88278	16	0.11722	9.90028	6	64	4 3.6 5 4.5 6 5.4 7 6.3 8 7.2
37	9.78316	10	9.88294	16	0.11706	9.90022	6	63	
38	9.78326	10	9.88310	15	0.11690	9.90016	5	62 61	9 8.1
39	9.78336	10	9.88325	16	0.11675	9.90011	6		
40	9.78346	10	9.88341	16	0.11659	9.90005	6	60	
41	9.78356	10	9.88357	15	0.11643	9.89999	6	59	5
42	9.78366	9	9.88372	16	0.11628	9.89993	6	58	I 0.5
43	9.78375	10	9.88388	16	0.11612	9.89987	5	57	2 I.O 3 I.5
44	9.78385	10	9.88404	16	0.11596	9.89982	6	56	4 2.0
45	9.78395	IO	9.88420	15	0.11580	9.89976	6	55	4 2.0 5 2.5 6 3.0
46	9.78405	10	9.88435	16	0.11565	9.89970	6	54	6 3.0 7 3.5
47	9.78415	10	9.88451	16	0.11549	9.89964	6	53	7 3.5
48	9.78425	10	9.88467	15	0.11533	9.89958 9.89952	6	52 51	9 4.5
49	9.78435	- 10		16			- 5	50	
50	9.78445	-	9.88498	ļ	0.11502	9.89947	-	30	D D
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.78445		9.88498	16	0.11502	9.89947	-	50	
51	9.78455	10	9.88514	1	0.11486	9.89941	6	49	16
52	9.78464	9	9.88529	15	0.11471	9.89935	6	48	1 1.6
53	9.78474	IO	9.88545	16	0 11455	9.89929	6	47	2 3.2
54	9.78484	10	9.88561	16	0.11439	9.89923	_	46	3 4.8
55	9.78494	10	9.88577	15	0.11423	9.89918	5	45	4 6.4 5 8.0
56	9.78504	10	9.88592	16	0.11408	9.89912	6	44	5 8.0 6 9.6
57	9.78514	10	9.88608	16	0.11392	9.89906	6	43	7 11.2
58	9.78524	9	9.88624	15	0.11376	9.89900	6	42	8 12.8 9 14.4
59	9.78533	10	9.88639	16	0.11361	9.89894	6	41	9 (14.4
60	9.78543	10	9.88655	16	0.11345	9 89888	5	40	45
61	9.78553	10	9.88671	15	0.11329	9.89883	6	39	15
62 63	9.78563	10	9.88686	16	0.11314	9.89877 9.89871	6	38	I I.5 2 3.0
	9.78573	10	9.88718	16	0.11298		6	37	3 4.5
64 65	9.78583 9.78592	9	9.88733	15	0.11282	9.89865 9.89859	6	36 35	4 6.0 5 7.5
66	9.78602	10	9.88749	16	0.11251	9.89853	6	34	5 7.5 6 9.0
67	9.78612	10	9.88765	16	0.11235	9.89847	6	33	7 10.5
68	9.78622	10	9.88780	15	0.11233	9.89842	5	32	8 12.0 9 13.5
69	9.78632	10	9.88796	16	0.11204	9.89836		31	9 13.3
70	9.78642	10	9.88812	16	0.11188	9.89830	6	30	
71	9.78651	9	9.88827	15	0.11173	9.89824	6	29	10
72	9.78661	10	9.88843	16	0.11157	9.89818	6	28	1 1.0
73	9.78671	10	9.88859	16	0.11141	9.89812	6	27	2 2.0
74	9.78681	10	9.88874	15	0.11126	9.89806		26	3 3.0
75	9.78691	10	9.88890	16 16	0.11110	9.89801	5 6	25	4 4.0
76	9.78700	9	9.88906	15	0.11094	9.89795	6	24	5 5.0 6 6.0
77	9.78710	ļ.	9.88921	16	0.11079	9.89789	6	23	7 7.0 8 8.0
78	9.78720	10	9.88937	16	0.11063	9.89783	6	22	
79	9.78730	9	9.88953	15	0.11047	9.89777	6	21	9 9.0
80	9.78739	10	9.88968	16	0.11032	9.89771	6	20	.)
81	9.78749	10	9.88984	16	0.11016	9.89765	6	19	9
82	9.78759	10	9.89000	15	0.11000	9.89759	5	18	I 0.9 2 I.8
83	9.78769	10	9.89015	16	0.10985	9.89754	6	17	3 2.7
84	9.78779	9	9.89031	15	0.10969	9.89748	6	16	3 2.7 4 3.6
85	9.78788	10	9.89046	16	0.10954	9.89742	6	15	4 3.6 5 4.5 6 5.4
86	9.78798	10	9.89062	16	0.10938	9.89736	6	14	7 6.3
87 88	9.78808	10	9.89078	15	0.10922	9.89730	6	13	8 7.2
89	9.78818 9.78827	9	9.89093	16	0.10907	9.89724 9.89718	6	12 11	9 8.1
90		10		16	0.10891		6	10	
	9.78837	10	9.89125	15		9.89712	6		
91 92	9.78847 9.78856	9	9.89140 9.89156	16	o.10860 o.10844	9.89706 9.89701	5 6	o9 o8	6
93	9.78866	10	9.89150	16	0.10844	9.89695		07	I 0.6 2 1.2
94	9.78876	IO	9.89187	15	0.10813	9.89689	6	06	3 1.8
94	9.78886	IO	9.89203	16	0.10813	9.89683	6	05	4 2.4
96	9.78895	9	9.89218	15	0.10782	9.89677	6	04	5 3.0 6 3.6
97	9.78905	10	9.89234	16	0.10766	9.89671	6	03	7 4.2
98	9.78915	IO	9.89250	16	0.10750	9.89665	6	02	8 4.8
99	9.78924	9	9.89265	15	0.10735	9.89659	6	01	9 5.4
100	9.78934	10	9.89281	10	0.10719	9.89653	0	00	
	Cos	đ.	Cot	d. c.	Tan	Sin	d.		P. P.

30								141	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.78934	7.0	9.89281	16	0.10719	9.89653	6	100	
or	9.78944	10	9.89297	1	0.10703	9.89647	1	99	16
02	9.78954	10	9.89312	15	0.10688	9.89641	6	98	
03	9.78963	9	9.89328	15	0.10672	9.89635	6	97	I 1.6 2 3.2
04	9.78973	1	9.89343	16	0.10657	9.89630		96	3 4.8 4 6.4
05	9.78983	10	9.89359	16	0.10641	9.89624	6	95	4 6.4
06	9.78992	9	9.89375	15	0.10625	9.89618	6	94	5 8.0 6 9.6
07	9.79002	1	9.89390	16	0.10610	9.89612	1	93	7 11.2
о8	9.79012	10	9.89406	16	0.10594	9.89606	6	92	8 12.8
09	9.79021	9	9.89422	15	0.10578	9.89600	6	91	9 14.4
10	9.79031		9.89437	16	0.10563	9.89594	6	90	
11	9.79041	10	9.89453		0.10547	9.89588	1	89	15
12	9.79050	9	9.89468	15	0.10532	9.89582	6	88	I 1.5
13	9.79060	IO	9.89484	16 16	0.10516	9.89576	6	87	2 3.0
14	9.79070	10	9.89500	1	0.10500	9.89570	6	86	3 4.5 4 6.0
15	9.79079	9	9.89515	15	0.10485	9.89564	6	85	
16	9.79089	10	9.89531	16	0.10469	9.89558	6	84	5 7.5 6 9.0
17	9.79099	10	9.89546	15	0.10454	9.89552	6	83	7 10.5
18	9.79108	9	9.89562	16	0.10438	9.89546	6	82	
19	9.79118	10	9.89578	16	0.10422	9.89540	6	81	9 13.5
20	9.79128	10	9.89593	15	0.10407	9.89534	6	80	
21	9.79137	9	9.89609	16	0.10391	9.89528	6	79	
22	9.79147	10	9.89624	15	0.10391	9.89522	6	78	10
23	9.79156	9	9.89640	16	0.10360	9.89516	6	77	I I.O
24	9.79166	10	9.89656	16	0.10344	9.89510	6	76	2 2.0 3.0
25	9.79176	10	9.89671	15	0.10344	9.89504	6	75	4 4.0
26	9.79185	9	9.89687	16	0.10313	9.89499	5	74	5 5.0
27	9.79195	10	9.89702	15	0.10298	9.89493	6		4 4.0 5 5.0 6 6.0 7 7.0 8 8.0
28	9.79293	9	9.89718	16	0.10298	9.89493	6	73 72	7 7.0 8 8.0
29	9.79214	10	9.89734	16	0.10266	9.89481	6	71	9 9.0
30	9.79224	10	9.89749	15	0.10251	9.89475	6	70	
		9	9.89765	16		9.89469	6	69	9
31 32	9.79233 9.79243	10	9.89780	15	0.10235	9.89463	6	68	1 0.9
33	9.79243	9	9.89796	16	0.10220	9.89457	6	67	2 1.8
	9.79262	10	9.89811	15	0.10189	9.89451	6	66	3 2.7
34 35	9.79202	10	9.89827	16	0.10109	9.89451	6	65	4 3.6
36	9.79281	9	9.89843	16	0.10173	9.89439	6	64	5 4.5 6 5.4
37	9.79291	10	9.89858	15	0.10142	9.89433	6	63	7 6.3
38	9.79291	9	9.89874	16	0.10142	9.89433	6	62	
39	9.79310	10	9.89889	15	0.10111	9.89421	6	61	9 8.1
40	9.79319	9	9.89905	16	0.10095	9.89415	6	60	
		10	9.89920	15	0.10080	9.89409	6		
4I 42	9.79329 9.79339	10	9.89936	16	0.10064	9.89409	6	59 58	6
43	9.79339	9	9.89952	16	0.10048	9.89397	6	57	1 0.6
	9.79358	10	9.89967	15	0.10033		6		2 I.2 3 I.8
44 45	9.79350	9	9.89983	16	0.10033	9.89391 9.89385	6	56 55	4 2.4
46	9.79307	10	9.89998	15	0.10017	9.89379	6	55	5 3.0
		9	9 90014	16			6		
47 48	9.79386 9.79396	10	9.90014	15	0.09986	9.89373 9.89366	7	53 52	7 4.2 8 4.8
49	9.79390	9	9.90029	16	0.09971	9.89360	6	52	9 5.4
50		10	9.90061	16			6	50	
00	9.79415			-	0.09939	9.89354		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	-	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.79415		9.90061		0.09939	9.89354		50	
51	9.79424	9	9.90076	15	0.09924	9.89348	6	49	4.0
52	9.79434	10	9.90092	16	0.09908	9.89342	6	48	16
53	9.79444	10	9.90107	15 16	0.09893	9.89336	6	47	I 1.6 2 3.2
54	9.79453	9	9.90123		0.09877	9.89330		46	3 4.8 4 6.4
55	9.79463	10	9.90138	15	0.09862	9.89324	6	45	4 6.4
56	9.79472	9	9.90154	16 15	0.09846	9.89318	6	44	5 8.0 6 9.6
57	9.79482		9.90169	16	0.09831	9.89312	6	43	7 11.2
58	9.79491	9	9.90185	15	0.09815	9.89306	6	42	8 12.8
59	9.79501	9	9.90200	16	0.09800	9.89300	6	41	9 14.4
60	9.79510	10	9.90216	16	0.09784	9.89294	6	40	
61	9.79520		9.90232	15	0.09768	9.89288	6	39	15
62	9.79529	9	9.90247	16	0.09753	9.89282	6	38	I 1.5
63	9.79539	9	9.90263	15	0.09737	9.89276	6	37	3 4.5
64	9.79548	10	9.90278	16	0.09722	9.89270	6	36	4 6.0
65	9.79558	9	9.90294	15	0.09706	9 89264	6	35	5 7.5
66	9.79567	9	9.90309	16	0.09691	9.89258	6	34	
67	9.79576	10	9.90325	15	0.09675	9.89252	6	33	7 10.5 8 12.0
68	9.79586	9	9.90340	16	0.09660	9.89246	7	32	9 13.5
69	9.79595	10	9.90356	15	0.09644	9.89239	6	31	
70	9.79605	9	9 90371	16	0.09629	9.89233	6	30	
71	9.79614	10	9.90387	16	0.09613	9.89227	6	29	10
72	9.79624	9	9.90403	15	0.09597	9.89221	6	28	I I.O
73	9.79633	10	9.90418	16	0.09582	9.89215	6	27	2 2.0
74	9.79643	9	9.90434	15	0.09566	9.89209	6	26	3 3.0
75	9.79652	10	9.90449	16	0.09551	9.89203	6	25	5 5.0
76	9.79662	9	9.90465	15	0.09535	9.89197	6	24	
77 78	9.79671	9	9.90480	16	0.09520	9.89191 9.89185	6	23	7 7.0 8 8.0
78 79	9.79680 9.79690	10	9.90496	15	0.09304	9.89179	6.	21	9 9.0
80	9.79699	9		16	0.09473	9.89173	6	20	
		10	9.90527	15			7	-	9
81 82	9.79709	9	9.90542	16	0.09458	9.89166 9.89160	6	19	
83	9.79718 9.79728	10	9.90558 9.90573	15	0.09442	9.89154	6	17	2 1.8
84		9	9.90589	16	0.09411	9.89148	6	16	3 2.7 4 3.6
85	9.79737 9.79746	9	9.90509	15	0.09396	9.89148	6	15	4 3.6 5 4.5
86	9.79746	10	9.90620	16	0.09390	9.89136	6	14	6 5.4
87	9.79765	9	9.90635	15	0.09365	9.89130	6	13	6 5.4 7 6.3 8 7.2
88	9.79775	10	9.90651	16	0.09349	9.89124	6	12	8 7.2 9 8.1
89	9.79784	9	9.90666	15	0.09334	9.89118	6	11	3 0.12
90	9.79793	9	9.90682	16	0.09318	9.89112		10	
91	9.79803	10	9.90697	15	0.09303	9.89105	7	09	7
92	9.79812	9	9.90097	16	0.09387	9.89099	6	08	1 0.7
93	9.79822	10	9.90728	15	0.09272	9.89093	6	07	2 1.4
94	9.79831	9	9.90744	16	0.09256	9.89087	1	06	3 2.1
95	9.79840	9	9.90759	15	0.09241	9.89081	6	05	4 2.8
96	9.79850	10	9.90775	16	0.09225	9.89075	6	04	5 3.5 6 4.2
97	9.79859	9	9.90790		0.09210	9.89069	6	03	7 4.9
98	9.79868	9	9.90806	16	0.09194	9.89063	7	02	7 4.9 8 5.6 9 6.3
99	9.79878	10	9.90821	16	0.09179	9.89056	6	OI	910.3
100	9.79887		9.90837		0.09163	9.89050		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

									2.2
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.79887	10	9.90837	15	0.09163	9.89050	6	100	
or	9.79897	9	9.90852	16	0.09148	9.89044	6	99	16
02	9.79906	9	9.90868	15	0.09132	9.89038	6	98	1 1.6
03	9.79915	10	9.90883	16	0.09117	9.89032	6	97	2 .3.2
04	9.79925	9	9.90899	15	0.09101	9.89026	6	96	3 4.8 4 6.4
. 02	9.79934	9	9.90914	16	0.09086	9.89020	7	95	5 8.0
06	9.79943	10	9.90930	15	0.09070	9.89013	6	94	
07	9.79953	9	9.90945	16	0.09055	9.89007	6	93 92	7 II.2 8 I2.8
o8 o9	9.79962	9	9.90961	15	0.09039	9.89001 9.88995	6	92	9 14.4
-	9.79971	10		16		9.88989	6	90	
10	9.79981	9	9.90992	15	0.09008		6	89	15
II	9.79990	9	9.91007	16	o.o8993 o.o8977	9.88983 9.88976	7	88	1 1.5
12	9.79999	10	9.91023 9.91038	15	0.08977	9.88970	6	87	2 3.0
	9.80009	9		16	0.08946	9.88964	6	86	3 4·5 4 6.0
14 15	9.80018	9	9.91054	15	0.08940	9.88958	6	85	4 6.0 5 7.5
16	9.80027	10	9.91009	16	0.08931	9.88952	6	84	6 9.0
17	9.80037	9	9.91003	15	0.08900	9.88946	6	83	7 10.5
18	9.80040	9	9.91116	16	0.08884	9.88939	7	82	8 12.0 9 13.5
19	9.80064	9	9.91131	15	0.08869	9.88933	6	81	9 13.3
20	9.80074	10	9.91147	16	0.08853	9.88927	6	80	
21	9.80083	9	9.91162	15	0.08838	9.88921	6	79	10
21	9.80092	9	9.91102	16	0.08822	9.88915	6	78	1 1.0
23	9.80102	10	9.91193	15	0.08807	9.88909	6	77	2 2.0
24	9,80111	9	9.91209	16	0.08791	9.88902	7	76	3 3.0
25	9.80120	9	9.91224	15	0.08776	9.88896	6	75	4 4.0
26	9.80129	9	9.91239	15 16	0.08761	9.88890	6	74	4 4.0 5 5.0 6 6.0
27	9.80139	10	9.91255		0.08745	9.88884	6	73	7 7.0 8 8.0
28	9.80148	9	9.91270	15 16	0.08730	9.88878	1	72	8 8.0
29	9.80157	9	9.91286	15	0.08714	9.88871	7 6	71	9 9.0
30	9.80166	10	9.91301	16	0.08699	9.88865	6	70	
31	9.80176		9.91317		0.08683	9.88859	6	69	9
32	9.80185	9	9.91332	15	0.08668	9.88853	6	68	I 0.9 2 1.8
33	9.80194	10	9.91348	15	0.08652	9.88847	7	67	3 2.7
34	9.80204	9	9.91363	16	0.08637	9.88840	6	66	4 3.6
35	9.80213	9	9.91379	15	0.08621	9.88834	6	65	5 4.5 6 5.4
36	9.80222	9	9.91394	16	0.08606	9.88828	6	64	7 6.3
37	9.80231	9	9.91410	15	0.08590	9.88822	7	63	8 7.2 9 8.1
38	9.80240	10	9.91425	16	0.08575	9.88815	6	62 61	9 8.1
39	9.80250	9	9.91441	15			6		
40	9.80259	. 9	9.91456	15	0.08544	9.88803	6	60	
41	9.80268	9	9.91471	. 16	0.08529	9.88797	6	59	6
42	9.80277	10	9.91487	15	0.08513	9.88791	7	58 57	1 0.6
43	9.80287	9	9.91502	16	1		6		2 I.2 3 I.8
44	9.80296	9	9.91518	15	0.08482	9.88778 9.88772	6	56 55	4 2.4
45 46	9.80305	9	9.91533	16	0.08451	9.88766	6	54	4 2.4 5 3.0 6 3.6
		9	9.91564	15	0.08436	9.88759	7	53	7 4.2
47 48	9.80323	10	9.91504	16	0.08420	9.88753	6	53	8 4.8
49	9.80333	9	9.91595	15	0.08405	9.88747	6	51	9 5.4
50	9.80351	9	9.91610	- 15	0.08390	9.88741	- 6	50	
-	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.
_	Cos	ı u.	· COL	· u. c.	1 Lan	DIII	· u.	EOO	1111

								140	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.80351	9	9.91610	16	0.08390	9.88741	-	50	
51	9.80360	(9.91626		0.08374	9.88734	7	49	16
52	9.80369	9	9.91641	15 16	0.08359	9.88728	6	48	1 1.6
53	9.80379	9	9.91657	15	0.08343	9.88722	6	47	2 3.2
54	9.80388		9.91672	1	0.08328	9.88716		46	3 4.8
55	9.80397	9	9.91688	16	0.08312	9.88709	7	45	3 4.8 4 6.4
56	9.80406	9	9.91703	15 16	0.08297	9.88703	6	44	4 6.4 5 8.0 6 9.6
57	9.80415		9.91719		0.08281	9.88697		43	
58	9.80425	10	9.91734	15	0.08266	9.88691	6	42	7 II.2 8 I2.8
59	9.80434	9	9.91749	15 16	0.08251	9.88684	7 6	41	9 14.4
60	9.80443	-	9.91765		0.08235	9.88678		40	
61	9.80452	9	9.91780	15	0.08220	9.88672	6	39	15
62	9.80461	9	9.91796	16	0.08204	9.88665	7	38	1 1.5
63	9.80470	9	9.91811	15	0.08189	9.88659	6	37	2 3.0
64	9.80479	9	9.91827	16	0.08173	9.88653	6	36	3 4.5 4 6.0
65	9.80489	10	9.91842	15	0.08158	9.88647	6	35	4 6.0
66	9.80498	9	9.91857	15	0.08143	9.88640	7	34	5 7.5 6 9.0
67	9.80507	9	9.91873	16	0.08127	9.88634	6	33	7 10.5
68	9.80516	9	9.91873	15	0.08127	9.88628	6	33	
69	9.80525	9	9.91904	16	0.08096	9.88621	7	31	9 13.5
70	9.80534	9	9.91919	15	0.08081	9.88615	6	30	
		9		16			6		
71	9.80543	10	9.91935	15	0.08065	9.88609	6	29	10
72	9.80553 9.80562	9	9.91950	15	0.08050	9.88603	7	28	I I.O
73		9	9.91965	16	0.08035	9.88596	6	27	2 2.0
74	9.80571	9	9.91981	15	0.08019	9.88590	6	26	3 3.0
75	9.80580	9	9.91996	16	0.08004	9.88584	7	25	5 5.0
76	9.80589	9	9.92012	15	0.07988	9.88577	6	24	4 4.0 5 5.0 6 6.0 7 7.0 8 8.0
77	9.80598	9	9.92027	15	0.07973	9.88571	6	23	7 7.0
78	9.80607	9	9.92042	16	0.07958	9.88565	7	22	9 9.0
79	9.80616	9	9.92058	15	0.07942	9.88558	6	21	9 9.0
80	9.80625	10	9.92073	16	0.07927	9.88552	6	20	
81	9.80635		9.92089		0.07911	9.88546	6	19	9
82	9.80644	9	9.92104	15 16	0.07896	9.88540		18	I 0.9 2 I.8
83	9.80653	9	9.92120	15	0.07880	9.88533	7	17	2 1.8
84	9.80662		9.92135		0.07865	9.88527		16	3 2.7 4 3.6
85	9.80671	9	9.92150	15	0.07850	9.88521	6	15	5 4.5
86	9.80680	9	9.92166	16	0.07834	9.88514	7	14	6 5.4 7 6.3
87	9.80689	9	9.92181	15	0.07819	9.88508		13	3 2.7 4 3.6 5 4.5 6 5.4 7 6.3 8 7.2
88	9.80698	9	9.92197	16	0.07803	9.88502	6	12	8 7.2 9 8.1
89	9.80707	9	9.92212	15	0.07788	9.88495	7 6	11	
90	9.80716	9	9.92227	15	0.07773	9.88489	-	10	
91	9.80725	9	9,92243	16	0.07757	9.88483	6	09	7
92	9.80734	9	9.92243	15	0.07742	9.88476	7	08	
93	9.80743	9	9.92274	16	0.07726	9.88470	6	07	I 0.7 2 I.4
94	9.80752	9	9.92289	15	0.07711	9.88464	6	06	3 2.1
95	9.80752	10	9.92209	15	0.07/11	9.88457	7	05	
96	9.80771	9	9.92304	16	0.07680	9.88451	6	04	4 2.8 5 3.5 6 4.2
		9		15		9.88444	7		6 4.2
97 98	9.80790 9.80789	9	9.92335 9.92351	16	0.07665	9.88438	6	03 02	7 4.9 8 5.6 9 6.3
99	9.80798	9	9.92351	15	0.07634	9.88432	6	01	9 6.3
100		9		15			7	00	
100	9.80807		9.92381		0.07619	9.88425			
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

Sin d. Tan d. c. Cot Cos d.	16 1 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8 9 14.4 15 1 1.5 2 3.0
01 9.80816 9 9.92397 16 0.07603 9.88419 6 98 02 9.80825 9 9.92412 15 0.07588 9.88413 6 98 03 9.80834 9 9.92428 16 0.07572 9.88406 6 97 04 9.80843 9 9.92438 15 0.07572 9.88394 6 97 05 9.80852 9 9.92438 15 0.07524 9.88394 7 95 06 9.80876 9 9.92454 15 0.07526 9.88394 7 95 08 9.80879 9 9.92504 15 0.07450 9.88381 7 93 09 9.80888 9 9.92520 16 0.07480 9.88368 6 91 10 9.80997 9 9.92535 16 0.07465 9.88362 7 80 11 9.80915 9 9.9256	I 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8 9 14.4
02 9.80825 9 9.92421 15 0.07588 9.88413 0 98 03 9.80843 9 9.92428 15 0.07572 9.88400 6 97 05 9.80852 9 9.92443 15 0.07526 9.83394 6 95 06 9.80861 9 9.92474 16 0.07526 9.83374 7 94 07 9.80879 9 9.92489 15 0.07511 9.88381 7 94 08 9.80879 9 9.92504 15 0.07496 9.88374 7 92 09 9.80888 9 9.92520 16 0.07465 9.88368 6 91 10 9.80897 9 9.92531 16 0.07469 9.88355 6 90 11 9.80960 9 9.92551 15 0.07469 9.88355 6 88 13 9.80915 9 9.9256	I 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8 9 14.4
03 9.80834 9 9.92428 15 0.07572 9.88406 6 96 04 9.80843 9 9.92438 15 0.07572 9.88400 6 96 05 9.80852 9 9.92438 16 0.07527 9.88394 7 94 07 9.80870 9 9.92474 15 0.07511 9.88381 7 94 08 9.80879 9 9.92504 16 0.07496 9.88374 7 92 09 9.80888 9 9.92525 15 0.07486 9.88364 6 91 11 9.80906 9 9.92551 15 0.07465 9.88362 7 90 12 9.80915 9 9.92561 15 0.07449 9.88335 6 88 13 9.80942 9 9.9257 15 0.07449 9.88336 7 80 16 9.80942 9 9.92612	2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8 9 14.4
04 9.80843 9 9.92443 15 0.07557 9.88400 6 95 06 9.80861 9 9.92474 15 0.07526 9.88387 7 94 07 9.80870 9 9.92489 15 0.07511 9.88381 7 94 08 9.80879 9 9.92524 15 0.07496 9.88374 6 92 10 9.80888 9 9.92525 16 0.07480 9.88368 6 91 11 9.80906 9 9.92551 15 0.07449 9.88355 7 89 12 9.80915 9 9.92581 15 0.07449 9.88343 6 88 13 9.80942 9 9.92581 16 0.07449 9.88343 7 14 9.80942 9 9.92612 15 0.0743 9.88330 7 15 9.80960 9 9.92628 15 0.	3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8 9 14.4
o5 9.80852 9 9.92438 15 0.07542 9.88394 7 95 o6 9.80870 9 9.92474 15 0.07526 9.88387 7 98 o8 9.80879 9 9.92524 15 0.07496 9.88374 7 92 o9 9.80888 9 9.92520 16 0.07480 9.88368 6 91 10 9.80906 9 9.92531 16 0.07465 9.88362 7 90 11 9.80905 9 9.92566 15 0.07449 9.88355 6 88 13 9.80924 9 9.92581 15 0.07449 9.88343 6 88 14 9.80933 9 9.92597 0.07449 9.88335 6 88 15 9.80942 9 9.92612 15 0.07349 9.88336 7 86 16 9.80951 9 9.92628 1	5 8.0 6 9.6 7 11.2 8 12.8 9 14.4
06 9.80861 9 9.92474 16 0.07326 9.88387 7 94 07 9.80870 9 9.92489 15 0.07511 9.88381 7 93 08 9.80879 9 9.92504 16 0.07496 9.88374 6 91 09 9.80888 9 9.92530 16 0.07496 9.88366 6 91 10 9.80967 9 9.92531 16 0.07465 9.88362 7 90 11 9.80915 9 9.92531 16 0.07449 9.88349 6 88 13 9.80924 9 9.92581 15 0.07449 9.88343 7 86 88 14 9.80933 9 9.92571 15 0.07403 9.88336 6 87 15 9.80942 9 9.92612 15 0.07343 9.88336 6 86 16 0.80951 9 <th>7 11.2 8 12.8 9 14.4</th>	7 11.2 8 12.8 9 14.4
07 9.80870 9 9.92489 15 0.07511 9.88381 7 93 08 9.80879 9 9.92524 15 0.07496 9.88374 7 92 09 9.80888 9 9.92525 16 0.07469 9.88368 6 91 10 9.80969 9 9.92531 16 0.07449 9.88355 7 89 12 9.80915 9 9.92561 15 0.07449 9.88343 6 88 13 9.80942 9 9.92581 16 0.07419 9.88343 7 14 9.80942 9 9.92507 15 0.07439 9.88336 6 85 15 9.80942 9 9.92612 15 0.07388 9.88330 7 8 85 16 9.80960 9 9.92628 15 0.07372 9.88317 6 83 17 9.80960 9 9.9268<	7 11.2 8 12.8 9 14.4
08 9.88879 9 9.92504 16 0.07496 9.88374 7 92 09 9.80889 9 9.92520 15 0.07480 9.88368 6 91 10 9.80897 9 9.92535 16 0.07465 9.88362 7 89 11 9.80966 9 9.92556 15 0.07449 9.88355 6 88 13 9.80924 9 9.92561 15 0.07419 9.88343 6 87 14 9.80933 9 9.92581 16 0.07403 9.88336 6 86 15 9.80942 9 9.92612 15 0.07388 9.88336 7 85 16 9.80942 9 9.92628 16 0.07372 9.88336 6 85 17 9.80960 9 9.92683 15 0.07373 9.88317 6 83 18 9.80969 9 9.9268	9 14.4 15 1 1.5
og 0.80888 9 9.92520 16 0.07480 9.88368 6 91 10 9.80897 9 9.92535 16 0.07465 9.88362 7 90 11 9.80915 9 9.92516 15 0.07449 9.88343 7 89 13 9.80924 9 9.92561 15 0.07419 9.88343 7 87 14 9.80933 9 9.92597 15 0.07403 9.88336 86 87 16 0.80951 9 9.92628 16 0.07372 9.88336 7 85 17 9.80960 9 9.92643 15 0.07372 9.88317 6 83 18 9.80969 9 9.92658 15 0.07372 9.88317 6 83 10 8.80078 9 9.92658 16 0.07374 9.88317 6 83 10 0.8004 9 9.9265	15 1 1.5
10 9.80897 9 9.92535 16 0.07465 9.88362 7 90 11 9.80915 9 9.92531 16 0.07449 9.88355 6 89 12 9.80915 9 9.92561 15 0.07434 9.88349 6 88 13 9.80924 9 9.92581 15 0.07419 9.88343 7 86 14 9.80933 9 9.92597 15 0.07430 9.88336 6 86 15 9.80942 9 9.92612 15 0.07343 9.88336 6 86 16 9.80951 9 9.92628 16 0.07372 9.88323 7 84 17 9.80960 9 9.92643 15 0.07336 9.88317 6 83 18 9.80969 9 9.92653 16 0.07342 9.88317 6 83 10 9.80278 9 9.9267	1 1.5
11 9.80906 9 9.92551 15 0.07449 9.88355 7 89 12 9.80915 9 9.92566 15 0.07434 9.88349 6 88 13 9.80924 9 9.92581 16 0.07419 9.88343 7 87 14 9.80933 9 9.92597 15 0.07343 9.88336 6 85 15 9.80942 9 9.92612 15 0.07372 9.88330 6 85 16 9.80951 9 9.92643 15 0.07372 9.88317 6 83 17 9.80969 9 9.92683 15 0.07357 9.88317 6 83 18 9.80969 9 9.92673 16 0.07364 9.88341 7 81 10 0.8078 9 0.92673 16 0.07364 9.88341 7 81	1 1.5
12 9.80915 9 9.92566 15 0.07434 9.88349 6 88 13 9.80924 9 9.92581 15 0.07419 9.88343 6 87 14 9.80933 9 9.92597 15 0.07403 9.88336 7 86 15 9.80942 9 9.92612 15 0.07388 9.88336 85 16 9.80951 9 9.92628 16 0.07372 9.88323 7 84 17 9.80960 9 9.92643 15 0.07372 9.88317 6 83 18 9.80969 9 9.92643 15 0.07374 9.88317 7 83 18 9.80969 9 9.92653 16 0.07374 9.88311 7 82 10 0.80078 9 9.92654 16 0.07374 9.88311 7 82	
13 9.80924 9 9.92581 15 0.07419 9.88343 7 87 14 9.80933 9 9.92527 0.07403 9.88336 6 86 15 9.80942 9 9.92612 15 0.07388 9.88330 7 85 16 9.80951 9 9.92628 16 0.07372 9.88337 6 85 17 9.80960 9 9.92643 15 0.07357 9.88317 6 83 18 9.80969 9 9.92658 15 0.07342 9.88311 6 83 10 9.8078 9 9.92658 15 0.07342 9.88311 6 82 10 9.8078 9 9.92658 15 0.07346 9.88311 6 83	2 30
14 9.8933 9 9.92597 16 0.07403 9.88336 7 86 15 9.89942 9 9.92612 15 0.07388 9.88330 6 85 16 9.89951 9 9.92628 16 0.07372 9.88323 7 84 17 9.80960 9 9.92633 15 0.07357 9.88317 6 83 18 9.80969 9 9.92633 15 0.07336 9.88311 6 82 10 0.80078 9 0.92674 16 0.07336 0.88304 7 81 10 0.80078 9 0.9674 16 0.07336 0.88304 7 81	
15 9.80942 9 9.92612 15 0.07388 9.88330 7 85 16 9.80951 9 9.92628 16 0.07372 9.88323 7 84 17 9.80960 9 9.92643 15 0.07357 9.88317 6 83 18 9.80969 9 9.92658 15 0.07357 9.88317 6 83 18 9.80969 9 9.92658 15 0.07342 9.88311 82 10 0.80078 9 9.92658 16 0.07342 9.88311 7 82	3 4.5
16 9.89951 9 9.92628 16 0.07372 9.88323 7 84 17 9.80960 9 9.92643 15 0.07357 9.88317 6 83 18 9.80969 9 9.92658 15 0.07342 9.88311 7 81 10 9.8078 9 9.92658 16 0.07342 9.88311 7 81 10 0.8078 9 9.92658 16 0.07346 9.88311 7 81	
17 9.80960 9 9.92643 15 0.07357 9.88317 6 83 18 9.80969 9 9.92658 15 0.07342 9.88311 6 82 10 0.80078 9 9.92658 15 0.07342 9.88311 6 82	6 9.0
18 9.80969 9 9.92658 15 0.07342 9.88311 6 82 0.80078 9 9.92674 16 0.07326 9.88304 7 81	7 10.5
10 0 80078 9 0 02674 16 0 07326 0 88304 7 81	8 12.0
	9 23.3
20 0 80087 0 02680 0 07277 0 88208 80	
0 2006 9 0 0000 15 0 0000 7 70	9
22 0 81005 9 0 02720 16 0 07280 0 88285 6 78	_
23 0 81014 9 0 02725 15 0 07265 0 88270 0 77	1 0.9
24 0 87023 9 0 02777 10 0 07240 0 88272 7 76	3 2.7
25 0 81032 9 0 02766 15 0 07234 0 88266 0 75	3 2.7 4 3.6
26 0 81041 9 0 02781 15 0 07210 0 88250 7 74	5 4.5
AM 0 87040 0 00707 0 07202 0 88252 72	
28 0 81058 9 0 02812 15 0 07188 0 88246 7 72	8 7.2
20 0 81067 9 0 02827 15 0 07173 0 88240 0 71	9 8.1
20 0 87076 9 0 00842 10 0 07157 0 88224 0 70	
9 0 0000 15 0 0000 7 60	8
31 9.81035 9 9.92873 15 0.07142 9.30227 6 68 9.92873 15 0.07127 9.88221 6 68	1 0.8
32 0.81102 9 0.02880 16 0.07111 0.88214 7 67	2 1.6
24 0 87772 9 0 02004 15 0 02006 0 88208 0 66	3 2.4
35 0 87737 9 0 03030 16 0 07080 0 88307 7 65	4 3.2 5 4.0
26 0 81120 9 0 02025 I5 0 07065 0 88105 6 64	6 4.8
9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	4 3.2 5 4.0 6 4.8 7 5.6 8 6.4
28 0 81148 9 0 02066 16 0 07024 0 88182 7 62	8 0.4
20 0 81757 9 0 02081 15 0 07010 0 88176 6 61	311.2
10 0 87766 9 0 0 00006 15 0 07004 0 88760 7 60	
47 0 8 7 7 7 8 0 0 0 0 0 0 0 0 0 0 0 0 0	7
42 0 81182 9 0 02027 15 0 06072 0 88156 7 58	1 0.7
42 0 81102 9 0 02042 15 0 06058 0 88150 0 57	2 1.4
44 0 87207 9 0 02058 10 0 06042 0 88743 7 56	3 2.1
45 0 81210 9 0 02073 15 0 06027 0 88137 6 55	
46 0 81210 9 0 02088 15 0 06012 0 88120 7 54	4 2.8 5 3.5 6 4.2
47 0 81228 9 0 02104 16 0 06806 0 88124 6 53	7 4.9 8 5.6
48 0 87227 9 0 02170 15 0 06887 0 88717 7 52	7 4.9 8 5.6 9 6.3
40 0 87246 9 0 03735 16 0 06865 0 88711 0 51	9 6.3.
50 9.81254 8 9.93150 15 0.06850 9.88105 6 50	
Cos d. Cot d. c. Tan Sin d.	

40								139	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.81254	9	9.93150	15	0.06850	9.88105	-	50	ā.
51	9.81263		9.93165	_	0.06835	9.88098	7	49	16
52	9.81272	9	9.93181	16	0.06819	9.88092	6	48	
53	9.81281	9	9.93196	15 15	0.06804	9.88085	7	47	1 1.6 2 3.2
54	9.81290		9.93211		0.06789	9.88079		46	3 4.8
55	9.81299	9	9.93227	16	0.06773	9.88072	7	45	4 0.4
56	9.81308	9	9.93242	15	0.06758	9.88066	6	44	5 8.0
57	9.81316	8	9.93257	15	0.06743	9.88059	7	43	6 9.6
58	9.81325	9	9.93273	16	0.06727	9.88053	6	43	7 II.2 8 I2.8
59	9.81334	9	9.93288	15	0.06712	9.88046	7	41	9 14.4
60	9.81343	9	9.93303	15	0.06697	9.88040	6	40	
		9		16			7		15
61	9.81352	9	9.93319	15	0.06681	9.88033	6	39	
62	9.81361	9	9.93334	15	0.06666	9.88027	7	38	1 1.5
63	9.81370	8	9.93349	16	0.06651	9.88020	6	37	
64	9.81378	9	9.93365	15	0.06635	9.88014	7	36	3 4.5 4 6.0
65	9.81387	9	9.93380	15	0.06620	9.88007	6	35	5 7.5
66	9.81396	9	9.93395	16	0.06605	9.88001	7	34	
67	9.81405	9	9.93411	15	0.06589	9.87994	6	33	7 IO.5 8 I2.0
68	9.81414	8	9.93426	15	0.06574	9.87988	7	32	9 13.5
69	9.81422	9	9.93441	16	0.06559	9.87981	6	31	
70	9.81431	_	9.93457		0.06543	9.87975		30	
71	9.81440	9	9.93472	15	0.06528	9.87968	7	29	8
72	9.81449	9	9.93487	15	0.06513	9.87962	6	28	_
73	9.81458	9	9.93503	16	0.06497	9.87955	7	27	I 0.8 2 I.6
74	9.81467	9	9.93518	15	0.06482	9.87949	6	26	
75	9.81475	8	9.93518	15	0.06467	9.87949	7	25	4 3.2
76	9.81484	9	9.93549	16	0.06451	9.87935	7	24	5 4.0
77	9.81493	9	9.93564	15	0.06436	9.87929	6		6 4.8
78	9.81502	9	9.93504	15	0.00430	9.87929	7	23	7 5.6 8 6.4
79	9.81510	8		16	0.06405	9.87922	6	21	9 7.2
80		9	9.93595	15			7		
	9.81519	9	9.93610	15	0.06390	9.87909	6	20	7
81	9.81528	9	9.93625	16	0.06375	9.87903	7	19	
82	9.81537	9	9.93641	15	0.06359	9.87896	6	18	I 0.7 2 I.4
83	9.81546	8	9.93656	15	0.06344	9.87890	7	17	3 2.1
84	9.81554	9	9.93671	16	0.06329	9.87883	6	16	4 2.8
85	9.81563	9	9.93687	15	0.06313	9.87877	7	15	4 2.8 5 3.5 6 4.2
86	9.81572	9	9.93702	15	0.06298	9.87870	7	14	6 4.2
87	9.81581	8	9.93717	16	0.06283	9.87863	6	13	7 4.9 8 5.6 9 6.3
88	9.81589	9	9.93733	15	0.06267	9.87857	7	12	9 6.3
89	9.81598	9	9.93748	15	0.06252	9.87850	6	11	
90	9.81607	-	9.93763	-	0.06237	9.87844		10	
91	9.81616	9	9.93778	15	0.06222	9.87837	7	09	6
92	9.81624	8	9.93794	16	0.06206	9.87831	6	08	1 0.6
93	9.81633	9	9.93809	15	0.06191	9.87824	7	07	2 1.2
94	9.81642	9	9.93824	15	0.06176	9.87817	7	06	3 1.8
95	9.81651	9	9.93840	16	0.06160	9.87811	6	05	
96	9.81659	8	9.93855	15	0.06145	9.87804	7	04	4 2.4 5 3.0 6 3.6 7 4.2 8 4.8
97	9.81668	9	9.93870	15	0.06130	9.87798	6	03	7 4.2
98	9.81677	9	9.93870	16	0.00130	9.87798	7	03	8 4.8 9 5.4
99	9.81686	9	9.93000	15	0.06099	9.87785	6	OI	9 5.4
100		8		15			7	00	
100	9.81694		9.93916		0.06084	9.87778		-00	- D D
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

41°								138°	
	Sirì	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.81694		9.93916	16	0.06084	9.87778	-	100	
01	9.81703	9	9.93932		0.06068	9.87771	7	99	16
02	9.81712	9	9.93947	15 15	0.06053	9.87765	6	98	1 1.6
03	9.81720	9	9.93962	16	0.06038	9.87758	6	97	2 3.2
04	9.81729	9	9.93978	15	0.06022	9.87752	7	96	3 4.8
05	9.81738	9	9.93993	15	0.06007	9.87745	7	95	4 6.4 5 8.0
	9.81747	8	9.94008	15	0.05992	9.87738	6	94	6 9.6
07 08	9.81755 9.81764	9	9.94023 9.94039	16.	0.05977 0.05961	9.87732 9.87725	7	93 92	7 II.2 8 I2.8
09	9.81773	9	9.94054	15	0.05946	9.87719	6	91	9 14.4
10	9.81781	8	9.94069	15	0.05931	9.87712	7	90	
11	9.81790	9	9.94085	16	0.05915	9.87705	7	89	15
12	9.81790	9	9.94100	15	0.05900	9.87699	6	88	1 1.5
13	9.81807	8	9.94115	15	0.05885	9.87692	7	87	2 3.0
14	9.81816	9	9.94131	16	0.05869	9.87686	6	86	3 4.5 4 6.0
15	9.81825	9	9.94146	15 15	0.05854	9.87679	7	85	5 7.5
16	9.81833	9	9.94161	15	0.05839	9.87672	7 6	84	6 9.0
17	9.81842	9	9.94176	16	0.05824	9.87666	7	83	7 10.5 8 12.0
18	9.81851	8	9.94192	15	0.05808	9.87659	7	82	9 13.5
19	9.81859	9	9.94207	15	0.05793	9.87652	6	81	
20	9.81868	9	9.94222	16	0.05778	9.87646	7	80	
21	9.81877	8	9.94238	15	0.05762	9.87639	7	79	9
22	9.81885 9.81894	9	9.94253 9.94268	15	0.05747	9.87632 9.87626	6	78 77	1 0.9
		9		16	0.05716		7	76	2 1.8 3 2.7
24 25	9.81903	8	9.94284	15	0.05710	9.87619 9.87613	6	75	3 2.7 4 3.6
26	9.81920	9	9.94299	15	0.05686	9.87606	7	74	5 4.5
27	9.81929	9	9.94329	15	0.05671	9.87599	7	73	
28	9.81937	8	9.94345	16	0.05655	9.87593	6	72	8 7.2
29	9.81946	9	9.94360	15 15	0.05640	9.87586	7 7	71	9 8.1
30	9.81955	8	9.94375	16	0.05625	9.87579	6	70	
31	9.81963	9	9.94391	15	0.05609	9.87573	7	69	8
32	9.81972	8	9.94406	15	0.05594	9.87566	7	68	1 0.8 2 1.6
33	9.81980	9	9.94421	15	0.05579	9.87559	6	67	3 2.4
34	9.81989	9	9.94436 9.94452	16	0.05564	9.87553 9.87546	7	66 65	4 3.2 5 4.0
35 36	9.82006	8	9.94452	15	0.05533	9.87539	7	64	6 4.8
37	9.82015	9	9.94482	15	0.05518	9.87533	6	63	7 5.6
38	9.82023	8	9.94498	16	0.05502	9.87526	7	62	8 6.4
39	9.82032	9	9.94513	15	0.05487	9.87519	7	61	
40	9.82041	9	9.94528	15 15	0.05472	9.87513	7	60	
41	9.82049		9.94543	16	0.05457	9.87506		59	7
42	9.82058	9	9.94559	15	0.05441	9.87499	7 7	58	1 0.7
43	9.82066	9	9.94574	15	0.05426	9.87492	6	57	2 1.4
44	9.82075	9	9.94589	15	0.05411	9.87486	7	56	3 2.1 2.8
45 46	9.82084 9.82092	8	9.94604	16	0.05396	9.87479 9.87472	7	55	5 3.5
		9	1	15			6	54	6 4.2 7 4.9
47 48	9.82101	8	9.94635	15	0.05365	9.87466 9.87459	7	53 52	8 5.6
49	9.82118	9	9.94666	16	0.05334	9.87459	7	51	9 6.3
50	9.82126	8	9.94681	15	0.05319	9.87446	6	50	
<u> </u>	Cos	d.	Cot	d. c.	Tan	Sin	d.	-	P. P.
	. 003	u.		и, с.		· Dill			****

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.82126		9.94681		0.05319	9.87446		50	
51	9.82135	9	9.94696	15	0.05304	9.87439	7	49	16
52	9.82144	9 8	9.94711	15	0.05289	9.87432	7	48	
53	9.82152	9	9.94727		0.05273	9.87425	7	47	I I.6 2 3.2
54	9.82161		9.94742	15	0.05258	9.87419		46	3 4.8
55	9.82169	8	9.94757	15	0.05243	9.87412	7	45	4 6.4
56	9.82178	9	9.94772	15 16	0.05228	9.87405	7 6	44	5 8.0 6 9.6
57	9.82186		9.94788	,	0.05212	9.87399		43	
58	9.82195	9	9.94803	15	0.05197	9.87392	7	42	7 II.2 8 12.8
59	9.82203	9	9.94818	15 16	0.05182	9.87385	7	41	9 14 4
60	9.82212		9.94834		0.05166	9.87378	7	40	
61	9.82221	9	9.94849	15	0.05151	9.87372	6	39	15
62	9.82229	8	9.94864	15	0.05136	9.87365	7	38	I I.5
63	9.82238	9	9.94879	15	0.05121	9.87358	7	37	2 3.0
64	9.82246		9.94895	16	0.05105	9.87351	7	36	3 4.5 4 6.0
65	9.82255	9	9.94910	15	0.05090	9.87345	6	35	
66	9.82263		9.94925	15	0.05075	9.87338	7	34	6 9.0
67	9.82272	9	9.94940	15	0.05060	9.87331	7	33	7 10.5
68	9.82280	8	9.94956	16	0.05044	9.87325	6	32	
69	9.82289	9	9.94971	15	0.05029	9.87318	7	31	9 13.5
70	9.82297		9.94986	15	0.05014	9.87311	7	30	
71	9.82306	9	9.95001	15	0.04999	9.87304	7		
72	9.82314	8	9.95017	16	0.04999	9.87304	6	29 28	8
73	9.82323	9	9.95032	15	0.04968	9.87291	7	27	I 0.8
74	9.82331	8		15			7		2 I.6 3 2.4
75	9.82340	9	9.95047 9.95062	15	0.04953	9.87284 9.87277	7	26	4 3.2
76	9.82348	8	9.95078	16	0.04938	9.87277	7	25	5 4.0
		9		15			6	24	6 4.8
77 78	9.82357 9.82365	8	9.95093	15	0.04907	9.87264	7	23	7 5.6 8 6.4
79	9.82374	9	9.95108	16	0.04892	9.87257	7	22 2I	9 7.2
80		8	9.95124	15			7		
	9.82382	9	9.95139	15	0.04861	9.87243	6	20	7
81	9.82391	8	9.95154	15	0.04846	9.87237	7	19	
82	9.82399	9	9.95169	16	0.04831	9.87230	7	18	I 0.7 2 I.4
83	9.82408	8	9.95185	15	0.04815	9.87223	7	17	3 2.1
84	9.82416	8	9.95200	15	0.04800	9.87216	7	16	4 2.8
8 ₅	9.82424	9	9.95215	15	0.04785	9.87209	6	15	5 3.5 6 4.2
	9.82433	8	9.95230	16	0.04770	9.87203	7	14	7 4.9
87	9.82441	9	9.95246	15	0.04754	9.87196	7	13	7 4.9 8 5.6 9 6.3
88	9.82450	8	9.95261	15	0.04739	9.87189	7	12	9 6.3
89	9.82458	9	9.95276	15	0.04724	9.87182	7	II	
90	9.82467	8	9.95291	16	0.04709	9.87175	6	10	
91	9.82475	9	9.95307	15	0.04693	9.87169		09	6
92	9.82484	8	9.95322	15	0.04678	9.87162	7	08	1 0.6
93	9.82492	9	9.95337	15	0.04663	9.87155	7	07	2 1.2
94	9.82501	8	9.95352	16	0.04648	9.87148		06	3 I.8 4 2.4
95	9.82509	8	9.95368	15	0.04632	9.87141	7 6	05	
96	9.82517	9	9.95383	15	0.04617	9.87135	7	04	6 3.6
97	9.82526	8	9.95398	15	0.04602	9.87128		03	7 4.2 8 4.8
98	9.82534	9	9.95413	16	0.04587	9.87121	7	02	8 4.8
99	9.82543	8	9.95429	15	0.04571	9.87114	7	01	9 3.4
100	9.82551		9.95444		0.04556	9.87107		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.82551	9	9.95444	15	0.04556	9.87107	6	100	
OI	9.82560	8	9.95459	15	0.04541	9.87101	7	99	16
02	9.82568	8	9.95474	15	0.04526	9.87094	7	98	1 1.6
03	9.82576	9	9.95489	16	0.04511	9.87087	7	97	2 3.2
04	9.82585	8	9.95505	15	0.04495	9.87080	7	96	3 4.8 4 6.4
05 06	9.82593	9	9.95520 9.95535	15	0.04480	9.87073 9.87066	7	95 94	5 8.0
07	9.82610	8	9.95550	15	0.04450	9.87060	6	93	
08	9.82618	8	9.95566	16	0.04434	9.87053	7	93	7 II.2 8 I2.8
09	9.82627	9	9.95581	15	0.04419	9.87046	7	91	9 14.4
10	9.82635		9.95596	15	0.04404	9.87039	7	90	
11	9.82644	9	9.95611	15	0.04389	9.87032	7	89	15
12	9.82652	8	9.95627	16	0.04373	9.87025	7	88	1 1.5
13	9.82660	9	9.95642	15 15	0.04358	9.87018	7 6	87	2 3.0 3 4.5
14	9.82669	8	9.95657	15	0.04343	9.87012	7	86	3 4.5 4 6.0
15	9.82677	8	9.95672	16	0.04328	9.87005	7	85	5 7.5
16	9.82685	9	9.95688	15	0.04312	9.86998	7	84	6 9.0
17	9.82694	8	9.95703	15	0.04297	9.86991	7	83	8 12.0
18 19	9.82702	9	9.95718	15	0.04282	9.86984 9.86977	7	82 81	9 13.5
20	9.82711	8	9.95733	15		9.86970	7	80	
		8	9.95748	16	0.04252		7		
2I 22	9.82727 9.82736	9	9.95764 9.95779	15	0.04236	9.86963 9.86957	6	79 78	9
23	9.82744		9.95779	15	0.04221	9.86950	7	77	I 0.9 2 1.8
24	9.82752	8	9.95809	15	0.04191	9.86943	7	76	3 2.7 4 3.6
25	9.82761	9	9.95825	16	0.04191	9.86936	7	75	4 3.6
26	9.82769	8 8	9.95840	15	0.04160	9.86929	7	74	4 3.6 5 4.5 6 5.4
27	9.82777	-	9.95855	15	0.04145	9.86922	7	73	7 6.3
28	9.82786	9	9.95870	15 16	0.04130	9.86915	7	72	8 7.2 9 8.1
29	9.82794	8	9.95886	15	0.04114	9.86908	7	71	9 0.1
30	9.82802	9	9.95901	15	0.04099	9.86902	7	70	8
31	9.82811	8	9.95916	15	0.04084	9.86895	7	69	
32	9.82819	8	9.95931	15	0.04069	9.86888	7	68	1 0.8
33	9.82827	9	9.95946	16	0.04054	9.86881	7	67	3 2.4
34	9.82836	8	9.95962	15	0.04038	9.86874	7	66	4 3.2 5 4.0 6 4.8
35	9.82844 9.82852	8	9.95977 9.95992	15	0.04023	9.86867 9.86860	7	65 64	6 4.8
36	9.8286I	9	9.95992	15		9.86853	7	63	7 5.6 8 6.4
37 38	9.82869	8	9.96023	16	0.03993	9.86846	7	62	8 0.4
39	9.82877	8	9.96023	15	0.03962	9.86839	7	61	3 1
40	9.82885	8	9.96053	15	0.03947	9.86832	7	60	
41	9.82894	9	9.96068	15	0.03932	9.86826	6	59	7
42	9.82902	8	9.96083	15 16	0.03917	9.86819	7	58	1 0.7
43	9.82910	9	9.96099	15	0.03901	9.86812	7	57	2 1.4
44	9.82919	8	9.96114	15	0.03886	9.86805		56	3 2.I 4 2.8
45	9.82927	8	9.96129	15	0.03871	9.86798	7	55	5 3.5
46	9.82935	9	9.96144	16	0.03856	9.86791	7	54	6 4.2
47	9.82944	8	9.96160	15	0.03840	9.86784	7	53	7 4.9 8 5.6 9 6.3
48	9.82952	8	9.96175	15	0.03825	9.86777	7	52	9 6.3
49	9.82960	8	9.96190	15	0.03810	9.86770	7	51 50	
50	9.82968		9.96205	-	0.03795 Tan	9.86763 Sin	d.	00	P. P.
	Cos	d.	Cot	d.c.	Tan	Sin	a.	470	r.r.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.82968		9.96205	u. c.		9.86763	_u.	50	F. F.
		9		15	0.03795		7		
51	9.82977	8	9.96220	16	0.03780	9.86756	7	49	16
52	9.82985	8	9.96230	15	0.03764	9.86749	7	48	1 1.6
5 3	9.82993	8		15	0.03749	9.86742	7	47	2 3.2
54	9.83001	9	9.96266	15	0.03734	9.86735	7	46	3 4.8 4.6.4
55 56	9.83010	8	9.96281 9.96297	16	0.03719	9.86728 9.86721	7	45	
		8		15	0.03703		7	44	6 9.6
57	9.83026	8	9.96312	15	0.03688	9.86714	7	43	7 II.2 8 I2.8
58 59	9.83034 9.83043	9	9.96327 9.96342	15	0.03673 0.03658	9.86707	7	42	8 12.8 9 14.4
		8		15			6	41	9 1 14.4
60	9.83051	8	9.96357	16	0.03643	9.86694	7	40	4.5
61	9.83059	8	9.96373	15	0.03627	9.86687	7	39	15
62	9.83067	9	9.96388	15	0.03612	9.86680	7	38	1 1.5
63	9.83076	8	9.96403	15	0.03597	9.86673	7	37	
64	9.83084	8	9.96418	15	0.03582	9.86666	7	36	3 4.5 4.6.0
65	9.83092	8	9.96433	16	0.03567	9.86659	7	35	5 7.5
66	9.83100	9	9.96449	15	0.03551	9.86652	7	34	
67	9.83109	8	9.96464	15	0.03536	9.86645	7	33	7 IO.5 8 I2.0
68	9.83117	8	9.96479	15	0.03521	9.86638	7	32	9 13.5
69	9.83125	8	9.96494	16	0.03506	9.86631	7	31	
70	9.83133	8	9.96510	15	0.03490	9.86624	7	30	
71	9.83141	9	9.96525	15	0.03475	9.86617	7	29	9
72	9.83150	8	9.96540	15	0.03460	9.86610	7	28	1 0.9
73	9.83158	8	9.96555	15	0.03445	9.86603	7	27	2 1.8
74	9.83166	8	9.96570	16	0.03430	9.86596	7	26	3 2.7 4 3.6
75	9.83174	8	9.96586	15	0.03414	9.86589	7	25	4 3.6 5 4.5
76	9.83182	9	9.96601	15	0.03399	9.86582	7	24	6 5.4
77	9.83191	8	9.96616	15	0.03384	9.86575	7	23	7 6.3
78	9.83199	8	9.96631	15	0.03369	9.86568	7	22	8 7.2 9 8.1
79	9.83207	8	9.96646	16	0.03354	9.86561	7	21	9 0.1
80	9.83215	8	9.96662	15	0.03338	9.86554	7	20	
81	9.83223	_	9.96677	-	0.03323	9.86547		19	8
82	9.83232	9	9.96692	15	0.03308	9.86540	7	18	I 0.8
83	9.83240	8	9.96707	15 15	0.03293	9.86533	7 7	17	2 1.6 3 2.4
84	9.83248	8	9.96722	1	0.03278	9.86526	8	16	4 3.2
85	9.83256	8	9.96738	16	0.03262	9.86518		15	5 4.0
86	9.83264	8	9.96753	15 15	0.03247	9.86511	7 7	14	6 4.8
87	9.83272		9.96768	1	0.03232	9.86504		13	7 5.6 8 6.4
88	9.83281	9	9.96783	15 15	0.03217	9.86497	7 7	12	9 7.2
89	9.83289	8	9.96798	16	0.03202	9.86490	7	11	
90	9.83297	8	9.96814	15	0.03186	9.86483	7	10	
91	9.83305	1 -	9.96829	"	0.03171	9.86476	1	09	7
92	9.83313	8	9.96844	15	0.03156	9.86469	7	08	I 0.7
93	9.83321	9	9.96859	15 15	0.03141	9.86462	7	07	2 1.4
94	9.83330	-	9.96874	-	0.03126	9.86455		06	3 2.I 4 2.8
95	9.83338	8	9.96890	16	0.03110	9.86448	7	05	
96	9.83346	8	9.96905	15	0.03095	9.86441	7	04	6 4.2
97	9.83354		9.96920	15	0.03080	9.86434	7	03	7 4.9 8 5.6 9 6.3
98	9.83362	8	9.96935	15	0.03065	9.86427	7	02	8 5.6
99	9.83370	8	9.96950	15 16	0.03050	9.86420	7 7	01	9 0.3
100	9.83378	8	9.96966	10	0.03034	9.86413	7	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	CUS	· u.	COL	a. c.	Lan	OIII	. ц.	•	F.1.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.83378	8	9.96966	15	0.03034	9.86413	7	100	
OI	9.83386	9	9.96981	15	0.03019	9.86406		99	16
02	9.83395	8	9.96996	15	0.03004	9.86399	7 7	98	1 1.6
03	9.83403	8	9.97011	15	0.02989	9.86392	8	97	2 3.2
04	9.83411	8	9.97026	16	0.02974	9.86384		96	3 4.8
05	9.83419	8	9.97042	15	0.02958	9.86377	7 7	95	4 6.4
06	9.83427	8	9.97057	15	0.02943	9.86370	7	94	5 8.0 6 9.6
07	9.83435	8	9.97072	15	0.02928	9.86363		93	7 11.2
08	9.83443	8	9.97087	15	0.02913	9.86356	7 7	92	
09	9.83451	8	9.97102	16	0.02898	9.86349	7	91	9 14.4
10	9.83459	9	9.97118	15	0.02882	9.86342	7	90	
11	9.83468		9.97133	-	0.02867	9.86335		89	15
12	9.83476	8	9.97148	15	0.02852	9.86328	7	88	1 1.5
13	9.83484	8	9.97163	15	0.02837	9.86321	7	87	2 3.0
14	9.83492	8	9.97178	15	0.02822	9.86314	7	86	3 4.5 6.0
15	9.83500	8	9.97193	15	0.02807	9.86306	8	85	4 6.0 5 7.5
16	9.83508	8	9.97209		0.02791	9.86299	7	84	6 9.0
17	9.83516		9.97224	15	0.02776	9.86292	7	83	7 IO.5 8 I2.0
18	9.83524	8	9.97239	15	0.02761	9.86285	7	82	8 12.0 9 13.5
19	9.83532	8	9.97254	15	0.02746	9.86278	7	81	9 13.3
20	9.83540		9.97269	15	0.02731	9.86271	7	80	
21	9.83548	8	9.97285	16	0.02715	9.86264	7	79	9
22	9.83556	8	9.97203	15	0.02700	9.86257	7	78	-
23	9.83565	9	9.97315	15	0.02685	9.86250	7	77	I 0.9 2 I.8
24	9.83573	1	9.97330	15	0.02670	9.86242	8	76	
25	9.83581	8	9.97345	15	0.02655	9.86235	7	75	- 4 3.6
26	9.83589	8	9.97361	16	0.02639	9.86228	7	74	5 4.5 6 5.4
27	9.83597	8	9.97376	15	0.02624	9.86221	7	73	
28	9.83605	8	9.97391	15	0.02609	9.86214	7	72	8 7.2
29	9.83613	8	9.97406	15	0.02594	9.86207	7	71	9 8.1
30	9.83621	8	9.97421	15	0.02579	9.86200	7	70	
	9.83629	8	9.97437	16	0.02563	9.86192	8	69	8
31 32	9.83637	8	9.97457	15	0.02503	9.86185	7	68	1 0.8
33	9.83645	8	9.97452	15	0.02548	9.86178	7	67	2 1.6
		8		15			7	66	3 2.4
34 35	9.83653 9.83661	8	9.97482 9.97497	15	0.02518	9.86171 9.86164	7	65	4 3.2 5 4.0
36	9.83669	8	9.97512	15	0.02303	9.86157	7	64	6 4.8
	9.83677	8		16		9.86150	7		7 5.6 8 6.4
37 38	9.83685	8	9.97528 9.97543	15	0.02472 0.02457	9.86142	8	63 62	8 0.4
39	9.83693	8	9.97558	15	0.02437	9.86135	7	61	9 1 1.2
40		8		15			7		
	9.83701	8	9.97573	15	0.02427	9.86128	7	60	7
41	9.83709	8	9.97588	16	0.02412	9.86121	7	59	
42	9.83717 9.83725	8	9.97604 9.97619	15	0.02396	9.86114 9.86107	7	58	I 0.7 2 I.4
43		8		15	0.02381		8	57	
44	9.83733	8	9.97634	15	0.02366	9.86099	7	56	4 2.8
45 46	9.83741 9.83749	8	9.97649 , 9.97664	15	0.02351	9.86092 9.86085	7	55	5 3.5 6 4.2
		8		15			7	54	7 4.9
47	9.83757	8	9.97679	16	0.02321	9.86078	7	53	7 4.9 8 5.6 9 6.3
48 49	9.83765	8	9.97695	15	0.02305	9.86071 9.86063	8	52	9 6.3
	9.83773	8	9.97710	15	0.02290		7	51	
50	9.83781		9.97725		0.02275	9.86056		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.83781	8	9.97725		0.02275	9.86056		50	
51	9.83789	8	9.97740	15	0.02260	9.86049	7	49	
52	9.83797	8	9.97755	15	0.02245	9.86042	7	48	40
53	9.83805	8	9.97771	15	0.02229	9.86035	8	47	16
54	9.83813	8	9.97786	15	0.02214	9.86027	7	46	1 1.6
55	9.83821	8	9.97801	15	0.02199	9.86020	7	45	3 4.8
56	9.83829	8	9.97816	15	0.02184	9.86013	7	44	4 6.4
57	9.83837	8	9.97831	15	0.02169	9.86006	7	43	5 8.0
58 59	9.83845 9.83853	8	9.97846 9.97862	16	0.02154	9.85999 9.85991	8	42 41	6 9.6
60	9.83861	8	9.97877	15	0.02138	9.85984	7	40	7 II.2 8 I2.8
61	9.83869	8	9.97892	15	0.02108	9.85977	7	39	8 I2.8 9 I4.4
62	9.83877	8	9.97892	15	0.02103	9.85970	7	38	31, 24.4
63	9.83885	8	9.97922	15	0.02078	9.85962	8	37	
64	9.83898	8	9.97938	16	0.02062	9.85955	7	36	15
65	9.83901	8	9.97953	15	0.02047	9.85948	7	35	1 1.5
66	9.83909	8	9.97968	15 15	0.02032	9.85941	7	34	2 3.0
67	9.83917	8	9.97983		0.02017	9.85934	8	33	3 4.5
68	9.83925	7	9.97998	15 15	0.02002	9.85926	7	32	4 6.0
69	9.83932	8	9.98013	16	0.01987	9.85919	7	31	5 7.5 6 9.0
70_	9.83940	8	9.98029	15	0.01971	9.85912	7	30	7 10.5
71	9.83948	8	9.98044	15	0.01956	9.85905	8	29	8 12.0
72	9.83956	8	9.98059	15	0.01941	9.85897	7	28	9 13.5
73	9.83964	8	9.98074	15	0.01926	9.85890	7	27	
74	9.83972	8	9.98089	15	0.01911	9.85883	7	26	
75 76	9.83980 9.83988	8	9.98104 9.98120	16	0.01896	9.85876 9.85868	8	25 24	
	9.83996	8	9.98125	15	0.01865	9.85861	7	23	
77 78	9.83990	8	9.98150	15	0.01850	9.85854	7	22	8
79	9.84012	8	9.98165	15	0.01835	9.85847	7	21	1 0.8
80	9.84020	8	9.98180	15	0.01820	9.85839	8	20	2 1.6
81	9.84027	7	9.98195	15	0.01805	9.85832	7	19	3 2.4
82	9.84035	8	9.98211	16	0.01789	9.85825	7	18	4 3.2
83	9.84043	8	9.98226	15 15	0.01774	9.85817	8 7	17	5 4.0 6 4.8
84	9.84051	8	9.98241		0.01759	9.85810		16	7 5.6
85	9.84059	8	9.98256	15 15	0.01744	9.85803	7	15	8 6.4
86	9.84067	8	9.98271	16	0.01729	9.85796	8	14	9 7.2
87	9.84075	8	9.98287	15	0.01713	9.85788	7	13	
88 89	9.84083	8	9.98302	15	0.01698	9.85781	7	I2 II	
	9.84091	7	9.98317	15	0.01668	9.85774	8	10	7
90	9.84098	8	9.98332	15		9.85766	7		1 0.7
91	9.84106	8	9.98347 9.98362	15	0.01653	9.85759 9.85752	7	o9 o8	2 I.4 3 2.I
92 93	9.84114	8	9.98302	16	0.01622	9.85745	7	07	4 2.8
93	9.84130	8	9.98393	15	0.01607	9.85737	8	06	5 3.5
94	9.84138	8	9.90393	15	0.01592	9.85730	7	05	6 4.2
96	9.84146	8	9.98423	15	0.01577	9.85723	7 8	04	7 4.9
97	9.84154	-	9.98438	15	0.01562	9.85715		03	8 5.6
98	9.84161	7	9.98453	15	0.01547	9.85708	7	02	9.0.3
99	9.84169	8 8	9.98469	16 15	0.01531	9.85701	7 8	OI	
100	9.84177		9.98484		0.01516	9.85693		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

44								130	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.84177		9.98484	15	0.01516	9.85693	7	100	
01	9.84185	8	9.98499		0.01501	9.85686		99	
02	9.84193	8	9.98514	15	0.01486	9.85679	7 8	98	40
03	9.84201	8	9.98529	15 15	0.01471	9.85671	7	97	16
04	9.84209		9.98544		0.01456	9.85664		96	1 1.6
05	9.84216	7	9.98560	16	0.01440	9.85657	7 8	95	2 3.2
06	9.84224	8	9.98575	15 15	0.01425	9.85649	7	94	3 4.8
07	9.84232		9.98590		0.01410	9.85642		93	4 6.4 5 8.0
о8	9.84240	8	9.98605	15	0.01395	9.85635	7 8	92	6 9.6
09	9 84248	8 7	9.98620	15 15	0.01380	9.85627	7	91	7 11.2
10	9.84255	8	9.98635	16	0.01365	9.85620	7	90	8 12.8
11	9.84263	-	9.98651		0.01349	9.85613		89	9 14.4
12	9.84271	8	9.98666	15	0.01334	9.85605	8	88	
13	9.84279	8	9.98681	15	0.01319	9.85598	7	87	
14	9.84287	-	9.98696	15	0.01304	9.85591		86	15
15	9.84295	8	9.98711	15	0.01289	9.85583	8	85	1 1.5
16	9.84302	7	9.98726	15 16	0.01274	9.85576	7	84	2 3.0
17	9.84310	8	9.98742	ł	0.01258	9.85569		83	3 4.5
18	9.84318	8	9.98757	15	0.01243	9.85561	8	82	4 6.0
19	9.84326	8	9.98772	15	0.01228	9.85554	7	81	5 7.5
20	9.84334	8	9.98787	15	0.01213	9.85547	8	80	6 9.0
21	9.84341	7	9.98802	15	0.01198	9.85539	_	79	7 10.5 8 12.0
22	9.84349	8	9.98817	15	0.01183	9.85532	7	78	9 13.5
23	9.84357	8	9.98833	16	0.01167	9.85524	8	77	9 13.3
24	9.84365	8	9.98848	15	0.01152	9.85517	7	76	
25	9.84373	8	9.98863	15	0.01137	9.85510	7	75	
26	9.84380	7	9.98878	15	0.01122	9.85502	8	74	
27	9.84388	8	9.98893	15	0.01107	9.85495	7	73	
28	9.84396	8	9.98908	15	0.01092	9.85487	8	72	8
29	9.84404	8	9.98924	16	0.01076	9.85480	7	71	1 0.8
30	9.84411	7	9.98939	15	ô.01061	9.85473	7	70	2 1.6
31	9.84419	8	9.98954	15	0.01046	9.85465	8	69	3 2.4
32	9.84427	8	9.98969	15	0.01031	9.85458	7	68	4 3.2
33	9.84435	8	9.98984	15	0.01016	9.85450	8	67	5 4.0 6 4.8
34	9.84442	7	9.98999	15	0.01001	9.85443	7	66	7 5.6
35	9.84450	8	9.99015	16	0.00985	9.85436	7	65	8 6.4
36	9.84458	8	9.99030	15	0.00970	9.85428	8	64	9 7.2
37	9.84466	8	9.99045	15	0.00955	9.85421	7	63	
38	9.84473	7	9.99060	15	0.00940	9.85413	8	62	
39	9.84481	8	9.99075	15	0.00925	9.85406	7 7	61	7
40	9.84489	8	9.99090	15	0.00910	9.85399	8	60	1 0.7
41	9.84497	8	9.99106	16	0.00894	9.85391	1	59	2 1.4
42	9.84504	7	9.99121	15	0.00879	9.85384	7	58	3 2.1
43	9.84512	8	9.99136	15	0.00864	9.85376	8 7	57	4 2.8
44	9.84520	8	9.99151	15	0.00849	9.85369		56	5 3.5
45	9.84528	8	9.99166	15	0.00834	9.85361	8	55	6 4.2
46	9.84535	7	9.99181	15	0.00819	9.85354	7 7	54	7 4.9 8 5.6
47	9.84543	8	9.99196	15	0.00804	9.85347		53	9 6.3
48	9.84551	8	9.99212	16	0.00788	9.85339	8	52	3 , 5.0
49	9.84558	7 8	9.99227	15	0.00773	9.85332	7 8	51	
50	9.84566	8	9.99242	15	0.00758	9.85324		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

44								135	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.84566	8	9.99242	15	0.00758	9.85324	7	50	
51	9.84574	8	9.99257	_	0.00743	9.85317	8	49	
52	9.84582	7	9.99272	15	0.00728	9.85309	7	48	4.0
53	9.84589	8	9.99287	16	0.00713	9.85302	8	47	16
54	9.84597	8	9.99303		0.00697	9.85294	_	46	1 1.6
55	9.84605	7	9.99318	15 15	0.00682	9.85287	7 8	45	2 3.2
56	9.84612	8	9.99333	15	0.00667	9.85279	7	44	3 4.8 4.6.4
57	9.84620	8	9.99348	15	0.00652	9.85272	7	43	4 6.4 5 8.0
58	9.84628	7	9.99363	15	0.00637	9.85265	8	42	6 9.6
59	9.84635	8	9.99378	16	0.00622	9.85257	7	41	7 11.2
60	9.84643	8	9-99394	15	0.00606	9.85250	8	40	8 12.8
61	9.84651		9.99409		0.00591	9.85242	_	39	9 14.4
62	9.84659	8	9.99424	15	0.00576	9.85235	7 8	38	
63	9.84666	7 8	9.99439	15	0.00561	9.85227	7	37	
64	9.84674		9.99454		0.00546	9.85220		36	15
65	9.84682	8	9.99469	15 16	0.00531	9.85212	8	35	I I.5
66	9.84689	7 8	9.99485	15	0.00515	9.85205	8	34	2 3.0
67	9.84697	8	9.99500		0.00500	9.85197		33	3 4.5
68	9.84705	7	9.99515	15 15	0.00485	9.85190	7 8	32	4 6.0
69	9.84712	8	9.99530	15	0.00470	9.85182	7	31	5 7.5
70	9.84720	8	9.99545	15	0.00455	9.85175	8	30	6 9.0
71	9.84728		9.99560	_	0.00440	9.85167		29	8 12.0
72	9.84735	7	9.99576	16	0.00424	9.85160	7 8	28	9 13.5
73	9.84743	8 8	9.99591	15 15	0.00409	9.85152	7	27	9 20.3
74	9.84751		9.99606		0.00394	9.85145		26	
75	9.84758	7 8	9.99621	15	0.00379	9.85137	8	25	
76	9.84766	7	9.99636	15 15	0.00364	9.85130	7 8	24	
77	9.84773	8	9.99651		0.00349	9.85122		23	
78	9.84781	8	9.99666	15 16	0.00334	9.85115	7 8	22	8
79	9.84789	7	9.99682	15	0.00318	9.85107	7	21	I 0.8
80	9.84796	8	9.99697	15	0.00303	9.85100	8	20	2 1.6
81	9.84804		9.99712	_	0.00288	9.85092		19	3 2.4 4 3.2
82	9.84812	8	9.99727	15	0.00273	9.85085	7 8	18	4 3.2 5 4.0
83	9.84819	7 8	9.99742	15 15	0.00258	9.85077	8	17	6 4.8
84	9.84827		9.99757	_	0.00243	9.85069	- 1	16	7 5.6
85	9.84835	8 7	9.99773	16 15	0.00227	9.85062	7 8	15	8 6.4
86	9.84842	8	9.99788	15	0.00212	9.85054	7	14	9 7.2
87	9.84850	7	9.99803		0.00197	9.85047	8	13	
88	9.84857	8	9.99818	15 15	0.00182	9.85039	7	12	
89	9.84865	8	9.99833	15	0.00167	9.85032	8	II	7
90	9.84873	7	9.99848	16	0.00152	9.85024	7	10	I 0.7
91	9.84880		9.99864		0.00136	9.85017	8	09	2 1.4
92	9.84888	8 7	9.99879	15 15	0.00121	9.85009	8	08	3 2.1
93	9.84895	8	9.99894	15	0.00106	9.85001	7	07	4 2.8
94	9.84903	8.	9.99909	15	0.00091	9.84994	8	06	5 3.5 6 4.2
95	9.84911	7	9.99924	15	0.00076	9.84986	7	05	7 4.9
96	9.84918	8	9.99939	16	0.00061	9.84979	8	04	8 5.6
97	9.84926	7	9.99955	15	0.00045	9.84971	7	03	9 6.3
98	9.84933	8	9.99970	15	0.00030	9.84964	8	02	
99	9.84941	8	9.99985	15	0.00015	9.84956	7	OI	
100	9.84949		10.00000		0.00000	9.84949		00	
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

TABLE XXVI.—Logarithmic Versed Sines and External Secants Log vs = $2\log\alpha^\circ + V$ Log exsec = $2\log\alpha^\circ + E$

Hun-		0	٥		Hun-		1	٥	
dredths	Vers	V	E	Exsec	dredths	Vers	V	E	Exsec
		6.	182				6.	182	
00	Inf. neg.	725	725	Inf. neg.	00	6.18271	714	780	6.18278
02	2.78478	725	725	2.78478	02	.19991	713	782	.19998
04	3.38684	725	725	3.38684	04	.21678	713	785	.21685
06	.73903	725	725	.73903	06	.23332	712	787	.23339
08	.98890 4.18272	725 725	725 725	.98890 4.18272	08 10	.24956 6.26549	712 711	789 791	.24964 6.26557
12	.34109	725	726	.34109	12	.28115	711	791	,28123
14	.47498	725	726	.47498	14	.29652	711	797	.29661
16	.59096	724	726	.59096	16	.31163	710	799	.31172
18	.69327	724	727	.69327	18		709	801	.33470
20	4.78478	724	727	4.78479	20	6.34107	709	804	6.34116
22	.86757	724	727	.86757	22	-35543	708	807	-35553
24	.94315	724	728	.94315	24	.36955	708	810	.36965
26 28	5.01267	724	729	5.01268	26 28	.38345	707	812	.38356
30	.07704 5.13697	724 724	729 730	5.13697	30	.39713 6.41059	707 706	815 818	.39724 6.41070
32	.19302	724	731	.19303	32	.42385	706	821	.42397
34	,24568	723	73I	.24569	34	.43691	705	824	.43703
36	.29533	723	732	.29534	36	-44977	704	827	.44989
38	.34229	723	733	.34230	38	.46246	704	830	. 46259
40	5.38684	723	734	5.38685	40	6.47496	703	833	6.47509
42	.42922	723	735	.42923	42	. 48728	703	836	.48741
44	.46962	722	735	.46964	44	-49943	702	839	-49957
46 48	.50824	722	736	.50825	46	.51141	701	842	.51155
50	.5452I 5.58066	722 722	737 739	5.58068	48 50	.52322 6.53488	700 700	845 849	6.53503
52	.61473	722	740	.61475	52	.54639	699	852	.54654
54	.64751	721	740	.64753	54	-55774	699	855	.55790
56	.67910	721	742	.67912	56	.56895	698	859	.56911
58	.70958	721	743	.70960	58	.58001	697	863	.58018
60	5.73902	721	745	5.73904	60	6.59093	697	866	6.59110
62	.76750	720	746	.76753	62	.60173	696	870	.60190
64 66	.79508 .82181	720 720	747	.79511	64 66	.61238 .62291	695 694	873 877	.61256
68	.84774	720	749 750	.84777	68	.63331	694	881	.63350
70	5.87292	719	752	5.87295	70	6.64359	693	884	6.64378
72	.89738	719	753	.89742	72	.65375	692	888	.65395
74	.92118	719	755	.92122	74	.66379	692	892	.66399
76	.94435	718	756	.94438	76	.67372	691	896	.67392
78	.96691	718	758	.96695	78	.68353	690	900	.68374
80	5.98890	718	760	5.98894	80	6.69323	689	903	6.69345
82 84	6.01034	717	762 764	6.01039	82 84	.70383	688 687	907	.70405
86	.03128	717 717	766	.03132	86	.71232 .72171	686	911	.71254 .72194
88	.07168	716	767	.07173	88	.73100	686	919	.73123
90	6.09120	716	769	6.09125	90	6.74019	685	924	6.74043
92	.11029	715	772	.11035	92	.74929	684	928	.74953
94	.12897	715	774	.12903	94	.75829	683	932	.75854
96 98	.14726	715	776	.14732	96	.76718	682 681	936	.76743
100		714	778	.16523	98	.77601	1	941	.77627
100	6.18271	714	780	6.18278	100	6.78474	681	945	6.78500

TABLE XXVI.—Logarithmic Versed Sines and External Secants Log vs = $2 \log \alpha^{\circ} + V$ Log exsec = $2 \log \alpha^{\circ} + E$

Hun-		2	٥		Hun-		3	0	
dredths	Vers	V	E	Exsec	dredths	Vers	V	E	Exsec
		6.	182				6.182	6.183	
00	6.78474	681	945	6.78501	00	7.13687	626	221	7.13746
02	.79338	680	950	.79365	02	.14264	624	228	. 14324
04	.80194	679	954	.80221	04	.14837	623	234	.14898
06	.81041	678	958	.81069	06	.15406	621	241	.16468
08	.81880 6.82712	677 676	963 968	.81909 6.82741	08	.15972 7.16534	620 619	248 255	.16035 7.16598
12	.83535	675	973	.83565	12	.17093	618	253	.17157
14	.84350	674	978	.84381	14	.17648	616	268	.17713
16	.85158	673	982	.85189	16	.18199	614	275	.18265
18	.85959	672	987	.85990	18	. 18747	613	283	.18814
20	6.86752	671	992	6.86784	20	7.19291	612	290	7.19359
22	.87538	670	997	.87570	22	.18832	610	296	.19901
24 26	.88317	669 668	*002	.88350	24 26	.20370	609 607	303 311	.20439
28	.89854	667	011	.89888	28	.21435	606	318	.20975
30	6.90612	666	016	6.90647	30	7.21963	605	325	7.22035
32	.91364	665	022	.91400	32	.22488	603	333	.22561
34	.92110	664	027	.92146	34	.23010	602	340	. 23083
36	.92849	663	032	.92886	36	.23528	600	348	.23603
38	.93582	662	037	.93619	38	.24043	599	355	.24119
40	6.94308	661	042	6.94347	40	7.24556	597	362	7.24632
42	.95029	660	048	.95068	42	.25065	596	370	.25142
44 46	.95744 .96453	659 658	o53 o58	.95783	44 46	.25571	595 593	377 385	. 25649 . 26154
48	.97156	657	063	.97197	48	.26575	59I	393	. 26655
50	6.97854	656	069	6.97895	50	7.27073	590	400	7.27154
52	.98546	655	075	.98588	52	. 27567	588	408	. 27649
54	.99232	654	081	.99275	54	.28059	587	416	.28142
56	.99913	652	286	•99957	56	.28549	585	424	. 28632
58 60	.00589	651	092 098	.00633	58	.29035	583	432	. 29120
	7.01260	650	-	7.01304	60	7.29519	582	440	7.29605
62 64	.01925	649 648	103	.01971	62 64	.30000	581 579	448 456	.30087
66	.03241	646	115	.03288	66	.30954	577	464	.31043
68	.03891	645	121	.03939	68	.31427	575	472	.31517
70	7.04537	644	127	7.04585	70	7.31898	574	480	7.31988
72	.05178	643	133	.05227	72	.32366	572	488	-32457
74	.05814	642	139	.05864	74	.32831	571	496	.32924
76 78	.06446	640 639	145 151	.06496	76 78	.33294	569 567	504 512	.33388
80	7.07695	638	157	7.07747	80	7.34213	566	521	7.34309
82	.08314	637	163	.08366	82	.34669	564	529	.34766
84	.08927	636	169	.08981	84	.35122	562	538	.35220
86	.09537	634	176	.09 5 91	86	-35574	560	547	.35672
88	.10142	633	182	. 10197	88	.36022	558	556	.36122
90	7.10743	632	189 195	7.10799	90	7.36469	557	564	7.36569
92	.11340	631 630	201	.11396	92	.36913	555	572 581	.37014
94 96	.11932	628	208	.11790	94 96	-37355 -37794	553 552	590	.37457 .37898
98	.13106	627	215	.13165	98	.38232	550	599	.38337
100	7.13687	626	22Ĭ *183	7.13746	100	7.38667	548	608	7.38773
			* 183			7	· .		

		4	0				5	٥	
Hun- dredths		Diff.		Diff.	Hun- dredths		Diff.		Diff.
dredtiis	Vers	.001	Exsec	.001	dicams	Vers.	.001	Exsec	.001
00	7.38667	21.65	7.38773	21.75	00	7.58039	17.30	7.58204	17.40
02	.39100	21.55	.39207	21.75	02	. 58385	17.30	.58552	17.35
04	.39531	21.33	.39639	.21.50	04	.58731	17.15	. 58899	17.25
06	.39960	21.30	.40069	21.35	06	. 59074	17.15	.59244	17.20
· 08	.40386	21.25	.40496 7.40922	21.30	08 10	.59417 7.59758	17.05	.59588 7.59930	17.10
12	.41233	21.10	.41346	21.20	12	.60098	17.00	.60271	17.05
14	.41654	21.05	.41767	21.05	14	.60436	16.90	.60611	17.00
16	.42072	20.90	.42187	21.00	16	.60773	16.85 16.80	.60949	16.90 16.90
18	.42488	20.75	.42604	20.80	18	.61109	16.70	.61287	16.75
20	7.42903	20.60	7.43020	20.65	20	7.61443	16.70	7.61622	16.75
22	.43315	20.55	-43433	20.60	22	.61777	16.55	.61957	16.65
24 26	.43726	20.40	.43845	20.50	24 26	.62108 .62439	16.55	.62290	16.60
28	.44134	20.35	.44255	20.35	28		16.50		16.55
28 30	.4454I 7.44946	20.25	.44662 7.45068	20.30	28 30	.62769 7.63097	16.40	.62953 7.63283	16.50
32	.45349	20.15	.45472	20.20	32	.63424	16.35	.63611	16.40
34	.45750	20.05	.45874	20.10	34	.63749	16.25	.63938	16.35
36	.46149	19.95	.46275	20.05	36	.64074	16.25	.64264	16.30
38	.46546	19.80	.46673	19.85	38	.64397	16.10	.64589	16.15
40	7.46942	19.65	7.47070	19.75	40	7.64719	16.05	7.64912	16.15
42	·47335	19.60	.47465	19.65	42	.65040	16.00	.65235	16.05
44	.47727	19.55	.47858	19.55	44	.65360 .65678	15.90	.65556	16.00
46 48	.48506	19.40	.48249	19.50	46 48		15.85	.66194	15.90
50	7.48893	19.35	.48639 7.49027	19.40	50	.65995 7.66312	15.85	7.66512	15.90
52	.49278	19.25	.49413	19.30	52	.66627	15.75	.66829	15.85
54	.49661	19.15	.49797	19.20	54	.66941	15.70	.67144	15.75
56	.50043	19.10	.50180	19.15	56	.67253	15.60	.67458	15.70
58	.50422	18.95	.50561	19.00	58	.67565	15.55	.67771	15.60
60	7.50801	18.80	7.50941	18.90	60	7.67876	15.45	7.68083	15.55
62	.51177	18.75	.51319	18.80	62	.68185	15.40	.68394	15.50
64 66	.51552	18.70	.51695	18.75	64 66	.68493	15.35	.68704	15 45
68	.52297	18.55	.52443	18.65	68	.69107	15.35	.69320	15.35
70	7.52668	18.55	7.52814	18.55	70	7.69412	15.25	7.69627	15.35
72	.53036	18.40	.53184	18.50	72	.69716	15.20	.69932	15.25
74	.53403	18.30	-53552	18.35	74	.70019	15.05	.70237	15.15
76	.53769	18.20	.53919	18.25	76	.70320	15.05	.70540	15.15
78	.54133	18.10	.54284	18.20	78	.70621	15.00	.70843	15.05
80	7.54495	18.05	7.54648	18.10	80	7.70921	14.95	7.71144	15.00
82 84	.54856	17.90	.55010	18.05	8 ₂ 8 ₄	.71220	14.85	.71444	14.95
86	.55216	17.90	.55371	17.95	86	.71517	14.85	.71743	14.95
88	.55930	17.80	.56088	17.90	88	.72110	14.80	.72339	14.85
90	7.56285	17.75	7.56444	17.80	90	7.72405	14.75	7.72635	14.80
92	.56639	17.70	.56799	17.75	92	.72698	14.65	.72930	14.75
94	.56991	17.55	.57153	17.60	94	.72991	14.60	.73225	14.65
96	.57342	17.45	.57505	17.50	96	.73283	14.50	.73518	14.60
98	.57691	17.40	.57855	17.45	. 98	.73573	14.50	.73810	14.55
100	7.58039		7.58204	1	100	7.73863	1	7.74102	

TABLE XXVI. — (Continued)

			0			7°			
Hun-			0		Hun-				
dredths	Vers	Diff. .001	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	7.73863	14.45	7.74102	14.50	00	7.87238	12.40	7.87563	12.45
02	.74152	14.40	.74392	14.45	02	.87486	12.30	.87812	12.45
04 06	.74440	14.35	.74681	14.45	04 06	.87732	12.30	.88061	12.40
08	.74727	14.25	.74970	14.35		.87978	12.30	.88309	12.35
10	.75012 7.75297	14.25	.75257 7.75544	14.35	08 10	.88224 7.88469	12.25	.88556 7.88803	12.35
12	.75581	14.20	.75830	14.30	12	.88713	12.20	.89049	12.30
14	.75865	14.20	.76114	14.20	14	.88956	12.15	.89294	12.25
16	.76147	14.10	.76398	14.20	16	.89199	12.15	.89539	12.25
18	.76428	14.05	.76681	14.15	18	.89441	12.10	.89782	12.15
20	7.76708	14.00	7.76963	14.05	20	7.89682	12.00	7.90026	12.10
22	.76988	13.90	.77244	14.05	22	.89922	12.00	.90268	12.10
24	.77266	13.90	.77525	13.95	24	.90162	12.00	.90510	12.10
26	•77544	13.85	.77804	13.90	26	.90402	11.90	.90751	12.05
28 30	.77821 7.78097	13.80	.78082 7.78360	13.90	28 30	.90640 7.90878	11.90	.90992 7.91232	12.00
32	.78372	13.75	.78637	13.85	32	.91116	11.90	.91471	11.95
34	.78646	13.70	.78912	13.75	34	.91352	11.80	.91710	11.95
36	78919	13.65	.79187	13.75	36	.91588	11.80	.91948	11.90
38	.79192	13.65	.79462	13.75 13.65	38	.91824	11.80	.92185	11.85
40	7.79463		7.79735		40	7.92058		7.92422	11.80
42	.79734	13.55	.80007	13.60	42	.92293	11.75	.92658	
44	.80004	13.50	.80279	13.60	44	.92526	11.65	.92893	11.75
46	.80273	13.40	.80550	13.50	46	.92759	11.60	.93128	11.70
48	.80541	13.40	.80820	13.45	48	.92991	11.60	.93362	11.70
50 52	7.80809	13.30	7.81089	13.40	50 52	7.93223 •93454	11.55	7.93596	11.65
54	.81341	13.30	.81624	13.35	54	.93434	11.50	.93029	11.60
56	.81606	13.25	.81891	13.35	56	.93914	11.50	.94293	11.60
58	.81870	13.20	.82157	13.30	58	.94143	11.45	.94524	11.55
60	7.82133	13.15	7.82422	13.25	60	7.94372	11.45	7.94755	11.55
62	.82396	13.15	.82686	13.20	62	-94599	11.35	.94985	11.50
64	.82657	13.05	.82950	13.20 13.10	64	.94827	11.40	.95214	II.45 II.45
66	.82918	13.05	.83212	13.10	66	.95054	11.30	-95443	11.40
68	.83179	12.95	.83474	13.10	68	.95280	11.25	.95671	11.40
70 72	7.83438 .83697	12.95	7.83736	13.00	70 72	7.95505	11.25	7.95899	11.35
74	.83954	12.85	.84256	13.00	74	.95730	11.25	.96352	11.30
76	.84211	12.85	.84514	12.90	76	.95955	11.15	.96578	11.30
78	.84468	12.85	.84773	12.95	78	.96402	11.20	.96803	11.25
80	7.84723	12.75	7.85030	12.85	80	7.96624	11.10	7.97028	11.25
82	.84978	12.75	.85286	12.80	82	.96846	11.10	.97252	11.20
84	.85232	12.70	.85542	12.80	84	.97068	11.10	.97476	II.20 II.15
86	.85485	12.65	.85797	12.75	86	.97289	11.00	.97699	11.15
88	.85738	12.60	.86052	12.70	88	.97509	11.00	.97921	11.10
90 92	7.85990 .86241	12.55	7.86306 .86558	12.60	90 9 2	7.97729 .97948	10.95	7.98143	11.10
94	.86491	12.50	.86811	12.65	94	.98167	10.95	.98585	11.00
96	.86741	12.50	.87062	12.55	96	.98385	10.90	.98806	11.05
98	.86990	12.45	.87313	12.55	98	.98603	10.90	.99025	10.95
100	7.87238	12.40	7.87563	12.50	100	7.98820	10.85	7.99245	11.00

		8	0		**		9	0	
Hun- dredths		Diff.		Diff.	Hun- dredths	77	Diff.	- D	Diff.
diedths	Vers	.001	Exsec	100.	arcanno	Vers	.001	Exsec	.001
00	7.98820	10.80	7.99245	10.90	00	8.09032	9.60	8.09570	9.70
02	.99036	10.80	.99463	10.90	02	.09224	9.60	.09764	9.65
04 06	.99252 .99468	10.80	.99681	10.90	04 06	.09416 .09608	9.60	.09959	9.60
08	.99408	10.75	8.00116	10.85	08	.09799	9.55	.10346	9.65
10	7.99897	10.70	8.00333	10.85	10	8.09989	9.50	8.10540	9.70
12	8.00111	10.70	.00549	10.80	12	.10180	9.55 9.50	.10732	9.60
14	.00324	10.65	.00764	10.75	14	.10370	9.45	. 10925	9.55
16	.00537	10.60	.00979	10.70	16 18	.10559	9.45	.11116	9.60
18	.00749	10.60	.01193	10.70	20		9.45	8.11499	9.55
20	8.00961	10.55	8.01407	10.70		8.10937	9.40	.11690	9.55
22 24	.01172	10.55	.01021	10.65	22 24	.11125	9.40	.11880	9.50
26	.01593	10.50	.02046	10.60	26	.11500	9.35	.12070	9.50
28	.01803	10.50	.02258		28	.11687	9.35	.12259	9.45 9.45
30	8.02012	10.45	8.02469	10.55	30	8.11874	9.35	8.12448	9.45
32	.02221	10.40	.02680	10.55	32	.12060	9.30	.12637	9.40
34	.02429	10.40	.02891	10.50	34	.12246	9.25	.12825	9.40
36 38	.02637	10.35	.03101	10.45	36 38	.12431	9.25	.13013	9.40
40	8.03051	10.35	8.03519	10.45	40	8.12801	9.25	8.13388	9.35
42	.03257	10.30	.03727	10.40	42	.12985	9.20	.13574	9.30
44	.03462	10.25	.03935	10.40	44	.13169	9.20	.13761	9.35 9.30
46	.03668	10.30	.04143	10.40	46	.13352	9.15	.13947	9.35
48	.03872	10.25	.04350	10.30	48	.13535	9.15	.14132	9.25
50	8.04077	10.15	8.04556	10.30	50	8.13718	9.10	8.14317	9.25
52 54	.04280	10.20	.04762	10.20	52	.13900	9.10	.14502	9.25
54 56	.04484	10.10	.05173	10.25	54 56	.14062	9.05	.14871	9.20
58	.04889	10.15	.05378	10.25	58	.14444	9.05	.15054	9.15
60	8.05091	10.10	8.05582	10.15	60	8.14625	9.00	8.15238	9.10
62	.05292	10.05	.05785	10.13	62	.14805	9.00	.15420	9.15
64	.05493	10.00	.05989	10.10	64	.14985	9.00	.15603	9.10
66	.05693	10.00	.06191	10.15	66	.15165	8.95	.15785	9.10
68 70	.05893 8.06093	10.00	8.06394	10.05	68	.15344 8.15523	8.95	.15967 8.16148	9.05
70	.06292	9.95	.06797	10.10	70	.15702	8.95	.16330	9.10
74	.06491	9.95	.06998	10.05	74	.15880	8.90	.16510	9.00
76	.06689	9.90	.07198	10.00	76	.16057	8.85	.16691	9.05
78	.06886	9.90	.07398	10.00	78	.16235	8.85	. 16871	8.95
80	8.07084	9.80	8.07598	9.95	80	8.16412	8.80	8.17050	8.95
82	.07280	9.85	.07797	9.95	82	.16588	8.85	.17229	8.95
84 86	.07477	9.80	.07996	9.90	84 86	.16765	8.80	.17408	8.95
88	.07868	9.75	.08392	9.90	88	.17116	8.75	.17765	8.90
90	8.08063	9.75	8.08589	9.85	90	8.17291	8.75	8.17943	8.90
92	.08258	9.75	.08786	9.85	92	.17466	8.75	.18120	8.90
94	.08452	9.70	.08983	9.80	94	.17641	8.70	.18298	8.80
96 98	.08646	9.65	.09179	9.75	96	.17815	8.70	.18474	8.85
100	.08839	9.65	.09374	9.80	98 100	.17989	8.65	8.18827	8.80
100	8.09032	1	8.09570	1	100	8.18162	1	1 8.18827	1

Hun-		10	0°		Hun-		11	•	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	8,18162	.001	8.18827	.001	- 00	8.26418	.001	8.27223	.001
02	.18335	8.65	.19003	8.80	02	.26575	7.85	.27383	8.00
04	.18508	8.65	.19178	8.75	04	.26732	7.85	.27543	8.00
06	.18680	8.60 8.65	.19353	8.75	06	. 26889	7.85	.27703	8.00
08	.18853	8.55	.19528	8.75 8.75	о8	. 27045	7.80	. 27862	7.95
10	8.19024	8.60	8.19703	8.70	10	8.27201	7.80	8.28021	7.95 7.95
12	.19196	8.55	.19877	8.65	12	.27357	7.80	.28180	7.95
14 16	.19367	8.50	.20224	8.70	14 16	.27513	7.75	. 28339	7.90
18	.19537	8.55	.20224	8.65	18	.27823	7.75	.28655	7.90
20	8.19878	8.50	8.20570	8.65	20	8.27978	7.75	8.28813	7.90
22	.20047	8.45	.20742	8.60	22	.28132	7.70	.28970	7.85
24	.20217	8.50	.20914	8.60	24	.28286	7.70	.29128	7.90
26	.20386	8.45	.21086	8.60	26	. 28440	7.70	.29284	7.80
28	.20555	8.45	.21257	8.55	28	. 28594	7.70	. 29441	7.85
30	8.20723	8.40	8.21428	8.55	30	8.28747	7.65	8.29598	7.80
32	. 20891	8.40	.21599	8.55	32	. 28900	7.65	.29754	7.75
34	.21059	8.35	.21770	8.50	34	.29053	7.65	.29909	7.80
36 38	.21226	8.35	.21940	8.50	36 38	.29206	7.60	.30065	7.75
40	8.21560	8.35	8.22279	8.45	40	8.29510	7.60	8.30376	7.80
	,21726	8.30	.22448	8.45	42	.29662	7.60	.30530	7.70
42 44	.21720	8.30	.22440	8.45	44	.29813	7.55	.30685	7.75
46	. 22058	8.30	.22786	8.45	46	. 29965	7.60	.30839	7.70
48	.22224	8.30	.22954	8.40	48	.30116	7.55	.30993	7.70
50	8.22389	8.25 8.25	8.23122	8.40	50	8.30266	7.50 7.55	8.31147	7.70
52	.22554	8.20	.23290	8.35	52	.30417	7.50	.31300	7.70
54	.22718	8.20	.23457	8.35	54	.30567	7.50	.31454	7.65
56 58	.22882	8.20	.23624	8.35	56 58	.30717 .30866	7.45	.31607	7.60
60	8.23210	8.20	.23791	8.30	60	8.31016	7.50	8.31912	7.65
		8.15	8.23957	8.30	62		7.45	.32064	7.60
62 64	.23373 .23536	8.15	.24123	8.30	64	.31165	7.45	.32004	7.60
66	. 23699	8.15	.24455	8.30	66	.31462	7.40	.32368	7.60
68	.23861	8.10	. 24620	8.25	68	.31611	7.45	.32519	7.55
70	8.24023	8.10	8.24785	8.25	70	8.31759	7.40	8.32671	7.60 7.55
72	.24185	8.05	. 24949	8.25	72	.31907	7.40	.32822	7.50
74	. 24346	8.05	.25114	8.20	74	. 32054	7.35	.32972	7.55
76	.24507	8.05	.25278	8.15	76	.32201	7.35	.33123	7.50
78	.24668	8.05	.25441	8.20	78 80		7.35	.33273	7.50
80	8.24829	8.00	8.25605	8.15	82	8.32495	7.35	8.33423	7.50
82 84	.24989	8.00	.25768	8.15	82	.32642	7.30	.33573 .33722	7.45
86	.25149	7.95	.25931	8.10	86	.32788	7.30	.33871	7.45
88	. 25468	8.00	.26255	8.10	88	,33080	7.30	.34020	7.45
90	8.25627	7.95	8.26417	8.10	90	8.33226	7.30	8.34169	7.45
92	.25785	7.90 7.95	.26579	8.10	92	.33371	7.25 7.25	.34318	7.45
94	.25944	7.90	.26740	8.10	94	.33516	7.25	.34466	7.40
96	.26102	7.90	.26902	8.00	96	.33661	7.25	.34614	7.40
98	.26260	7.90	.27062	8.05	98	.33806	7.20	34762	7.35
100	8.26418		8.27223	1	100	8.33950		8.34909	

TABLE XXVI. — (Continued)

		1	2° 14		TT		1	3°	
Hun- dredths	77	Diff.	1	Diff.	Hun- dredths	*7	Diff.	177	Diff.
	Vers	.001	Exsec	.001		Vers	.001	Exsec	.001
00	8.33950	7.20	8.34909	7.40	00	8.40875	6.65	8.42002	6.85
02	.34094	7.20	.35057	7.35	02 04	.41008	6.60	.42139	6.80
04 06	.34238	7.20	.35351	7.35	06	.41140	6.65	.42391	6.80
о8	.34525	7.15	-35497	7.30	о8	.41405	6.60	.42547	6.80 6.80
10	8.34668	7.15 7.15	8.35644	7.35 7.30	10	8.41537	6.60 6.60	8.42683	6.75
12	.34811	7.15	.35790	7.30	12	.41669	6.60	.42818	6.75
14 16	.34954 .35096	7.10	.35936	7.30	14 16	.41801 .41933	6.60	.42953	6.75
18	.35238	7.10	.36227	7.25	18	.42064	6.55	.43223	6.75
20	8.35380	7.10	8.36372	7.25	20	8.42195	6.55	8.43358	6.75
22	.35522	7.10	.36517	7.25	22	.42326	6.55	-43492	6.70
24	.35664	7.10	.36662	7.25 7.25	24	.42457	6.55	.43627	6.75
26	.35805	7.05	.36807	7.20	26	.42587	6.55	.43761	6.70
28	.35946 8.36087	7.05	.36951 8.37095	7.20	28 30	.42718 8.42848	6.50	.43895 8.44028	6.65
30 32	.36227	7.00	.37239	7.20	32	.42978	6.50	.44162	6.70
34	.36368	7.05	.37383	7.20	34	.43107	6.45	.44295	6.65
36	.36508	7.00	.37526	7.15	36	-43237	6.50	.44428	6.65 6.65
38	.36648	6.95	.37669	7.15	38	.43366	6.45	.44561	6.65
40	8.36787	7.00	8.37812	7.15	40	8.43495	6.45	8.44694	6.65
42	.36927	6.95	.37955	7.15	42	.43624	6.45	.44827	6.60
44 46	.37066 .37205	6.95	.38240	7.10	44 46	.43753 .43882	6.45	.44959 .45091	6.60
48	.37344	6.95	.38382	7.10	48	.44010	6.40	.45223	6.60
50	8.37482	6.90 6.90	8.38524	7.10	50	8.44138	6.40 6.40	8.45355	6.60
′ 52	.37620	6.95	.38666	7.10	52	.44266	6.40	.45487	6.55
54	.37759	6.85	.38807	7.05	54	-44394	6.40	.45618	6.55
56 58	.37896	6.90	.38948	7.05	56 58	.44522	6.35	.45749 .45880	6.55
60	8.38171	6.85	8.39230	7.05	60	8.44776	6.35	8.46011	6.55
62	.38309	6.90	·3937I	7.05	62	.44903	6.35	.46142	6.55
64	.38446	6.85 6.80	.39511	7.00	64	.45030	6.35	.46273	6.50
66.	.38582	6.85	.39651	7.00	66	.45157	6.35 6.30	.46403	6.50
68	.38719	6.80	.39791	7.00	68	.45283	6.35	.46533	6.50
70 72	8.38855	6.80	8.39931	7.00	70 72	8.45410 .45536	6.30	8.46663 .46793	6.50
74	.39127	6.80	.40210	6.95	74	.45662	6.30	.46923	6.50
76	.39263	6.80 6.80	.40349	6.95 6.95	76	.45787	6.25	.47052	6.45 6.45
78	-39399	6.75	.40488	6.95	78	.45913	6.25	.47181	6.45
80	8.39534	6.75	8.40627	6.90	80	8.46038	6.25	8.47310	6.45
82	.39669	6.75	.40765	6.90	82	.46163	6.25	.47439	6.45
8 ₄ 86	.39804	6.70	.40903	6.95	84 86	.46288	6.25	.47568	6.40
88	.40073	6.75	.41179	6.85	88	.46538	6.25	.47825	6.45
90	8.40207	6.70	8.41317	6.90	90	8.46662	6.20	8.47953	6.40
92	.40341	6.70	.41455	6.90	92	.46787	6.20	.48081	6.40
94	.40475	6.65	.41592	6.85	94	.46911	6.20	.48209	6.40
96 98	.40608	6.70	.41729 .41866	6.85	96 98	.47035 .47158	6.15	.48337	6.35
100	8.40875	6.65	8.42002	6.80	100	8.47282	6.20	8.48591	6.35
100	6.40075		0.42002		100	0.4/202		0.40391	

			10						
Hun-			4°	1 D:0	Hun-			5°	
dredths	Vers]	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	8.47282	6.15	8.48591	6.40	00	8.53243	5.75	8.54748	5.05
02	.47405	6.15	.48719	6.35	02	•53358		.54867	5.95
04	.47528	6.15	.48846	6.30	04	.53473	5.75	.54986	5.95 5.95
06	.47651	6.15	.48972	6.35	06	-53587	5.75	.55105	5.95
08	.47774 8.47897	6.15	.49099 8.49226	6.35	08	.53702	5.70	.55224	5.90
12	.48019	6.10	.49352	6.30	12	8.53816	5.75	8.55342	5.95
14	.48142	6.15	.49478	6.30	14	.54045	5.70	-55579	5.90
16	.48264	6.10	.49604	6.30	16	.54159	5.70	.55697	5.90
18	.48386	6.10	.49730	6.30	18	.54273	5.7° 5.65	.55815	5.90
20	8.48508	6.05	8.49855	6.30	20	8.54386		8.55933	5.90
22	.48629	6.10	.49981	6.20	22	.54500	5.70	.56051	5.90
24	.48751	6.05	.50105	6.30	24	.54613	5.65	.56168	5.85
26	.48872	6.05	.50231	6.25	26	.54727	5.65	.56285	5.90
28	.48993	6.05	.50356 8.50481	6.25	28	.54840	5.65	.56403	5.85
30 32	8.49114 .49235	6.05	.50606	6.25	30 32	8.54953 .55065	5.60	8.56520	5.85
34	.49355	6.00	.50730	6.20	34	.55178	5.65	.56753	5.80
36	.49486	6.05	.50864	6.20	36	.55290	5.60	.56870	5.85
38	.49596	6.00	.50979	6.25	38	.55403	5.65	.56987	5.85
40	8.49716	6.00	8.51103	6.15	40	8.55515	5.60	8.57103	5.80
42	.49836	6.00	.51226	6.20	42	.55627	_	.57219	5.80
44	.49956	5.95	.51350	6.20	44	-55739	5.60 5.60	-57335	5.80
46	.50075	6.00	.51474	6.15	46	.55851	5.55	-57451	5.80
48	.50195	5.95	.51597	6.15	48	.55962	5.60	.57567	5.80
50 52	8.50314 .50433	5.95	8.51720	6.15	50 52	8.56074 .56185	5.55	8.57683 .57798	5.75
54	.50552	5.95	.51966	6.15	54	.56296	5.55	.57914	5.80
56	.50671	5.95	.52089	6.15	56	.56407	5.55	.58029	5.75
58	.50789	5.90	. 52211	6.10	58	.56518	5.55	.58144	5.75 5.7 5
60	8.50908	5.90	8.52333	6.15	60	8.56629	5.55 5.55	8.58259	5.75
62	.51026		.52456	6.10	62	.56740		.58374	5.75
64	.51144	5.90	. 52578	6.10	64	.56850	5.50 5.50	.58489	5.75
66	.51262	5.90	.52700	6.05	66	.56960	5.50	.58603	5.70
68 70	.51380 8.51498	5.90	.52821 8.52943	6.10	68 70	.57070 8.57181	5.55	.58717 8.58832	5.75
72	.51615	5.85	.53064	6.05	70 72	.57290	5.45	.58946	5.70
74	.51732	5.85	.53186	6.10	74	.57400	5.50	.59060	5.70
76	.51849	5.85	.53307	6.05	76	.57510	5.50	.59174	5.70
78	.51966	5.85	. 53428	6.05	78	.57619	5 · 45 5 · 45	.59288	5.70
80	8.52083	5.85	8.53548	6.05	80	8.57728	5.50	8.59401	5.70
82	.52200	5.80	. 53669	6.05	82	.57838	5.45	.59515	5.65
84 86	.52316	5.85	.53790	6.00	84	-57947	5.45	.59628	5.65
88	-52433	5.80	.53910	6.00	86	.58056	5.40	.59741	5.65
90	.52549 8.52665	5.80	.54030 8.54150	6.00	88 90	.58164 8.58273	5.45	.59854 8.59967	5.65
92	.52781	5.80	.54270	6.00	92	.58381	5.40	.60080	5.65
94	.52896	5.75	.54390	6.00	94	.58490	5.45	.60193	5.65
96	.53012	5.80	.54509	5.95 6.00	96	.58598	5.40	.60305	5.60
98	.53127	5.75 5.80	.54629	5.95	98	.58706	5.40	.60418	5.60
100	8.53243	0.00	8.54748	0.55	100	8.58814	-	8.60530	

TABLE XXVI. — (Continued)

		16	°°		Hun-		17	7°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
		.001		100.		4	.001		.001
00	8.58814	5.40	8.60530	5.60	00	8.64043	5.10	8.65984	5.30
02	.58922	5.40	.60642	5.60	02 04	.64145	5.05	.66090 .66196	5.30
04 06	.59030	5.35	.60754	5.60	06	.64347	5.05	.66301	5.25
08	.59244	5.35	.60078	5.60	08	.64448	5.05	.66407	5.30
10	8.59352	5.40	8.61089	5.55	10	8.64549	5.05	8.66513	5.30
12	-59459	5.35	.61201	5.60	12	.64650	5.05	.66618	5.25 5.25
14	. 59566	5.35	.61312	5.55 5.60	14	.64751	5.00	.66723	5.30
16	. 59673	5.35	.61424	5.55	16	.64851	5.00	.66829	5.25
18	.59779	5.35	.61535	5.55	18	.64951	5.05	.66934	5.25
20	8.59886	5.30	8.61646	5.50	20	8.65052	5.00	8.67039	5.25
22	.59992	5.35	.61756 .61867	5.55	22	.65152 .65252	5.00	.67144 .67248	5.20
24 26	.60099	5.30	.61978	5.55	24 26	.65352	5.00	.67353	5.25
28	.60311	5.30	.62088	5.50	28	.65452	5.00	.67458	5.25
30	8.60417	5.30	8.62199	5.55	30	8.65551	4.95	8.67562	5.20
32	.60523	5.30	.62309	5.50	32	.65651	5.00	.67666	5.20 5.25
34	.60628	5.25	.62419		34	.65751	4.95	.67771	5.20
36	.60734	5.30	.62529	5.50	36	.65850	4.95	.67875	5.20
38	.60839	5.30	.62639	5.45	38	.65949	4.95	.67979	5.20
40	8.60945	5.25	8.62748	5.50	40	8.66048	4.95	8.68083	5.15
42	.61050	5.25	.62858	5.50	42	.66147 .66246	4.95	.68186	5.20
44 46	.61155	5.25	.63077	5.45	44 46	.66345	4.95	.68393	5.20
48	.61364	5.20	.63786	5.45	48	.66444	4.95	.68497	5.20
50	8.61469	5.25	8.63295	5.45	50	8.66542	4.90	8.68600	5.15
52	.61573	5.20	.63404	5.45 5.45	52	.66641	4.95	.68703	5.15 5.20
54	.61678	5.25	.63513		54	.66739	4.90	.68807	5.15
56	.61782	5.20	.63622	5.45	56	.66837	4.90	.68910	5.10
58	.61886	5.20	.63730	5.45	58	.66935	4.90	.69012	5.15
60	8.61990	5.20	8.63839	5.40	60	8.67033	4.90	8.69115	5.15
62	.62094	5.20	.63947	5.45	62 64	.67131	4.90	.69218	5.15
64 66	.62301	5.15	.64164	5.40	66	.67327	4.90	.69423	5.10
68	,62405	5.20	.64272	5.40	68	.67424	4.85	.69525	5.10
70	8.62508	5.15	8.64380	5.40	70	8.67521	4.85	8.69628	5.15
72	.62611	5.15	.64487	5.35	72	.67619	4.90	.69730	5.10
74	.62714	5.15	.64595	5.40	74	.67716	4.85	.69832	5.10
76	.62817	5.15	.64703	5.35	76	.67813	4.85	.70036	5.10
78	.62920	5.15	.64810	5.35	78	.67910	4.85		5.05
80	8.63023	5.15	8.64917	5.35	80	8.68007	4.85	8.70137	5.10
82 84	.63126	5.10	.65024	5.40	82 84	.68104	4.80	.70239	5.05
86	.63330	5.10	.65238	5.30	86	.68297	4.85	.70442	5.10
88	.63433	5.15	.65345	5.35	88	.68393	4.80	.70543	5.05
90	8.63535	5.10	8.65452	5.35	90	8.68490	4.85	8.70644	5.05
92	.63637	5.10	.65559	5.35	92	.68586	4.80	.70745	5.05
94	.63739	5.05	.65665	5.30	94	.68682	4.80	.70846	5.05
96 98	.63840	5.10	.65771	5.35	96	.68778	4.80	.70947	5.05
100	.63942 8.64043	5.05		5.30	100	8.68969	4.75	8.71149	5.05
100	8.04043		8.65984		1 100	8.08909		8.71149	1

		-	8°			1			
Hun-			.8-	- D:«	Hun-			9°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	8.68969	4.80	8.71149	5.00	00	8.73625	4.50	8.76058	4.80
02	.69065	4.80	.71249	5.05	02	·73715	4.55	.76154	
04 06	.69161 .69256	4.75	.71350	5.00	04 06	.73806	4.50	.76249	4.75 4.80
08		4.75	.71450	5.05	08	.73896	4.50	.76345	4.75
10	.69351 8.69447	4.80	8.71551 8.71651	5.00	10	.73986 8.74077	4.55	.76440 8.76536	4.80
12	.69542	4.75	.71751	5.00	12	.74167	4.50	.76631	4.75
14	.69637	4.75	.71851	5.00	14	-74257	4.50	.76726	4.75
16	.69732	4.75 4.75	.71951	5.00	16	.74346	4 . 45	.7682i	4.75
18	.69827	4.70	.72051	4.95	18	.74436	4.50	.76916	4.75 4.75
20	8.69921	4.75	8.72150	5.00	20	8.74526	4.50	8.77011	4.75
22	.70016	4.70	.72250	4.95	22	.74616	4.45	.77106	4.75
24 26	.70110	4.75	.72349	5.00	24 26	.74705 .74794	4.45	.77201	4.75
28	.70203	4.70	.72548	4.95	28	.74884	4.50	.77296	4.70
30	8.70393	4.70	8.72548	4.95	30	8.74973	4.45	.77390 8.77485	4.75
32	.70487	4.70	.72746	4.95	32	.75062	4.45	.77579	4.70
34	.70581	4.70	.72845	4.95	34	.75151	4 - 45	.77674	4.75
36	.70675	4.70	.72944	4.95	36	.75240	4.45	.77768	4.70
38	.70769	4.65	.73043	4.95	38	.75329	4.40	.77862	4.70
40	8.70862	4.70	8.73142	4.90	40	8.75417	4.45	8.77956	4.70
42	.70956	4.65	.73240	4.95	42	. 75506	4.45	.78050	4.70
44 46	.71049	4.70	·73339 ·73437	4.90	44 46	.75595 .75683	4.40	.78144	4.70
48	.71236	4.65	.73535	4.90	48	.75772	4 · 45	.78331	4.65
50	8.71329	4.65	8.73634	4.95	50	8.75860	4.40	8.78425	4.70
52	.71422	4.65	.73732	4.90	52	.75948	4.40	.78519	4.70
54	.71515	4.65 4.65	. 73830	4.90	54	.76036	4.40	.78612	4.65
56	.71608	4.65	.73928	4.90	56	.76124	4.40	.78706	4.70
58	.71701	4.60	.74025	4.90	58	.76212	4.40	.78799	4.65
60	8.71793	4.65	8.74123	4.90	60	8.76300	4.35	8.78892	4.65
62	.71886	4.60	.74221	4.85	62	.76387	4.40	.78985	4.65
64 66	.71978	4.65	.74318 .74416	4.90	64 66	.76475 .76563	4.40	.79078	4.65
68	.72163	4.60	.74513	4.85	68	.76650	4.35	.79264	4.65
70	8.72255	4.60	8.74610	4.85	70	8.76737	4.35	8.79357	4.65
72	.72347	4.60 4.60	.74707	4.85	72	.76825	4.40	.79449	4.60
74	.72439	4.60	.74804	4.85	74	.76912		.79542	4.65
76	.72531	4.55	.74901	4.85	76	.76999	4.35 4.35	.79635	4.60
78	.72622	4.60	.74998	4.85	78	.77086	4.35	.79727	4.60
80	8.72714	4.60	8.75095	4.85	80	8.77173	4.35	8.79819	4.65
82 84	.72806 .72897	4.55	.75192 .75288	4.80	82 84	.77260 .77346	4.30	.79912	4.60
86	.72988	4.55	.75200	4.85	86	.77340	4.35	.80004	4.60
88	.73080	4.60	.75481	4.80	88	.77520	4.35	.80188	4.60
90	8.73171	4.55	8.75578	4.85 4.80	90	8.77606	4.30	8.80280	4.60 4.60
92	.73262	4.55 4.55	.75674	4.80	92	.77692	4.30	.80372	4.60
94	·73353	4.50	.75770	4.80	94	.77779	4.30	.80464	4.55
96 98	-73443	4.55	.75866	4.80	96 98	.77865	4.30	.80555	4.60
100	•73534	4.55	.75962	4.80	100	.77951	4.30		4.55
100	8.73625		8.76058	- 1	100	8.78037		8.80738	

Hun-		20	°		Hun-		21	0	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff. .001
-00	8.78037		8.80738		- 00	8.82230		8.85214	
02	.78123	4.30	.80830	4.60	- 02	.82311	4.05	.85302	4.40
04	.78209	4.30	.80921	4.55 4.60	04	.82393	4.10 4.10	.85390	4.40
06	.78295	4.25	.81013	4.55	06	.82475	4.05	.85477	4.35
08	.78380 8.78466	4.30	.81104 8.81195	4.55	08 10	.82556 8.82638	4.10	.85564 8.85652	4.40
10	.78551	4.25	.81286	4.55	12	.82719	4.05	.85739	4.35
14	.78637	4.30	.81377	4.55	14	.82800	4.05	.85826	4.35
16	.78722	4.25	.81468	4.55	16	.82881	4.05	.85913	4.35 4.35
18	.78807	4.25 4.25	.81559	4.55 4.50	18	.82963	4.10	.86000	4.35
20	8.78892	4.25	8.81649	4.55	20	8.83044	4.05	8.86087	4.35
22	.78977	4.25	.81740	4.55	22	.83125	4.00	.86174	4.35
24 26	.79062	4.25	.81831 .81921	4.50	24 26	.83205	4.05	.86261	4.30
28	.79147	4.25	.82011	4.50	28	.83367	4.05	.86434	4.35
30	.79232 8.79317	4.25	8.82102	4.55	30	8.83448	4.05	8.86520	4.30
32	.79402	4.25	.82192	4.50	32	.83528	4.00	.86607	4.35
34	.79486	4.20	.82282	4.50	34	.83609	4.05	.86693	4.30
36	.79571	4.25	.82372	4.50	36	.83689	4.00	.86780	4.35
38	.79655	4.20	.82462	4.50	38	.83769	4.05	.86866	4.30
40	8.79739	4.20	8.82552	4.50	40	8.83850	4.00	8.86952	4.30
42	.79823	4.25	.82642	4.50	42	.83930	4.00	.87038	4.25
44 46	.79908	4.20	.82732	4.50	44 46	.84010 .84090	4.00	.87123	4.35
48	.80076	4.20	.82911	4.45	48	.84170	4.00	.87296	4.30
50	8.80159	4.15	8.83001	4.50	50	8.84250	4.00	8.87382	4.30
52	.80243	4.20	.83090	4.45	52	.84330	4.00	.87468	4.30
54	.80327	4.20	.83180	4.45	54	.84410	3.95	.87554	4.25
56	.80411	4.15	.83269	4.45	56	.84489	4.00	.87639	4.30
58	.80494	4.20	.83358	4.45	58 60	.84569	3.95	.87725	4.25
60	8.80578	4.15	8.83447	4.45		8.84648	4.00	8.87810	4.30
62 64	.80661 .80744	4.15	.83536 .83625	4.45	62 64	.84728	3.95	.87896 .87981	4.25
66	.80827	4.15	.83714	4.45	66	.84886	3.95	.88067	4.30
68	.80911	4.15	.83803	4.45	68	.84966	4.00	.88152	4.25
70	8.80994	4.15	8.83892	4.45	70	8.85045	3.95	8.88237	4.25
72	.81077	4.13	.83981	4.40	72	.85124	3.95	.88322	4.25
74	.81159	4.15	.84069	4.45	74 76	.85203	3.95	.88407	4.25
76 78	.81242	4.15	.84158	4.40	78	.85360	3.90	.88577	4.25
80	8.81408	4.15	8.84335	4.45	80	8.85439	3.95	8.88661	4.20
82	.81490	4.10	.84423	4.40	82	.85518	3.95	.88746	4.25
84	.81573	4.15	.84511	4.40	84	.85596	3.90	.88831	4.25
86	.81655	4.10	.84599	4.40	86	85675	3.95	.88916	4.25
88	.81737	4.15	.84687	4.40	88	.85754	3.90	.89000	4.25
90 92	8.81820	4.10	8.84775	4.40	90 92	8.85832	3.90	8.89085	4.20
	.81984	4.10	.84951	4.40	92	.85988	3.90	.89254	4.25
94 96	.82066	4.10	.85039	4.40	94	.86067	3.95	.89338	4.20
98	.82148	4.10	.85127	4.40	98	.86145	3.90	.89422	4.20
100	8.82230	4.10	8.85214	4.35	100	8.86223	3.90	8.89506	4.25

		2:	2°		77		23	٥	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	Exsec	Diff.
00	8,86223		8.89506		-00	8.90034		8.93631	
02	.86301	3.90	.89590	4.20	02	.90109	3.75	.93712	4.05
04	.86379	3.90	.89674	4.20	04	.90183	3.70	.93793	4.05
06	.86456	3.90	.89758	4.20	06	.90257	3 70	.93874	4.05
08	.86534	3.90	.89842	4.20	08	.90332	3.70	.93955	4.00
10 12	8.86612 .86689	3.85	8.89926 .90010	4.20	10 12	8.90406	3.70	8.94035	4.05
1	.86767	3.90	.90093	4.15	14	.90554	3.70		4.05
14	.86844	3.85	.90093	4.20	16	.90534	3.70	.94197	4.00
18	.86922	3.90	.90261	4.20	18	.90702	3.70	.94358	4.05
20	8.86999	3.85	8.90344	4.15	20	8.90776	3.70	8.94438	4.00
22	.87076	3.85	.90427	4.15	22	.90850	3.70	.94518	4.00
24	.87153	3.85	.90511	4.20 4.15	24	.90923	3.65	.94599	4.05
26	.87231	3.85	.90594	4.15	26	.90997	3.70	.94679	4.00
28	.87308	3.85	.90677	4.20	28	.91071	3.65	-94759	4.00
30	8.87385 .87461	3.80	8.90761 .90844	4.15	30 32	.91144	3.70	8.94839	4.00
32	.87538	3.85	.90044	4.15	34	.91210	3.65	.94919	4.00
34 36	.87615	3.85	.91010	4.15	36	.91291	3.65	.94999	4.00
38	.87692	3.85	.91093	4.15	38	.91448	3.65	.95169	4.00
40	8.87768	3.80	8.91175	4.10	40	8.91511	3.65	8.95238	3.95
42	.87845	3.85	.91258	4.15	42	.91584	3.65	.95318	4.00
44	.87921	3.80	.91341	4.15	44	.91657	3.65	.95398	4.00
46	.87998	3.80	.91423	4.15	46	.91730	3.65	.95478	3.95
48	.88074	3.80	.91506	4.15	48	.91803	3.65	.95557	4.00
50 52	8.88150 .88226	3.80	8.91589	4.10	50 52	8.91876 .91949	3.65	8.95637	3.95
54	.88302	3.80	.91753	4.10	54	.92022	3.65	.95795	3.95
56	.88378	3.80	.91733	4.15	56	.92022	3.65	.95875	4.00
58	.88454	3.80	.91918	4.10	58	.92167	3.60	-95954	3.95
60	8.88530	3.80	8.92000	4.10	60	8.92240	3.65	8.96033	3.95
62	.88606	3.80	.92082	4.10	62	.92313	3.65	.96112	3.95
64	.88682	3.80	.92165	4.15	64	.92385	3.60	.96192	3.95
66	.88758	3.75	.92247	4.05	66	-92457	3.65	.96271	3.95
68	.88833	3.80	.92328	4.10	68	.92530	3.60	.96350	3.90
70 72	8.88909	3.75	8.92410	4.10	70 72	8.92602 .92674	3.60	.96507	3.95
74	.89060	3.80	.92574	4.10	74	.92746	3.60	.96586	3.95
76	.89135	3.75	.92656	4.10	76	.92740	3.60	.96665	3.95
78	.89210	3.75	.92737	4.05	78	.92891	3.65	.96744	3.95
80	8.89286	3.75	8.92819	4.05	80	8.92962	3.60	8.96822	3.95
82	.89361		.92900	4.05	82	.93034	3.60	.96901	3.90
84	.89436	3.75	.92982	4.10	84	.93106	3.60	.96979	3.95
86	.89511	3.75	.93063	4.10	86	.93178	3.60	.97058	3.90
88 90	.89586 8.89661	3.75	.93145 8.93226	4.05	88 90	.93250 8.93321	3.55	.97136 8.97215	3.95
90	.89735	3.70	.93307	4.05	92	.93393	3.60	.97293	3.90
94	.89810	3.75	.93388	4.05	94	.93465	3.60	.97371	3.90
96	.89885	3.75	.93469	4.05	96	.93536	3.55	.97450	3.95
98	.89960	3.75	.93550	4.05	98	.93607	3.55	.97528	3.90
100	8.90034	3.,0	8.93631	4.35	100	8.93679		8.97606	

**		24	°		Hun-		2	25°			
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.		
00	8.93679	3.55	8.97606	3.90	00	8.97170	3.45	9.01443	3.75		
02	.93750	3.55	.97684	3.90	02	.97239	3.40	.01518	3.80		
04	.93821	3.55	.97762	3.90	04 06	.97307	3.40	.01594	3.75		
06	.93892	3.60	.97840	3.90	08	.97375	3.40		3.75		
08 10	.93964 8.94035	3.55	.97918 8.97995	3.85	10	.97443 8.97512	3.45	.01744 9.01819	3.75		
12	.94106	3.55	.98073	3.90	12	.97580	3.40	.01895	3.80		
14	.94177	3.55	.98151	3.90	14	.97648	3.40	.01970	3.75		
16	.94247	3.50	.98229	3.90	16	.97716	3.40	.02045	3.75		
18	.94318	3·55 3·55	.98306	3.90	18	.97784	3.40	.02120	3.75 3.75		
20	8.94389	3.55	8.98384	3.85	20	8.97851	3.40	9.02195	3.75		
22	.94460	3.50	.98461	3.90	22	.97919	3.40	.02270	3.75		
24	.94530	3.55	.98539	3.85	24 26	97987	3.40	.02345	3.70		
26	.94601	3.50	.98616	3.85		.98055	3.35	.02419	3.75		
28	.94671 8.94742	3.55	.98693 8.98771	3.90	28 30	.98122 8.98190	3.40	9.02569	3.75		
30 32	.94742	3.50	.98848	3.85	32	.98257	3.35	.02644	3.75		
34	.94882	3.50	.98925	3.85	34	.98325	3.40	.02718	3.70		
36	.94953	3.55	.99002	3.85	36	.98392	3.35	.02793	3.75		
38	.95023	3.50	.99079	3.85	38	.98459	3.35	.02867	3.70		
40	8.95093	3.50	8.99156	3.85	40	8.98527	3.45	9.02942	3.75		
42	.95163	3.50	.99233	3.85	42	.98594		.03016			
44	-95233	3.50	.99310	3.85	44	.98661	3.35 3.35	.03091	3.75		
46	.95303	3.50	.99387	3.85	46	.98728	3.35	.03165	3.70		
48	.95373	3.50	.99464	3.85	48	.98795	3.35	.03239	3.75		
50 52	8.95443 .95513	3.50	8.99541	3.80	50 52	8.98862 .98929	3.35	9.03314	3.70		
	.95582	3.45	.99694	3.85	54	.98996	3.35	.03462	3.70		
54 56	.95552	3.50	.99094	3.85	56	.99963	3.35	.03536	3.70		
58	.95722	3.50	.99847	3.80	58	. 99130	3.35	.03610	3.70		
60	8.95791	3.45	8.99924	3.85	60	8.99197	3.35	9.03684	3.70		
62	.95861	3.50	9.00000	3.80	62	.99263	3.30	.03758	3.70		
64	.95930	3.45	.00076	3.80	64	.99330	3.35	.03832	3.70		
66	.96000	3.50	.00153	3.80	66	-99397	3.30	.03906	3.70		
68	.96069	3.45	.00229	3.80	68	.99463	3.35	.03980	3.70		
70	8.96138 .96207	3.45	9.00305	3.85	70 72	8.99530	3 30	9.04054	3.65		
72		3.50	1	3.80		.99596	3.35	.04127	3.70		
74 76	.96277	3.45	.00458	3.80	74 76	.99663 .99729	3.30	.04201	3.70		
78	.96415	3 - 45	.00610	3.80	78	.99795	3.30	.04348	3.65		
80	8.96484	3.45	9.00686	3.80	80	8.99861	3.30	9.04422	3.70		
82	.96553	3.45	.00762	3.80	82	.99928	3.35	.04495	3.65		
84	.96621	3.40	.00838	3.80	84	-99994	3.30	.04569	3.70		
86	.96690	3.45 3.45	.00913	3.75	86	9.00060	3.30	.04642	3.65		
88	.96759	3.45	.00989	3.80	88	.00126	3.30	.04715	3.70		
90	8.96828	3.40	9.01065	3.80	90 92	9.00192	3.30	9.04789	3.65		
92	.96896	3.45	.01141	3.75		_	3.25		3.65		
94 96	.96965	3.40	.01210	3.80	94 96	.00323	3.30	.04935	3.65		
98	.97102	3.45	.01367	3.75	98	.00309	3.30	.05082	3.70		
100	8.97170	3.40	9.01443	3.80	100	9.00521	3.30	9.05155	3.65		

I			20	5°		1 ,,		2'	7°	
ı	Hun- dredths	37	Diff.		Diff.	Hun- dredths	77	Diff.	1 72	Diff.
ı		Vers	.001	Exsec	100.		Vers	.001	Exsec	.001
ı	00	9.00521	3.25	9.05155	3.65	00	9.03740	3.15	9.08752	3.55
ı	02	.00586	3.30	.05228	3.65	02	.03803	3.15	.08823	3.55
ı	04 06	.00652	3.25	.05301	3.65	04 06	.03866	3.15	.08894	3.50
ı	08	,00783	3.30	.05446	3.60	08	.03992	3.15	.09035	3.55
ı	10	9.00848	3.25	9.05519	3.65	10	9.04055	3.15	9.09106	3.55
1	12	.00914	3.30	.05592	3.65 3.65	12	.04118	3.15	.09176	3.50 3.55
1	14	.00979	3.25	.05665	3.65	14	.04181	3.15	.09247	3.55
ı	16 18	.01044	3.25	.05738	3.60	16 18	.04244	3.10	.09318	3.50
ı	20	9.01175	3.30	9.05883	3.65	20	9.04369	3.15	9.09459	3.55
ı	22	.01240	3.25	.05955	3.60	22	.04432	3.15	.09529	3.50
ı	24	.01305	3.25	.06028	3.65	24	.04494	3.10	.09529	3.50
ı	26	.01370	3.25	.06101	3.65 3.60	26	.04557	3.15 3.10	.09670	3.55
ı	28	.01435	3.25	.06173	3.60	28	.04619		.09740	3.50
ı	30	9.01500	3.25 3.25	9.06245	3.65	30	9.04682	3.15	9.09810	3.50
ı	32	.01565	3.20	.06318	3.60	32	.04744	3.15	.09881	3.50
ı	34 36	.01629	3.25	.06390	3.60	34 36	.04807	3.10	.10021	3.50
1	38	.01759	3.25	.06535	3.65	38	.04931	3.10	.10021	3.50
1	40	9.01824	3.25	9.06607	3.60	40	9.04993	3.10	9.10161	3.50
1	42	.01888	3.20	.06679	3.60	42	.05055	3.10	.10231	3.50
ı	44	.01953	3.25	.06751	3.60	44	.05118	3.15	.10301	3.50
ı	46	.02017	3.20	.06823	3.60	46	.05180	3.10	.10371	3.50
ı	48	.02082	3.20	. 06895	3.65	48	.05242	3.10	.10441	3.50
ı	50 52	9.02146	3.20	9.06968	3.55	50 52	9.05304	3.10	9.10511	3.50
1	54	.02275	3.25	.07111	3.60	54	.05427	3.05	.10550	3.45
1	56	.02275	3.20	.07183	3.60	56	.05489	3.10	.10030	3.50
1	58	.02403	3.20	.07254	3.55 3.60	58	.05551	3.10	.10790	3.50
ı	60	9.02467	3.20	9.07326	3.60	60	9.05613	3.10	9.10860	3.50
ı	62	.02531	_	.07398	-	62	.05675	_	.10929	3.45
1	64	.02596	3.25	.07469	3.55 3.60	64	.05736	3.05	.10999	3.50 3.45
ı	66	.02660	3.15	.07541	3.60	66	.05798	3.05	.11068	3.50
1	68	9.02723	3.20	9.07684	3.55	68 70	.05859 9.05921	3.10	9.11207	3.45
1	72	.02851.	3.20	.07756	3.60	72	.05982	3.05	.11277	3.50
1	74	.02915	3.20	.07827	3.55	74	.06044	3.10	.11346	3.45
	76	.02979	3.20	.07898	3.55 3.60	76	.06105	3.05	.11415	3.45
4	78	.03043	3.15	.07970	3.55	78	.06166	3.10	.11485	3.45
1	80	9.03196	3.20	9.08041	3.55	80	9.06228	3.05	9.11554	3.45
1	82	.03170	3.15	.08112	3.60	82	.06289	3.05	.11623	3 45
	84 86	.03233	3.20	.08184	3.55	84 86	.06350	3.05	.11692 .11762	3.50
	88	.03297	3.15	.08326	3.55	88	.06472	3.05	.11831	3.45
	90	9.03424	3.20	9.08397	3.55	90	9.06533	3.05	9.11900	3.45
1	92	.03487	3.15	.08468	3.55 3.55	92	.06594	3.05	.11969	3·45 3·45
1	94	.03550	3.20	.08539	3.55	94	.06655	3.05	.12038	3.45
	96 98	.03614	3.15	.08610	3.55	96	.06716	3.05	.12107	3.45
	100	.03677	3.15		3.55	98 100	.06777	3.05		3.45
1	100	9.03740		9.08752		100	9.06838		9.12245	

**		28	•		Hun-		29	0	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.06838	3.05	9.12245	3.40	00	9.09823	2.95	9.15641	3.35
02	.06899	3.05	.12313	3.45	02	.09882	2.90	.15708	3.35
04	.06960	3.00	.12382	3.45	04	.09940	2.95	.15775	3.35
06	.07020	3.05	.12451	3.45	.06 08	.09999	2.90	.15842	3.35
08	.07081	3.00	.12520 9.12588	3.40	10	.10057	2.90	.15909 9.15976	3.35
12	07202	3.05	12657	3 45 3.45	12	.10174	2 95 2.90	.16043	3 35 3.30
14	.07263	3.00	.12726	3.40	14	.10232	2.95	.16109	3.35
16	.07323	3.00	.12794	3.45	16	.10291	2.90	.16176	3.35
18	.07383	3.05	.12863	3.40	18 20	.10349	2.90	9.16309	3.30
20	9.07444	3.00	9.12931	3.45		9.10407	2.90		3.35
22 24	.07504	3.00	.13000	3.40	22 24	.10465	2.90	.16376	3.35
26	.07625	3.05	.13137	3.45	26	.10581	2.90	.16509	3.30
28	.07685	3.00	.13205	3.40	28	.10639	2.90	. 16576	3.30
30	9.07745	3.00	9.13273	3.40	30	9.10697	2.90	9.16642	3.35
32	.07805	3.00	.13341	3.45	32	.10755	2.90	.16709	3.30
34 36	.07865	3.00	.13410	3.40	34 36	.10813	2.90	.16775	3.35
38	.07923	3.00	.13546	3.40	38	.10929	2.90	.16908	3.30
40	9.08045	3.00	9.13614	3.40	40	9.10987	2.90	9.16974	3.35
42	.08105	3.00	.13682	3.40	42	.11045	2.85	.17041	3.30
44	.08165	3.00	.13750	3.40	44	.11102	2.00	.17107	3.30
46	.08225	2.95	.13818	3.40	46	.11160	2.90	.17173	3.30
48	.08284	3.00	.13886	3.40	48 50	.11218 9.11275	2.85	9.17306	3.35
50 52	9.08344	3.00	9.13954	3.40	52	.11333	2.90	.17372	3.30
54	.08463	2.95	.14090	3.40	54	.11390	2.85	.17438	3.30
56	.08523	3.00	.14158	3.40	56	.11448	2.90	.17504	3.30
58	.08583	2.95	.14226	3.35	58	.11505	2.90	.17570	3.30
60	9.08642	2.95	9.14293	3.40	60	9.11563	2.85	9.17636	3.30
62	.08701	3.00	.14361	3.40	62 64	.11620	2.85	.17702	3.30
64 66	.08761	2.95	.14429	3.35	66	.110//	2.85	.17834	3.30
68	.08880	3.00	.14564	3.40	68	.11792	2.85	.17900	3.30
70	9.08939	2.95	9.14632	3.40	70	9.11849	2.85	9.17966	3.30
72	.08998	2.95	.14699	3.40	72	.11906	2.85	.18031	3.30
74	.09057	2.95	.14767	3.35	74 76	.11963	2.85	.18097	3.30
76 78	.09116	3.00	.14834	3.40	78	.12020	2.85	.18229	3.30
80	9.09235	2.95	9.14969	3.35	80	9.12134	2.85	9.18294	3.25
82	.09294	2.95	.15036	3.35	82	.12191	2.85	.18360	3.30
84	.09353	2.95	.15104	3.40	84	.12248	2.85	.18426	3.30
86	.09412	2.90	.15171	3.35	86	.12305	2.85	.18491	3.30
88	.09470	2.95	.15238	3.35	88	.12362	2.85	9.18622	3.25
90 92	9.09529	2.95	9.15305	3.40	90 92	9.12419	2.85	.18688	3.30
94	.09647	2.95	.15440	3.35	94	.12532	2.80	.18753	3.25
96	.09706	2.95	.15507	3·35 3·35	96	.12589	2.85	.18818	3.25
98	.09764	2.95	.15574	3.35	98	.12646	2.80	.18884	3.25
100	9.09823		9.15641		100	9.12702		9.18949	1

		30)°		77		31	L°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	Exsec	Diff.
00	9.12702	2.85	9.18949	3.25	00	9.15483	2.70	9.22176	3.20
02	.12759	2.80	.19014	3.30	02	.15537	2.75	.22240	3.20
04 06	.12815	2.85	.19080	3.25	04 06	.15592	2.75	. 22304	3.15
		2.80	.19145	3.25	08	.15647	2.70	.22367	3.20
08	.12928	2.85	.19210 9.19275	3.25	10	.15701 9.15756	2.75	9.22431	3.20
12	.13041	2.80	.19341	3.30	12	.15810	2.70	.22558	3.15
14	.13097	2.80	.19406	3.25	14	.15865	2.75	.22622	3.20
16	.13154	2.80	.19471	3.25	16	.15919	2.70	.22685	3.15
18	.13210	2.80	.19536	3.25	18	.15973	2.75	.22749	3.15
20	9.13266	2.80	9.19601	3.25	20	9.16028	2.70	9.22812	3.20
22	.13322	2.80	.19666	3.25	22	.16082	2.70	.22876	3.15
24 26	.13378	2.80	.19731	3.25	24 26	.16136	2.70	.22939	3.20
28	.13434	2.80	.19796	3.25	28	.16190	2.70	.23003	3.15
30	.13490 9.13546	2.80	9.19926	3.25	30	.16244 9.16299	2.75	. 23066 9. 23129	3.15
32	.13602	2.80	.19990	3.20	32	.16353	2.70	.23193	3.20
34	.13658	2.80	. 20055	3.25	34	.16407	2.70	.23256	3.15
36	.13714	2.80	.20120	3.25	36	.16461	2.70	.23319	3.15
38	.13770	2.80	.20185	3.20	38	.16515	2.70	. 23383	3.15
40	9.13826	2.80	9.20249	3.25	40	9.16569	2.70	9.23446	3.15
42	.13882	2.75	.20314	3.25	42	.16623	2.65	.23509	3.15
44	.13937	2.80	.20379	3.20	44	.16676	2.70	.23572	3.15
46	.13993	2.80	.20443	3.25	46	.16730	2.70	.23635	3.15
48	.14049 9.14104	2.75	.20508 9.20572	3.20	48	.16784 9.16838	2.70	. 23698	3.15
50 52	.14160	2.80	.20637	3.25	50 52	.16892	2.70	9.23761	3.15
54	.14216	2.80	.20701	3.20	54	.16945	2.65	.23887	3.15
56	.14271	2.75	.20766	3.25	56	.16999	2.70	.23950	3 15
58	.14327	2.80	. 20830	3.20	58	.17053	2.70	.24013	3.15
60	9.14382	2.75	9.20895	3.20	60	9.17106	2.70	9.24076	3.15
62	.14437	2.80	.20959	3.20	62	.17160	2.65	.24139	3.15
64	.14493	2.75	.21023	3.25	64	.17213	2.70	.24202	3.15
66	.14548	2.75	.21088	3.20	66	.17267	2.65	.24265	3.15
68	.14603	2.80	.21152	3.20	68	.17320	2.70	.24328	3.10
70 72	9.14659	2.75	9.21216	3.20	70 72	9.17374	2.65	9.24390	3.15
74	.14714	2.75	.21345	3.25	74	.17427	2.65	.24516	3.15
76	.14709	2.75	.21343	3.20	74	.17534	2.70	.24578	3.10
78	.14879	2.75 2.75	.21473	3.20	78	.17587	2.65	.24641	3.15
80	9.14934	2.75	9.21537	3.20	80	9.17640	2.65	9.24704	3.15
82	.14989	2.75	.21601	3.20	82	.17693	2.70	.24766	3.15
84	.15044	2.75	.21665	3.20	84	.17747	2.65	.24829	3.15
86	.15099	2.75	.21729	3.20	86	.17800	2.65	24891	3.15
88	.15154	2.75	.21793	3.20	88	.17853	2.65	.24954	3.15
90 92	9.15264	2.75	9.21857	3.20	90 92	9.17906	2.65	9.25017	3.10
		2.75		3.20		.17959	2.65	.25079	3.10
94 96	.15319	2.70	.21985	3.20	94 96	.18065	2.65	.25141	3.15
98	.15428	2.75	.22112	3.15	98	.18118	2.65	.25266	3.10
100	9.15483	2.75	9.22176	3.20	100	9.18171	2.05	9.25329	3.15
	3 34-0 1							J 30-7 (

		3	2°		1		3:	3°	
Hun- dredths		Diff.		Diff.	Hun- dredths		Diff.		Diff.
dredths	Vers	.001	Exsec	.001	diedins	Vers	.001	Exsec	.001
00	9.18171	2.60	9.25329	3.10	00	9.20771	2.60	9.28412	3.05
02	.18223	2.65	.25391	3.10	02	.20823	2 55	.28473	3.05
04 06	.18276	2.65	.25453	3.10	04 06	. 20874	2.55	.28534	3.05
08	.18382	2.65	.25515	3.15	08	.20925	2.55	.28656	3.05
10	9.18435	2.65	.25578 9.25640	3.10	10	.20976 9.21027	2.55	9.28717	3.05
12	.18487	2.60	.25702	3.10	12	.21078	2.55	.28778	3.05
14	. 18540	2.60	. 25764	3.10	14	.21129	2.55	. 28839	3.05
16	. 18592	2.65	. 25826	3.10	16	.21180	2.55	. 28900	3.05
18	.18645	2.65	. 25889	3.10	18	.21231	2.55	. 28961	3.00
20	9.18698	2.60	9.25951	3.10	20	9.21282	2.50	9.29021	3.05
22	.18750	2.65	.26013	3.10	22	.21332	2.55	.29082	3.05
24 26	.18803	2.60	.26075	3.10	24 26	.21383	2.55	.29143	3.00
28	.18907	2.60	.26199	3.10	28	.21485	2.55	.29264	3.05
30	9.18960	2.65	9.26261	3.10	30	9.21535	2.50	9.29325	3.05
32	.19012	2.60	. 26323	3.10	32	.21586	2.55 2.55	.29385	3.00
34	.19064	2.65	.26384	3.10	34	.21637	2.50	.29446	3.05
36	.19117	2.60	. 26446	3.10	36	.21687	2.55	.29507	3.00
38	.19169	2.60	. 26508	3.10	38	.21738	2.50	. 29567	3.05
40	9.19221	2.60	9.26570	3.10	40	9.21788	2.55	9.29628	3.00
42	.19273	2.60	.26632	3.10	42	.21839	2.50	.29688	3.05
44 46	.19325	2.60	. 26694 . 26755	3.05	44 46	.21889	2.55	.29749	3.00
48		2.65	.26817	3.10	48	.21940	2.50	.29870	3.05
50	.19430 9.19482	2.60	9.26879	3.10	50	9.22041	2.55	9.29930	3.00
52	.19534	2.60	.26940	3.05	52	.22091	2.50	.29990	3.00
54	.19586	2.55	.27002	3.10	54	.22141	2.55	.30051	3.00
56	.19637	2.55	.27064	3.10	56	.22192	2.50	.30111	3.00
58	.19689	2.60	. 27125	3.10	58	.22242	2.50	.30171	3.05
60	9.19741	2.60	9.27187	3.05	60	9.22292	2.50	9.30232	3.00
62	.19793	2.60	.27248	3.10	62	.22342	2.50	.30292	3.00
64 66	.19845	2.60	.27310 .27371	3.05	64 66	.22392	2.50	.30352	3.00
68	.19097	2.55	.27433	3.10	68	.22493	2.55	.30473	3.05
70	9.20000	2.60	9.27494	3.05	70	9.22543	2.50	9.30533	3.00
72	.20052	2 60 2.55	.27555	3.05	72	.22593	2.50	.30593	3.00
74	. 20103	2.55	.27617	3.05	74	.22643	2.50	.30653	3.00
76	.20155	2.55	. 27678	3.05	76	. 22693	2.50	.30713	3.00
78	.20206	2.60	. 27739	3.10	78	.22743	2.50	.30773	3.00
80	9.20258	2.55	9.27801	3.05	80	9.22793	2.50	9.30833	3.00
82	.20309	2.60	.27862	3.05	82	.22843	2.45	.30893	3.00
84 86	.20361	2.55	.27923	3.05	84 86	.22892	2.50	.30953	3.00
88	.20464	2.60	.28046	3.10	88	,22992	2.50	.31073	3.00
90	9.20515	2.55	9.28107	3.05	90	9.23042	2.50	9.31133	3.00
92	.20566	2.55	.28168	3.05	92	.23091	2.45	.31193	3.00
94	.20618	2.55	.28229	3.05	94	.23141	2.50	.31253	3.00
96	.20669	2.55	.28290	3.05	96	.23191	2.45	.31313	3.00
98	.20720	2.55	.28351	3.05	98	.23240	2.50	.31373	3.00
100	9.20771		9.28412		100	9 - 23290		9.31433	

		34	10				31	50	
Hun- dredths	**	Diff.		Diff.	Hun- dredths		Diff.		Diff.
Lancarino	Vers	.001	Exsec	.001	dictions	Vers	.001	Exsec	.001
00	9.23290	2.50	9.31433	2.95	00	9.25731	2.40	9.34395	2.95
02	.23340	2.45	.31492	3.00	02	.25779	2.40	-34454	2.90
04 06	.23389	2.50	.31552	3.00	04 06	.25827	2.40	.34512	2.95
08	.23488	2.45	.31672	3.00	08	.25923	2.40	.34630	2.95
10	9.23538	2.50	9.31731	2.95	10	9.25971	2.40	9.34688	2.90
12	.23587	2.45 2.45	.31791	3.00	12	. 26019	2.40	•34747	2.95
14	.23636	2.45	.31851	2.95	14	. 26067	2.40	.34805	2.90
16 18	.23686	2.45	.31910	3.00	16	.26115	2.40	.34864	2.90
20	.23735	2.45	.31970	3.00	18	.26163	2.40	.34922	2.95
	9.23784	2.50	9.32030	2.95	20	9.26211	2.35	9.34981	2.90
22 24	. 23834	2.45	.32089	3.00	22 24	.26258	2.40	.35039	2.95
26	.23932	2.45	.32149	2.95	26	.26354	2.40	.35156	2.90
28	.23981	2.45	.32268	3.00	28	,26402	2.40	.35215	2.95
30	9.24030	2.45	9.32327	2.95	30	9.26449	2.35	9.35273	2.90
32	. 24079	2.45 2.50	. 32387	3.00 2.95	32	.26497	2.40	·35331	2.90
34	.24129	2.45	.32446	3.00	34	.26545	2.35	.35390	2.90
36 38	.24178	2.45	.32506	2.95	36	.26592	2.40	.35448	2.90
40	9.24276	2.45	.32565	2.95	38 40	.26640	2.35	.35506	2.95
		2.45	9.32624	3.00	1	9.26687	2.40	9.35565	2.90
42 44	.24325	2.45	.32684	2.95	42 44	. 26735 . 26782	2.35	.35623	2.90
46	.24422	2.40	.32802	2.95	46	.26830	2.40	.35739	2.90
48	.24471	2.45	.32861	. 2.95	48	.26877	2.35	.35798	2.95
50	9.24520	2.45	9.32921	3.00 2.95	50	9.26924	2.35	9.35856	2.90
52	.24569	2.45	.32980	2.95	52	.26972	2.40	.35914	2.90
54	.24618	2.40	. 33039	2.95	54	. 27019	2.35	-35972	2.90
56 58	.24666	2.45	.33098 .331 5 8	3.00	56 58	.27066	2.40	.36030	2.90
60	9.24764	2.45	9.33217	2.95	60	9.27161	2.35	9.36146	2.90
62	.24813	2.45	.33276	2.95	62	.27208	2.35	.36204	2.90
64	.24861	2.40	-33335	2.95	64	.27255	2.35	.36262	2.90
66	.24910	2.45	.33394	2.95	66	.27302	2.35	.36320	2.90
68	24958	2.40	.33453	2.95	68	.27349	2.35	.36378	2.90
70	9.25007	2.45	9.33512	2.95 2.95	70	9.27396	2.35	9.36436	2.90
72	.25055	2.45	-3357I	2.95	72	.27444	2.35	.36494	2.90
74 76	.25104	2.40	.33630	2.95	74 76	.27491	2.35	.36552	2.90
78	.25201	2.45	.33069	2.95	78	.27538	2.35	.36668	2.90
80	9.25249	2.40	9.33807	2.95	80	9.27632	2.35	9.36726	2.90
82	.25297	2.40	.33866	2.95	82	.27678	2.30	.36784	2.90
84	.25346	2.45	.33925	2.95	84	.27725	2.35	.36842	2.90
86	·25394	2.40	.33984	2.95	86	.27772	2.35	.36900	2.85
88	.25442	2.45	. 34042	2.95	88	.27819	2.35	.36957	2.90
90 92	9.25491	2.40	9.34101	2.95	90 92	9.27866	2.35	9.37015	2.90
94	.25587	2.40	.34100	2.95	92	.27913	2.30	.37131	2.90
94	.25635	2.40	.34219	2.90	94	.27959	2.35	.37188	2.85
98	. 25683	2.40	.34336	2.95	98	.28053	2.35	.37246	2.90
100	9.25731	2.40	9.34395	2.95	100	9.28099	2.30	9.37304	2.90

Hun-		36	S°		Hun-		3	7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff. .∞ı
00	9.28099	2.35	9.37304	2.85	00	9.30398	2.30	9.40163	2.85
02	.28146	2.35	.37361	2.90	02	.30444	2.30	. 40220	2.85
04	.28193	2.30	.37419	2.90	04	.30489	2.25	. 40277	2.85
06	.28239	2.35	-37477	2.85	06	-30534	2.25	.40334	2.80
08	. 28286	2.30	.37534 9.37592	2.90	08 10	.30579 9.30624	2.25	.40390 9.40447	2.85
12	.28379	2.35	.37649	2.85	12	.30670	2.30	.40503	2.80
14	.28425	2.30	.37707	2.90	14	.30715	2.25	.40560	2.85
16	.28472	2.35	.37764	2.85	16	.30760	2.25	.40617	2.85
18	.28518	2.30	. 37822	2.90	18	.30805	2.25	. 40673	2.80
20	9.28565	2.30	9.37879	2.90	20	9.30850	2.25	9.40730	2.80
22	. 28611	2.30	-37937	2.85	22	. 30895	_	.40786	
24	. 28657	2.35	-37994	2.85	24	. 30940	2.25	.40843	2.85
26	.28704	2.30	.38052	2.85	26	. 30985	2.25	.40899	2.85
28	.28750	2.30	.38109	2.90	28	.31030	2.25	. 40956	2.80
30 32	9.28796	2.30	9.38167	2.85	30 32	9.31075	2.25	9.41012	2.85
_	.28889	2.35	.38281	2.85	_	.31120	2.25	.41125	2.80
34 36	.28935	2.30	.38339	2.90	34 36	.31105	2.25	.41125	2.85
38	.28981	2.30	.38396	2.85	38	.31254	2.20	.41238	2.80
40	9.29027	2.30	9.38453	2.85	40	9.31299	2.25	9.41294	2.80
42	.29073	2.30	.38511	2.90	42	.31344	2.25	.41351	2.85
44	.29119	2.30	. 38568	2.85	44	.31389	2.25	.41407	2.80
46	.29165	2.30	.38625	2.85	46	.31433	2.20	.41464	2.80
48	.29211	2.30	. 38682	2.85	48	.31478	2.25	.41520	2.80
50	9.29257	2.30	9.38739	2.90	50	9.31523	2.20	9.41576	2.80
52	.29303	2.30	.38797	2.85	52	.31567	2.25	.41632	2.85
54	.29349	2.30	.38854	2.85	54	.31612	2.25	.41689	2.80
56 58	.29395	2:30	.38968	2.85	56 58	.31057	2.20	.41745	2.80
60	9.29487	2.30	9.39025	2.85	60	9.31746	2.25	9.41857	2.80
62	29533	2.30	.39082	2.85	62	.31790	2.20	.41914	2.85
64	.29578	2.25	.39139	2.85	64	.31835	2.25	.41970	2.80
66	.29624	2.30	.39196	2.85	66	.31879	2.20	. 42026	2.80
68	.29670	2.30	. 39253	2.85	68	.31924	2.25	. 42082	2.80
70	9.29716	2.30	9.39310	2.85 2.85	70	9.31968	2.20	9.42138	2.80
72	.29761	2.25	.39367	2.85	72	.32013	2.25	.42194	2.80
74	.29807	2.30	.39424	2.85	74	.32057	2.20	.42250	2.85
76 78	.29853	2.25	.39481	2.85	76 78	.32101	2.25	.42307	2.80
80		2.30		2.85	80	9.32190	2.20	9.42419	2.80
82	9.29944	2.25	9.39595	2.85	82		2.20		2.80
84	.29989	2.30	.39652	2.85	84	.32234	2.20	. 42475 . 42531	2.80
86	.30080	2.25	.39766	2.85	86	.32323	2.25	.42587	2.80
88	.30126	2.30	.39823	2.85	88	.32367	2.20	. 42643	2.80
90	9.30171	2.25	9.39880	2.85	90	9.32411	2.20	9.42699	2.80
92	.30217	2.30	.39936	2.80	92	.32455	2.20	.42755	2.75
94	.30262	2.30	-39993	2.85	94	. 32499	2.20	.42810	2.80
96	. 30308	2.25	.40050	2.85	96	.32543	2.20	.42866	2.80
98	.30353	2.25	.40107	2.80	98	.32587	2.20	.42922	2.80
100	9.30398		9.40163		100	9.32631		9.42978	

Hun-		38	3°		Hun-		39)°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.32631	2.20	9.42978	2.80	00	9.34802	2.15	9.45752	2.75
02	.32675	2.20	. 43034	2.80	02	.34845	2.15	.45807	2.75
04 06	.32719 .32763	2.20	.43090	2.80	04 06	.34888	2.13	.45862	2.75
08	.32703	2.20	.43146	2.80	08	.34930	2.15	.45917	2.75
10	9.32851	2.20	. 43202 9 · 43257	2.75	10	.34973 9.35016	2.15	. 45972 9. 46027	2.75
12	.32895	2.20	.43313	2.80	12	.35058	2.10	.46082	2.75
14	.32939	2.20	.43369	2.80	14	.35101	2.15	.46137	2.75
16 18	.32983	2.20	.43425	2.75	16 18	.35144	2.13	.46192	2.75
20	9.33027	2.15	.43480	2.80	20	.35186	2.15	9.46302	2.75
22	.33114	2.20	9.43536	2.80	22	9.35229	2.15	.46357	2.75
24	.33114	2.20	.43592	2.75	24	.35272 .35314	2.10	.46412	2.75
26	.33202	2.20	.43703	2.80	26	-35357	2.15 2.10	.46467	2.75
28	.33245	2.15	-43759		28	-35399		.46522	2.75
30	9.33289	2.20	9.43814	2.75	30	9.35442	2.15	9.46576	2.75
32	.33333	2.15	.43870	2.80	32	.35484	2.10	.46631	2.75
34 36	.33376	2.20	.43926	2.75	34 36	.35526	2.15	.46686	2.75
38	.33463	2.15	.44037	2.80	38	.35611	2.10	.46796	2.75
40	9.33507	2.20	9.44092	2.75	40	9.35654	2.15	9.46851	2.75
42	-33550	2.15	.44148	2.80	42	.35696	2.10	.46905	2.70
44	-33594	2.20 2.15	.44203	2.75	44	.35738	2.10	.46960	2.75 2.75
46	.33637	2.20	.44259	2.75	46	.35780	2.15	.47015	2.75
48	.33681	2.15	.44314	2.80	48	.35823	2.10	.47070	2.70
50 52	9.33724 .33768	2.20	9.44370	2.75	50 52	9.35865	2.10	9.47124	2.75
54	.33811	2.15	.44481	2.80	54	.35949	2.10	.47234	2.75
56	.33854	2.15	. 44536	2.75	56	.35991	2.10	.47288	2.70
58	.33898	2.15	.44592	2.80	58	. 36034	2.15	-47343	2.75 2.75
60	9.33941	2.15	9.44647	2.75	60	9.36076	2.10	9.47398	2.70
62	.33984	2.20	.44702	2.80	62	.36118	2.10	.47452	2.75
64 66	.34028 .34071	2.15	.44758	2.75	64 66	.36160 .36202	2.10	.47507	2.75
68	.34114	2.15	.44868	2.75	68	.36244	2.10	.47616	2.70
70	9.34157	2.15	9.44924	2.80	70	9.36286	2.10	9.47671	2.75
72	.34200	2.15	-44979	2.75 2.75	72	.36328	2.IO 2.IO	.47725	2.70 2.75
74	.34244	2.15	.45034	2.80	74	.36370	2.10	.47780	2.70
76 78	.34287	2.15	.45090	2.75	76 78	.36412	2.10	.47834	2.75
80	.34330	2.15	.45145	2.75	78 80	.36454	2.10		2.75
82	9.34373	2.15	9.45200	2.75	82	9.36496 .36538	2.10	9.47944	2.70
84	.34410	2.15	.45255	2.80	84	.30538	2.05	.48053	2.75
86	. 34502	2.15	.45366	2.75	86	.36621	2.10	.48107	2.70
88	-34545	2.15	.45421	2.75	88	.36663	2.10	.48161	2.75
90	9.34588	2.15	9.45476	2.75 2.75	90	9.36705	2.10	9.48216	2.75
92	.34631	2.15	.45481	2.75	92	.36747	2.05	.48270	2.75
94 96	.34674	2.10	.45586	2.80	94 96	.36788	2.10	.48325	2.70
98	.34710	2.15	.45697	2.75	98	.36872	2.10	.48433	2.70
100	9.34802	2.15	9.45752	2.75	100	9.36913	2.05	9.48488	2.75
	2.04032		2.43132		, 200	3.303.3		3.42430	

			40°				4	1°	
Hun- dredths		Diff.	-	Diff.	Hun- dredths		Diff.		Diff.
dicaths	Vers	.001	Exsec	.001		Vers	.001	Exsec	.001
00	9.36913	2.10	9.48488	2.70	00	9.38968	2.05	9.51190	2.65
02	. 36955	2.10	.48542	2.75	02	. 39009	2.00	.51243	2.70
04 06	.36997	2.05	.48597	2.70	04 06	.39049	2.05	.51297 .51351	2.70
08	.37080	2.10	. 48705	2.70	08	.39130	2.00	.51405	2.70
. 10	9.37121	2.05	9.48760	2.75	10	9.39171	2.05	9.51459	2.70
12	.37163	2.10	.48814	2.70	12	.39211	2.00	.51512	2.65
14	.37204	2.10	.48868	2.70	14	. 39251	2.05	.51566	2.65
16 18	.37246	2.05	.48922	2.75	16 18	.39292	2.00	.51619	2.70
20	9.37329	2.10	.49031	2.70	20	9.39372	2.00	9.51727	2.70
22	-37370	2.05	.49085	2.70	22	.39413	2.05	.51780	2.65
24	.37412	2.10	.49149	2.70	24	.39453	2.00	.51834	2.70
26	-37453	2.05	.49194	2.75	26	.39493	2.00	.51887	2.65
28	-37494	2.05	.49248	2.70	28	-39534	2.05	.51941	2.70
30	9.37536	2.10	9.49302	2.70	30	9.39574	2.00	9.51995	2.65
32	-37577	2.05	.49356	2.70	32	.39614	2.00	.52048	2.70
34 36	.37618 .37659	2.05	.49410	2.75	34 36	.39654	2.00	.52102	2.65
38	.37701	2.10	.49519	2.70	38	39735	2.05	.52209	2.70
40	9.37742	2.05	9.49573	2.70	40	9.39775	2,00	9.52262	2.65
42	.37783	2.05	.49627	2.70	42	.39815	2.00	.52316	2.70
44	.37824	2.05	.49681	2.70	44	. 39855	2.00	.52369	2.05
46	.37865	2.05	-49735	2.70	46	.39895	2.00	.52423	2.65
48	.37906	2.10	. 49789	2.70	48	-39935	2.00	.52476	2.65
50 52	9.37948	2.05	9.49843	2.70	50 52	9.39975	2.00	9.52529	2.70
54	.38030	2.05	.49951	2.70	54	.40055	2.00	.52636	2.65
56	.38071	2.05	.50005	2.70	56	.40095	2.00	.52690	2.70
58	.38112	2.05	.50059	2.70	58	.40135	2.00	.52743	2.65
60	9.38153	2.05	9.50113	2.70	60	9.40175	2.00	9.52796	2.70
62	.38194	2.05	.50167	2.70	62	.40215	2.00	.52850	2.65
64 66	.38235 .38276	2.05	.50221	2.70	64 66	.40255	1.95	.52903	2.65
68	.38317	2.05	.50329	2.70	68	.40334	2.00	.53010	2.70
70	9.38357	2.00	9.50383	2.70	70	9.40374	2.00	9.53063	2.65
72	.38398	2.05	.50437	2.70	72	.40414	2.00	.53116	2.65
74	. 38439	2.05	.50491	2.65	74	.40454	1.95	.53170	2.65
76	. 38480	2.05	.50544	2.70	76 -0	.40493	2.00	.53223	2.65
78 80	.38521	2.05	.50598	2.70	78 80	.40533	2.00	.53276	2.70
80	9.38562	2.00	9.50652	2.70	80	9.40573	2.00	9.53330	2.65
82 84	.38643	2.05	.50706	2.70	84	.40652	1.95	.53383	2.65
86	.38684	2.05	.50814	2.70	86	.40692	2.00	.53489	2.65
88	.38724	2.00	. 50867	2.65	88	.40731	1.95	.53542	-
90	9.38765	2.05	9.50921	2.70	90	9.40771	2.00	9.53596	2.70
92	.38806	2.00	.50975	2.70	92	.40811	1.95	.53649	2.65
94 96	. 38846 . 38887	2.05	.51029	2.70	94 96	.40850	2.00	.53702	2.65
98 98	.38928	2.05	.51083	2.65	98	.40890	1.95	-53755 -53808	2.65
100	9.38968	2.00	9.51190	2.70	100	9.40969	2.00	9.53861	2.65
	. 5.55900		9.31193			9.40909		9.33001	

77 1		42	0		Hun-		43	o	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.40969	1.95	9.53861	2.70	00	9.42918	1.95	9.56505	2.65
02	.41008	2.00	.53915	2.65	02	. 42957	1.90	. 56558	2.65
04	.41048	1.95	. 53968	2.65	04 06	. 42995	1.90	.56611	2.60
o6 o8	.41087	2.00	.54021	2.65	08	. 43033	1.95	.56716	2.65
10	.41127 9.41166	1.95	.54074 9.54127	2.65	10	.43072	1.90	9.56768	2.60
12	.41205	1.95	.54180	2.65	12	.43149	1.95	.56821	2.65
14	.41245	1.95	.54232	2.60	14	.43187	1.90	. 56873	2.65
16	.41284	1.95	. 54286	2.70	16	.43225	1.90	. 56926	2.65
18	.41323	2.00	-54339	2.65	18	.43264	1.90	. 56979	2.60
20	9.41363	1.95	9.54392	2.65	20	9.43302	1.90	9.57031	2.65
22	.41402	1.95	-54445	2.65	22	.43340	1.90	.57084	2.60
24 26	.41441	1.95	.54498 .54551	2.65	24 26	.43378	1.95	.57189	2.65
28	.41520	2.00	.54604	2.65	28	.43455	1.90	.57241	2.60
30	9.41559	1.95	9.54657	2.65	30	9.43493	1.90	9.57294	2.65
32	.41598	1.95	.54710	2.65	32	·4353I	1.90	.57346	2.60
34	.41637	1.95	. 54763	2.65	34	. 43569	1.95	.57399	2.60
36	.41676	1.95	.54816	2.65	36	. 43608	1.95	.57451	2.60
38	.41715	2.00	.54869	2.65	38	.43646	1.90	.57503	2.65
40	9.41755	1.95	9.54922	2.65	40	9.43684	1.90	9.57556	2.60
42 44	.41794	1.95	. 54975 . 55028	2.65	42	.43722	1.90	.57608	2.65
44	.41872	1.95	.55020	2.65	44 46	.43700	1.90	.57713	2.60
48	.41911	1.95	.55134	2.65	48	. 43836	1.90	.57766	2.65
50	9.41950	1.95	9.55187	2.65	50	9.43874	1.90	9.57818	2.60
52	.41989	1.95	. 55240	2.65	52	. 43912	1.90	.57870	2.65
54	. 42028	1.95	.55292	2.65	54	. 43950	1.90	.57923	2.60
56	. 42067	1.95	-55345	2.65	56	.43988	1.90	.57975	2.60
58 60	.42106	1.90	.55398	2.65	58 60	.44026	1.90	9.58080	2.65
62	9.42144	1.95	9.55451	2.70	1	9.44064	1.90		2.60
64	.42183	1.95	.55505	2.60	62 64	.44102	1.90	.58132	2.60
66	.42261	1.95	.55609	2.60	66	.44177	1.85	.58237	2.65
68	.42300	1.95	. 55662	2.65	68	.44215	1.90	. 58289	2.60
70	9.42339	1.90	9.55715	2.65	70	9.44253	1.90	9.58341	2.65
72	.42377	1.95	.55768	2.60	72	.44291	1.90	.58394	2.60
74 76	.42416	1.95	.55820	2.65	74 76	.44329	1.85	.58446	2.60
78	.42455	1.95	.55926	2.65	78	.44404	1.90	.58550	2.60
80	9.42532	1.90	9.55979	2.65	80	9.44442	1.90	9.58603	2.60
82	.42571	1.95	.56c31	2.60	82	.44480	1.90	.58655	2.60
84	.42610	1.95	.56084	2.65	84	.44517	1.85	.58707	2.60
86	.42648	1.95	.56137	2.65	86	-44555	1.90	.58759	2.65
88	. 42687	1.90	.56189	2.65	88	.44593	1.85	.58812	2.60
90	9.42725	1.90	9.56242	2.65	90	9.44630	1.90	9.58864	2.60
92	.42764	1.95	.56347	2.60	92		1.85	.58968	2.60
94 96	.42841	1.90	.56400	2.65	94 96	.44705	1.90	.59020	2.60
98	.42880	1.95	. 56453	2.65	98	.44781	1.90	.59073	2.65
100	9.42918	1	9.56505	2.00	100	9.44818	1.05	9.59125	100

Hun-		44	0		Hun-		45	٥	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.44818		9.59125	2.60	00	9.46671	- 0=	9.61722	2.60
02	.44856	1.90	.59177		02	.46708	1.85	.61774	
04	. 44893	1.85	.59229	2.60	04	. 46744	1.80	.61826	2.60
06	.4493I	1.85	.59281	2.60	06	.46781	1.80	.61878	2.55
08	.44968	1.85	-59333	2.60	08	. 46817	1.85	.61929	2.60
10	9.45005	1.90	9.59385	2.60	10	9.46854	1.80	9.61981	2.60
12	.45043	1.85	.59437	2.65	12	.46890	1.85	.62033	2.60
14	.45080	1.90	.59490	2.60	14 16	.46927	1.80	.62085	2.55
16 18	.45118	1.85	.59542 .59594	2.60	18	.46963	1.85	.62188	2.60
20		1.85	9.59646	2.60	20	9.47036	1.80	9.62240	2.60
	9.45192	1.90		2.60	22		1.80	.62291	2.55
22	.45230	1.85	.59698	2.60	22	.47072 .47109	1.85	.62343	2.60
24 26	.45267 .45304	1.85	.59802	2.60	26	.47109	1.80	.62395	2.60
28		1.90	.59854	2.60	28	.47182	1.85	.62446	2.55
30	.45342 9.45379	1.85	9.59906	2.60	30	9.47218	1.80	9.62498	2.60
32	.45416	1.85	.59958	2.60	32	.47254	1.80	.62550	2.60
34	.45453	1.85	.60010	2.60	34	.47291	1.85	.62601	2.55
36	.45490	1.85	.60062	2.60	36	.47327	1.80	.62653	2.60
38	.45528	1.90	.60114	2.60	38	.47363	1.80	.62705	2.55
40	9.45565	1	9.60166	2.60	40	9.47399	1.85	9.62756	2.60
42	.45602	1.85	.60218		42	.47436		.62808	
44	.45639	1.85	.60270	2.60	44	.47472	1.80	. 62859	2.55 2.60
46	.45676	1.85	.60322	2.60	46	.47508	1.80	.62911	2.60
48	.45713	1.85	.60374	2.60	48	-47544	1.80	.62963	2.55
50	9.45750	1.85	9.60426	2.60	50	9.47580	1.80	9.63014	2.60
52	.45787	1.85	.60478	2.60	52	.47616	1.85	.63066	2.55
54	.45824	1.85	.60530	2.60	54	.47653	1.80	.63117	2.60
56	.45861	1.85	.60582	2.60	56 58	.47689	1.80	.63169	2.55
58	.45898	1.85	9.60686	2.60	60	9.47761	1.80	9.63272	2.60
60	9.45935	1.85		2.60			1.80		2.55
62	.45972	1.85	.60738	2.60	62 64	.47797	1.80	.63323	2.60
64 66	.46009	1.85	.60790	2.55	66	.47869	1.80	.63427	2.60
68	.46083	1.85	.60893	2.60	68	.47905	1.80	.63478	2.55
70	9.46120	1.85	9.60945	2.60	70	9.47941	1.80	9.63530	2.60
72	.46157	1.85	.60997	2.60	72	-47977	1.80	.63581	2.55
74	.46194	1.85	.61049	2.60	74	.48013	1	.63633	
76	. 46230	1.80	.61101	2.60	76	.48049	1.80	.63684	2.55
78	. 46267	1.85	.61153	2.55	78	.48085	1.80	.63736	2.55
80	9.46304	1.85	9.61204	2.60	80	9.48121	1.75	9.63787	2.60
82	.46341		.61256	2.60	82	.48156	1.80	.63839	2.55
84	.46378	1.85	.61308	2.60	84	.48192	1.80	.63890	2.55
86	.46414	1.85	.61360	2.60	86	. 48228	1.80	.63941	2.60
88	.46451	1.85	.61412	2.60	88	.48264	1.80	.63993	2.55
90	9.46488	1.80	9.61464	2.55	90	9.48300	1.80	9.64044	2.60
92	.46524	1.85	.61515	2.60	92	.48336	1.75		2.55
94	.46561	1.85	.61567	2.60	94 96	.48371	1.80	.64147	2.60
96 98	. 46598	1.80	.61671	2.60	98	.48443	1.80	.64250	2.55
100		1.85	9.61722	2.55	100	9.48479	1.80	9.64301	2.55
100	9.46671	1	9.01722	1	1 100	9.40479	1	1 9.04301	1

						1				
	Hun-		46	0		Hun-	-	47	7°	
ı	dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
ı	00	9.48479	1.75	9.64301	2,60	00	9.50243	1.75	9.66865	2.55
ı	02	.48514	1.80	.64353	2.55	02	.50278	1.75	.66916	2.55
ı	04	. 48550	1.80	.64404	2.60	04	.50313	1.75	.66967	2.55
	06	.48586	1.75	.64456	2.55	06	.50347	1.70	.67018	2.55
ı	08	.48621 9.48657	1.80	.64507 9.64558	2.55	08	.50382	1.75	.67069 9.67120	2.55
1	12	.48693	1.80	.64610	2.60	12	9.50417 .50452	1.75	.67171	2.55
ı	14	.48728	1.75	.64661	2.55	14	.50487	1.75	.67222	2.55
1	16	.48764	1.80	.64713	2.60	16	.50521	1.70	.67273	2.55
ı	18	. 48799	I.75 I.80	.64764	2.55	18	. 50556	1.75	.67325	2.60
1	20	9.48835		9.64815	2.55	20	9.50591	1.75	9.67376	2.55
ı	22	.48870	1.75	.64867	2.60	22	.50625	1.70	.67427	2.55
H	24	. 48906	1.80	.64918	2.55	24	.50660	1.75	.67478	2.55
ı	26	.48941	1.75	.64969	2.55	26	.50695	I.75 I.70	.67529	2.55 2.55
ı	28	.48977	1.75	.65021	2.55	28	.50729	1.75	.67580	2.55
ı	30	9.49012	1.80	9.65072	2.55	30	9.50764	1.75	9.67631	2.55
ı	32	.49048	1.75	.65123	2.60	32	.50799	1.70	1	2.55
1	34 36	.49083	1.80	.65175 .65226	2.55	34 36	. 50833	1.75	.67733	2.55
1	38	.49119	1.75	.65277	2.55	38	.50902	1.70	.67835	2.55
1	40	9.49189	1.75	9.65328	2.55	40	9.50937	1.75	9.67886	2.55
ı	42	.49225	1.80	.65380	2.60	42	.50971	1.70	.67937	2.55
1	44	.49223	1.75	.65431	2.55	44	.51006	1.75	.67988	2.55
1	46	.49295	1.75	.65482	2.55	46	.51040	1.70	.68039	2.55
ı	48	.49331	1.80	.65534	2.60	48	.51075	1.75	.68090	2.55
1	50	9.49366	I.75 I.75	9.65585	2.55	50	9.51109	I.70 I.75	9.68141	2.55 2.55
1	52	.49401	1.75	.65636	2.55	52	.51144	1.70	.68192	2.55
1	54	-49437	1.75	.65687	2.60	54	.51178	1.75	.68243	2.55
1	56 58	.49472	1.75	.65739	2.55	56 58	.51213	1.70	.68294	2.55
1	60	. 49507	1.75	.65790	2.55	60		1.70		2.55
1		9.49542	1.75	9.65841	2.55		9.51281	1.75	9.68396	2.55
ı	62 64	.49577 .49613 ·	1.80	.65892	2.60	62 64	.51316	1.70	.68447	2.55
ı	66	.49648	1.75	.65995	2.55	66	.51384	1.70	.68549	2.55
ı	68	.49683	1.75	.66046	2.55	68	.51419	1.75	.68600	2.55
ı	70	9.49718	1.75	9.66097	2.55	70	9.51453	1.70	9.68651	2.55
ı	72	.49753	1.75	.66148	2.55	72	.51487	1.70 1.75	.68702	2.55
ı	74	.49788	1.75	.66200		74	.51522	1.70	.68753	2.55
1	76	.49823	1.75 1.75	.66251	2.55 2.55	76	.51556	1.70	.68804	2.55
ı	78	.49858	1.75	.66302	2.55	78	.51590	1.70	. 68855	2.50
ı	80	9.49893	1.75	9.66353	2.55	80	9.51624	1.75	9.68905	2.55
ı	82	.49928	1.75	.66404	2.55	82	.51659	1.70	.68956	2.55
ı	8 ₄ 86	.49963	1.75	.66455	2.55	8 ₄ 86	.51693	1.70	.69007	2.55
	88	.50033	1,75	.66558	2.55	88	.51761	1.70	.69109	2.55
	90	9.50068	1.75	9,66609	2.55	90	9.51795	1.70	9.69160	2.55
	92	.50103	1.75	.66660	2.55	92	.51829	1.70	.69201	2.55
	94	.50138	1.75	.66711	2.55	94	.51863	1.70	.69262	2.55
	96	.50173	I.75 I.75	.66762	2.55	96	.51898	I.70 I.70	.69313	2.55
	98	.50208	I.75	.66813	2.60	98	.51932	1.70	.69364	2.55
	100	9.50243		9.66865		100	9.51966		9.69415	

Hun-		48	0		Hun-		49	٥	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
- 00	0 57066	.001	9.69415	001		9.53648	.001	9.71954	.001
	9.51966	1.70	.69465	2.50	02	.53682	1.70	.72005	2.55
02 04	.52000	1.70	.69516	2.55	04	.53715	1.65	.72055	2.50
06	.52054	1.70	.69567	2.55	06	.53748	1.65	.72106	2.55
08	.52102	1.70	.69618	2.55	08	.53781	1.65	.72157	2.55
10	9.52136	1.70	9.69669	2.55	10	9.53815	1.70	9.72208	2.55
12	.52170	1.70	.69720	2.55	12	. 53848	1.65	.72258	2.50
14	.52204	1.70	.69771	2.55	14	.53881	1.65	.72309	2.55
16	.52238	1.70	.69822	2.55	16	.53914	1.65	.72360	2.55
18	.52271	1.65	.69872	2.50 2.55	18	.53947	1.65	.72410	2.55
20	9.52305	1.70	9.69923	2.55	20	9.53980	1.65	9.72461	2.55
22	.52339		.69974		22	.54013	_	.72512	
24	.52373	1.70	.70025	2.55 2.55	24	.54046	1.65	. 72562	2.50
26	.52407	I.70 I.70	.70076	2.55	26	. 54080	1.65	.72613	2.55
28	.52441	1.70	.70127	2.50	28	.54113	1.65	.72664	2.50
30	9.52475	1.65	9.70177	2.55	30	9.54146	1.65	9.72714	2.55
32	. 52508	1.70	.70228	2.55	32	.54179	1.65	.72765	2.55
34	.52542	1.70	.70279	2.55	34	.54212	1.65	.72816	2.50
36	.52576	1.70	.70330	2.55	36	.54245	1.65	.72866	2.55
38	.52610	1.65	.70381	2.50	38	.54278	1.65	.72917	2.55
40	9.52643	1.70	9.70431	2.55	40	9.54311	1.65	9.72968	2.50
42	.52677	1.70	.70482	2.55	42	-54344	1.65	.73018	2.55
44	.52711	1.70	.70533	2.55	44 46	-54377	1.60	.73069	2.55
46	.52745	1.65	.70584	2.55		.54409	1.65		2.50
48	.52778	1.70	9.70685	2.50	48 50	.54442 9.54475	1.65	.73170 9.73221	2.55
50	9.52812	1.70	.70736	2.55	52	.54508	1.65	.73271	2.50
52	.52879	1.65	.70787	2.55	54	.54541	1.65	.73321	2.50
54 56	.52079	1.70	.70838	2.55	54 56	.54574	1.65	.73372	2.55
58	.52946	1.65	.70889	2.55	58	.54607	1.65	.73423	2.55
60	9.52980	1.70	9.70939	2.50	60	9.54639	1.60	9.73474	2.55
62	.53014	1.70	.70990	2.55	62	.54672	1.65	.73524	2.50
64	.53047	1.65	.71041	2.55	64	.54705	1.65	.73575	2.55
66	.53081	1.70	.71092	2.55	66	.54738	1.65	.73626	2.55
68	.53114	1.65	.71142	2.50	68	.54771	1.65	.73676	2.50
70	9.53148	1.70	9.71193	2.55	70	9.54803	1.60	9.73727	2.55
72	.53181	1.05	.71244	2.55	72	. 54836	1.65	.73778	2.50
74	.53215	1.65	.71295	2.50	74	.54869	1.60	.73828	2.55
76	.53248	1.05	.71345	2.55	76	.54901	1.65	.73879	2.50
78	.53282	1.65	.71396	2.55	78	-54934	1.65	.73929	2.55
80	9.53315	1.65	9.71447	2.55	80	9.54967	1.60	9.73980	2.55
82	.53348	1.70	.71498	2.50	82	-54999	1.65	.74031	2.50
84	.53382	1.65	.71548	2.55	84 86	.55032	1.65	.74081	2.55
86	.53415	1.70	.71599	2.55	1	.55065	1.60	.74132	2.50
88	-53449	1.65	.71650	2.50	88	.55097	1.65	9.74233	2.55
90 92	9.53482	1.65	9.71700	2.55	90	9.55130	1.60	9.74233	2.55
1	1	1.70	.71751	2.55	94	.55195	1.65	.74334	2.50
94 96	.53549	1.65	.71853	2.55	94	.55228	1.65	.74385	2.55
98	.53562	1.65	.71903	2.50	98	.55260	1.60	.74435	2.50
100	9.53648	1.65	9.71954	2.55	100	9.55293	1.65	9.74486	2.55
100	9.33048	1	1 9.71934	1	1 200	9.33293	1	3.74400	1

Hun-		50)°		Hun-		51	l°	
dredths	Vers	Diff.	Exsec	Diff. .001	dredths	Vers	Diff. .∞ı	Exsec	Diff.
00	9.55293	1.60	9.74486	2.50	00	9.56900	1.60	9.77013	2.50
02	- 55325	1.65	.74536		02	. 56932	1.55	.77063	-
04	-55358	1.60	.74587	2.55 2.55	04	. 56963	1.60	.77114	2.55
06	.55390	1.65	. 74638	2.50	06	.56995	1.60	.77164	2.55
08	- 55423	1.60	. 74688	2.55	08	.57027	1.60	.77215	2.50
10 12	9.55455 .55487	1.60	9.74739 .74789	2.50	10 12	9.57059 .57090	1.55	9.77265 .77316	2.55
14	.55520	1.65	.74840	2.55	14	.57122	1.60	.77366	2.50
16	.55552	1.60	.74890	2.50	16	.57154	1.60 1.55	.77417	2.55
18	· 55 585	1.65 1.60	.74941	2.55	18	.57185	1.60	.77467	2.50
20	9.55617	1.60	9.74992	2.55	20	9.57217	1.60	9.77518	2.55
22	.55649		. 75042	2.50	22	.57249	1.55	.77568	2.50
24	.55682	1.65	.75093	2.55	24	.57280	1.60	.77619	2.55
26	.55714	1.60	.75143	2.55	26	.57312	1.55	.77669	2.55
28	.55746	1.65	.75194	2.50	28	-57343	1.60	.77720	2.50
30	9.55779 .55811	1.60	9.75244	2.55	30	9.57375	1.60	9.77770	2.55
32		1.60	.75295	2.50	32	.57407	1.55	.77821	2.50
34 36	.55843 .55875	1.60	· 75345 · 75396	2.55	34 36	.57438 .57470	1.60	.77871	2.55
38	.55908	1.65	.75447	2.55	38	.57501	1.55	.77972	2.50
40	9.55940	1.60	9.75497	2.50	40	9.57533	1.60	9.78023	2.55
42	.55972	1.60	.75548	2.55	42	.57564	1.55 1.60	.78073	2.50
44	.56004	1.60	.75598	2.50	44	. 57596	1.55	.78124	2.55
46	. 56036	1.60 1.65	.75649	2.55	46	. 57627	1.60	.78174	2.50
48	. 56069	1.60	. 75699	2.55	48	. 57659	1.55	.78225	2.50
50	9.56101	1.60	9.75750	2.50	50	9.57690	1.55	9.78275	2.55
52	.56133	1.60	.75800	2.55	52	.57721	1.60	. 78326	2.50
54 56	. 56165 . 56197	1.60	.75851	2.50	54	-57753	1.55	.78376	2.55
58	.56229	1.60	.75901	2.55	56 58	.57784 .57816	1.60	.78477	2.50
60	9.56261	1.60	9.76002	2.50	60	9.57847	1.55	9.78527	2.50
62	.56293	1.60	.76053	2.55	62	.57878	1.55	.78578	2.55
64	.56325	1.60	.76103	2.50	64	.57910	I.60	.78628	2.50
66	. 56357	1.60	.76144	2.55	66	.57941	1.55	. 78679	2.55
68	. 56390	1.60	. 76204	2.50	68	.57972	1.55	.78729	2.50
70	9.56422	1.60	9.76255	2.55 2.55	70	9.58004	1.55	9.78780	2.55
72	. 56454	1.55	. 76306	2.50	72	. 58035	1.55	.78830	2.55
74	. 56485	1.60	.76356	2.55	74	. 58066	1.55	.78881	2.50
76 78	.56517 .56549	1.60	.76407	2.50	76 78	. 58097 . 58129	1.60	.78931	2.55
80	9.56581	1.60	9.76508	2.55	80	9.58160	1.55	9.79032	2.50
82	.56613	1.60	.76558	2.50	82	.58191	1.55	.79083	2.55
84	.56645	1.60	.76609	2.55	84	.58222	I.55	.79133	2.50
86	. 56677	1.60	.76659	2.50	86	.58253	1.55	.79184	2.55
88	.56709	ł	.76710	2.55	88	. 58285	1.55	.79234	2.50
90	9.56741	1.60	9.76760	2.50	90	9.58316	1.55	9.79285	2.55
92	.56773	1.55	.76811	2.50	92	.58347	1.55	-79335	2.55
94	. 56804	1.60	.76861	2.55	94	. 58378	1.55	.79386	2.50
96 98	. 56836 . 56868	1.60	.76912	2.50	96 98	. 58409	1.55	.79436	2.55
100	9.56900	1.60		2.55	100	9.58471	1.55		2.50
100	9.50900		9.77013		100	9.504/1		9.79537	

Hun-		52	20		Hun-		53	53°			
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	D1ff. .001		
00	9.58471	1.55	9.79537	2.55	00	9.60008	1.55	9.82062	2.55		
02	. 58502	1.60	. 79588	2.50	02	. 60039	1.50	.82113	2.50		
04	. 58534	1.55	.79638	2.55	04	.60069	1.55	.82163	2.55		
06	.58565	1.55	. 79689	2.50	06		1.50	.82214	2.50		
08 10	. 58596 9. 58627	1.55	.79739 9.79790	2.55	08	.60130 9.60160	1.50	.82264 9.82315	2.55		
13	.58658	1.55	.79840	2.50	12	.60191	1.55	.82365	2.50		
14	.58689	1.55	.79891	2.55	14	.60221	1.50	.82416	2.55		
16	.58720	1.55	.79941	2.50	16	.60251	I.50 I.55	.82466	2.50		
18	.58751	I.55	.79992	2.55	18	. 60282	1.50	.82517	2.55 2.55		
20	9.58782	1.50	9.80042	2.55	20	9.60312	1.50	9.82568	2.50		
22	.58812	1.55	.80093	2.50	22	.60342	1.50	.82618	2.55		
24	.58843	1.55	.80143	2.55	24	.60372	1.55	.82669	2.50		
26	.58874	1.55	.80194	2.50	26	.60403	1.50	.82719	2.55		
28	. 58905	1.55	.80244 9.80295	2.55	28	.60433 9.60463	1.50	.82770	2.50		
30 32	9.58936 .58967	1.55	.80345	2.50	30 32	.60493	1.50	.82871	2.55		
34	.58998	1.55	.80395	2.50	34	.60523	1.50	.82921	2.50		
36	.59029	1.55	.80446	2.55	36	.60554	1.55	.82972	2.55		
38	.59059	1.50	.80496	2.50	38	.60584	I.50 I.50	.83022	2.50 2.55		
40	9.59090	1.55	9.80547	2.50	40	9.60614	1.50	9.83073	2.50		
42	.59121		.80597	-	42	.60644	1.50	.83123			
44	.59152	1.55 1.55	.80648	2.55	44	.60674	1.50	.83174	2.55 2.55		
46	.59183	1.50	.80698	2.55	46	.60704	1.50	.83225	2.50		
48	.59213	1.55	.80749	2.50	48	.60734	1.50	.83275	2.55		
50 52	9.59244 .59275	1.55	9.80799 .80850	2.55	50 52	9.60764 .60795	1.55	9.83326 .83376	2.50		
_		1.55	.80900	2.50	54	.60825	1.50	.83427	2.55		
54 56	. 59306 . 59336	1.50	.80900	2.50	54 56	.60855	1.50	.83477	2.50		
58	.59367	1.55	.81001	2.55	58	.60885	1.50	.83528	2.55		
60	9.59398	1.55	9.81052	2.55	60	9.60915	1.50	9.83579	2.55		
62	.59428	1.50	.81102	2.50	62	.60945	1.50	.83629	2.50		
64	-59459	I.55 I.55	.81153	2.55	64	.60975	I.50 I.50	.83680	2.55 2.50		
66	. 59490	1.50	.81203	2.55	66	.61005	1.50	.83730	2.55		
68	.59520	1.55	.81254	2.50	68	.61035	1.50	.83781	2.50		
70	9.59551	1.50	9.81304	2.55	70	9.61065	1.50	9.83831	2.55		
72	.59581	1.55	.81355	2.50	72	.61124	1.45	.83933	2.55		
74 76	.59612	1.55	.81405 .81456	2.55	74 76	.61154	1.50	.83983	2.50		
78	.59673	1.50	.81507	2.55	78	.61184	1.50	.84034	2.55		
80	9.59704	1.55	9.81557	2.50	80	9.61214	1.50	9.84084	2.50		
82	-59734	1.50	.81608	2.55	82	.61244	1.50	.84135	2.55		
84	.59765	1.55	.81658	2.50	84	.61274	1.50	.84186	2.55		
86	-59795	1.50	.81709	2.50	86	.61304	1.50	.84236	2.55		
88	. 59826	1.50	.81759	2.55	88	.61334	1.45	.84287	2.50		
90	9.59856	1.55	9.81810	2.50	90	9.61363	1.50	9.84337	2.55		
92	. 59887	1.50	.81860	2.55	92	.61393	1.50	.84388	2.55		
94 96	.59917	1.55	.81911 .81961	2.50	94 96	.61423 .61453	1.50	.84439 .84489	2.50		
96	.59948	1.50	.81901	2.55	98	.61483	1.50	.84540	2.55		
100	9.60008	1.50	9.82062	2.50	100	9.61512	1.45	9.84590	2.50		

						55°			
Hun-		54	f.o.		Hun-			5°	
dredths	Vers	Diff.	Exsec	Diff. .001	dredths	Vers	Diff.	Exsec	Diff.
00	9.61512	1.50	9.84590	2.55	_00	9.62984	1.45	9.87125	2.55
02	.61542	1.50	.84641	2.55	02	.63013	I.45	.87176	2.55
04	.61572 .61602	1.50	.84692	2.50	04 06	.63042 .63071	1.45	.87227	2.50
o6 o8	.61631	1.45	.84742	2.55	08	.63101	1.50	.87277	2.55
10	9.61661	1.50	9.84844	2.55	10	9.63130	1.45	9.87379	2.55
12	.61691	1.50	.84894	2.50	12	.63159	1.45	.87430	2.55
14	.61720	I.45 I.50	.84945	2.55	14	.63188	1.45	.87480	2.50
16	.61750	1.50	.84996	2.55	16	.63217	I.45 I.45	.87531	2.55 2.55
18	.61780	1.45	.85046	2.55	18	.63246	1.45	.87582	2.55
20	9.61809	1.50	9.85097	2.50	20	9.63275	1.45	9.87633	2.55
22	.61839	1.45	.85147	2.55	22	.63304	1.45	.87684	2.55
24 26	.61898	1.50	.85198 .85249	2.55	24 26	.63333 .63362	1.45	.87735 .87785	2.50
28	.61928	1.50	.85299	2.50	28	.63391	1.45	.87846	2.55
30	9.61957	1.45	9.85350	2.55	30	9.63420	1.45	9.87887	2.55
32	.61987	I.50 I.45	.85401	2.55	32	.63448	I.40 I.45	.87938	2.55 2.55
34	.62016	1.50	.85451	2.55	34	.63477	I.45	.87989	2.55
36	.62046	1.45	.85502	2.55	36	.63506	1.45	.88040	2.50
38	.62075	1.50	.85553	2.50	38 40	.63535	1.45	.88090	2.55
40	9.62105	1.45	9.85603	2.55		9.63564	1.45	9.88141	2.55
42 44	.62134	1.50	.85654 .85705	2.55	42 44	.63593	1.45	.88192	2.55
46	.62193	1.45	.85755	2.50	46	.63651	1.45	.88294	2.55
48	.62223	1.50	.85806	2.55	48	.63679	1.40	.88345	2.55
50	9.62252	I.45 I.50	9.85857	2.55 2.50	50	9.63708	I.45 I.45	9.88395	2.50
52	.62282	1.45	.85907	2.55	52	.63737	1.45	.88446	2.55
54	.62311	1.45	.85958	2.55	54	.63766	1.45	.88497	2.55
56 58	.62340 .62370	1.50	. 86009 . 86060	2.55	56 58	.63795 .63823	1.40	.88548	2.55
60	9.62399	1.45	9.86110	2.50	60	9.63852	1.45	9.88650	2.55
62	.62429	1.50	.86161	2.55	62	.63881	1.45	.88701	2.55
64	.62458	1.45	.86212	2.55	64	.63910	1.45	.88752	2.55
66	.62487	I.45 I.50	.86262	2.50 2.55	66	.63938	I.40 I.45	.88803	2.55 2.55
68	.62517	1.45	.86313	2.55	68	.63967	1.45	.88854	2.50
70	9.62546	1.45	9.86364	2.55	70	9.63996	I.45	9.88904	2.55
72	.62575	1.45	.86415	2.50	72	.64025	1.40	.88955	2.55
74 76	.62604 .62634	1.50	.86465 .86516	2.55	74 76	.64053	1.45	.89006	2.55
78	.62663	1.45	.86567	2.55	78	.64111	1.45	.89108	2.55
80	9.62692	1.45	9.86617	2.50	80	9.64139	1.40	9.89159	2.55
82	.62722	1.50	.86668	2.55	82	.64168	1.45	.89210	2.55
84	.62751	I.45 I.45	.86719	2.55 2.55	84	.64197	I.45 I.40	.89261	2.55 2.55
86	.62780	1.45	.86770	2.50	86	.64225	1.45	.89312	2.55
88	.62809	1.45	.86820	2.55	88	.64254	1.40	.89363	2.55
90 92	9.62838	1.50	9.86871	2.55	90 92	9.64282	1.45	9.89414	2.55
94	.62897	1.45	.86973	2.55	94	.64339	1.40	.89516	2.55
94	.62926	1.45	.87023	2.50	94	.64368	1.45	.89567	2.55
98	.62955	I.45 I.45	.87074	2.55	98	.64396	1.40	.89618	2.55 2.55
100	9.62984	1.43	9.87125	2.33	100	9.64425	3.43	9.89669	2.33

Hun-		5	6°		Hun-		5	7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.64425		9.89669		00	9.65836		9.92225	
02	.64453	1.40	.89720	2.55	02	.65863	1.35	.92276	2.55
04	.64482	1.45	.89771	2.55	04	.65891	1.40	.92327	2.55
06	.64510	I.40 I.45	.89822	2.55 2.55	06	.65919	I.40 I.40	.92379	2.55
o8	. 64539	1.40	.89873	2.55	08	.65947	1.40	.92430	2.55
10	9.64567	1.45	9.89924	2.55	10	9.65975	1.40	9.92481	2.55
12	.64596	1.40	.89975	2.55	12	.66003	1.40	.92532	2.55
14 16	.64624	1.45	.90026	2.55	14 16	.66031 .66059	1.40	.92584	2.60
18	.64681	1.40	.90128	2.55	18	.66086	1.35	.92686	2.55
20	9.64709	1.40	9.90179	2.55	20	9.66114	1.40	9.92738	2.60
22	.64738	1.45	.90230	2.55	22	,66142	1.40	.92789	2.55
24	.64766	1.40	.90281	2.55	24	.66170	1.40	.92840	2.55
26	.64794	1.40	.90332	2.55	26	.66198	1.40	.92892	2.60
28	.64823	1.45	.90383	2.55	28	.66225	1.35	.92943	2.55
30	9.64851	I.40 I.40	9.90434	2.55	30	9.66253	1.40	9.92994	2.55
32	.64880	1.40	.90485	2.55 2.55	32	.66281	I.40 I.40	.93046	2.55
34	.64908	1.40	.90536	2.55	34	.66309	1.35	.93097	2.60
36	.64936	1.40	.90587	2.55	36	.66336	1.40	.93149	2.55
38	.64964	1.45	.90638	2.55	38	.66364	1.40	.93200	2.55
40	9.64993	1.40	9.90689	2.60	40	9.66392	1.35	9.93251	2.60
42	.65021	1.40	.90741	2.55	42	.66419 .66447	1.40	.93303	2.55
44 46	.65049 .65077	1.40	.90792	2.55	44 46	.66475	1.40	·93354 ·93405	2.55
48	.65106	1.45	.90894	2.55	48	.66502	1.35	93457	2.60
50	9.65134	1.40	9.90945	2.55	50	9.66530	1.40	9.93508	2.55
52	.65162	I.40 I.40	.90996	2.55	52	.66558	1.40	.93560	2.60
54	.65190		.91047	2.55	54	.66585	1.35	.93611	2.55
56	.65218	I.40 I.45	.91098	2.55 2.55	56	.66613	I.40 I.35	.93663	2.55
58	.65247	1.40	.91149	2.60	58	.66640	1.40	.93714	2.60
60	9.65275	1.40	9.91201	2.55	60	9.66668	1.40	9.93766	2.55
62	.65303	1.40	.91252	2.55	62	.66696	1.35	.93817	2.60
64 66	.65331	1.40	.91303	2.55	64	.66723	1.40	.93869	2.55
68	.65359	1.40	.91354	2.55	66	.66751	1.35	.93920	2.55
70	.65387 9.65415	1.40	9.91456	2.55	68 70	.66778 9.66806	1.40	9.94023	2.60
72	.65444	1.45	.91508	2.60	70	.66833	1.35	.94074	2.55
74	.65472	1.40	91559	2.55	74	.66861	1.40	.94126	2.60
76	.65500	1.40	.91610	2.55	76	.66888	1.35	.94177	2.55
78	.65528	I.40 I.40	.91661	2.55 2.55	78	.66916	1.40	.94229	2.60
80	9.65556	1.40	9.91712	2.60	80	9.66943	1.40	9.94281	2.55
82	.65584	I.40	.91764	2.55	82	.66971	1.35	.94332	2.60
84	.65612	1.40	.91815	2.55	84	.66998	1.40	.94384	2.55
86	.65640	1.40	.91866	2.55	86	.67026	1.35	-94435	2.60
88 90	,65668 9.65696	1.40	9.91917	2.55	88 90	.67053	1.35	9.94538	2.55
92	.65724	1.40	.92020	2.60	90	.67108	1.40	.94590	2.60
94	.65752	1.40	.92071	2.55	94	.67135	1.35	.94641	2.55
96	.65780	1.40	.92122	2.55	96	.67163	1.40	.94693	2.60
98	.65808	I.40 I.40	.92173	2.55	98	.67190	1.35 1.35	.94745	2.55
100	9.65836		9.92225	2.00	100	9.67217	55	9.94796	55

		5	8°		1		5.0	9°	
Hun-		Diff.		Diff.	Hun-		Diff.	1	Diff.
dredths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001
00	9.67217	1.40	9.94796	2.60	00	9.68571	1.35	9.97387	2.60
02	.67245	I.35	.94848	2.60	02	.68598	1.30	-97439	2.60
04 06	.67272	1.35	.94900	2.55	04	.68624	1.35	.97491	2.60
08	.67299	1.40	.94951	2.60	08	.68651	1.35	.97543	2.60
10	.67327 9.67354	1.35	.95003 9.95054	2.55	10	.68678 9.68705	1.35	-97595 9.97647	2.60
12	.67381	1.35	.95106	2.60	12	.68731	1.30	.97699	2.60
14	.67408	1.35	.95158	2.60	14	.68758	1.35	.97751	2.60
16	.67436	1.40	.95209	2.55	16	.68785	1.35	.97803	2.60
18	.67463	1.35	.95261	2.60	18	.68811	I.30 I.35	.97855	2.65
20	9.67490	1.35	9.95313	2.55	20	9.68838	1.35	9.97908	2.60
22	.67517	1.40	.95364	2.60	22	.68865	1.35	.97960	2.60
24	.67545	1.40	.95416	2.60	24	.68892	1.30	.98012	2.60
26	.67572	1.35	.95468	2.60	26	.68918	1.35	.98064	2.60
28	.67599	1.35	.95520	2.55	28	.68945	1.30	.98116	2.60
30 32	9.67626 .67653	1.35	9.95571 .95623	2.60	30 32	9.68971 .68998	1.35	9.98168	2.60
34	.67681	1.40	.95675	2.60	34	.69025	1.35	.98273	2.65
36	.67708	1.35	.95726	2.55	36	.69023	1.30	.98325	2.60
38	.67735	1.35	.95778	2.60	38	.69078	1.35	.98377	2.60
40	9.67762	1.35	9.95830	2.60	40	9.69104	1.30	9.98429	2.60
42	.67789	1.35	.95882		42	.69131	1.35	.98481	2.60
44	.67816	1.35	- 95934	2.60	44	.69158	I.35 I.30	.98534	2.60
46	.67843	1.35	.95985	2.60	46	.69184	1.35	.98586	2.60
48	.67870	1.35	.96037	2.60	48	.69211	1.30	. 98638	2.60
50 52	9.67897 .67925	1.40	9.96089	2.60	50 52	9.69237	1.35	9.98690	2.65
	.67952	1.35	.96193	2.60	_		1.30	.98743	2.60
54 56	.67979	1.35	.96244	2.55	54 56	.69290 .69317	1.35	.98847	2.60
58	.68006	1.35	.96296	2.60	58	.69343	1.30	.98899	2.60
60	9.68033	1.35	9.96348	2.60	60	9.69370	1.35	9.98952	2.60
62	.68060	1.35	.96400	2.60	62	.69396	1.30	.99004	2.60
64	.68087	1.35	.96452	2.60	64	.69423	1.35	.99056	2.65
66	.68114	1.35	.96504	2.60	66	.69449	1.30	.99109	2.60
68	.68141	I.35	.96556	2.55	68	.69476	I.30	.99161	2.60
70	9.68168	1.35	9.96607	2.60	70	9.69502	1.30	9.99213	2.65
72	.68195	1.35	.96659	2.60	72	.69528	1.35	.99266	2.60
74 76	.68222	1.30	.96711 .96763	2.60	74 76	.69555 .69581	1.30	.99318	2.65
78	.68275	1.35	.96815	2.60	78	.69608	1.35	.99371	2.60
80	9.68302	1.35	9.96867	2.60	80	9.69634	1.35	9.99475	2.60
82	.68329	1.35	.96919	2.60	82	,69660	1.30	.99528	2.65
84	.68356	1.35	.96971	2.60	84	.69687	1.35	99580	2.60
86	.68383	I.35 I.35	.97023	2.60	86	.69713	1.30	.99633	2.60
88	.68410	1.35	.97075	2.60	88	.69739		.99685	2.65
90	9.68437	I.30	9.97127	2.60	90	9.69766	1.35	9.99738	2.60
92	.68463	1.35	.97179	2.60	92	.69792	1.30	.99790	2.65
94 96	.68490	1.35	.97231	2.60	94 96	.69818 .69844	1.30	.99843	2.60
98	.68544	1.35	.97283	2.60	98	.69871	1.35	.99895	2.60
100	9.68571	1.35	9.97387	2.60	100	9.69897	1.30	0.00000	2.65
200	9.003/1		9.91301		100	9.09097		0.00000	

00 9.69897 -69923 1.30 1.30 0.00000 0.00053 2.65 2.65 2.65 00 0.71197 9.71197 1.30 1.30 0.71223 0.01 1.30 0.00000 0.00153 0.001 0.00153	Diff. .001
02 .69923 1.30 .00053 2.65 02 .71223 1.30 .71223 1.30 .00053 2.65 04 .71248 1.25 1.30 .00158 2.65 04 .71248 1.25 1.30 .00158 2.60 04 .71248 1.25 1.30 .00158 2.60 08 .71248 1.30 .0016 .0026 2.65 10 .71300 1.30 .0026 2.65 10 .971300 1.25 .0036 .0026 2.65 12 .71351 1.30 .0036 1.30 .0036 1.30 .00473 2.65 14 .71377 1.25 .0036 1.30 .00473 2.65 18 .71428 1.30 .00473 2.65 18 .71428 1.30 .00473 2.65 18 .71428 1.30 .00578 2.65 20 .714428 1.30 .00578 2.65 22 .714779 1.25 .0 .00473 2.65 24 .71595 <th>2 65</th>	2 65
02 .69923 1.30 .00053 2.60 04 .71223 1.25 .25 06 .69949 1.35 .00158 2.65 04 .71248 1.35 .25 08 .70002 1.30 .00210 2.65 06 .71274 1.30 .25 .25 10 9.70028 1.30 .00210 2.65 10 9.71325 1.25 .25 12 .70054 1.35 .00368 2.65 12 .71351 1.30 .26 .265 12 .71351 1.30 .25 .26 14 .71372 1.30 .26 .265 14 .71372 1.30 .25 .265 18 .71402 1.25 .25 .265 18 .71402 1.25 .25 .265 18 .71428 1.30 .25 .265 18 .71428 1.30 .25 .265 22 .714428 1.30 .25 .265 22 .714749	
04 .09949 1.35 .00165 2.65 04 .71248 1.30 .006 .06976 1.35 .00168 2.65 06 .71274 1.30 .03 1.30 .00210 2.65 06 .71274 1.30 .03 1.30 .00210 2.65 10 9.71325 1.25 0.26 1.20 1.20 1.25 0.26 1.20 1.35 1.30 1.25 1.30 1.25 1.30 1.25 1.30 1.25 1.30 1.25 1.30 1.25 1.30 1.25 1.30	02693
08 .79097 I.30 .00188 2.60 08 .71302 I.30 .0210 2.65 10 .971325 I.30 I.25 0.00263 1.26 10 .971325 I.30 I.25 0.00263 1.26 10 .971325 I.30 I.30 1.30	2 65
10	2.65
1.2	02852
14 .70081 1.35 .00368 2.65 14 .71377 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.30 1.25 1.30 1.25 1.30 1.25 1.30 1.30 1.30 1.30 1.30 2.65 18 .71428 1.30 1.30 1.30 1.30 1.30 2.65 2.65 2.65 2.65 1.30 <	02058 2.05
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2.70
18	03065 2.65
20 9.70159 1.30 0.00526 2.60 22 22 271479 1.30 2.65 24 271505 1.30 2.65 24 2.71505 1.30 2.65	2.65
22	2.65
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	03224
28	2 65
30 9.70290 1.30 0.00789 2.65 30 9.71582 1.30 0.00789 32 0.00842 2.65 32 0.71607 1.30 1.30 34 7.70342 1.30 0.00842 2.65 34 7.71607 1.30 1.30 38 7.70384 1.30 0.0000 2.65 36 7.71633 1.25 0.0000 38 7.70394 1.30 0.01052 2.65 38 7.71684 1.30 0.01052 2.65 38 7.71684 1.25 0.01052 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 44 7.71760 1.25 0.0158 2.65 0.0158	2,65
32 .70316 1.30 .00842 2.65 32 .71607 1.25 1.30 34 .70342 1.30 .00894 2.65 34 .71633 1.25 1.30 38 .70394 1.30 .01000 2.65 36 .71658 1.35 1.30 40 9.70420 1.30 0.01052 2.65 40 9.71709 1.30 0.01052 42 .70476 1.30 .01105 2.65 42 .71735 1.35 0.0158 44 .70476 1.30 .01158 3.65 44 .71760 1.25 1.25	03384
34	2.70
36	2.05
40 9.70420 1.30 0.01052 2.65 40 9.71709 1.30 0. 42 70446 1.30 0.0158 2.65 42 71735 1.25 0. 44 .70472 1.30 0.0158 2.65 44 71760 1.30 0.	2.05
40 9.70420 1.30 0.01052 2.65 40 9.71709 1.30 0.01105 2.65 42 .71735 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 1.25 .71760 .	03651 2.65
42 .70446 1.30 .01105 2.65 42 .71735 1.25	2.65
44 .70472 1 30 .01158 3 65 44 .71700 1 30 .	03757 2.70
4b 70408 1.30 01211 2.03 4b 71786 1.30	03811
40 .70490 T 30 .01211 2 60 40 .71760 T 35 .	2.65
48 .70524 T 20 .01263 2 65 48 .71811 T 20 .	03917
9.70550 1.30 0.01310 2.65 50 9.71837 1.35 0.	03971 2.65
1.30	04078 2.70
56 70628 I.30 01475 2.65 56 71012 I.25	2.05
58 70654 I.30 01528 2.65 58 71030 I.30	2.05
60 9.70680 1.30 0.01580 2.60 60 9.71964 1.25 0.	04238 2.70
62 70706 1.30 2.65 62 71990 1.30 3.01633 2.65 62 71990 1.30 3.00 3.00 3.00 3.00 3.00 3.00 3.0	2.65
64 .70732 1.30 .01686 2.05 64 .72015 1.25	04345 2.65
1.30 .01739 2.65 00 .72041 1.25	04398 2.70
08 .70784 T 30 .01792 2 65 68 .72066 T 25	2 65
9.70010 1 25 0.01045 2 65 70 9.72091 1 20 0.	2 70
1.30 .01898 2.65 72 .72117 1.25	04559 2.65
76 70887 1.30 02004 2.65 76 72167 1.25	2.70
78 70013 1.30 02056 2.60 78 72103 1.30	2.70
80 9.70939 I.30 0.02109 2.65 80 9.72218 I.25 0.	2.65
82 70065 1.30 02162 2.05 82 72243 1.25	2.70
84 .70991 1.30 .02215 2.65 84 .72269 1.30 .	04880 2.05
30 .71010 I.30 .02208 2.65 80 .72294 I.25	2.70
88 .71042 J. 30 .02321 3 65 88 .72319 J. 30 .	04988
90 9.71000 1.30 0.02374 3 65 90 9.72345 7.35 0.1	2 70
1.30 .02427 2.65 92 .72370 1.25	2.70
96 71145 1.25 02534 2.70 96 72420 1.25	2.65
98 .71171 1.30 .02587 2.65 98 .72446 1.30	
100 9.71197 1.30 0.02640 2.65 100 9.72771 1.25 0.	05202 05256 2.70

		62	o°			63°			
Hun- dredths		Diff.		Diff.	Hun- dredths		Diff.		Diff.
dredths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001
00	9.72471	1.25	0.05310	2.70	00	9.73720	1.25	0.08015	2.75
02	.72496	1.25	.05364	2.65	02	.73745	1.20	.08070	2.70
04 06	.72521	1.30	.05417	2.70	04 06	.73769 .73794	1.25	.08124	2.75
08	.72572	1.25	.05525	2.70	08	.73819	1.25	.08233	2.70
10	9.72597	1.25	0.05579	2.70	10	9.73844	1.25	0.08288	2.75
12	.72622	I.25 I.25	.05633	2.70	12	. 73868	I.20 I.25	.08343	2.75
14	.72647	1.25	.05686	2.70	14	. 73893	1.25	.08397	2.75
16 18	.72672	1.30	.05740	2.70	16	.73918	1.20	.08452	2.70
20	.72698	1.25	.05794	2.70	20	.73942	1.25	.08506	2.75
	9.72723	1.25	0.05848	2.70	22	9.73967	1.25	0.08561	2.75
22 24	.72748	1.25	.05902	2.70	22	.73992 .74016	. I.20	.08616	2.70
26	.72798	1.25	.05930	2.70	26	.74031	1.25	.08715	2.75
28	.72823	1.25	.06064	2.70	28	.74065	1.20	.08780	2.75
30	9.72848	1.25	0.06118	2.70	30	9.74090	1.25	0.08835	2.75
32	. 72873	I.25 I.25	.06172	2.70	32	.74115	I.25 I.20	.08889	2.70
34	. 72898	1.25	.06226	2.70	34	.74139	1.25	.08944	2.75
36 38	.72923	1.25	.06280	2.70	36 38	.74164	1.20	.08999	2.75
40	.72948	1.25	0.06334	2.70	40		1.25	0.09108	2.70
	9.72973	1.30		2.70	42	9.74213	1.20		2.75
42 44	.72999	1.25	.06442	2.70	44	.74237 .74262	1.25	.09163	2.75
46	.73049	1.25	.06550	2.70	46	.74286	1.20	.09273	2.75
48	.73074	1.25	.06604	2.70	48	.74311	1.25	.09328	2.75
50	9.73099	I.25 I.20	0.06658	2.70	50	9.74335	I.20 I.25	0.09383	2.75
52	.73123	1.25	.06712	2.70	52	.74360	1.20	.09438	2.75
54	.73148	1.25	.06766	2.70	54	.74384	1.25	.09493	2.75
56 58	.73173	1.25	.06820	2.70	56 58	.74409 .74433	1.20	.09548	2.70
60	9.73223	1.25	0.06929	2.75	60	9.74458	1.25	0.09657	2.75
62	.73248	1.25	.06983	2.70	62	.74482	1.20	.09712	2.75
64	.73243	1.25	.07037	2.70	64	.74507	1.25	.09767	2.75
66	. 73298	1.25	.07091	2.70	66	.74531	I.20 I.25	.09823	2.80
68	. 73323	1.25 1.25	.07146	2.75	68	. 74556	1.25	.09878	2.75
70	9.73348	1.25	0.07200	2.70	70	9.74580	1.20	0.09933	2.75
72	-73373	1.25	.07254	2.75	72	.74604	1.25	.09988	2.75
74 76	.73398 .73422	1.20	.07308	2.70	74 76	.74629 .74653	1.20	.10043	2.75
78	.73422	1.25	.07303	2.70	78	.74678	1.25	.10093	2.75
80	9.73472	1.25	0.07471	2.70	80	9.74702	1.20	0.10208	2.75
82	.73497	1.25	.07526	2.75	82	.74726	1.20	,10263	2.75
84	.73522	I.25 I.25	.07580	2.70	84	.74751	1.25	.10319	2.80
86	.73547	1.25	.07634	2.75	86	-74775	1.20	.10374	2.75
88	.73571	1.25	.07689	2.70	88	.74799	1.25	.10429	2.75
90 92	9.73596 .73621	1.25	0.07743	2.75	90 92	9.74824	1.20	.10540	2.80
92	.73646	1.25	.07798	2.70	92	.74872	1.20	.10540	2.75
94 96	.73671	1.25	.07906	2.70	94	.74896	1.20	.10595	2.75
98	.73695	I.20 I.25	.07961	2.75	98	.74921	I.25 I.20	.10705	2.75
100	9.73720	1.25	0.08015	2.70	100	9.74945	1.20	0.10761	2.00

,,		64	۰		Hun-		65	۰	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.74945		0.10761		00	9.76146	I.20	0.13551	2.85
02	.74969	I.20 I.20	. 10816	2.75 2.75	02	.76170	1.20	. 13608	2.80
04	-74993	I.25	. 10871	2.75	04	.76194 .76218	1.20	.13664	2.80
06	.75018	1.20	. 10927	2.75	o6 o8		1.15	.13720	2.85
08	. 75042 9 . 75066	1.20	.10982	2.80	10	.76241 9.76265	1.20	.13777 o.13833	2.80
12	.75090	1.20	.11093	2.75	12	.76289	I.20 I.20	.13890	2.85
14	.75115	I.25 I.20	.11149	2.80	14	.76313	1.15	. 13946	2.85
16	.75139	I.20	.11204	2.75	16	.76336	I.15	.14003	2.80
18	.75163	1.20	.11260	2.75	18	.76360	1.20	.14059	2.85
20	9.75187	1.20	0.11315	2.80	20	9.76384	1.20	0.14116	2.80
22 24	.75211 .75235	1.20	.11371	2.75	22 24	.76408 .76431	1.15	.14172	2.85
26	.75260	1.25	.11420	2.80	26	.76455	1.20	.14285	2.80
28	.75284	1.20	.11537	2.75	28	. 76479	1.20	.14342	2.85
30	9.75308	I.20 I.20	0.11593	2.80	30	9.76502	1.15	0.14398	2.80
32	.75332	1.20	.11649	2.75	32	.76526	1.20	.14455	2.85
34	.75356	1.20	.11704	2.80	34	.76550	1.15	.14512	2.80
36 38	.75380 .75404	1.20	.11760	2.80	36 38	.76573 .76597	1.20	.14505	2.85
40	9.75428	1.20	0.11871	2.75	40	9.76620	1.15	0.14682	2.85
42	·75452	1.20	.11927	2.80	42	.76644	1.20	.14738	2.80
44	.75476	I.20 I.20	.11983	2.80	44	.76668	1.20	.14795	2.85
46	.75500	1.20	.12039	2.75	46	.76691	1.15	.14852	2.85
48	.75524	1.25	.12094	2.80	48	.76715	1.15	.14909	2.85
50	9.75549	1.20	0.12150	2.80	50 52	9.76738 .76762	1.20	0.14966	2.80
52 54	-75573 -75597	1.20	.12262	2.80	54	.76785	1.15	.15022	2.85
56	.75621	1.20	.12318	2.80	56	.76809	1.20	.15136	2.85
58	.75645	I.20	.12373	2.75 2.80	58	.76833	1.20	.15193	2.85
60	9.75669	1.15	0.12429	2.80	60	9.76856	1.20	0.15250	2.85
62	.75692	1.20	.12485	2.80	62	.76880	1.15	.15307	2.85
64 66	.75716	1.20	.12541	2.80	64 66	.76903	1.20	.15364	2.85
68	.75740	1.20	.12597	2.80	68	.76927	1.15	.15421	2.85
70	9.75788	1.20	0.12709	2.80	70	.76950 9.76974	1.20	0.15535	2.85
72	.75812	I.20	.12765	2.80	72	.76997	1.15	.15592	2.85
74	.75836	1.20	.12821	2.80	74	.77021	1.15	. 15649	2.85
76	.75860	1.20	.12877	2.80	76	.77044	1.20	.15706	2.90
78 80	.75884	1.20	.12933	2.80	78 80	.77068	1.15	. 15764	2.85
82	9.75908	1.20	0.12989	2.85	82	9.77091	1.15	0.15821	2.85
84	.75932 .75956	1.20	.13046	2.80	84	.77114	1.20	.15878	2.85
86	.75980	I.20 I.15	.13158	2.80	86	.77161	I.15 I.20	.15992	2.85
88	76003	1.13	.13214	2.80	88	.77185	1.15	.16049	2.90
90	9.76027	1.20	0.13270	2.80	90	9.77208	1.15	0.16107	2.85
92	.76051	1.20	.13326	2.85	92	.77231	1.20	.16164	2.85
94 96	.76075	1.20	.13383	2.80	94 96	.77255	1.15	.16221	2.90
98	.76123	1.20	.13439	2.80	98	.7730I	1.15	.16336	2.85
100	9.76146	1.15	0.13551	2.80	100	9.77325	1,20	0.16393	2.05

TABLE XXVI. — (Continued)

				_		67°			
Hun-			5°		Hun-			7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff. .001	Exsec	Diff.
00	9.77325	1.15	0.16393	2.90	00	9.78481	1.15	0.19293	2.95
02	.77348	1.15	.16451	2.85	02	. 78504	1.15	. 19352	2.90
04	.77371	1.20	. 16508	2.90	04 06	. 78527	1.15	.19410	2.95
o6 o8	-77395	1.15	.16566	2.85	08	.78550 .78572	1.10	.19469	2.95
10	.77418 9.77441	1.15	0.16681	2.90	10	9.78595	1.15	0.19587	2.95
12	.77465	1.20	. 16738	2.85	12	.78618	1.15	.19645	2.90
14	.77488	1.15	. 16796	2.90	14	.78641	1.15	.19704	2.95
16	.77511	1.15	. 16853	2.85	16	.78664	I.15 I.15	.19763	2.95 2.95
18	-77534	1.15	.16911	2.90	18	.78687	1.15	.19822	2.95
20	9.77558	1.15	0.16969	2.85	20	9.78710	1.10	0.19881	2.90
22	.77581	1.15	.17026	2.90	22	. 78732	1.15	.19939	2.95
24	.77604	1.15	.17084	2.90	24 26	.78755	1.15	.19998	2.95
26	.77627	1.20	.17142	2.85		.78778	1.15	.20057	2.95
28 30	.77651 9.77674	1.10	.17199	2.90	28 30	.78801 9.78823	1.10	.20116	2.95
32	.77697	1.15	.17315	2.90	32	.78846	1.15	.20234	2.95
34	.77720	1.15	.17372	2.85	34	.78869	1.15	.20293	2.95
36	.77744	I.20	.17430	2.90	36	.78892	1.15	.20352	2.95 3.00
38	.77767	1.15	.17488	2.90	38	.78915	1.15	.20412	2.95
40	9.77790	1.15	0.17546	2.90	40	9.78937	1.15	0.20471	2.95
42	.77813	1.15	.17604	2.90	42	.78960	1.15	. 20530	2.95
44	. 77836	1.15	.17662	2.90	44	.78983	1.10	. 20589	2.95
46	.77859	1.15	.17720	2.90	46	.79005	1.15	.20648	3.00
48	.77882	1.20	.17778	2.90	48	.79028	1.15	0.20767	2.95
50 52	9.77906 .77929	1.15	0.17836	2 90	50 52	9.79051	1.10	.20826	2.95
54	.77952	1.15	.17952	2.90	54	.79096	1.15	.20885	2.95
56	.77975	1.15	.18010	2.90	56	.79119	1.15	.20945	3.00
58	.77998	I.15 I.15	. 18068	2.90	58	.79141	1.15	.21004	3.00
60	9.78021	1.15	0.18126	2.90	60	9.79164	1.15	0.21064	2.95
62	. 78044	1.15	. 18184		62	.79187	1.15	.21123	3.00
64	.78067	1.15	.18242	2.90	64	.79209	1.15	,21183	2.95
66	. 78090	1.15	.18300	2.90	66	. 79232	1.15	.21242	3.00
68	.78113	1.15	. 18358	2.95	68	.79255	1.10	0.21302	2.95
70 72	9.78136 .78159	1.15	0.18417	2.90	70 72	9.79277	1.15	.21421	3.00
74	.78182	1.15	.18533	2.90	74	.79322	1.10	.21480	2.95
76	.78205	1.15	.18592	2.95	76	.79345	1.15	.21540	3.00
78	.78228	1.15	.18650	2.90	78	.79368	1.15	.21600	3.00
80	9.78251	1.15	0.18708		80	9.79390	1.15	0.21659	3.00
82	.78274	1.15	.18767	2.95	82	.79413	1.10	.21719	3.00
84	.78297	1.15	. 18825	2.90	84	.79435	1.15	.21779	3.00
86	.78320	1.15	.18883	2.95	86	.79458	1.10	.21839	2.95
88	.78343	1.15	.18942	2.90	88	.79480	1.15	.21898	3.00
90 92	9.78366 .78389	1.15	0.19000	2.95	90 92	9.79503 .79525	1.10	0.21958	3.00
92	.78412	1.15	.19039	2.90	92	.79548	1.15	.22078	3.00
94 96	.78435	1.15	.19117	2.95	94	.79540	1.10	.22138	3.00
98	.78458	1.15	.19234	2.90	98	.79593	1.15	.22198	3.00
100	9.78481	1.15	0.19293	2.95	100	9.79615	1.10	0.22258	3.00

(222)

						69°			
Hun-		68	3°		Hun-)°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.79615		0.22258		00	9.80729		0.25296	
02	.79638	1.15	. 22318	3.00	02	.80751	1.10	. 25357	3.05
04	.79660	I.10 I.15	. 22378	3.00	04	.80773	I.10 I.10	.25419	3.10
06	.79683	1.10	. 22438	3.00	06	.80795	1.10	. 25480	3.10
08	.79705	1.15	. 22498	3.00	08	.80817	1.10	. 25542	3.10
10	9.79728	1.10	0.22558	3.00	10	9.80839	1.10	0.25604	3.10
12	.79750	1.10	.22618	3.00	12	.80861	1.10	.25666	3.05
14 16	.79772	1.15	.22678	3.05	14 16	.80883	1.10	.25727	3.10
18	.79795 .79817	1.10	.22739	3.00	18	.80905 .80927	1.10	.25789	3.10
20		1.15	0.22859	3.00	20	9.80949	1.10		3.10
	9.79840	1.10		3.05			1.10	0.25913	3.10
22 24	.79862	1.10	. 22920	3.00	22	.80971 .80993	1.10	.25975	3.10
26	.79884	1.15	.23041	3.05	26	.81015	1.10	.26099	3.10
28		1.10	.23101	3.00	28	.81037	1.10	.26161	3.10
30	.79929 9.79952	1.15	0.23161	3.00	30	9.81059	1.10	0.26223	3.10
32	.79974	1.10	.23222	3.05	32	.81080	1.05	.26285	3.10
34	.79996	1.10	.23282	3.00	34	.81102	1.10	.26347	3.10
36	.80019	1.15	.23343	3.05	36	.81124	1.10	.26409	3.10
38	.80041	1.10	.23403	3.00	38	.81146	I.10 I.10	. 26471	3.10
40	9.80063	1.10	0.23464	3.05	40	9.81168	1.10	0.26533	
42	.80085		.23524	3.00	42	.81190		. 26596	3.15
44	.80108	1.15	.23585	3.05	44	.81212	1.10	. 26658	3.10
46	.80130	1.10	. 23646	3.05	46	.81234	1.10	. 26720	3.15
48	.80152	1.15	.23706	3.05	48	.81256	1.05	.26783	3.10
50	9.80175	1.10	0.23767	3.05	50	9.81277	1.10	0.26845	3.10
52	.80197	1.10	.23828	3.05	52	.81299	1.10	.26907	3.15
54	.80219	1.10	. 23889	3.00	54	.81321	1.10	. 26970	3.10
56 58	.80241 .80264	1.15	.23949	3.05	56 58	.81343 .81365	1.10	.27032	3.15
60		1.10		3.05	60		1.10	.27095	3.10
62	9.80286	1.10	0.24071	3.05	62	9.81387	1.05	0.27157	3.15
64	.80308 .80330	1.10	.24132	3.05	64	.81408 .81430	1.10	.27220	3.15
66	.80352	1.10	.24254	3.05	66	.81452	1.10	.27345	3.10
68	.80375	1.15	.24315	3.05	68	.81474	1.10	.27408	3.15
70	9.80397	1.10	0.24376	3.05	70	9.81496	1.10	0.27471	3.15
72	80419	1.10	.24437	3.05	72	.81517	1.05	.27533	3.10
74	.80441		.24498	3.05	74	.81539		.27596	3.15
76	.80463	1.10	.24559	3.05	76	.81561	I.10 I.10	. 27659	3.15
78	.80485	1.15	.24621	3.05	78	.81583	1.05	.27722	3.15
80	9.80508	1.10	0.24682	3.05	80	9.81604	1.10	0.27785	3.15
82	.80530	1.10	. 24743	3.05	82	.81626	1.10	.27848	3.15
84	.80552	1.10	.24804	3.10	84 1	.81648	1.10	.27911	3.15
86	.80574	1.10	.24866	3.05	86	.81670	1.05	.27974	3.15
88	.80596	1.10	.24927	3.05	88	.81691	1.10	.28037	3.15
90 92	9.80618	1.10	0.24988	3.10	90 92	9.81713	1.10	0.28100	3.15
	.80662	1.10		3.05	94	.81756	1.05	.28226	3.15
94 96	.80684	1.10	.25111	3.10	94 96	.81778	1.10	.28220	3.20
98	.80707	1.15	.25234	3.05	98	.81800	1.10	.28353	3.15
100	9.80729	1.10	9.25296	3.10	100	9.81821	1.05	0.28416	3.15

		77)°				7	L°	
Hun-			J-	. To:es	Hun-				Diff.
dredths	Vers	Diff. .001	Exsec	Diff.	dredths	Vers	Diff. .001	Exsec	.001
00	9.81821	1.10	0.28416	3.15	00	9.82894	1.05	0.31630	3.25
02	.81843	1.10	. 28479	3.20	02	.82915	1.05	.31695	3.25
04	.81865	1.10	. 28543	3.15	04	.82936	1.10	.31760	3.30
06	.81886	1.10	. 28606	3.20	06	.82958	1.05	.31826	3.25
08	.81908	1.05	.28670	3.15	08	.82979	1.05	.31891	3.30
10 12	9.81929 .81951	1.10	0.28733	3.20	10 12	9.83000	1.05	0.31957	3.25
		1.10	.28860	3.15		.83042	1.05	_	3.30
14 16	.81973 .81994	1.05	.28924	3.20	14 16	.83042	1.10	.32088	3.25
18	.82016	1.10	.28987	3.15	18	.83085	1.05	.32219	3.30
20	9.82037	1.05	0.29051	3.20	20	9.83106	1.05	0.32285	3.30
22	.82058	1.05	. 29114	3.15	22	.83127	1.05	.32350	3.25
34	.82080	1.10	.29114	3.20	24	.83148	1.05	.32350	3.30
26	.82102	1.10	.29242	3.20	26	.83169	1.05	.32482	3.30
28	.82124	1.10	,29306	3.20	28	.83191	1.10	.32548	3.30
30	9.82145	1.05	0.29370	3.20	30	9.83212	1.05	0.32614	3.30
32	.82167	1.10	.29434	3.20	32	.83233	1.05	.32680	3.30
34	.82188	1.05	.29498	3.20	34	.83254	1.05	.32746	3.30
36	.82210	1.10	.29562	3.20	36	.83275	1.05	.32812	3.30
38	.82231	1.05	. 29626	3.20	38	.83296	1.05	.32878	3.30
40	9.82253	1.05	0.29690	3.20	40	9.83317	1.05	0.32944	3.30
42	.82274	-	.29754		42	.83338	-	.33010	
44	.82296	I.10 I.05	. 29818	3.20	44	.83359	1.05	.33076	3.30
46	.82317	1.10	. 29882	3.20	46	.83381	1.05	.33142	3.35
48	.82339	1.05	.29946	3.20	48	.83402	1.05	.33209	3.30
50	9.82360	1.05	0.30010	3.25	50	9.83423	1.05	0.33285	3.30
52	.82381	1.10	.30075	3.20	52	.83444	1.05	.33341	3.35
54	.82403	1.05	.30139	3.20	54	.83465	1.05	.33408	3.30
56	.82424 .82446	1.10	.30203	3.25	56 58	.83486 .83507	1.05	·33474 ·33541	3.35
58		1.05		3.20	60		1.05		3.30
60	9.82467	1.10	0.30332	3.25		9.83528	1.05	0.33607	3.35
62	.82489	1.05	.30397	3.20	62	.83549	1.05	.33674	3.35
64 66	.82510 .82531	1.05	.30461 .30526	3.25	64 66	.83570 .83591	1.05	.33741	3.30
68		1.10		3.20	68	.83612	1.05	.33874	3.35
70	.82553 9.82574	1.05	.30590 0.30655	3.25	70	9.83633	1.05	0.33941	3.35
70	.82595	1.05	.30720	3.25	72	.83654	1.05	.34008	3.35
74	.82617	1.10	.30784	3.20	74	.83675	1.05	.34075	3.35
76	.82638	1.05	.30849	3.25	76	.83696	1.05	.34142	3.35
78	.82660	1.10	.30914	3.25	78	.83717	1.05	.34209	3.35
80	9.82681	1.05	0.30979	3.25	80	9.83738	1.05	0.34276	3.35
82	.82702	1.05	.31044	3.25	82	.83759	1.05	·34343	3.35
84	.82724	1.10	.31109	3.25	84	.83780	1.05	.34410	3.35
86	.82745	1.05	.31174	3.25 3.25	86	.83800	1.05	-34477	3.35 3.35
88	.82766	- 1	.31239		88	.83821		.34544	3.35
90	9.82787	1.05	0.31304	3.25 3.25	90	9.83842	1.05	0.34611	3.35
92	.82809	1.10	.31369	3.25	92	.83863	1.05	.34679	3.40
94	.82830	1.05	.31434	3.25	94	.83884	1.05	.34746	3.40
96	.82851	1.10	.31499	3.25	96	.83905	1.05	.34814	3.35
98	.82873	1.05	.31564	3.30	98	.83926	1.05	.34881	3.35
100	9.82894		0.31630		100	9.83947		0.34948	

		7	'2°				73	20	
Hun- dredths		Diff.		Diff.	Hun- dredths		Diff.		Diff.
	Vers	.001	Exsec	.001		Vers	.001	Exsec	.001
00	9.83947	1.05	0.34948	3.40	00	9.84981	1.00	0.38387	3.50
02	.83968	1.00	. 35016	3.40	02	.85001	1.00	. 38457	3.50
04 06	.83988	1.05	.35084	3.35	04 06	.85021 .85042	1.05	.38527	3.50
08	.84030	1.05	.35219	3.40	08	.85062	1.00	.38668	3.55
10	9.84051	1.05	0.35287	3.40	10	9.85083	1.05	0.38738	3.50
12	.84072	1.05	· 3 5354	3.35 3.40	12	.85104	I.05 I.00	.38809	3.55 3.50
14	.84093	1.00	.35422	3.40	14	.85124	1.00	.38879	3.50
16 18	.84113 .84134	1.05	.35490	3.40	16 18	.85144 .85165	1.05	.38949	3.55
20	9.84155	1.05	0.35626	3.40	20	9.85185	1.00	0.39090	3.50
22	.84176	1.05	.35694	3.40	22	.85205	1.00	.39161	3.55
24	.84197	I.05 I.00	.35762	3.40	24	.85226	1.05	.39232	3.55
26	.84217	1.05	.35830	3.40	26	.85246	1.00	.39303	3.55 3.50
28	.84238	1.05	.35899	3.40	28	.85267	1.00	-39373	3.55
30 32	9.84259	1.05	0.35967 .36035	3.40	30 32	9.85287	1.00	0.39444	3.55
34	.84300	1.00	.36103	3.40	34	.85328	1.05	.39515	3.55
36	.84321	1.05	.36172	3.45	36	.85348	1.00	.39667	3.55
38	.84342	1.05	.36240	3.40	38	.85368	I.00 I.05	.39728	3.55 3.60
40	9.84363	1.00	0.36309	3.40	40	9.85389	1.00	0.39800	3.55
42	.84383	1.05	.36377	3.45	42	.85409	1.00	.39871	3.55
44 46	.84404 .84425	1.05	. 36446	3.40	44 46	.85429 .85450	1.05	.39942	3.55
48	.84445	1.00	.36583	3.45	48	.85470	1.00	.40013	3.60
50	9.84466	1.05	0.36652	3.45	50	9.85490	1.00	0.40156	3.55
52	.84487	1.05	.36721	3.45	52	.85511	1.05	.40228	3.60
54	.84507	1.05	. 36789	3.45	54	.85531	1.00	.40299	3.60
56 58	.84528 .84549	1.05	.36858	3.45	56 58	.85551	1.05	.40371	3.60
60	9.84569	1.00	0.36927	3.45	60	.85572	1.00	.40443	3.55
62	.84590	1.05	.37965	3.45	62	9.85592	1.00	.40586	3.60
64	.84611	1.05	.37134	3.45	64	.85632	1.00	.40658	3.60
66	.84631	1.00	.37204	3.50	66	.85653	1.05	.40730	3.60 3.60
68	.84652	1.00	.37273	3.45	68	.85673	1.00	.40802	3.60
70 72	9.84672	1.05	0.37342	3.45	70	9.85693	1.00	0.40874	3.60
74	.84714	1.05	.37411	3.50	72	.85713	1.00	.40946	3.60
76	.84734	1.00	.37481	3.45	74 76	.85733	1.05	.41018	3.60
78	.84755	1.05	.37619	3.45 3.50	78	.85774	1.00	.41163	3.65 3.60
80	9.84775	1.05	0.37689	3.50	80	9.85794	1.00	0.41235	3.60
82	.84796	1.00	.37759	3.45	82	.85814	1.00	.41307	3.65
8 ₄ 86	.84816 .84837	1.05	.37828	3.50	84 86	.85834	1.05	.41380	3.60
88	.84857	1.00	.37898	3.50	88	.85855 .85875	1.00	.41452	3.65
90	9.84878	1.05	0.38037	3.45	90	9.85895	1.00	0.41598	3.65
92	.84899	I.05 I.00	.38107	3.50	92	.85915	1.00	.41670	3.60 3.65
94	.84919	1.05	.38177	3.50	94	.85935	1.00	.41743	3.65
96 98	.84940	1.00	.38247	3.50	96	.85955	1.00	.41816	3.65
98 100	9.84981	1.05	.38317	3.50	98	.85975	1.05	.41889	3.65
100	9.84981		0.38387		100	9.85996		0.41962	

TABLE XXVI. — (Continued)

						75°				
Hun-		74	ľ.		Hun-			5°		
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.	
00	9.85996	1.00	0.41962	3.65	00	9.86992	1.00	0.45693	3.80	
02	.86016	1.00	. 42035	3.65	02	.87012	1.00	.45769	3.85	
04 06	.86036 .86056	1.00	.42108 .42181	3.65	04 06	.87032 .87052	1.00	.45846	3.80	
08	.86076	1.00		3.65	08	.87032	-95	.45922	3.85	
10	9.86096	1.00	.42254 0.42328	3.70	10	9.87091	1.00	. 45999 o. 46075	3.80	
12	.86116	1.00	.42401	3.65	12	.87111	1.00	.46152	3.85	
14	.86136	1.00	. 42474	3.65	14	.87131	1.00	.46228	3.80	
16	.86156	I.00 I.00	. 42548	3.70 3.65	16	.87150	.95	.46306	3.90	
18	.86176	1.00	.42621	3.70	18	.87170	1.00	. 46383	3.85	
20	9.86196	1.00	0.42695	3.65	20	9.87190	.95	0.46460	3.85	
22	.86216	1.00	.42768	3.70	22	.87209	1.00	. 46537	3.85	
24 26	.86236 .86257	1.05	.42842	3.70	24 26	.87229 .87249	1.00	.46614	3.85	
28	.86277	1.00	.42910	3.70	28	.87268	-95	.46769	3.90	
30	9.86297	1.00	0.43064	3.70	30	9.87288	1.00	0.46846	3.85	
32	.86317	1.00	.43138	3.70	32	.87308	1.00	.46923	3.85	
34	.86337	1.00	.43212	3.70	34	.87327	.95	.47001	3.90	
36	.86357	I.00	. 43286	3.70	36	.87347	I.00	.47079	3.90	
38	.86377	1.00	.43360	3.70	38	.87367	-95	.47156	3.90	
40	9.86397	1.00	0.43434	3.75	40	9.87386	1.00	0.47234	3.90	
42	.86417	.95	.43509	3.70	42	.87406	.95	.47312	3.90	
44 46	.86436 .86456	1.00	. 43583	3.70	44 46	.87425 .87445	1.00	.47390	3.90	
	.86476	1.00	43732	3.75	48	.87465	1.00	.47546	3.90	
48 50	9.86496	1.00	0.43806	3.70	50	9.87484	-95	0.47624	3.90	
52	.86516	I.00	.43881	3.75	52	.87504	1.00	.47702	3.90	
54	.86536	1.00	. 43956	3.75	54	.87523	1.00	.47781	3.95	
56	.86556	I.00	.44030	3.70 3.75	56	.87543	.95	.47859	3.90	
58	.86576	1.00	.44105	3.75	58	.87562	1.00	.47938	3.90	
60	9.86596	1.00	0.44180	3.75	60	9.87582	.95	0.48016	3.95	
62	.86616	1.00	-44255	3.75	62	.87601	1.00	.48095	3.90	
64 66	.86636 .86656	I.00	.44330	3.75	64 66	.87621 .87641	1.00	.48173	3.95	
68	.86675	.95	.44481	3.80	68	.87660	-95	.48331	3.95	
70	9.86695	1.00	0.44556	3.75	70	9.87680	1.00	0.48410	3.95	
72	.86715	I.00	.44631	3.75	72	.87699	.95	.48489	3.95	
74	.86735	1.00	.44706	3.75 3.80	74	.87719	.95	. 48568	3.95	
76	.86755	1.00	.44782	3.80	76	.87738	1.00	.48647	4.00	
78	.86775	1.00	. 44857	3.80	78	.87758	-95	.48727	3.95	
80	9.86795	.95	0.44933	3.80	80	9.87777	.95	0.48806	3.95	
8 ₂ 8 ₄	.86814 .86834	1.00	.45009	3.75	82 84	.87796 .87716	1.00	. 48885	4.00	
86	.86854	1.00	.45084	3.80	86	.87835	-95	.49044	3.95	
88	.86874	1.00	.45236	3.80	88	.87855	1.00	.49124	4.00	
90	9.86894	1.00	0.45312	3.80	90	9.87874	1.00	0.49204	4.00	
92	.86913	.95 1.00	.45388	3.80	92	.87894	.95	.49284	4.00	
94	.86933	1.00	. 45464	3.80	94	.87913	1.00	.49364	4.00	
96	.86953	1.00	.45540	3.85	96	.87933	.95	49444	4.05	
98	.86973	.95	.45617	3.80	98 100	.87952	.95	.49525	3.95	
100	9.86992		0.45693		100	9.87971	l	0.49604		

		76	0			77°				
Hun-		Diff.		Diff.	Hun-		Diff.		Diff.	
dredths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.00I	
00	9.87971	1.00	0.49604	4.00	00	9.88933	.95	0.53724	4.25	
02	.87991	.95	. 49684	4.00	02	.88952	.95	. 53809	4.25	
04	.88010	1.00	. 49764	4.05	04	.88971	.95	-53894	4.25	
06	.88030	-95	.49845	4.00	o6	.88990	.95	·53979	4.25	
08	.88049	.95	.49925 0.50006	4.05	08	.89009 9.89028	.95	.54064	4.25	
10	9.88o68 .88o88	1.00	.50087	4.05	12	.89047	.95	.54234	4.25	
	.88107	.95	.50167	4.00	14	.89066	.95	.54320	4.30	
14 16	.88126	.95	.50248	4.05	16	.89085	-95	.54405	4.25	
18	.88146	1.00	. 50329	4.05	18	.89104	.95	.54491	4.30	
20	9.88165	.95	0.50410	4.05	20	9.89123	.95	0.54576	4.25	
22	.88184	.95	.50491	4.05	22	.89142	.95	. 54662	4.30	
24	.88204	1.00	.50572	4.05	24	.89161	-95	.54748	4.30	
26	.88223	.95	. 50654	4.10	26	.89180	.95 .95	. 54834	4.30	
28	.88242	1.00	.50735	4.10	28	.89199	.95	.54920	4.30	
30	9.88262	.95	0.50817	4.05	30	9.89218	.95	0.55006	4.30	
32	.88281	.95	.50898	4.10	32	.89237	.95	.55092	4.35	
34 36	.88300	1.00	.50980	4.05	34 36	.89256 .89275	.95	.55179	4.30	
38	.88339	-95	.51143	4.10	38	.89294	-95	.55352	4.35	
40	9.88358	.95	0.51225	4.10	40	9.89313	-95	0.55439	4.35	
42	.88377	.95	.51307	4.10	42	.89332	.95	-55525	4.30	
44	.88397	1.00	.51389	4.10	44	.89351	-95	.55612	4.35	
46	.88416	-95	.51471	4.10	46	.89369	.90	.55699	4·35 4·35	
48	.88435	.95	.51553	4.10	48	.89388	.95	.55786	4.40	
50	9.88454	.95	0.51636	4.15	50	9.89407	. 95 . 95	0.55874	4.40	
52	.88474	.95	.51718	4.15	52	.89426	.95	.55961	4.35	
54	.88493 .88512	.95	.51801	4.10	54 56	.89445	.95	.56048	4.40	
56 58	.88531	.95	.51966	4.15	58	.89464 .89483	.95	.56224	4.40	
60	9.88550	-95	0.52049	4,15	60	9.89502	.95	0.56311	4.35	
62	.88570	1.00	.52132	4.15	62	.89520	.90	.56399	4.40	
64	.88589	.95	.52215	4.15	64	.89539	.95	.56487	4.40	
66	.88608	.95	.52298	4.15	66	.89558	-95	.56575	4.40	
68	.88627	.95	.52381	4.15	68	.89577	.95	.56663		
70	9.88646	· 95	0.52464	4.15	70	9.89596	·95	0.56752	4.45	
72	.88665	1.00	.52547	4.20	72	.89615	.90	.56840	4.45	
74	.88685	.95	.52631	4.15	74	.89633	.95	. 56929	4.40	
76 78	.88704 .88723	.95	.52714	4.20	76 78	.89652 .89671	.95	.57017	4.45	
80	9.88742	-95	0.52882	4.20	80	9.89690	.95	0.57195	4 - 45	
82	.88761	.95	.52966	4.20	82	.89709	.95	.57284	4.45	
84	.88780	-95	.53049	4.15	84	.89727	.90	.57373	4.45	
86	.88799	-95	.53133	4.20	86	.89746	.95	.57462	4.45	
88	.88818	.95	.53218	4.25	88	.89765	-95	-57551	4.45	
90	9.88838	.95	0.53302	4.20	90	9.89784	.95	0.57641	4.45	
92	.88857	.95	.53386	4.20	92	.89802	.95	.57730	4.50	
94	.88876	.95	-53470	4.25	94	.89821	.95	.57820	4.50	
96 98	.88895	.95	·53555 ·53639	4.20	96 98	.89840 .89859	.95	.57910	4.45	
100	9.88933	.95		4.25	100		.90	0.58089	4.50	
100	9.00933		0.53724		. 100	9.89877	1	0.50009		

77		7:	3°		TT		79	9°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	Exsec	Diff.
00	9.89877		0.58089		00	9.90805		0.62745	
02	.89896	.95	.58180	4.55	02	.90823	.90	.62842	4.85
04	.89915	.95	.58270	4.50	04	.90842	.95	.62938	4.80
06	.89933	.95	. 58360	4.55	06	.90860	.90	. 63036	4.80
08	.89952	.95	.58451	4.50	08	. 90879	.90	.63132	4.85
10 12	9.89971	.95	.58632	4.55	10 12	9.90897	.90	.63326	4.85
14	.90008	.90	.58723	4.55	14	.90913	-95	.63423	4.85
16	.90003	-95	.58814	4.55	16	.90934	.90	.63521	4.90
18	.90046	-95	.58905	4.55	18	.90970	.90	.63618	4.85
20	9.90064	.90	0.58996	4.55	20	9.90989	-95	0.63716	4.90
22	.90083	-95	.59087	4.55	22	.91007	.90	.63814	4.90
24	.90102	-95 .90	.59178	4.55 4.60	24	.91025	.90	.63912	4.90
26	.90120	- 95	.59270	4.60	26	.91044	.90	.64010	4.90
28	.90139	.90	. 59362	4.55	28	.91062 9.91080	.90	.64108	4.95
30 32	9.90157	-95	0.59453 .59545	4.60	30 32	.91099	.95	0.64207	4.90
34	.90195	-95	.59637	4.60	34	.91117	.90	.64404	4.95
36	.90213	.90	.59729	4.60	36	.91135	.90	.64503	4.95
38	.90232	.95 .90	.59822	4.65 4.60	38	.91153	.90	.64602	4.95
40	9.90250	.95	0.59914	4.65	40	9.91172	.90	0.64701	4.95 5.∞
42	.90269	.95	.60007	4.60	42	.91190	.90	.64801	5.05
44	.90288	.90	.60099	4.65	44	.91218	.90	.64900	5.00
46	.90306	.90	.60192	4.60	46	.91226	.95	.65000	5.00
48 50	.90324 9.90343	-95	.6c284 0.6c378	4.70	48 50	.91245 9.91263	.90	0.65200	5.00
52	.90362	. 95	.60471	4.65	50	.91281	.90	.65300	5.00
54	.90380	.90	.60564	4.65	54	.91299	.90	.65400	5.00
56	.90399	.95	.60658	4.70	56	.91317	.90	.65500	5.00
58	.90417	.90 .95	.60751	4.65	58	.91336	·95	.65601	5.05
60	9.90436	.95	0.60845	4.65	60	9.91354	.90	0.65702	5.00
62	.90455	.90	.60938	4.70	62	.91372	.90	.65802	5.05
64 66	.90473	.95	.61032	4.70	64	.91390	.90	.65903	5.05
68	.90492	.90	.61126	4.75	66	.91408	-95		5.05
70	.90510 9.90529	.95	.61221 0.61315	4.70	68 70	.91427 9.91445	.90	.66106 0.66207	5.05
72	.90547	.90	.61409	4.70	72	.91463	.90	.66309	5.10
74	.90565	.90	.61504	4.75	74	.91481	.90	.66411	5.10
76	.90584	· 95 · 90	.61599	4.75 4.70	76	.91499	.90	.66513	5.10
78	.90602	.95	.61693	4.75	78	.91517	-95	.66615	5.10
80	9.90621	.90	0.61788	4.75	80	9.91536	.90	0.66717	5.15
82 84	.90639	.95	.61883	4.80	82	.91554	.90	.66820	5.10
86	.90658	.90	.61979 .62074	4.75	84 86	.91572	.90	.67025	5.15
88	.90695	.95	.62169	4.75	88	.91595	. 90	.67128	5.15
90	9.90713	. 90	0.62265	4.80	90	9.91626	.90	0.67231	5.15
92	.90731	.90 .95	.62361	4.80	92	.91644	.90 .90	.67335	5.20 5.15
94	.90750	.90	.62457	4.80	94	.91662	.90	.67438	5.20
96 98	.90768	-95	.62543	4.80	96	.91680	.90	.67542	5.20
100	.90787	.90	.62649	4.80	98	.91698	.90	.67646	5.15
100	9.90805		0.62745		100	9.91716		0.67749	

		86)°			81°					
Hun- dredths		Diff.	n	Diff.	Hun- dredths	77	Diff.	77	Diff.		
	Vers	.001	Exsec	.001		Vers	.001	Exsec	.001		
00	9.91716	-95	0.67749	5.25	00	9.92612	.90	0.73179	5.65		
02	.91735	.90	.67854 .67958	5.20	02 04	.92630	.85	.73292	5.70		
04 06	.91753	.90	.68062	5.20	04	.92647 .92665	.90	.73406 .73520	5.70		
08	.91789	.90	.68167	5.25	08	.92683	.90	.73634	5.70		
10	9.91807	.90	0.68272	5.25	10	9.92701	.90	0.73749	5.75		
12	.91825	.90 .90	.68377	5.25 5.25	12	.92718	.85	.73863	5.70 5.75		
14	.91843	.90	.68482	5.25	14	.92736	.90	.73978	5.75		
16	.91861 .91879	.90	.68587	5.30	16 18	.92754 .92771	.85	.74093	5.75		
20	9.91897	.90	0.68799	5.30	20	9.92789	.90	0.74324	5.80		
22	.91915	.90	.68904	5.25	22	.92807	.90	.74440	5.80		
34	.91913	.90	.69010	5.30	24	.92824	.85	.74556	5.80		
26	.91951	.90	.69117	5.35	26	92842	.90	.74671	5.85 5.85		
28	.91969	.90	.69223	5.30	28	.92860	.90	.74788	5.85		
30	9.91987	.90 .90	0.69330	5.35 5.30	30	9.92877	.90	0.74905	5.85		
32	.92005	.90	.69436	5.35	32	.92895	.90	.75022	5.85		
34 36	.92023 .92041	.90	.69543	5.35	34 36	.92913	.85	.75139 .75256	5.85		
38	.92059	.90	.69758	5.40	38	.92948	.90	.75373	5.85		
40	9.92077	.90	0.69865	5.35	40	9.92966	.90	0.75491	5.90		
42	.92095	.90	.69973	5.40	42	.92983	.85	.75609	5.90		
44	.92111	.90	.70080	5.35 5.45	44	.93001	.90	.75727	5.90		
46	.92130	.90	.70189	5.40	46	.93018	.90	.75846	5.95		
48	.92148 9.92166	.90	.70297	5.40	48	.93036	.90	.75965 o.76083	5.90		
50 52	.92184	.90	.70514	5.45	50 52	9.93054	.85	.76203	6.00		
54	.92202	.90	.70623	5.45	54	.93089	.90	.76322	5.95		
56	.92220	.90	.70732	5.45	56	.93106	.85	.76442	6.00		
58	.92238	.90	.70841	5.45 5.45	58	.93124	.90	.76561	5.95 6.05		
60	9.92256	.90	0.70950	5.50	60	9.93142	.85	0.76682	6.00		
62	.92274	.85	.71060	5.45	62	.93159	.85	.76802	6.00		
64 66	.92291 .92309	.90	.71169	5.50	64 66	.93176 .93194	.90	.76922	6.05		
68	.92327	.90	.71389	5.50	68	.93194	.90	.77165	6.10		
70	9.92345	.90	0.71500	5.55	70	9.93229	.85	0.77286	6.05		
72	.92363	.90	.71610	5.50 5.55	72	.93247	.90	.77407	6.05		
74	.92381	.85	.71721	5.55	74	.93264	.90	.77529	6.10		
76 78	.92398	.90	.71832	5.55	76	.93282	.85	.77651	6.15		
78 80	.92416	.90	.71943	5.55	78 80	.93299	.90	.77774	6.10		
82	9.92434	.90	.72166	5.60	82	9.93317	.85	0.77896	6.15		
84	.92452	.90	.72100	5.60	84	·93334 ·93352	.90	.78142	6.15		
86	.92487	.85	.72389	5.55	86	.93369	.85	.78265	6.15		
88	.92505	.90	.72502	5.65	88	.93387	.90	. 78389	6.20		
90	9.92523	.90	0.72614	5.60	90	9.93404	.85	0.78513	6.20		
92	.92541	.90	.72726	5.65	92	.93422	.85	.78637	6.20		
94 96	.92559 .92576	.85	.72839	5.65	94 96	.93439 .93457	.90	.78761	6.25		
98	.92570	.90	.73065	5.65	98	.93457	.85	.79011	6.25		
100	9.92612	.90	0.73179	5.70	100	9.93492	.90	0.79136	6.25		

		9,	2 °				9	3°			
Hun-		Diff.	2	Diff.	Hun-		Diff.		Diff.		
dredths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001		
00	9.93492	.85	0.79136	6,25	00	9.94356	.85	0.85766	7.05		
02	.93509	.85	.79261	6.30	02	-94373	.85	.85907	7.05		
04 06	.93526	.90	.79387 .79513	6.30	04 06	.94390	.85	.86048 .86190	7.10		
08	·93544	.85	.79513	6.35	08	.94424	.85	.86332	7.10		
10	.93561 9.93579	.90	0.79766	6.30	10	9.94442	.90	0.86474	7.10		
12	.93596	.85	.79893	6.35	12	.94459	.85 .85	.86616	7.10		
14	.93614	.90	.80020	6.35	14	.94476	.85	.86759	7.20		
16	.93631	.85	.80147	6.40	16	-94493	.85	.86903	7.15		
18	.93648	.90	.80275	6.40	18 20	.94510	.85	.87046	7.20		
20	9.93666	.85	0.80403	6.40		9.94527	.85	0.87190	7.25		
22 24	.93683	.85	.80531 .80659	6.40	22 24	.94544 .94561	.85	.87470	7.25		
26	.93718	.90	.80788	6.45	26	.94578	.85	.87625	7.25		
28	93735	.85	.80917	6.45	28	-94595	.85	.87770	7.25		
30	9.93752	.85	0.81046	6.45 6.50	30	9.94612	.85 .85	0.87916	7.30		
32	.93770	.90 .85	.81176	6.50	32	.94629	.85	.88062	7.35		
34	.93787	.85	.81306	6.50	34	.94646	.85	.88209	7.35		
36 38	.93804 .93822	.90	.81436 .81567	6.55	36 38	.94663 .94680	.85	.88356	7.40		
40	9.93839	.85	0.81697	6.50	40	9.94697	.85	0.88651	7.35		
42	.93856	.85	.81829	6.60	42	.94714	.85	.88800	7.45		
42	.93874	.90	.81960	6.55	44	.94731	.85	.88948	7.40		
46	.93891	.85	.82092	6.60 6.60	46	.94748	.85 .85	.89097	7.45		
48	.93908	.85	.82224	6.60	48	.94765	.85	.89247	7.50		
50	9.93926	.90 .85	0.82356	6.60	50	9.94782	.85	0.89397	7.50		
52	-93943	.85	.82488	6.65	52	-94799	.85	.89547	7.50		
54 56	.93960 .93977	.85	.82621 .82755	6.70	54 56	.94816 .94833	.85	.89697 .89848	7.55		
58	.93977	.90	.82888	6.65	58	.94850	.85	.90000	7.60		
60	9.94012	.85	0.83022	6.70	60	9.94867	.85	0.90152	7.60		
62	.94029	.85	.83156	6.70	62	.94884	.85	,90304	7.60		
64	.94047	.90	.83290	6.70	64	.94901	.85	.90457	7.65		
66	.94064	.85	.83425	6.75	66	.94918	.85	.90610	7.70		
68	.94081	.85	.83560	6.80	68	.94935	.85	.90764	7.70		
70 72	9.94098	.85	0.83696	6.85	70 72	9.94952 .94969	.85	0.90918	7.70		
74	.94113	.90	.83968	6.85	74	.94986	.85	.91227	7.75		
76	.94133	.85	.84104	6.80	76	.95003	.85	.91383	7.80		
78	.94167	.85 .85	-84241	6.85	78	.95020	.85	.91538	7.75		
80	9.94184	.85	0.84378	6.85	80	9.95037	.80	0.91694	7.85		
82	.94201	.90	.84515	6.90	82	.95053	.85	.91851	7.85		
84	.94219	.85	.84653	6.90	84 86	.95070	.85	.92008	7.90		
86	.94236	.85	.84791	6.90	88	.95087	.85	.92100	7.90		
88 90	.94253 9.94270	.85	.84929 o.85068	6.95	90	.95104 9.95121	.85	0.92482	7.90		
92	.94270	.85	.85207	6.95	92	.95138	.85	.92641	7.95		
94	.94304	.85	.85346	6.95	94	.95155	.85	.92801	8.00		
96	.94322	.90 .85	.85486	7.00	96	.95171	.80	.92961	8.00		
98	-94339	.85	.85626	7.00	98	.95188	.85	.93121	8.05		
100	9.94356		0.85766		100	9.95205		0.93282			

		84	0				85	0	85°			
Hun- dredths		Diff. 1		Diff.	Hun- dredths	77	Diff.		Diff.			
dredths	Vers	.001	Exsec	.001		Vers	.001	Exsec	.001			
00	9.95205	.85	0.93282	8.05	00	9.96040	.80	1.02010	9.50			
02	.95222	.85	-93443	8.10	02 04	.96056 .96073	.85	.02200	9.55			
-04 -06	.95239 .95256	.85	.93605	8.10	06	.96089	.80	.02583	9.60			
08	.95272	.80	.93930	8.15	08	.96106	.85	.02775	9.60			
10	9.95289	.85	0.94093	8.15	10	9.96122	.80 .85	1.02968	9.65			
12	.95306	.85	.94257	8.20	12	.96139	.80	.03162	9.70			
14	.95323	.85	.94421	8.25	14	.96155	.85	.03356	9.75			
16 18	.95340	.80	.94586 .94751	8.25	18	.96172	.80	.03551	9.80			
20	9.95373	.85	0.94917	8.30	20	9.96205	.85	1.03944	9.85			
22	.95390	.85	.95183	8.30	22	,96221	.80	.04141	9.85			
24	.95407	.85 .85	.95250	8.35 8.35	24	.96238	.85 .80	.04339	9.90			
26	.95424	.80	.95417	8.40	26	.96254	.85	.04538	10.00			
28	.95440	.85	.95585	8.45	28	.96271 9.96287	.80	1.04938	10.00			
30 32	9.95457 .95474	.85	0.95754	8.40	30 32	.96304	.85	.05140	10.10			
34	.95491	.85	.96092	8.50	34	.96320	.80	.05342	10.10			
36	.95507	.80	.96262	8.50 8.50	36	.96337	.85	.05544	10.10			
38	.95524	.85 .85	.96432	8.55	38	.96353	.80	.05748	10.25			
40	9.95541	.80	0.96603	8.60	40	9.96369	.85	1.05953	10.25			
42	-95557	.85	.96775	8.60	42	.96386	.80	.06158	10.30			
44 46	.95574 .95591	.85	.96947	8.65	44 46	.96419	.85	.06571	10.35			
48	.95608	.85	.97293	8.65	48	.96435	.80	.06779	10.40			
50	9.95624	.8o .85	0.97467	8.70	50	9.96451	.80	1.06987	10.40			
52	.95641	.85	.97641	8.75	52	.96468	.80	.07197	10.50			
54	.95658	,80	.97816	8.80	54	.96484	.85	.07407	10.55			
56 58	.95674	.85	.97992	8.80	56 58	.96501	.80	.07830	10.60			
60	9.95708	.85	0.98345	8.85	60	9.96533	.80	1.08043	10.65			
62	.95724	.80	.98522	8.85	62	.96550	.85	.08257	10.70			
64	.95741	.85	.98700	8.90	64	.96566	.80	.08472	10.75			
66	.95758	.80	.98879	8.95	66	.96582	.85	.08687	10.75			
68	.95774	.85	.99058	8.95	68	.96599	.80	1.09121	10.85			
70 72	9.95791	.80	0.99237	9.05	70 72	9.96615	.85	.09340	10.95			
74	.95824	.85	.99599	9.05	74	,96648	.80	.09559	10.95			
76	.95841	.85	.99780	9.05	76	.96664	.80	.09779	11.00			
78	.95857	85	.99963	9.15	78	.96680	.85	.10000	11.15			
80	9.95874	.85	1.00146	9.15	80	9.96697	.80	1.10223	11.15			
82	.95891	.80	.00329	9.20	8 ₂ 8 ₄	.96713	.80	.10446	11.25			
8 ₄ 86	.95907	.85	.00513	9.25	86	.96746	.85	.10896	11.25			
88	.95940	.80	.00883	9.25	88	.96762	.80	.11122	11.30			
90	9.95957	.85	1.01069	9.30	90	9.96778	.80	1.11349	11.35			
92	.95973	.85	.01256	9.35	92	.96795	.80	.11578	11.45			
94	.95990	.85	.01444	9.45	94 96	.96811	.80	.11807	11.55			
96 98	.96007	.80	.01821	9.40	98	.96843	.80	.12038	11.55			
100	9.96040	85	1.02010	9.45	100	9.96860	85	1.12501	11.60			
100	9.90040		1.02010	1	1 200	9.90000	1	, 1,1101				

		86	2.0				-	37°	-
Hun-		-) ·	Diff.	Hun-			7	70.130
dredths	Vers	Diff.	Exsec	.001	dredths	Vers	Diff.	Exsec	Diff.
00	9.96860	.80	1.12501	11.70	00	9.97665	.80	1.25785	15.35
02	.96876	.80	.12735	11.70	02	.97681	.80	.26092	
04	.96892	.80	.12969	11.80	04	.97697	.80	. 26400	15.40
06	.96908	.85	.13205	11.85	06	.97713	.80	.26710	15.60
08	.96925	.80	.13442	11.90	08	.97729	.80	.27022	15.70
10	9.96941	.80	1.13680	11.95	10	9.97745 .97761	.80	1.27336	15.80
14	.96973	.80	.14160	12.05	14		.80		15.95
16	.96990	.85	.14401	12.05	16	·97777 ·97793	.80	.27971	16.00
18	.97006	.80	.14644	12.15	18	.97809	.80	.28614	16.15
20	9.97022	.80 .80	1.14888	12.20	20	9.97825	.80	1.28939	16.25
22	.97038		.15133	12.25	22	.97841		. 29266	16.35
24	.97054	.80	.15379	12.30	24	.97857	.80	.29595	16.45
26	.97071	.80	.15626	12.45	26	.97873	.80	. 29926	16.70
28	.97087	.80	.15875	12.50	28	.97889	.75	.30260	16.80
30	9.97103	.80	1.16125	12.55	30	9.97904	.80	1.30596	16.95
32	.97119	.80	. 16376	12.65	32	.97920	.80	. 30935	17.05
34 36	.97135	.80	.16619	12.70	34 36	.97936	.80	.31276	17.15
38	.97151 .97168	.85	.17138	12.75	38	.97952 .97968	.80	.31019	17.30
40	9.97184	.80	1.17394	12.80	40	9.97984	.80	1.32314	17.45
42	.97200	.80	.17652	12.90	42	.98000	.80	.32665	17.55
44	.97216	.80	.17910	12.90	44	.98016	.80	.33018	17.65
46	.97232	.80 .80	.18172	13.10	46	.98031	.75 .80	-33375	17.85
48	.97248	.80	. 18434	13.10	48	.98047	.80	-33733	17.90
50	9.97264	.80	1.18697	I3.15 I3.20	50	9.98063	.80	1.34095	18.10
52	.97280	.85	.18961	13.35	52	.98079	.80	.34460	18.35
54	-97297	.80	. 19228	13.35	54	.98095	.80	.34827	18.50
56 58	.97313	.80	. 19495	13.45	56 58	.98111	-75	.35197	18.65
60		.80		13.55	60		.80	.35570	18.80
62	9.97345	.80	1.20035	13.60		9.98142	.80	1.35946	18.95
64	.97361 .97377	.80	.20307	13.65	62 64	.98158	.80	.36325	19.10
66	.97311	.80	.20855	13.75	66	.98190	.80	.37092	19.25
68	.97409	.80	.21132	13.85	68	.98205	-75	.37481	19.45
70	9.97425	.80	1.21410	13.90	70	9.98221	.80	1.37872	19.55
72	-97441	.80	.21690	I4.00 I4.05	72	.98237	.80	.38267	19.75
74	.97457	.80	.21971		74	.98253		. 38665	20.10
76	-97473	.80	.22254	14.15 14.25	76	.98268	-75 .80	.39067	20.10
78	.97489	.80	. 22539	14.25	78	.98284	.80	.39472	20.45
80	9.97505	.80	1.22825	14.40	80	9.98300	.80	1.39881	20.60
82	.97521	.80	.23113	14.50	82	.98316	.75	.40293	20.80
84 86	-97537	.80	.23403	14.60	84 86	.98331	.80	.40709	20.95
88	·97553	.80		14.65	88	.98363	.80		21.20
90	.97569 9.97585	.80	.23988 I.24283	14.75	90	9.98379	.80	.41552 1.41979	21.35
92	.97601	.80	.24580	14.85	92	.98394	-75	.42410	21.55
94	.97617	.80	.24878	14.90	94	.98410	.80	.42845	21.75
96	.97633	.80	.25179	14.95	96	.98426	.80	.43284	21.95
98	.97649	.80	.25481	15.10	98	.98442	.80	.43728	22.20
100	9.97665		1.25785	13.20	100	9.98457	. 13	1.44175	22.55

		88	3°		Hun-		89	0	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.98457		1.44175		00	9.99235		1.75050	
02	.98473	.80	.44627	22.60	02	.99251	.80	·75943	44.65
04	.98489	.80 .75	.45084	22.85	04	.99266	.75 .80	. 76853	45.50
06	.98504	.80	-45545	23.25	06	.99282	.75	.77783	47.45
08	.98520 9.98536	.80	.46010 1.46481	23.55	08	.99297 9.99312	.75	.78732 1.79702	48.50
12	.98551	.75	.46956	23.75	12	.99312	.80	.80694	49.60
14	.98567	.80	.47436	24.00	14	.99343	.75	.81707	50.65
16	.98583	.8o -75	.47921	24.25	16	.99359	.8o .75	.82744	51.85
18	. 98598	.80	. 48411	24.75	18	.99374	.75	. 83806	54.40
20	9.98614	.80	1.48906	25.05	20	9.99389	.80	1.84894	55.75
22	.98630	.75	.49407	25.30	22	.99405	.75	.86009	57.15
24 26	.98645	.80	.49913	25.60	26	.99420	.75	.88326	58.70
28	.98676	-75	,50942	25.85	28	.99451	.80	.89531	60.15
30	9.98692	.80	1.51466	26.20	30	9.99466	.75	1.90770	61.95
32	. 98708	.8o .75	.51995	26.45 26.80	32	.99481	.75 .80	.92044	63.70 65.60
34	.98723	.80	.52531	27.10	34	.99497	.75	.93356	67.55
36 38	.98739	.80	.53073	27.40	36 38	.99512	.75	.94707	69.70
40	9.98770	.75	1.54176	27.75	40	.99527	.80	1.97541	72.00
	.98786	.80	.54738	28.10	42	9.99543	-75	.99028	74.35
42 44	.98801	.75	.55306	28.40	44	.99558	.75	2.00568	77.00
46	.98817	.80	.55882	28.80	46	.99589	.80	.02162	79.70 82.75
48	. 98832	.75 .80	.56465	29.15	48	.99604	·75	.03817	85.90
50	9.98848	.80	1.57056	29.55 29.90	50	9.99619	.80	2.05535	89.40
52	.98864	.75	.57654	30.35	52	. 99635	.75	.07323	93.20
54 56	.98879	.80	.58261	30.70	54 56	.99650 .99665	-75	.09187	97.30
58	.98910	-75	.59498	31.15	58	.99680	.75	.13168	101.75
60	9.98926	.80	1.60130	31.60	60	9.99696	.80	2.15302	106.70
62	.98941	.75	.60770	32.00	62	,99711	.75	.17545	112.15
64	.98957	.80	.61419	32.45 32.95	64	.99726	.75 .80	.19909	118.20
66	.98972	.80	.62078	33.45	66	.99742	.75	.22406	132.40
68	.98988	.75	.62747	33.90	68	.99757	.75	.25054	140.90
70 72	9.99003	.80	1.63425	34.45	70 72	9.99772	.75	2.27872	150.60
74	.99034	.75	.64813	34.95	74	.99802	.75	.34118	161.70
76	.99050	.80	.65523	35.50	76	.99818	.80	.37609	174.55
78	.99065	.80	.66245	36.65	78	.99833	.75	.41403	207.70
80	9.99081	-75	1.66978	37.25	80	9.99848	-75	2.45557	229.55
82	. 99096	.80	.67723	37.90	82	.99863	.80	.50148	256.55
84 86	.99112	.75	.68481	38.55	84 86	.99879	-75	.55279	290.70
88	.99127	.80	.70036	39.20	88	.99994	-75	.67803	335.50
90	9.99158	.75	1.70834	39.90	90	9.99924	.75	2.75736	396.65
92	.99174	.80	.71646	40.60	92	.99939	.75 .75	.85443	485.45
94	.99189	.75	.72473	42.15	94	.99954	.80	.97952	881.20
96	.99204	.80	.73316	42.90	96	.99970	.75	3.15576	1505.90
98 100	.99220	.75	.74174	43.80	98	.99985	-75	.45694	
100	9.99235		1.75050		100	0.00000		∞	

TABLE XXVII. — Natural Sines, Tangents, Cotangents and Cosines

10	C:		T		Cohon	- 4	Caria	al .		D D
Deg.	Sin	<u>d.</u>	Tan	d.	Cotan	d.	Cosin	<u>d.</u>		P. P.
0.0	0.0000	17	0.0000	17	inf.		1.0000	0	90.0	
1	0.0017	18	0.0017	18	572.9572		1.0000	0	9	
2	0.0035	17	0.0035	17	286.4777		1.0000	0	8	
3	0.0052	18	0.0052	18	190.9842		1.0000	0	7	
4	0.0070	17	0.0070	17	143.2371		1.0000	0	6	
5	0.0087	18	0.0087	18	114.5887		I.0000	I	5	
6	0.0105	17	0.0105	17	95.4895		0.9999	0	4	
7	0.0122	18	0.0122	18	81.8470		0.9999	0	3	
8	0.0140	17	0.0140	17	71.6151		0.9999	0	2 I	
9	0.0157	18	0.0157	18	63.6567		0.9999	I		
1.0	0.0175	17	0.0175	17	57.2900		0.9998	0	89.0	
I	0.0192	17	0.0192	17	52.0807		0.9998	0	9	1 40
2	0.0209	18	0.0209	18	47.7395		0.9998	I	8	18 1 1.8
3	0.0227	17	0.0227	17	44.0661		0.9997	0	7	1 1.8 2 3.6
4	0.0244	18	0.0244	18	40.9174		0.9997	0	6	3 5.4
5	0.0262	17	0.0262	17	38.1885		0.9997	I	5	4 7.2
6	0.0279	18	0.0279	18	35.8006		0.9996	0	4	5 9.0
. 7	0.0297	17	0.0297	17	33.6935		0.9996	1	3	6 10.8
8	0.0314	18	0.0314	18	31.8205		0.9995	o	2	7 12.6
9	0.0332	17	0.0332	17	30.1446		0.9995	1	I	8 14.4
2.0	0.0349	17	0.0349	18	28.6363		0.9994	1	88.0	9 16.2
1	0.0366	18	0.0367	17	27.2715		0.9993	0	9	
2	0.0384	17	0.0384	18	26.0307		0.9993	I	8	
3	0.0401	18	0.0402	17	24.8978		0.9992	ī	7	
4	0.0419	17	0.0419	18	23.8593	0555	0.9991	I	6	
5	0.0436	18	0.0437	17	22.9038	9555 8821	0.9990	0	5	
6	0.0454	17	0.0454	18	22.0217	8168	0.9990	I	4	
7	0.0471	17	0.0472	17	21.2049	7584	0.9989	1	3	
8	0.0488	18	0.0489	18	20.4465	7062	0.9988	I	2	
9	0.0506	17	0.0507	17	19.7403	6592	0.9987	I	I	
3.0	0.0523	18	0.0524	18	19.0811	6166	0.9986	I	87.0	17
1	0.0541		0.0542		18.4645	5782	0.9985	ī	9	I I.7
2	0.0558	17	0.0559	17	17.8863	5/02 543I	0.9984	I	8	2 3.4
3	0.0576	17	0.0577	17	17.3432	5113	0.9983	I	7	3 5.1
4	0.0593	17	0.0594	18	16.8319	4820	0.9982	I	6	4 6.8 5 8.5
5	0.0610	18	0.0612	17	16.3499	4554	0.0981	1	5	5 8.5 6 10.2
6	0.0628	17	0.0629	18	15.8945	4307	0.9980	1	4	7 11.9
7	0.0645	18	0.0647	17	15.4638	4081	0.9979	I	3	8 13.6
8	0.0663	17	0.0664	18	15.0557	3872	0.9978	1	2	9 15.3
9	0.0680	18	0.0682	17	14.6685	3678	0.9977	I	I	
4.0	0.0698	17	0.0699	18	14.3007	3500	0.9976	2	86.0	
1	0.0715		0,0717		13.9507		0.9974	I	9	
2	0.0732	17	0.0734	17 18	13.6174	3333 3178	0.9973	1 I	8	
3	0.0750	17	0.0752	17	13.2996	3034	0.9972	I	7	
4	0.0767	18	0.0769	18	12.9962	2900	0.9971	2	6	- 4
5	0.0785	17	0.0787	18	12.7062	2774	0.9969	1	5	
6	0.0802	17	0.0805	17	12.4288	2656	0.0968	2	4	
7	0.0819	18	0.0822	18	12.1632	2545	0.9966	I	3	
8	0.0837	17	0.0840	17	11.9087	2545	0.9965	2	2	
9	0.0854	18	0.0857	18	11.6645	2344	0,9963	I	I	
5.0	0.0872	10	0.0875	10	11.4301	-344	0.9962		85.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
5.0	0.0872		0.0875		11.4301		0.9962	_	85.0	
1	0.0872	17	0.0892	17	11.2048	2253	0.9960	2	9	
2	0.0906	17	0.0010	18	10.9882	2166	0.9959	I	8	
3	0.0924	18	0.0928	18 17	10.7797	2085	0.9957	2 I	7	
4	0.0941		0.0945	18	10.5789	1935	0.9956	2	6	
5	0.0958	17 18	0.0963	18	10.3854	1866	0.9954	2	5	
6	0.0976	17	0.0981	17	10.1988	1801	0.9952	1	4	
7	0.0993	18	0.0998	18	10.0187	1739	0.9951	2	3 2	
8 9	0.1011	17	0.1016	17	9.8448 9.6768	1680	0.9949	2	I	
6.0		17	0.1051	18	9.5144	1624	0.9945	2	84.0	
	0.1045	18		18		1572	0.9943	2	9	18
I 2	0.1063	17	0.1069 0.1086	17	9.3572 9.2052	1520	0.9943	I	8	1 1.8
3	0.1097	17	0.1104	18	9.0579	1473	0.9940	2	7	2 3.6
4	0.1115	18	0.1122	18	8.9152	1427	0.9938	2	6	3 5.4
	0.1132	17 17	0.1139	17 18	8.7769	1383 1342	0.9936	2	5	4 7.2 5 9.0
5 6	0.1149	18	0.1157	18	8.6427	1342	0.9934	2	4	6 10.8
7	0.1167	17	0.1175	17	8.5126	1263	0.9932	2	3	7 12.6
8	0.1184	17	0.1192	18	8.3863	1227	0.9930	2	2 I	8 14.4
9	0.1201	18	0.1210	18	8.2636	1193	0.9928	3	83.0	9 16.2
7.0	0.1219	17	0.1228	18	8.1443	1158	0.9925	2		
1	0.1236	17	0.1246	17	8.0285 7.9158	1127	0.9923	2	9	
3	0.1253	18	0.1203	18	7.8062	1096	0.9919	2	7	
4	0.1288	17	0.1299	18	7.6996	1066	0.9917	2	6	
5	0.1305	17	0.1317	18	7.5958	1038	0.9914	3	5	
6	0.1323	18	0.1334	17	7.4947	985	0.9912	2 2	4	
7	0.1340	17	0.1352	18	7.3962	960	0.9910	3	3	
8	0.1357	17	0.1370	18	7.3002	936	0.9907	2	2	
9	0.1374	18	0.1388	17	7.2066	912	0.9905	2	I	
8.0	0.1392	17	0.1405	18	7.1154	890	0.9903	3	82.0	17
I	0.1409	17	0.1423	18	7.0264	869	0.9900	2	9	I I.7 2 3.4
2	0.1426	18	0.1441	18	6.9395	847	0.9898	3	7	3 5.I
3	0.1461	17		18	6.7720	828	0.9893	2	6	4 6.8
4 5	0.1401	17	0.1477	18	6.6912	808	0.9890	3	5	5 8.5
6	0.1495	17	0.1512	17	6.6122	790	0.9888	2	4	6 10.2
7	0.1513		0.1530	18	6.5350	772	0.9885	3	3	7 II.9 8 I3.6
8	0.1530	17	0.1548	18	6.4596	754 737	0.9882	3 2	2	9 15.3
9	0.1547	17	0.1566	18	6.3859	721	0.9880	3	I	
9.0	0.1564	18	0.1584	18	6.3138	706	0.9877	3	81.0	
1	0.1582	17	0.1602	18	6.2432	690	0.9874	3	9	
2	0.1599	17	0.1620	18	6.1742	676	0.9871	2	8	
3	1	17	0.1638	17		661	0.9869	3	7	
4 5	0.1633	17	0.1655	18	6.0405 5.9758	647	0.9863	3	5	
5 6	0.1668	18	0.1691	18	5.9124	634	0.9860	3	4	
7	0.1685	17	0.1709	18	5.8502	622	0.9857	3	3	
8	0.1702	17	0.1727	18	5.7894	608 597	0.9854	3	2	
9	0.1719	17	0.1745	18	5.7297	584	0.9851	3	I	
10.0	0.1736		0.1763		5.6713		0.9848	_	80.0	
	Cosin	đ.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

Deg	g.	Sin	d.	Tan	đ.	Cotan	đ.	Cosin	đ.		P. P.
10.0	히	0.1736		0.1763		5.6713		0.9848		80.0	
	ı	0.1754	18	0.1781	18	5.6140	573	0.9845	3	9	
	2	0.1771	17	0.1799	18	5.5578	562	0.9842	3	8	
1 :	3	0.1788	17	0.1817	18 18	5.5026	552	0.9839	3	7	
	4	0.1805	17	0.1835		5.4486	540	0.9836	3	6	
	5	0.1822	17 18	0.1853	18 18	5 - 3955	531	0.9833	3	5	
	6	0.1840	17	0.1871	19	5.3435	520 511	0.9829	4	4	19
	7	0.1857		0.1890	18	5.2924	-	0.9826		3	1 1.9
1 3	8	0.1874	17 17	0.1908	18	5.2422	502 493	0.9823	3	2	2 3.8 3 5.7
	9	0.1891	17	0.1926	18	5.1929	483	0.9820	4	I	4 7.6
11.0	ᅃ	0.1908	17	0.1944	18	5.1446	476	0.9816	3	79.0	5 9.5
	1	0.1925		0.1962	18	5.0970	466	0.9813	3	9	6 11.4
	2	0.1942	17	0.1980	18	5.0504	459	0.9810	4	8	7 13.3
	3	0.1959	18	0.1998	18	5.0045	459 451	0.9806	3	7	8 15.2
	4	0.1977	17	0.2016	19	4.9594	442	0.9803	4	6	9 17.1
	5	0.1994	17	0.2035	18	4.9152	436	0.9799	3	5	
	6	0.2011	17	0.2053	18	4.8716	428	0.9796	4	4	
	7	0.2028	17	0.2071	18	4.8288	421	0.9792	3	3	
	8	0.2045	17	0.2089	18	4.7867	414	0.9789	4	2 I	
	9		17	0.2107	19	4.7453	407	0.9785	4		
12.0	۰I	0.2079	17	0.2126	18	4.7046	400	0.9781	3	78.0	1.40
	1	0.2096	17	0.2144	18	4.6646	394	0.9778	4	9	1 1.8
	2	0.2113	17	0.2162	18	4.6252	388	0.9774	4	8	2 3.6
	3	0.2130	17	0.2180	19	4.5864	381	0.9770	3	7	3 5.4
	4	0.2147	17	0.2199	18	4.5483	376	0.9767	4	6	4 7.2
	5 6	0.2164	17	0.2217	18	4.5107	370	0.9763	4	5 4	5 9.0
	- 1		17	0.2235	19	4 · 4737	364	0.9759	4		6 10.8
	7 8	0.2198	17	0.2254	18	4.4373 4.4015	358	0.9755	4	3 2	7 12.6
	أو	0.2213	18	0.2272	18	4.4013	353	0.9748	3	ī	8 14.4 9 16.2
13.		0.2250	17	0.2309	19	4.3315	347	0.9744	4	77.0	9 16.2
			17		18		343		4	9	
	1 2	0.2267	17	0.2327	18	4.2972	337	0.9740	4	8	
	3	0.2300	16	0.2343	19	4.2303	332	0.9732	4	7	
	- 1	0.2317	17	0.2382	18	4.1976	327	0.9728	4	6	
	4 5	0.2317	17	0.2302	19	4.1970	323	0.9724	4	5	
	ة	0.2351	17	0.2419	18	4.1335	318	0.9720	4	4	17
	7	0.2368	17	0.2438	19	4.1022	313	0.9715	5	3	I I.7
	á	0.2385	17	0.2456	18	4.0713	309	0.9711	4	2	2 3.4
	9	0.2402	17	0.2475	19 18	4.0408	305	0.9707	4	1	3 . 5.I
14.0	0	0.2419	17	0.2493		4.0108	300	0.9703	4	76.0	4 6.8
	1	0.2436	17	0.2512	19	3.9812	296	0.9699	4	9	5 8.5
	2	0.2453	17	0.2530	18	3.9520	292	0.9694	5	8	6 10.2
	3	0.2470	17	0.2549	19	3.9232	288 285	0.9690	4	7	7 II.9 8 I3.6
1	4	0.2487	17	0.2568	19	3.8947	_	0.9686		6	9 15.3
	5	0.2504	17	0.2586	18	3.8667	280 276	0.9681	5 4	5	J0.0
	6	0.2521	17	0.2605	18	3.8391	273	0.9677	4	4	
	7	0.2538	16	0.2623	19	3.8118	270	0.9673	5	3	
	8	0.2554	17	0.2642	19	3.7848	265	0.9668	4	2	
	9	0.2571	17	0.2661	18	3.7583	262	0.9664	5	I	
15.0	<u>-</u>	0.2588		0.2679		3.7321		0.9659	_	75.0	
		Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

TABLE XXVII. - (Continued)

_										
Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	đ.		P. P.
15.0	0.2588	17	0.2679	19	3.7321	259	0.9659	4	75.0	
I	0.2605	17	0.2698	19	3.7062	256	0.9655	5	9	
2	0.2622	17	0.2717	19	3.6806	252	0.9650	4	8	
3	0.2639	17	0.2736	18	3.6554	249	0.9646	5	7	19
4	0.2656	16	0.2754	19	3.6305 3.6059	246	0.9641	5	6	1 1.9
5 6	0.2689	17	0.2792	19	3.5816	243	0.9632	4	5 4	2 3.8
7	0.2706	17	0.2811	19	3.5576	240	0.9627	5	3	3 5.7
8	0.2723	17	0.2830	19	3.5339	237	0.9622	5	2	5 9.5
9	0.2740	17 16	0.2849	19 18	3.5105	234	0.9617	5	I	6 11.4
16.0	0.2756		0.2867		3.4874	231	0.9613	4	74.0	7 13.3
r	0.2773	17	0.2886	19	3.4646	228	0.9608	5	9	8 15.2
2	0.2790	17 17	0.2905	19 19	3.4420	226 223	0.9603	5	8	9 17.1
3	0.2807	16	0.2924	19	3.4197	223	0.9598	5	7	
4	0.2823	17	0.2943	19	3.3977	218	0.9593	5	6	
5	0.2840	17	0.2962	19	3.3759	215	0.9588	5	5	18
6	0.2857	17	0.2981	19	3.3544	212	0.9583	5	4	1 1.8
7 8	0.2874	16	0.3000	19	3.3332	210	0.9578	5	3	2 3.6 3 5.4
9	0.2907	17	0.3019	19	3.3122	208	0.9568	5	2 I	4 7.2
17.0	0.2924	17	0.3057	19	3.2709	205	0.9563	5	73.0	5 9.0
I	0.2940	16	0.3076	19	3.2506	203	0.9558	5	9	6 10.8
2	0.2957	17	0.3096	20	3.2305	201	0.9553	5	8	7 12.6 8 14.4
3	0.2974	17 16	0.3115	19	3.2106	199	0.9548	5	7	8 14.4 9 16.2
4	0.2990		0.3134	19	3.1910	196	0.9542	1	6	9 10.2
5	0.3007	17	0.3153	19 19	3.1716	194	0.9537	5	5	
6	0.3024	16	0.3172	19	3.1524	192	0.9532	5	4	
7	0.3040	17	0.3191	20	3.1334	188	0.9527	6	3	17
8 9	0.3057	17	0.3211	19	3.1146	185	0.9521	5	2 I	I I.7 2 3.4
	0.3074	16	0.3230	19		184		5	72.0	3 5.1
18.0	0.3090	17	0.3249	20	3.0777	182	0.9511	6		4 6.8
I 2	0.3107	16	0.3269	19	3.0595	180	0.9505	5	9	5 8.5
3	0.3123	17	0.3200	19	3.0413	178	0.9494	6	7	6 10.2 7 11.9
4	0.3156	16	0.3327	20	3.0061	176	0.9489	5	6	8 13.6
	0.3173	17	0.3346	19	2.9887	174	0.9483	6	5	9 15.3
5	0.3190	17	0.3365	19 20	2.9714	173	0.9478	5	4	
7	0.3206	17	0.3385	19	2.9544	169	0.9472	6	3	
8	0.3223	16	0.3404	20	2.9375	167	0.9466	5	2	. 16
9	0.3239	17	0.3424	19	2.9208	166	0.9461	6	I	1 1.6
19.0	0.3256	16	0.3443	20	2.9042	164	0.9455	6	71.0	2 3.2
1	0.3272	17	0.3463	19	2.8878	162	0.9449	5	9 8	3 4.8
3	0.3289	16	0.3482	20	2.8716 2.8556	160	0.9444	6	0 7	4 6.4 5 8.0
4	0.3322	17	0.3522	20	2.8397	159	0.9432	6	6	6 9.6
	0.3322	16	0.3522	19	2.8239	158	0.9432	6	5	7 11.2
5 6	0.3355	17	0.3561	20 20	2.8083	156	0.9421	5	4	8 12.8
7	0.3371	1	0.3581	}	2.7929	154	0.9415	6	3	9 14.4
. 8	0.3387	16	0.3600	19 20	2.7776	-153 151	0.9409	6	2	
9	0.3404	16	0.3620	20	2.7625	150	0.9403	6	1	
20.0	0.3420		0.3640		2.7475		0.9397		70.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	đ.	Cotan	d.	Cosin	d.		P. P.
20.0		α.		и.				u.		P. P.
	0.3420	17	0.3640	19	2.7475	149	0.9397	6	70.0	
I 2	0.3437	16	0.3659 0.3679	20	2.7326	147	0.9391	6	9	
3	0.3469	16	0.3699	20	2.7034	145	0.9379	6	7	
4	0.3486	17	0.3719	20	2.6889	145	0.9373	6	6	22
5	0.3502	16	0.3739	20	2.6746	143	0.9367	6	5	I 2.2 2 4.4
6	0.3518	16 17	0.3759	20 20	2.6605	141 141	0.9361	6	4	3 6.6
7	0.3535	16	0.3779	20	2.6464		0.9354	6	3	4 8.8
8	0.3551	16	0.3799	20	2.6325	139 138	0.9348	6	2	5 11.0
9	0.3567	17	0.3819	20	2.6187	136	0.9342	6	I	6 13.2
21.0	0.3584	16	0.3839	20	2.6051	135	0.9336	6	69.0	7 15.4 8 17.6
I	0.3600	16	0.3859	20	2.5916	134	0.9330	7	9	9 19.8
2	0.3616	17	0.3879	20	2.5782	133	0.9323	6	8	3 23.0
3	0.3633	16	0.3899	20	2.5649	132	0.9317	6	7	
5	0.3649	16	0.3919	20	2.5517 2.5386	131	0.9311	7	6	
6	0.3681	16	0.3939	20	2.5257	129	0.9304	6	5 4	1 2.I
7	0.3697	16	0.3979	20	2.5129	128	0.9291	7	3	2 4.2
8	0.3714	17	0.4000	21	2.5002	127	0.9291	6	2	3 6.3
9	0.3730	16	0.4020	20 20	2.4876	126	0.9278	7	I	4 8.4
22.0	0.3746		0.4040		2.4751	125	0.9272	6	68.0	5 10.5
1	0.3762	16	0.4061	21	2.4627	124	0.9265	7	9	6 12.6
2	0.3778	16 17	0.4081	20 20	2.4504	123	0.9259	6	8	7 14.7 8 16.8
3	0.3795	16	0.4101	21	2.4383	121	0.9252	7 7	7	9 18.9
4	0.3811	16	0.4122	20	2,4262	120	0.9245	6	6	
5 6	0.3827	16	0.4142	21	2.4142	119	0.9239	7	5	
	0.3843	16	0.4163	20	2.4023	117	0.9232	7	4	. 17
7 8	0.3859	16	0.4183	21	2.3906	117	0.9225	6	3	1 1.7
9	0.3875	16	0.4204	20	2.3789 2.3673	116	0.9219	7	2 I	2 3.4
23.0	0.3907	16	0.4245	21	2.3559	114	0.9205	7	67.0	3 5.I
1	0.3923	16	0.4265	20	2.3445	114	0.9198	7		4 6.8
2	0.3923	16	0.4286	21	2.3332	113	0.9198	7	9 8	5 8.5 6 10.2
3	0.3955	16	0.4307	21	2.3220	II2	0.9184	7	7	6 10.2 7 11.9
4	0.3971	16	0.4327	20	2.3109	III	0.9178	6	6	8 13.6
5	0.3987	16 16	0.4348	2I 2I	2.2998	III	0.9171	7	5	9 15.3
6	0.4003	-16	0.4369	2I 2I	2.2889	109	0.9164	7	4	
7	0.4019	16	0.4390	21	2.2781	108	0.9157	7	3	
8	0.4035	16	0.4411	20	2.2673	103	0.9150	7	2	16
9	0.4051	16	0.4431	21	2.2566	106	0.9143	8	I	1 1.6
24.0	0.4067	16	0.4452	21	2.2460	105	0.9135	7	66.0	2 3.2
I	0.4083	16	0.4473	21	2.2355	104	0.9128	7	9 8	3 4.8
3	0.4099	16	0.4494	21	2.2251	103	0.9121	7	- 8	4 6.4 5 8.0
	0.4131	16	0.4536	21	2.2045	103	0.9114	7	6	5 8.0 6 9.6
4 5	0.4131	16	0.4530	21	2.1943	102	0.9107	7	5	7 11.2
6	0.4163	16	0.4578	21	2.1842	IOI	0.9092	8	4	8 12.8
7	0.4179	16	0.4599	21	2.1742	100	0.9085	7	3	9 14.4
8	0.4195	16 15	0.4621	22 2I	2.1642	100	0.9078	7 8	2	
9	0.4210	16	0.4642	21	2.1543	99 98	0.9070	7	I	
25.0	0.4226		0.4663		2.1445		0.9063		65.0	
	Cosin	đ.	Cotan	d.	Tan	đ.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	đ.		P. P.
25.0	0.4226	16	0.4663	21	2.1445	97	0.9063	_	65.0	
1	0.4242	16	0.4684		2.1348		0.9056	7	9	
2	0.4258	16	0.4706	22 2I	2.1251	97 96	0.9048	8 7	8	
3	0.4274	15	0.4727	21	2.1155	95	0.9041	8	7	23
4	0.4289	16	0.4748	22	2.1060	1	0.9033		6	I 2.3
5	0.4305	16	0.4770	21	2.0965	95 93	0.9026	7 8	5	2 4.6
6	0.4321	16	0.4791	22	2.0872	93	0.9018	7	4	3 6.9
7	0.4337	15	0.4813	21	2.0778	92	0.9011	8	3	4 9.2
8	0.4352	16	0.4834	22	2.0686	92	0.9003	7	2	5 11.5
9	0.4368	16	0.4856	21	2.0594	91	0.8996	8	I	6 13.8
26.0	0.4384	15	0.4877	22	2.0503	90	0.8988	8	64.0	7 16.1 8 18.4
1	0.4399	16	0.4899		2.0413	1	0.8980		9	8 18.4 9 20.7
2	0.4415	16	0.4921	22 2I	2.0323	90 90	0.8973	7 8	8	9 20.7
3	0.4431	15	0.4942	22	2.0233	88	0.8965	8	7	
4	0.4446	16	0.4964	22	2.0145	88	0.8957	8	6	
5	0.4462	16	0.4986	22	2.0057	87	0.8949	7	5	22
6	0.4478	15	0.5008	21	1.9970	87	0.8942	8	4	I 2.2
7	0.4493	16	0.5029	22	1.9883	86	0.8934	8	3	2 4.4
8	0.4509	15	0.5051	22	1.9797	86	0.8926	8	2	3 6.6
9	0.4524	16	0.5073	22	1.9711	85	0.8918	8	I	4 8.8 5 II.0
27.0	0.4540	15	0.5095	22	1.9626	84	0.8910	8	63.0	6 13.2
I	0.4555	16	0.5117	22	1.9542		0.8902	8	9	7 15.4
2	0.4571	15	0.5139	22	1.9458	84 83	0.8894	8	8	8 17.6
3	0.4586	16	0.5161	23	1.9375	83	0.8886	8	7	9 19.8
4	0.4602	15	0.5184	22	1.9292	82	0.8878	8	6	
5	0.4617	16	0.5206	22	1.9210	82	0.8870	8	5	
6	0.4633	15	0.5228	22	1.9128	81	0.8862	8	4	1 40
7	0.4648	16	0.5250	22	1.9047	80	0.8854	8	3	1 1.6
8	0.4664	15	0.5272	23	1.8967	80	0.8846	8	2	2 3.2
9	0.4679	16	0.5295	22	1.8887	80	0.8838	9	I	3 4.8
28.0	0.4695	15	0.5317	23	1.8807	79	0.8829	8	62.0	4 6.4
I	0.4710	16	0.5340	22	1.8728	78	0.8821	8	9	5 8.0
2	0.4726	15	0.5362	22	1.8650	78	0.8813	8	8	6 9.6
3	0.4741	15	0.5384	23	1.8572	77	0.8805	9	7	7 11.2
4	0.4756	16	0.5407	23	1.8495	77	0.8796	8	6	8 12.8
5	0.4772	15	0.5430	22	1.8418	77	o.8788 o.8780	8	5	9 14.4
1	0.4787	15	0.5452	23	-	76		9	4	
7 8	0.4802	16	0.5475	23	1.8265	75	0.8771	8	3	
9	0.4818	15	0.5490	22	1.8115	75	0.8755	8	2 I	15
29.0		15		23	1.8040	75		9	61.0	1 1.5
	0.4848	15	0.5543	23		74	0.8746	8		2 3.0
1	0.4863	16	0.5566	23	1.7966	73	0.8738	9	9	3 4.5
2	0.4879	15	0.5589	23	1.7893	73	0.8729	8	8	4 6.0
3	0.4894	15		23		73		9	7	5 7.5 6 9.0
4	0.4909	15	0.5635 0.5658	23	1.7747	72	0.8712	8	6	7 10.5
5	0.4924	15	0.5681	23	1.7603	72	0.8695	9	5 4	8 12.0
		16	0.5704	23	1.7532	71	0.8686	9		9 13.5
7 8	0.4955	15	0.5704	23	1.7532	71	0.8678	8	3 2	
9	0.4975	15	0.5750	23	1.7391	70	0.8669	9	ı	
30.0	0.5000	15	0.5774	24	1.7321	70	0.8660	9	60.0	
	Cosin	đ.	Cotan	d.	Tan	d.	Sin	đ.	Deg.	
L	COULT	٠.,	Journ		2411	ч.	OIII	u.	206.	

De	g.	Sin	đ.	Tan	đ.	Cotan	d.	Cosin	d.		P. P.
30		0.5000		0.5774		1.7321		0.8660		60.0	
30		0.5015	15	0.5797	23	1.7251	70	0.8652	8	9	
1	I 2	0.5015	15	0.5797	23	1.7182	69	0.8643	9	8	
1	3	0.5045	15	0.5844	24	1.7113	69	0.8634	9	7	24
	4	0.5060	15	0.5867	23	1.7045	68	0.8625	9	6	
		0.5075	15	0.5890	23	1.6977	68	0.8616	9	5	I 2.4 2 4.8
	5	0.5090	15	0.5914	24	1.6909	68 67	0.8607	9 8	4	3 7.2 4 9.6
	7	0.5105	15	0.5938	24	1.6842		0.8599	_	3	5 I2.0 6 I4.4
	8	0.5120	15 15	0.5961	23 24	1.6775	67 66	0.8590	9	2	
	9	0.5135	15	0.5985	24	1.6709	66	0.8581	9	I	7 16.8 8 19.2
31.	0	0.5150	15	0.6009	23	1.6643	66	0.8572	9	59.0	9 21.6
	1	0.5165		0.6032	_	1.6577	65	0.8563	1	9	
	2	0.5180	15 15	0.6056	24 24	1.6512	65	0.8554	9	8	25
1	3	0.5195	15	0.6080	24	1.6447	64	0.8545	9	7	I 2.5
	4	0.5210	15	0.6104	24	1.6383	64	0.8536	IO	6	2 5.0 3 7.5
ı	5 6	0.5225	15	0.6128	24	1.6319	64	0.8526	9	5	4 10.0
	- 1	0.5240	15	0.6152	24	1.6255	64	0.8517	9	4	5 12.5
	7 8	0.5255	15	0.6176	24	1.6191	63	o.8508 o.8499	9	3 2	
!	9	0.5270	14	0.6224	24	1.6066	62	0.8499	9	I	7 17.5 8 20.0
32.		0.5299	15	0.6249	25	1.6003	63	0.8480	10	58.0	9 22.5
32	- 1		15		24		62	0.8471	9		
	I	0.5314	15	0.6273	24	1.5941	61	0.8471	9	9	26
1	3	0.5344	15	0.6322	25	1.5818	62	0.8453	9	7	I 2.6 2 5.2
	4	0.5358	14	0.6346	24	1.5757	61	0.8443	10	6	3 7.8
ı		0.5373	15	0.6371	25	1.5697	60	0.8434	9	5	4 10.4
1	5	0.5388	15	0.6395	24	1.5637	60	0.8425	9	4	5 I3.0 6 I5.6
	7	0.5402	14	0.6420	25	I.5577	60	0.8415	10	3	7 18.2 8 20.8
	8	0.5417	15	0.6445	25	1.5517	60	0.8406	9	2	
ı	9	0.5432	15 14	0.6469	24 25	1.5458	59 59	0.8396	9	1	9 23.4
33.	0	0.5446		0.6494		1.5399		0.8387	10	57.0	
	1	0.5461	15	0.6519	25	1.5340	59	0.8377		9	I 1.5
1	2	0.5476	15	0.6544	25	1.5282	58 58	0.8368	9	8	I I.5 2 3.0
	3	0.5490	14	0.6569	25 25	1.5224	58	0.8358	10	7	3 4.5
	4	0.5505	14	0.6594	25	1.5166	58	0.8348	9	6	4 6.0
	5	0.5519	15	0.6619	25 25	1.5108	57	0.8339	10	5	6 9.0
l	6	0.5534	14	0.6644	25	1.5051	57	0.8329	9	4	7 10.5
1	7	0.5548	15	0.6669	25	1.4994	56	0.8320	10	3	8 12.0 9 13.5
	8	0.5563	14	0.6694	26	I.4938 I.4882	56	0.8310	10	I	3 20.3
34	_		15	0.6745	25	1.4826	56	0.8290	10	56.0	14
34		0.5592	14		26	<u> </u>	56		9		I I.4
	I 2	0.5606	15	0.6771	25	1.4770	55	0.8281	10	9 8	2 2.8
	3	0.5635	14	0.6822	26	1.4715	56	0.82/1	10	7	3 4.2 4 5.6
	4	0.5650	15	0.6847	25	1.4605	54	0.8251	10	6	5 7.0
1		0.5664	14	0.6873	26	1.4550	55	0.8231	10	5	
1	5	0.5678	14	0.6899	26	1.4496	54	0.8231	10	4	7 9.8 8 II.2
	7	0.5693	15	0.6924	25	1.4442	54	0.8221	10	3	9 12.6
	8	0.5707	14	0.6950	26	1.4388	54	0.8211	10	2	
	9	0.5721	14	0.6976	26 26	1.4335	53 54	0.8202	9	1	
35	.0	0.5736	15	0.7002	20	1.4281	34	0.8192	10	55.0	
Г		Cosin	đ.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	d.	Cotan	đ.	Cosin	đ.		P. P.
35.0	0.5736	14	0.7002	26	1.4281	52	0.8192	II	55.0	
I	0.5750		0.7028		1.4229	-	0.8181		9	
2	0.5764	14	0.7054	26 26	1.4176	53	0.8171	10	8	
3	0.5779	15	0.7080		1.4124	52	0.8161	10	7	27
4	0.5793	14	0.7107	27	1.4071	53	0.8151	10	6	I 2.7
5	0.5807	14	0.7133	26	1.4019	52	0.8141	10	5	2 5.4 3 8.1
6	0.5821	14	0.7159	26	1.3968	51	0.8131	10	4	
7	0.5835	14	0.7186	27	1.3916	52	0.8121	10	3	4 10.8 5 13.5
8	0.5850	15	0.7212	26	1.3865	51	0.8111	10	2	5 13.5 6 16.2
9	0.5864	14	0.7239	27	1.3814	51	0.8100	II	1	7 18.9 8 21.6
36.0	0.5878	14	0.7265	26	1.3764	50	0.8090	10	54.0	
		14		27		51		10	1	9 24.3
1 2	0.5892	14	0.7292	27	1.3713	50	0.8080	10	9	
	0.5906 0.5920	14	0.7319 0.7346	27	1.3663 1.3613	50	0.8070	11	7	28
3		14		27		49	-	10		1 2.8
4	0.5934	14	0.7373	27	1.3564	50	0.8049	10	6	2 5.6 3 8.4
5	0.5948	14	0.7400	27	1.3514	49	0.8039	11	5	4 11.2
	0.5962	14	0.7427	27	1.3465	49	0.8028	10	4	5 14.0
7	0.5976	14	0.7454	27	1.3416	49	0.8018	11	3	
8	0.5990	14	0.7481	27	1.3367	48	0.8007	IO	2	7 19.6 8 22.4
9	0.6004	14	0.7508	28	1.3319	49	0.7997	II	53.0	9 25.2
37.0	0.6018	14	0.7536	27	1.3270	48	0.7986	IO	03.0	
1	0.6032	1	0.7563		1.3222		0.7976		9	1 00
2	0.6046	14	0.7590	27	1.3175	47	0.7965	II	8	1 2.9
3	0.6060	14	0.7618	28 28	1.3127	48 48	0.7955	10	7	2 5.8
4	0.6074	14	0.7646		1.3079		0.7944		6	2 5.8 3 8.7
5	0.6088	14	0.7673	27	1.3032	47	0.7934	10	5	4 11.6
6	0.6101	13	0.7701	28	1.2985	47	0.7923	II	4	5 I4.5 6 I7.4
7	0.6115	14	0.7729	28	1.2938	47	0.7912	l	3	7 20.3
8	0.6129	14	0.7757	28	1.2892	46	0.7902	10	2	
9	0.6143	14	0.7785	28	1.2846	46	0.7891	11	1	9 26.1
38.0	0.6157	14	0.7813	28	1.2799	47	0.7880	11	52.0	
I	0.6170	13	0.7841	28	1.2753	46	0.7869	II	9	14
2	0.6184	14	0.7869	28	1.2708	45	0.7859	10	8	I I.4
3	0.6198	14	0.7898	29	1.2662	46	0.7848	11	7	2 2.8
	0.6211	13	0.7926	28	1.2617	45	0.7837	II	6	3 4.2 5.6
4	0.6225	14	0.7920	28	1.2572	45	0.7826	11	5	5 7.0
5 6	0.6239	14	0.7983	29	1.2527	45	0.7815	II	4	
1	0.6252	13	0.8012	29	1.2482	45	0.7804	II	3	7 9.8
7 8	0.6252	14	0.8012	28	1.2437	45	0.7793	11	3 2	9 12.6
9	0.6280	14	0.8069	29	1.2393	44	0.7782	11	. 1	
39.0	0.6293	13	0.8098	29		44		II	51.0	13
		14		29	1.2349	44	0.7771	11		
I	0.6307	13	0.8127	29	1.2305	44	0.7760	11	9 8	2 2.6
2	0.6320	14	0.8156	29	1.2261	43	0.7749	II	7	3 3.0
3		13		29		44	0.7738	11		4 5.2 5 6.5 6 7.8
4	0.6347	14	0.8214	29	1.2174	43	0.7727	11	6	5 6.5
5	0.6361	13	0.8243	30	1.2131	43	0.7716	II	5	7 9.1
	0.6374	14	0.8273	29		43	0.7705	11	4	
7	0.6388	13	0.8302	30	1.2045	43	0.7694	11	3	9 11.7
8	0.6401	13	0.8332	29	1.2002	43	0.7683	II	2	
9	0.6414	14	0.8361	30	1.1960	42	0.7672	12	I	
40.0	0.6428		0.8391		1.1918		0.7660		50.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	đ.	Deg.	
	1		1				L	1	1	

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D	eg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
40	0.0	0.6428		0.8391		1.1918		0.7660		50.0	
	I	0.6441	13	0.8421	30	1.1875	43	0.7649	II	9	
	2	0.6455	14	0.8451	30	1.1833	42	0.7638	II	8	31
1	3	0.6468	13	0.8481	30	1.1792	41	0.7627	II	7	
	4	0.6481	13	0.8511	30	1.1750	42	0.7615	12	6	I 3.I 2 6.2
1	5	0.6494	13	0.8541	30	1.1708	42	0.7604	II	5	3 9.3
1	6	0.6508	14	0.8571	30	1.1667	41	0.7593	II	4	4 12.4
1	7	0.6521	13	0.8601	30	1.1626	41	0.7581	12	3	5 15.5 6 18.6
	8	0.6534	13	0.8632	31	1.1585	41	0.7570	II	2	7 2I.7 8 24.8
ŧ.	9	0.6547	13	0.8662	30	1.1544	41	0.7559	II	1	
41	0	0.6561	14	0.8693	31	1.1504	40	0.7547	12	49.0	9 27.9
1 **	- 1		13		31		4I		II		
	I	0.6574	13	0.8724	30	1.1463	40	0.7536	12	9	32
1	2	0.6587	13	0.8785	31	1.1383	40	0.7513	II	7	I 3.2
	3		13		31		40	1	12	6	I 3.2 2 6.4 3 9.6
	4	0.6613	13	0.8816	31	1.1343	40	0.7501	II	5	3 9.6
	5	0.6626	13	0.8847	31	I.1303 I.1263	40	0.7490	12	4	
		0.6639	13		32	- 1	39		12		6 19.2
	7	0.6652	13	0.8910	31	1.1224	40	0.7466	II	3 2	7 22.4
	8	0.6665	13	0.8941	31	1.1164	39	0.7455 0.7443	12	I	8 25.6 9 28.8
1	9	0.6678	13	0.8972	32		39		12		9 20.0
42	3.0	0.6691	13	0.9004	32	1.1106	39	0.7431	II	48.0	
	I	0.6704	13	0.9036	31	1.1067	39	0.7420	12	9	33
	2	0.6717	13	0.9067	32	1.1028	38	0.7408	12	8	I 3.3 2 6.6
	3	0.6730	13	0.9099	32	1.0990	39	0.7396	II	7	
1	4	0.6743	13	0.9131	32	1.0951	38	0.7385	12	6	3 9.9 4 13.2
	5	0.6756	13	0.9163	32	1.0913	38	0.7373	12	5	5 16.5 6 19.8
1	6	0.6769	13	0.9195	33	1.0875	38	0.7361	12	4	6 19.8
1	7	0.6782	12	0.9228	32	1.0837	38	0.7349	12	3	7 23.I 8 26.4
	8	0.6794	13	0.9260	33	1.0799	38	0.7337	12	2	9 29.7
1	9	0.6807	13	0.9293	32	1.0761	37	0.7325	II	I	
43	3.0	0.6820		0.9325	33	1.0724	38	0.7314	12	47.0	
	I	0.6833	13	0.9358		1.0686		0.7302	12	9	34
1	2	0.6845	12	0.9391	33	1.0649	37	0.7290	12	8	I 3.4 2 6.8
1	3	0.6858	13	0.9424	33	1.0612	37	0.7278	12	7	3 10.2
	4	0.6871	13	0.9457	33	1.0575	37	0.7266	12	6	4 13.6
		0.6884	13	0.9490	33	1.0538	37	0.7254	12	5	5 17.0
	5 6	0.6896	12 13	0.9523	33	1.0501	37 37	0.7242	12	4	
	7	0.6909		0.9556		1.0464		0.7230	12	3	8 27.2
	8	0.6921	12	0.9590	34	1.0428	36 36	0.7218	12	2	9 30.6
	9	0.6934	13	0.9623	33	1.0392	37	0.7206	13	I	
44	4.0	0.6947	-	0.9657		1.0355		0.7193	12	46.0	13
	I	0.6959	12	0.9691	34	1.0319	36	0.7181		9	I I.3
	2	0.6972	13	0.9725	34	1.0283	36	0.7169	12	8	2 2.6
	3	0.6984	12	0.9759	34	1.0247	36	0.7157	I2 I2	7	3 3.9
	4	0.6997	13	0.9793	34	1.0212	35	0.7145		6	4 5.2 5 6.5 6 7.8
		0.7009	12	0.9827	34	1.0176	36	0.7133	12	5	5 6.5
	5 6	0.7022	13	0.9861	34	1.0141	35	0.7120	13	4	7 9.I
	7	0.7034	12	0.9896	35	1.0105	36	0.7108		3	8 IO.4 9 II.7
	8	0.7046	12	0.9930	34	1.0070	35	0.7096	12	2	9 ; 11.7
	9	0.7059	13	0.9965	35	1.0035	35	0.7083	13	I	
4	5.0	0.7071	12	1.0000	35	I.0000	35	0.7071	12	45.0	
		Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

TABLE XXVIII. — Natural Versed Sines and External Secants

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Angle	Vers	Exsec	Angle	I——	Exsec			Exsec		Vers	Exsec
0.0	.0000	.0000	5.0	.0038	.0038	10.0	.0152	.0154	15.0	.0341	.0353
ı.	.0000	.0000	ı,	. 0040	.0040	ı,	.0155	.0157	.I	.0345	.0358
.2	.0000	.0000	.2	.0041	.0041	.2	.0158	.0161	.2	.0350	.0363
-3	.0000	.0000	-3	.0043	.0043	-3	.0161	.0164	-3	.0354	.0367
.4	.0000	0000	-4	.0044	.0045	-4	.0164	.0167	-4	.0359	.0372
.5	.0000	.0000	.5	.0046	.0046	-5	.0167	.0170	.5	.0364	.0377
.6	.0001	.0001	.6	.0048	.0048	.6	.0171	.0174	.6	.0368	.0382
.7	.0001	.0001	.7	.0049	.0050		.0174	.0177	.7	.0373	.0388
.8	.0001	.0001	.8	.0051	.0051	.8	.0177	.0180	.8	.0378	.0393
.9	.0001	.0001	.9	.0053	.0053	.9	.0180	.0184	.9	.0383	.0398
1.0	.0002	.0002	6.0	.0055	.0055	11.0	.0184	.0187	16.0	.0387	.0403
.I	.0002	.0002	.I	.0057	.0057	.I	.0187	.0191	.I	.0392	.0408
.2	.0002	.0002	.2	.0058	.0059	.2	.0190	.0194	.2	.0397	.0413
.3	.0003	.0003	-3	.0060	.0061	-3	.0194	.0198	-3	.0402	.0419
.4	.0003	.0003	-4	.0062	.0063		.0197	.0201	.4	.0407	.0424
.5	.0003	.0003	.5 .6	.0064	.0065	-5	.0201	.0205	.5	.0412	.0429
.6	.0004	.0004		.0066	.0067	.6	.0204	.0209	.6	.0417	.0435
.7	.0004	.0004	.7	.0068	.0069	.7	.0208	.0212	.7	.0422	.0440
.8	.0005	.0005	.8	.0070	.0071	.8	.0211	.0216	8.	.0427	.0446
.9	.0005	.0005	.9	.0072	.0073	.9	.0215	.0220	.9	. 0432	.0451
2.0	.0006	.0006	7.0	.0075	.0075	12.0	.0219	.0223	17.0	.0437	.0457
. I	.0007	.0007	, I	.0077	.0077	ı.	.0222	.0227	.I	.0442	.0463
.2	.0007	.0007	.2	.0079	.0079	.2	.0226	.0231	.2	.0447	.0468
.3	,0008	.0008	.3	.0081	.0082	.3	. 0230	.0235	-3	.0452	.0474
.4	.0009	.0009	-4	.0083	.0084	-4	.0233	.0239	-4	.0458	.0480
·5 .6	.0010	.0010	.5 .6	.0086	.0086	.5 .6	.0237	.0243	.5 .6	.0463	.0485
	.0010	.0010					.0241	.0247		.0468	.0491
.7 .8	.0011	.0011	.7 .8	.0090	.0091	.7 .8	.0245	.0251	.7 .8	. 0473	.0497
.9	.0012	.0012	.9	.0093	.0093	.9	.0249	.0255	.9	.0479	.0503
3.0			8.0			13.0			18.0		
	.0014	.0014		.0097	.0098		.0256	.0263		.0489	.0515
I.	.0015	.0015	. I . 2	.0100	.0101	.I	.0260	.0267	Ι.	.0495	.0521
.2	.0016	.0016		.0102	.0103	.2	.0264	.0271	.2	.0500	.0527
.3	.0017	.0018	-3	.0107	.0108		.0272	.0280			
.4 .5	.0019	.0019	.4 .5	.0110	.0103	.4 .5	.0272	.0284	·4 ·5	.0511	.0539
.6	.0020	.0020	.6	.0112	.0114	.6	.0270	.0288	.6	.0522	.0551
.7	.0021	.0021	.7	.0115	.0116	.7	.0285	.0293	.7	.0528	.0557
.8	.0021	,0021	.8	.0113	.0110	.8	.0289	.0293	.8	.0534	.0564
.9	.0023	.0023	.9	.0120	.0122	.9	.0293	.0302	.9	.0539	.0570
4.0	.0024	.0024	9.0	.0123	.0125	14.0	.0297	.0306	19.0	.0545	.0576
.1	.0026	.0026	.I	.0126	.0127	.1	.0301	.0311	.1	.0551	.0583
.2	.0020	.0027	.2	.0120	.0130	.2	.0301	.0315	.2	.0556	.0589
-3	.0028	.0028	-3	.0131	.0133	.3	.0310	.0320	-3	.0562	.0595
.4	.0030	.0030	.4	.0134	.0136	.4	.0314	. 0324	.4	.0568	.0602
.5	.0031	.0031	.5	.0137	.0139	.5	.0319	. 0329	.5	.0574	. 0608
.6	.0032	.0032	.6	.0140	.0142	.6	.0323	.0334	.6	.0579	.0615
.7	.0034	.0034	.7	.0143	.0145	.7	.0327	.0338	.7	.0585	.0622
.8	.0035	.0035	.8	.0146	.0148	.8	.0332	.0343	.8	.0591	.0628
.9	.0037	.0037	.9	.0149	.0151	.9	.0336	.0348	.9	.0597	.0635
5.0	.0038	. 0038	10.0	.0152	.0154	15.0	.0341	.0353	20.0	.0603	.0642

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
20.0	. 0603	.0642	25.0	.0937	. 1034	30.0	.1340	. 1547	35.0	.1808	.2208
. т	, 0609	.0649	. т	.0944	.1043	т.	. 1348	. 1559	. т	.1819	.2223
.2	.0615	.0655	.2	.0952	.1052	.2	.1357	.1570	.2	. 1829	. 2238
-3	.0621	.0662	-3	.0959	.1061	-3	.1366	. 1582	-3	. 1839	. 2253
-4	. 0627	.0669	.4	.0967	.1070	.4	.1375	.1594	.4	. 1849	.2268
-5	.0633	.0676	-5	.0974	.1079	-5	.1384	. 1606	.5	. 1859	. 2283
.6	.0639	.0683	.6	.0982	.1089	.6	.1393	.1618	.6	.1869	.2299
.7	.0646	.0690	.7	. 0989	.1098	.7	.1401	.1630	.7	.1879	.2314
.8	.0651	. 0697	.8	.0997	.1107	.8 .9	.1410	.1642	.8 .9	.1889	.2329
.9		.0704	.9			1		.1666	36.0		.2361
21.0	.0664	.0711	26.0	.1012	.1126	31.0	.1428			.1910	
.I	.0670	.0719	. I	.1020	.1135	.1	. 1437	.1679 .1691	.1	.1920	.2376
.2	.0677	.0726	.2	.1027	.1145	.2	.1446	.1703	.2	.1930	.2408
	.0689	.0740		.1043	.1164		.1464	.1716	.4	.1951	.2424
.4 .5	.0696	.0748	·4 ·5	.1043	.1174	·4 ·5	.1474	.1728	.5	.1961	.2440
.6	.0702	.0755	.6	.1058	.1184	.6	.1483	.1741	.6	.1972	.2456
.7	.0709	.0763	.7	.1066	.1194	.7	.1492	.1753	.7	.1982	.2472
.8	.0715	.0770	.8	.1074	.1203	.8	.1501	1766	.8	.1993	.2489
.9	.0722	.0778	.9	.1082	.1213	.9	.1510	.1779	.9	.2003	.2505
22.0	.0728	.0785	27.0	.1090	.1223	32.0	.1520	.1792	37.0	.2014	.2521
. г	.0735	.0793	. т	.1098	.1233	. т	. 1529	. 1805	.1	.2024	.2538
.2	.0741	.0801	.2	.1106	.1243		. 1538	. 1818	.2	.2035	.2554
.3	.0748	.0808	-3	.1114	.1253	-3	.1547	.1831	.3	.2045	.2571
.4	.0755	.0816	-4	.1122	.1264		.1557	. 1844		. 2056	. 2588
- 5	.0761	.0824	-5	.1130	.1274		. 1566		.5	.2066	.2605
.6	.0768	.0832	.6	.1138	.1284		.1575	.1870		. 2077	.2622
.7	.0775	.0840	.7	.1146	.1294		.1585			.2088	.2639
.8	.0781	.0848	.8	.1154	.1305		.1594		.8	.2098	.2673
.9 23 .0	.0788		.9 28 .0		.1315		.1613	_	38.0	.2120	.2690
	.0795	.0864		.1171	.1326			-	1		
.I	.0802	.0872	.I	.1179	.1336		.1623		. I . 2	.2131	.2708
.2	.0809	.0888	.3	.1195	.1357		.1642			,2152	.2742
.3	.0822	.0896	.4	.1204	.1368	_	.1652	1	.4	.2163	1
.4 .5	.0822	.0904	-4	.1212	.1379		.1661			.2174	.2778
.6	.0836	.0913	.6	.1220	.1390		.1671		.6	.2185	.2796
.7	.0843	.0921	.7	.1229	.1401		.1680	.2020	.7	.2196	
.8	.0850	.0929	8	.1237	.1412		.1690		.8	.2207	.2831
.9	.0857	. 0938	.9	.1245	.1423	.9	.1700	.2048		.2218	.2849
24.0	.0865	.0946	29.0	. 1254	.1434	34.0	.1710	. 2062	39.0	. 2229	.2868
Ι.	.0872	.0955	т.	.1262	.1445	т.	.1719			.2240	
.2	.0879	.0963	.2	.1271	.1456		.1729			.2251	.2904
.3	.0886	.0972	-3	.1279	.146		.1739		_	. 2262	
.4	.0893	.0981	-4	.1288	.1478		.1749			.2273	
.5	.0900	.0989	.5	.1296	.1490		.1759		-	.2284	
.6	.0908	.0998	.6	.1305	.150	1	.1769				
.7	.0915	.1007	.7	.1314	.1512	1 1	.1779			.2306	1
.8	.0922	.1010	.9	.1322	.1524	1	.1798			.2328	_
25.0	.0937	.1034	30.0	.1340	.154		. 1808	-	- 1	.2340	
20.0	.0937	1.1034	150.5	1 . 1340	1.294	100.5	1 .2000	12360		1-54	10-54

Angl	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
40.0	.2340	.3054	45.0	.2929	.4142	50.0	.3572	-5557	55.0	.4264	-7434
Ι.	.2351	.3073	.I	. 2941	.4167	.r	.3586	.5590	.ı	.4279	.7478
.2	.2362	.3093	. 2	. 2954	.4192	.2	-3599	. 5622	.2	.4293	.7522
-3	.2373	.3102	.3	.2966	.4217	-3	.3612	. 5655	.3	.4307	.7566
.4	.2385	.3131	.4	. 2978	. 4242	-4	. 3626	. 5688	.4	. 4322	.7610
.5	.2396	.3151	.5	. 2991	.4267	.5	. 3639	.5721	.5	. 4336	.7655
.6	.2407	.3171	.6	.3003	.4293	.6	. 3653	-5755	.6	.4350	.7700
.7	.2419	.3190	.7	.3016	.4318	.7	.3666	.5788	.7	.4365	-7745
.8	.2430	.3210	.8	.3028	-4344	.8	.3680	.5822	.8	.4379	.7791
.9	.2441	.3230	.9	.3041	-4370	.9	. 3693	. 5856	.9	-4394	-7837
41.0	.2453	.3251	46.0	. 3053	.4396	51.0	.3707	. 5890	56.0	.4408	.7883
.I	.2464	.3270	ı,	.3066	.4422	.I	.3720	. 5925	.I	.4423	. 7929
.2	.2476	.3291	.2	.3079	.4448	.2	-3734	-5959	.2	-4437	.7976
.3	.2487	.3311	-3	.3091	-4474	-3	.3748	-5994	.3	.4452	
.4	.2499	.3331	-4	.3104	.4501	.4	.3761	. 6029 . 6064	-4	.4466 .4481	.8070 .8118
·5	.2510	·3352 ·3373	.6	.3116	.4527	.5 .6	.3775 .3789	.6004	·5 ·6	.4495	.8166
			.7	.3142	.4554		.3802	.6135	.7	.4510	.8214
.7 .8	.2534	.3393	.8	.3142	.4581	.7 .8	.3816	.6171	.8	.4524	.8263
.9	.2557	.3435	.9	.3167	.4635	.9	.3830	.6207	.9	4539	.8312
42.0	.2569	.3456	47.0	.3180	.4663	52.0	. 3843	.6243	57.0	-4554	.8361
1.	.2580	.3478	.1	.3193	.4690	т.	.3857	.6279	.1	. 4568	.8410
.1	.2592	.3499	.2	.3206	.4718	.2	.3871	.6316	.2	.4583	.8460
-3	.2604	.3520	-3	.3218	.4746	.3	.3885	.6353	.3	. 4598	.8510
.4	.2615	.3542	-4	.3231	.4774	.4	.3899	.6390	.4	.4612	.8561
	.2627	. 3563	-5	.3244	.4802	.5	.3912	.6427	-5	.4627	.8612
.5 .6	. 2639	.3585	.6	.3257	.4830	.6	.3926	.6464	.6	.4642	.8663
.7	. 2651	.3607	.7	.3270	. 4859	.7	.3940	.6502	.7	.4656	.8714
.8	. 2663	.3629	.8	. 3283	.4887	.8	-3954	.6540	.8	.4671	.8766
.9	. 2675	.3651	.9	. 3296	.4916	.9	. 3968	.6578	.9	. 4686	.8818
43.0	. 2686	.3673	48.0	. 3309	-4945	53.0	.3982	.6616	58.0	.4701	.8871
т.	. 2698	. 3696	ı.	.3322	-4974	ı.	. 3996	.6655	.I	.4716	.8924
.2	.2710	.3718	.2	-3335	.5003	.2	.4010	.6694	.2	. 4730	.8977
٠3	.2722	.3741	-3	.3348	.5032	-3	.4024	.6733	-3	·4745	.9031
.4	.2734	.3763	-4	.3361	.5062	-4	. 4038	.6772	-4	. 4760	.9084
·5	.2746	.3786	.5 .6	-3374	.5092	.5 .6	.4052	.6812	.5 .6	4775	.9139
	.2758	.3809	1	.3387	.5121	i e	.4066			.4790	.9194
.7 .8	.2770	.3832	.7	.3400	.5151	.7 .8	.4080	.6892	.7 .8	.4820	.9249
.9	.2702	.3055	.9	.3413	.5212	.9	.4094	.6972	.9	.4835	.9360
44.0	.2807	.3902	49.0	-3439	.5243		.4122	.7013	59.0	.4850	.9416
.1	.2819	-3902	.1	-3453	.5273	.1	.4136	.7054	.1	.4865	-9473
.1	.2831	3925	.1	.3453	.5273	.1	.4130	.7054	.2	.4880	
-3	.2843	.3949	.3	.3479	-5335	-3	.4165	.7137	-3	.4895	.9587
.4	.2855	.3996	.4	.3492	.5366		.4179	.7179	.4	.4910	.9645
.5	.2868	.4020	.5	.3506	.5398	-5	.4193	.7221	.5	.4925	.9703
.6	.2880	.4044	.6	.3519	.5429		.4207	.7263	.6	. 4940	.9762
.7	.2892	.4069	.7	.3532	.5461	.7	.4221	.7305	.7	. 4955	.9821
.8	.2904	.4093	.8	-3545	.5493	.8	.4236	.7348	.8	.4970	.9880
.9	.2917	.4118	.9	-3559	. 5525	.9	.4250	.7391	.9	.4985	.9940
45.0	.2929	.4142	50.0	.3572	-5557	55.0	.4264	.7434	60.0	.5000	1.0000

Amelo	Vers	Feee	A mode	Vers	E	1 11-	Vers	E
Angle		Exsec	Angle		Exsec	Angle		Exsec
60.0	.5000	1.0000	65.0	.5774	1.3662	70.0	.6580	1.9238
.1 .2	.5015	.0061	.I .2	. 5790 . 5805	.3751	.I	.6596 .6613	.9379
.3	.5030	.0122	.3	.5821	.3841	.3	.6629	.9521
.4	.5061	.0245	.4	.5837	.4022	.4	.6645	.9811
·4 ·5	.5076	1.0308	.5	.5853	1.4114	.5	.6662	1.9957
.6	.5091	.0371	.6	.5869	.4207	.6	.6678	2.0106
.7	.5106	.0434	.7	.5885	.4300	.7	.6695	.0256
.8	.5121	.0498	.8	.5901	-4395	.8	.6711	.0406
.9	.5137	.0562	.9	.5917	.4490	.9	.6728	.0561
61.0	.5152	1.0627	66.0	.5933	.4586	71.0	.6744	2.0716
r,	.5167	.0692	. т	.5949	.4683	ı.	.6761	.0872
.2	.5182	.0757	.2	. 5965	.4780	.2	.6777	. 1030
-3	.5198	.0824	-3	.5981	.4879	-3	.6794	.1190
.4	.5213	.0890	-4	-5997	. 4978	-4	.6810	.1352
.5	.5228	1.0957	.5	.6013	1.5078	.5	.6827	2.1515
.6	.5244	.1025	.6	.6029	.5180	.6	.6844	.1681
.7	.5259	.1093	.7	.6045	.5282	.7	.6860	.1848
.8	.5274	.1162	.8	.6061	.5384	.8	.6877	.2017
.9	. 5290	.1231	.9	.6077	.5488	.9	.6893	
62.0	.5305	.1301	67.0	. 6093	1.5593	72.0	.6910	2.2361
.1	.5321	.1371	.I	.6109	.5699	.1	.6926	.2535
.2	.5336 .5352	.1441	.2 .3	.6125 .6141	.5805	.2	.6943 .6960	.2891
	.5367	.1584		.6157	.6022		.6976	.3072
·4 ·5	.5383	1.1657	.4 .5	.6173	1.6131	4 ·5	.6993	2.3255
.6	.5398	.1730	.6	.6189	.6242	.6	.7010	.3440
.7	.5414	.1803	.7	.6205	.6354	.7	.7026	.3628
.8	-5429	. 1877	.8	.6222	.6466	.8	.7043	.3817
.9	-5445	. 1952	.9	.6238	. 6580	.9	. 7060	.4009
63.0	. 5460	I.2027	68.0	.6254	1.6695	73.0	.7076	2.4203
.1	.5476	.2103	.1	.6270	.6811	. I	.7093	-4399
.2	.5491	.2179	.2	,6286	.6927	.2	.7110	.4598
-3	. 5507	.2256	-3	. 6303	. 7046	-3	.7126	.4789
.4	.5522	.2333	-4	.6319	.7165	.4	.7143	.5003
·5 .6	- 5538	1.2412	.5 .6	.6335	1.7285	.5 .6	.7160	2.5209
	.5554	.2490		.6351	.7407		.7177	.5629
.7 .8	.5569 .5585	.2570	.7 .8	.636 7 .6384	.7529 .7653	.7 .8	.7193	.5843
.9	.5601	.2030	.9	.6400	.7778	.9	.7210	.6060
64.0	.5616	1.2812	69.0	.6416	.7904	74.0	.7244	2.6280
,1	.5632	.2894	.1	.6433	.8032	.1	.7260	.6502
.2	.5648	.2094	.2	.6449	.8161	.2	.7277	.6728
.3	.5663	.3060	-3	.6465	.8291	.3	.7294	.6955
.4	.5679	.3144	.4	.6482	.8422	.4	.7311	.7186
.5	. 5695	1.3228	.5	.6498	1.8554	-5	.7328	2.7420
.6	.5711	.3314	.6	.6514	.8688	.6	.7344	.7657
.7	. 5726	.3400	.7	.6531	.8824	.7	.7361	.7897
.8	.5742	. 3486	.8	.6547	.8960	.8	.7378	.8140
.9	.5758	-3574	.9	.6563	.9099	.9	-7395	.8387
65.0	- 5774	1.3662	70.0	.6580	1.9238	75.0	.7412	2.8637

					_			
Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
75.0	.7412	2.8637	80.0	.8264	4.7588	85.0	.9128	10.4737
I.	.7429	.8890	.I	.8281	.8164	.I	.9146	.7073
.2	.7446	.9147	.2	.8298	.8751	.2	.9163	.9506
.3	.7462	.9408	.3	.8315	.9351	٠3	.9181	11.2043
.4	.7479	.9672	-4	.8332	.9963	.4	.9198	. 4690
.5 .6	.7496	2.9939 3.02II	.5 .6	.8350 .8367	5.0589	·5 .6	.9215	11.7455
	.7513						.9233	
.7 .8	-7530	.0486	.7 .8	.8384 .8401	.1880 .2546	.7 .8	.9250 .9268	.3371 .6541
.9	.7547 .7564	.1048	.9	.8418	.3228	.9	.9285	.9865
76.0	.7581	3.1336	81.0	.8436	5.3925	86.o	.9302	13.3356
		.1627	.1	.8453	.4637	.1	.9320	.7026
.ī .2	.7598 .7615	.1027	.1	.8470	.5366	.1	.9320 -9337	14.0889
.3	.7632	.2223	.3	.8487	.6111	.3	-9355	.4961
.4	.7649	.2527	.4	.8505	.6874	.4	.9372	.9260
.5	.7666	3.2837	-5	.8522	5.7655	.5	.9390	15.3804
.6	.7683	.3150	.6	.8539	.8454	.6	.9407	.8616
.7	.7700	.3469	.7	.8556	.9273	.7	.9424	16.3720
.8	.7716	.3792	.8	.8574	6.0112	.8	.9442	.9142
.9	-7733	.4121	.9	.8591	.0972	.9	.9459	17.4915
77.0	.7750	3.4454	82.0	.8608	6.1853	87.0	-9477	18.1073
ı.	.7767	·4793	.ı	.8626	.2757	.ı	.9494	. 7656
.2	.7785	.5137	.2	.8643	.3684	.2	.9512	19.4709
-3	.7802	.5486	.3	.8660	.4635	-3	.9529	20,2285
.4	.7819	.5841	.4	.8677	.5611	-4	.9546	21.0444
-5	.7836	3.6202	-5	.8695	6.6613	-5	.9564	21.9256
.6	.7853	.6569	.6	.8712	.7642	.6	.9581	22.8802
.7	.7870	.6942	.7	.8729	.8700	.7	.9599	23.9179
.8	.7887	.7320	.8	.8747	.9787	.8	.9616	25.0499
.9	.7904	.7706	.9	.8764	7.0905	.9	.9634	26.2898
78.0	.7921	3.8097	83.0	.8781	7.2055	88.0	.9651	27.6537
I.	.7938	.8496	ı.	.8799	.3238	.I	.9668	29.1612
.2	-7955	.8901	.2	.8816 .8833	.5711	.2	.9686	30.8362
-3	.7972	.9313	-3			-3	.9703	
-4	.7989 .8006	.9732 4.0159	-4	.8851	7.8337	-4	.9721 .9738	34.8145
.6	.8023	.0593	.5 .6	.8885	.9711	.5 .6	.9756	39.9296
.7	.8041	.1034	.7	.8903	8.1129	.7	.9773	43.0775
.8	.8058	.1034	.8	.8920	.2593	.8	.9773	46.7500
.9	.8075	.1942	.9	.8937	.4105	.9	.9808	51.0903
79.0	.8092	4.2408	84.0	.8955	8.5668	89.0	.9825	56.2987
.т	.8100	.2883	.1	.8972	.7283	.1	.9843	62.6646
.2	.8126	.3367	.2	.8989	.8955	.2	.9860	70.6221
-3	.8143	.3860	.3	.9007	9.0685	-3	.9878	80.8532
.4	.8160	.4362	.4	.9024	.2477	-4	.9895	94.4947
.5	.8178	4.4874	-5	.9042	9.4334	-5	.9913	113.5930
.6	.8195	.5396	.6	.9059	.6261	.6	.9930	142.2406
.7	.8212	.5928	.7	.9076	.8260	.7	.9948	189.9868
.8	.8229	.6470	.8	.9094	10.0336	.8	.9965	285.4795
.9	.8246	.7023	.9	.9111	.2493	.9	.9983	571.9581
80.0	.8264	4.7588	85.0	.9128	10.4737	90.0	1.0000	∞

TABLE XXIX

			S	econo	ls in decir	nals	of a degree	Э			
Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree
1 2 3 4 5	0.00028 0.00056 0.00083 0.00111 0.00139	11 12 13 14 15	0.00306 0.00334 0.00361 0.00389 0.00417	2I 22 23 24 25	0.00584 0.00612 0.00639 0.00667 0.00695	31 32 33 34 35	0.00862 0.00890 0.00917 0.00945 0.00973	41 42 43 44 45	0.01139 0.01167 0.01195 0.01222 0.01250	51 52 53 54 55	0.01417 0.01445 0.01473 0.01500 0.01528
6 7 8 9	0.00167 0.00195 0.00222 0.00250 0.00278	16 17 18 19 20	0.00445 0.00473 0.00500 0.00528 0.00556	26 27 28 29 30	0.00723 0.00751 0.00778 0.00806 0.00834	36 37 38 39 40	0.01000 0.01028 0.01056 0.01083 0.01111	46 47 48 49 50	0.01278 0.01306 0.01334 0.01361 0.01389	56 57 58 59 60	0.01556 0.01584 0.01612 0.01639 0.01667

TABLE XXX

			М	inutes	in decir	nals of	a degree	;			
Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree
1 2 3 4 5	0.01667 0.03333 0.05000 0.06667 0.08333	12 13 14	0.18333 0.20000 0.21667 0.23333 0.25000	22 23	0.35000 0.36667 0.38333 0.40000 0.41667	32 33 34	0.51667 0.53333 0.55000 0.56667 0.58333	42 43	0.68333 0.70000 0.71667 0.73333 0.75000	52 53	o.85000 o.86667 o.88333 o.90000 o.91667
6 7 8 9	0.10000 0.11667 0.13333 0.15000 0.16667	17 18 19	0.26667 0.28333 0.30000 0.31667 0.33333	27 28 29	0.43333 0.45000 0.46667 0.48333 0.50000	37 38 39	o.60000 o.61667 o.63333 o.65000 o.66667	47 48	o.76667 o.78333 o.80000 o.81667 o.83333	57 58 59	0.93333 0.95000 0.96667 0.98333 1.00000

From Roberts' "Track Formulæ and Tables."

CHAPTER IV

LOCATION THEORIES AND TABLES

For problems relating to improvements of existing lines exact data and volumes of discussion of methods will be available. The methods here suggested are for use in locating new lines for which precise data respecting motive power, business, or expense are indeterminate. Most of the problems will relate to saving in operation of freight trains. A single locomotive may be assumed, since in the solution of problems the results will be practically the same relatively for any probable differences in locomotives. It must be remembered that not all of the trains will be affected by probable changes in ruling grades; the engineer must use his judgment in determining what trains will be affected. All trains must be considered in estimating the cost of distance, rise and fall, and curvature. The formulas given in what follows are based on the full discussion of the subjects in the author's "Elements of Railroad Engineering."

Tractive Effort. — For approximate computations the tractive effort of a locomotive may be assumed to be

$$T_b = \frac{146 \, H}{S}$$
 pounds, $T_c = \frac{P d^2 L}{D}$ pounds, $T_a = \frac{W}{4.25}$ pounds if W is pounds,

or

in which H is the square feet of heating surface.

S is the speed in miles per hour.

P is the mean effective pressure in the cylinders.

d is the diameter of the piston.

L is the length of the stroke.

D is the diameter of the drive wheels.

W is the weight on the drive wheels.

 T_b is to be used for speeds above that for which $T_b = T_c$ when P is 85 per cent of the working boiler pressure, and is known as the boiler

tractive effort; T_a is used only in case it is less than T_c for P=85 per cent of the boiler pressure. It is the tractive effort of adhesion and all that the locomotive can exert under normal conditions regardless of the values of T_b and T_c . T_c is called the cylinder tractive effort. T_a has been known to be as high as $\frac{W}{3}$, with sand on the track, and

it is probably as low as $\frac{W}{5}$ under unfavorable conditions of track. Theoretic values of T_b for a particular consolidation locomotive are tabulated in Table XXXIII.

Resistance. — Resistance to motion on a straight level track varies with speed and weight per car of train; it may be taken from Table XXXII. Grade resistance or acceleration is given by $R_g = 20 r$, in which R_g is resistance in pounds per ton and r is the rate per cent of grade expressed as a whole or mixed number; thus for a 2 per cent grade r is 2.0, etc. Curve resistance in pounds per ton varies with the degree of curve, somewhat with speed, being less as the speed is greater, and with the rigid wheel base of the car or locomotive. It may be averaged for a train at

$$R_c = 0.4 + 0.35 D$$

in which R_c is curve resistance in pounds per ton and D is the degree of curve. This is an empirical equation that does not vanish when D is 0 as it should to be mathematically correct. Ruling grades or others likely ever to become ruling because of the curves on them should be reduced or "compensated" in rate per cent through all curves as follows: For 1° curves reduce 0.04 per cent; for curves from 2° to 4° reduce 0.03 D per cent; for curves of 5° and over reduce 0.025 D per cent. Greater reductions will do no harm unless they make a steeper ruling grade necessary.

To Find the Maximum Load a Locomotive can Haul on a Given Grade at a Given Speed. — From Table XXXII find the train resistance for an assumed or known car weight at the given speed; add the grade resistance = 20 r, and divide the tractive effort for the given speed by the sum; subtract the weight of engine and tender. The values for a particular consolidation engine are tabulated in Table XXXIV.

Pusher Grade.— To find the grade up which two similar locomotives can haul the load that one can haul on a given grade. If X be the rate of grade sought,

$$X = \frac{\frac{1.9 \, T}{W + 2 \, E} - R_t}{\frac{20}{}},$$

in which R_t is train resistance in pounds per ton, T is the tractive effort of one locomotive, W is the weight of the train and E the weight of one locomotive and tender both in tons. If there are to be three locomotives the corresponding pusher grade is

$$X = \frac{\frac{2.85 T}{W + 3E} - R_t}{\frac{20}{20}}.$$

To Find the Length of Up Grade Required to Reduce the Speed from S₁ to S₂ Miles an Hour for a Given Locomotive and Train. — This is the so-called momentum or velocity grade problem and finds the length of grade steeper than the ruling grade that can still be operated if a sufficient velocity of approach may be had.

Let r be the rate of the grade steeper than that for which the locomotive is loaded. Find the tractive effort for the average speed; add the weight of the train and locomotive for gross load W in tons; find the train resistance R_t for the train at the average speed; find the quantity

$$V = \frac{I}{20} \left(\frac{T}{W} - R_t \right);$$

find the velocity heads for the speeds S1 and S2 from Table XXXI, then

$$L \text{ stations} = \frac{\text{difference in velocity heads}}{r - V};$$

V is the virtual grade, or grade that the locomotive can work at the given speed with the given load. If the steep grade differs only a little from the ruling grade for the given S_2 , the result is inaccurate but errs on the safe side, giving a grade somewhat shorter than true theory indicates.

Grades for Unbalanced Traffic. — If traffic is pretty certain to be permanently unbalanced with respect to direction of haul the grade against the lighter traffic may be steeper than that against the heavier traffic if economy of construction will result. The same number of engines and cars must go both ways, hence the lighter traffic trains will have a higher resistance per ton because the average car weight will be less. Having the ruling grade against the heavy traffic determined, the corresponding grade for a traffic in the opposite direction is found as follows:

Find the load that the assumed or known locomotive can haul behind the tender at a speed of about ten miles an hour on the ruling grade against the heavy traffic, using an assumed or known car weight to determine train resistance. If there is much variation in the traffic subtract the weight of the cars (taken at about 18 tons per car for preliminary purposes) from the load, reduce the remaining live or freight load by the assumed percentage of unbalancing, add the car weights and get the new total load and average car weight. Find the train resistance for the new car weight. If R_t be that resistance, T the tractive effort of the locomotive, E the weight of engine and tender and E the load behind the tender, then the grade, E0, against the lighter traffic may be

$$G = \frac{I}{20} \left(\frac{T}{L+E} - R_t \right).$$

The caboose or way car has not been considered. For a greater degree of precision than such problems generally warrant its weight should be included with the engine weight *E*.

Elements for Estimating.—1. Distance. — To estimate the cost of operating extra distance or the saving due to reducing distance assume a probable average train mile cost and assume a number of trains per day over the distance under consideration. All trains going both ways are to be included. Then if C be the train mile cost in dollars, M the miles of extra distance under consideration, and N the number of daily trains, the annual cost of operating the M miles, or the annual saving by omitting M miles, is given approximately by

$$K = 156 C \cdot M \cdot N$$

for moderate changes in distance.

The limit of justifiable expenditure to reduce the distance in miles is $\frac{K}{r}$, where r is the going rate of interest which should be taken somewhat higher than the nominal rate specified in the company's bonds. In the formula it should be used as a decimal, thus 8 per cent = 0.08. For large changes in long lines the coefficient may be increased up to, say, 315 for a change involving the addition of a whole division.

The average train mile cost for the United States is not far from \$1.55 in 1914. The figures for the year have not been computed at this writing. The cost has been increasing for a number of years, but recent economies have checked this increase somewhat. In 1908 the average cost was about \$1.47. The Interstate Commerce Commission divides the country into three great districts for reporting savings and expenses, the Eastern, Southern, and Western. The Eastern district comprises that portion of the country bounded on the west by the northern and western shores of Lake Michigan to Chicago, thence by a line to Peoria, thence to East St. Louis, thence down the Mississippi River to the

mouth of the Ohio River; and on the south by the Ohio River from its mouth to Parkersburg, West Virginia, thence by a line to the southwestern corner of Maryland, thence by the Potomac River to its mouth. The Southern district comprises the territory south of the Eastern district and east of the Mississippi River. The Western district includes the remainder of the United States, exclusive of Alaska and insular possessions.

The Commission also divides the railroads into three classes:

- I. Roads with annual gross operating revenues of \$1,000,000 or
- II. Roads with annual gross operating revenues of \$100,000 or more but less than \$1,000,000.
- III. Roads with annual gross operating revenues of less than \$100,000.

 Average train mile costs for the three classes in the three districts may be taken for purposes of estimating as follows (1914):

District	Class I	Class II	Class III
Eastern	\$1.60	\$1.19	\$1.02
	1.38	1.15	1.10
	1.59	1.52	1.45

2. Rise and Fall. — Rise and fall between any two points is the total vertical feet of rising grade with its corresponding vertical feet of fall. If the two points are at different levels it requires a round trip to realize the rise and fall due to this difference. In calculating the cost of rise and fall as between two lines, only the cost of the difference in rise and fall is of consequence and hence the following rule is satisfactory though inaccurate for a train going one way.

To find the rise and fall between two points add all vertical feet of rising grades and all vertical feet of falling grades and divide by two.

Three classes of rise and fall are recognized:

Class A. Rise and fall of small amounts on light grades apparently not felt by the locomotive, requiring no apparent change in effort, only varying the speed a little.

Class B. Rise and fall requiring the full power of the locomotive in the ascent, the shutting off of steam in the descent, but no use of brakes.

Class C. Rise and fall requiring the whole power of the locomotive in the ascent and the use of brakes and sometimes of sand on the descent.

If C be the train mile cost, N the number of daily trains (all trains both ways) and f the number of feet of rise and fall, the annual cost for operation may be estimated as follows — the result being in dollars.

Class A. $K_1 = 0.25 f \cdot C \cdot N$. Class B. $K_1 = 1.2 f \cdot C \cdot N$. Class C. $K_1 = f \cdot C \cdot N \times$ the factor of the following

Grade	0.4 and under	0.5	0.67	1.0	1.5	2.0	2.5	3.0	3.5	4.0
Cost factor	2.4	2.9	3.6	4.2	4.6	4.8	4.9	5.0	5.05	5.1

table.

The limit of justifiable expenditure to reduce the rise and fall by f feet is $\frac{K_1}{r}$, where r is the going rate of interest which should be somewhat larger than the rate of the company's bonds, and in the formula is to be expressed as a decimal, *i.e.*, 8 per cent = 0.08.

3. Curvature. — If C be the train mile cost and N the number of daily trains (all trains both ways) the annual operating cost saved by eliminating D degrees of curvature is found as follows, the result being in dollars:

$$K_2 = DC$$
 (0.11 $N + 2.55$),

and the limit of justifiable expenditure to eliminate D° of curvature is $\frac{K_2}{r}$, in which r is the going rate of interest expressed as a decimal and should be somewhat larger than that carried by the company's bonds.

4. Ruling Grade. — This is the most important of the four elements of location. The value of reducing the ruling grade from one rate to another is found by finding the saving in train miles due to the larger loads possible on the lighter grades and is assumed to be approximately proportional to the reduction in number of train miles. The ruling grade determines the weight of train for the whole operating division on which the grade occurs. The relative number of trains on two different ruling grades are assumed to be inversely as the loads behind the tender. To find the load behind the tender see page 259. If W be the train weight for ruling grade g and W' be the train weight for ruling grade g' and if N' be the number of daily trains one way to do a

given business on g', the number of trains to do the same business on g will be

$$N = \frac{W'}{W} N'.$$

If g' is steeper than g, the saving in daily trains one way will be N' - N, and the total train miles saved will be 2 (N' - N) L, L being the length of the division in miles. Having found this, substitute in the following formula for annual saving due to reduction in ruling grade from g' to g, C being the train mile cost on g'.

$$K_3 = 730 LC \left(0.43 (N' - N) - \frac{W - W'}{10 W'} N \right).$$

The N's of the foregoing discussion include only those full weight trains affected by the change. If the grade reduction is obtained at the expense of distance the extra distance should be figured against the improvement considering all trains to be run on the g grade and a train mile cost somewhat larger than C, say $\left(1 + \frac{W}{20\ W'}\right)C$, which supposes that about half the total trains may be affected. Precision is impossible. If rise and fall is reduced by the change the reduction should be credited to the change considering all trains for the g' grade at a train mile cost of C.

Table XXXV gives the relative number of trains for a consolidation locomotive for various grades. To use it for a reduction from an 0.8 per cent grade to a 0.6 per cent grade, there being 10 daily trains on the 0.8 per cent grade, divide the tabular quantity under 12 miles opposite 0.8 by that opposite 0.6 and multiply by 10. In any problem the maximum hauling capacity would probably be considered and hence the lower speeds. For fast freights slightly higher speeds may be considered. The limit of justifiable expenditure to reduce the ruling grade of the division from g' to g is $\frac{K_3}{r}$, in which r is the going interest rate expressed as a decimal and should be somewhat larger than the nominal rate carried by the company's bonds.

Cost of Pusher Service. — When helper engines must be maintained at intermediate points on a line the annual cost in dollars may be estimated as follows if the helpers can be kept busy:

$$K_4 = 155 \cdot N \cdot M,$$

in which N is the number of trains helped daily and M is the length of the pusher incline in miles. If the helper engine is not kept busy, say, making 100 miles a day, the part of 100 miles not run may be estimated to cost half as much per mile as the miles that are run.

TABLE XXXI. — Velocity Heads in Feet for Speed in Miles per Hour

Formula: $h = 0.035 s^2$

				1	1	1 = 0.03				
Speed	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03
1	0.03	0.04	0.05	0.06	0.07	0.08	0.09	0.10	0.11	0.13
2	0.14	0.15	0.17	0.19	0.20	0.22	0.24	0.26	0.27	0.29
3	0.31	0.34	0.36	0.38	0.40	0.43	0.45	0.48	0.51	0.53
4	0.56	0.59	0.62	0.65	0.68	0.71	0.74	0.77	0.81	0.84
5	0.87	0.91	0.95	0.98	1.02	1.06	1.10	1.14	1.18	I.22
6	1.26	1.30	1.35	1.39	1.43	1.48	1.52	1.57	1.62	1.67
7	1.72	1.76	1.81	1.87	1.92	1.97	2.02	2.08	2.13	2.18
8	2.24	2.30	2.35	2.41	2.47	2.53	2.59	2.65	2.71	2.77
9	2.84	2.90	2.96	.3.03	3.09	3.16	3.23	3.29	3.36	3.43
10	3.50	3.57	3.64	3.71	3.79	3.86	3.93	4.01	4.08	4.16
11	4.24	4.31	4.39	4.47	4.55	4.63	4.71	4.79	4.87	4.96
12	5.04	5.12	5.21	5.29	5.38	5.47	5.56	5.65	5.73	5.82
13	5.91	6.01	6.10	6.19	6.28	6.38	6.47	6.57	6.66	6.76
14	6.86	6.96	7.06	7.16	7.26	7.36	7.46	7.56	7.67	7.77
15 16	7.87	7.98	8.09	8.19	8.30	8.41	8.52	8.63	8.74	8.85
17	8.96	9.07	9.18	9.30	9.41	9.53 10.72	9.64	9.76 10.97	9.88	10.00 II.2I
18					11.85	11.98			1	
18	11.34	II.47 I2.77	11.59	11.72	13.17	13.31	12.11	12.24 13.58	12.37	12.50
20	14.00	14.14	14.28	14.42	14.57	14.71	14.85	15.00	13.72	15.29
21	15.44	15.58	15.73	15.88	16.03	16.18	16.33	16.48	16.63	16.79
22	16.94	17.10	17.25	17.41	17.56	17.72	17.88	18.03	18.19	18.35
23	18.52	18.68	18.84	19.00	19.17	19.33	19.50	19.66	19.82	19.99
24	20.16	20.33	20.50	20.67	20.84	21.01	21.18	21.35	21.53	21.70
25	21.88	22.05	22.22	22.40	22.58	22.76	22.94	23.12	23.30	23.48
26	23.66	23.84	24.03	24.21	24.40	24.58	24.77	24.95	25.14	25.33
27	25.52	25.70	25.90	26.09	26.28	26.47	26.66	26.86	27.05	27.25
28	27.44	27.64	27.83	28.03	28.23	28.43	28.63	28.83	29.03	29.23
29	29.44	29.64	29.84	30.05	30.25	30.46	30.67	30.88	31.08	31.29
30	31.50	31.71	31.92	32.13	32.35	32.56	32.78	32.98	33.20	33.42
31	33.64	33.85	34.07	34.29	34.51	34.73	34.96	35.18	35.40	35.62
32	35.84	36.06	36.29	36.52	36.74	36.97	37.19	37.42	37.65	37.88
33	38.11	38.34	38.58	38.81	39.05	39.27	39.51	39.75	39.98	40.22
34	40.46	40.70	40.94	41.18	41.42	41.66	41.90	42.14	42.38	42.63
35	42.87	43.12	43.37	43.61	43.86	44.11	44.36	44.61	44.86	45.11
36	45.36	45.61	45.87	46.12	46.38	46.63	46.88	47.14	47.40	47.66
37	47.91	48.18	48.43	48.70	48.96	49.22	49.48	49.74	50.01	50.28
38	50.54	50.81	51.08	51.34	51.61	51.88	52.16	52.42	52.69	52.96
39	53.24	53.51	53.78	54.06	54.34	54.61	54.89	55.17	55.44	55.72
	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
40	56.00	58.84	61.74	64.72	67.76	70.88	74.06	77.32	80.64	84.03
50 60	87.50 126.00	91.03	94.64	98.31 138.92	102.06	105.77	109.75 152.45	113.72 157.11	117.74	121.83
70		176.45	181.44	186.52		196.88	202.16			_
80	171.50 224.00	229.60	235.33	180.52	191.65 246.95	257.88	258.84	207.52 264.91	2I2.94 27I.04	218.42
90	283.50	289.82	296.23	302.70	309.25	315.86	322.55	329.31	336.15	343.05
100	350.00	29.02	- 50.23		359.23	323.00	022.33	J=5.31	330,23	343.03
100	330.00									

Note. — For the table the theoretical heads have been increased 4.63 per cent to allow for the energy of the rotating wheels.

TABLE XXXII. — TRAIN RESISTANCE AT DIFFERENT SPEEDS AND FOR TRAINS OF VARIOUS AVERAGE CAR WEIGHTS

									_					
Speed,				Tr	ain re	sistan	ce, po	unds į	per to	n*				Speed,
miles										60	6-			miles per
hour	tons	tons	25 tons	30 tons	35 tons	40 tons	45 tons	50 tons	55 tons	tons	65 tons	70 tons	75 tons	hour
<u></u>														
5 6	7.6	6.8	6.0	5.4	4.8	4.4	4.0	3.7	3.5	3.3	3.2	3. I	3.0	5 6
	7.7	6.9	6.1	5.5	4.9	4.4	4.I	3.8	3.5	3.3	3.2	3. I	3.0	
7 8	7.8 8.0	7.0	6.2	5.5 5.6	5.0	4.5	4.1	3.8	3.6	3.4	3.2	3.1	3.1	7 8
9	8.1	7.I 7.2	6.4	5.0	5.0 5.1	4.6	4.2	3.9	3.6	3.4	3.3	3.2	3. I 3. I	9
10	8.2	7.3	6.5	5.8	5.2	4.7	4.3	4.0	3.7	3.5	3.3	3.2	3.2	10
11	8.3	7.4	6.6	5.9	5.3	4.8	4.3	4.0	3.7	3.5	3.4	3.3	3.2	11
12	8.4	7.5	6.7	6.0 6.1	5.4	4.8	4.4	4.0	3.8	3.6	3.4	3.3	3.3	12
13	8.7	7.6	6.9	6.2	5·5 5·5	4.9 5.0	4.5	4.I 4.2	3.8	3.6	3.5	3.4	3.3	13
14 15	8.8	7.9	7.0	6.3	5.6	5.U 5.I	4.6	4.2	3.9	3.7	3.5	3.4	3.4	14 15
16	9.0	8.0	7.1	6.4	5.7	5.1	4.7	4.3	4.0	3.8	3.6	3.5	3.5	16
17	9.1	8.1	7.2	6.5	5.8	5.2	4.8	4.4	4.I	3.9	3.7	3.6	3.5	17
18	9.3	8.3	7.4	6.6	5.9	5.3	4.8	4.5	4.I	3.9	3.7	3.7	3.6	18
19	9.4	8.4	7.5 7.6	6.7	6.0 6.1	5.4	4.9	4.5 4.6	4.2	4.0	3.8	3.7	3.6	19
20 21	9.0	8.7	7.0	6.9	6.2	5.5 5.6	5.0 5.I	4.0	4.3	4.0 4.1	3.9	3.8	3.7 3.8	20 21
22	9.9	8.8	7.9	7.0	6.3	5.7	5.2	4.8	4.4	4.2	4.0	3.9	3.8	22
23	10.0	9.0	8.0	7.1	6.4	5.8	5.3	4.9	4.5	4.3	4.I	4.0	3.9	23
24	10.2	9.1	8.1	7.3	6.6	5.9	5.4	4.9	4.6	4.3	4.2	4.I	4.0	24
25	10.4	9.3	8.3	7.4	6.7	6.0	5.5	5.0	4.7	4.4	4.2	4. I	4.0	25
26 27	10.5	9.4	8.4 8.5	7.5	6.8	6.1	5.6 5.7	5.1 5.2	4.8	4.5 4.6	4.3	4.3	4.I 4.2	26 27
28	10.9	9.7	8.7	7.8	7.0	6.3	5.8	5.3	4.9	4.7	4.5	4.4	4.2	28
29	11.1	9.9	8.8	7.9	7.1	6.5	5.9	5.4	5.0	4.8	4.6	4.5	4.4	29
30	11.3	10.0	9.0	8.0	7.3	6.6	6.0	5.5	5.1	4.9	4.7	4.5	4.5	30
31	11.4	10.2	9.1	8.2	7-4	6.7	6.1	5.6	5.2	5.0	4.8	4.6	4.5	31
32 33	11.6	10.4	9.3 9.4	8.3 8.5	7.5 7.6	6.8 7.0	6.2	5.8	5.3 5.4	5.0	4.9 5.0	4.7	4.6	32
34	12.0	10.5	9.4	8.6	7.8	7.1	6.5	6.0	5.4	5.2	5.0 5.I	4.0	4.7 4.8	33 34
35	12.3	10.9	9.7	8.8	7.9	7.2	6.6	6.1	5.7	5.4	5.2	5.0	4.9	35
36	12.5	II.I	9.9	8.9	8.0	7.4	6.7	6.2	5.8	5.5	5.3	5.1	5.0	36
37	12.7	11.2	10.0	9.0	8.2	7.5	6.9	6.4	5.9	5.6	5.4	5.2	5.1	37
38	12.9	11.4	10.2 10.4	9.2	8.3	7.6 7.8	7.0	6.5	6.0	5.7	5.5	5.3	5.2	38
39 40	13.1 13.4	11.8	10.4	9.4 9.5	8.6	7.8	7.I 7.3	6.8	6.3	5.8 6.0	5.6 5.7	5.4	5.3 5.5	39 40
	1-5/4			5.5		1.9	7.3	5.0	0.3		3.7	3.0	3.3	

^{*} Column headings indicate the average car weights.

This table from experiments of Professor Edward C. Schmidt of the University of Illinois. See Transactions of the American Society of Mechanical Engineers for 1910.

TABLE XXXIII

TRACTIVE EFFORT IN POUNDS OF THE CONSOLIDATION LOCOMOTIVE, HAVING THE CHARACTERISTICS GIVEN BELOW, FOR DIFFERENT SPEEDS. NEAREST 50 POUNDS

Speed	0.0	10.0	20.0	30.0
0.0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 5.0 5.0 6.5 7.0 7.5 8.5 9.0	spunod coo'oS	50,000 50,000 48,700 44,800 43,100 41,500 40,000 38,650 37,350 36,150 33,950 32,950 32,950 32,000 31,100 30,300 29,500 28,750	28,000 27,350 26,700 26,050 25,450 24,900 24,350 23,850 22,400 21,950 21,950 21,150 20,750 20,000 19,650 19,000	18,650 18,350 18,950 17,800 17,500 17,250 16,700 16,500 16,250 16,000 15,800 15,350 15,350 15,150 14,750 14,750 14,550 14,550 14,550

Consolidation locomotive.

Weight on drivers: 210,000 pounds.

Weight of engine and tender: 400 00

Weight of engine and tender: 400,000 pounds.

Cylinders: 28" diam. by 32" stroke. Heating surface: 3837 sq. ft.

Diameter drive wheels: 63".

Boiler working pressure: 163 pounds.

For this locomotive:

 $T_c = 55,174 \text{ pounds (say 55,000 pounds);}$

 $T_a = 49,412$ pounds (say 50,000 pounds);

 $T_b = 50,000$ pounds at II.2 mi./hr., and as T_a limits the effort, this will be taken as constant and equal to 50,000 pounds at speeds below II mi./hr.

TABLE XXXIV

NET LOADS IN TONS OF 2000 POUNDS BEHIND THE TENDER OF THE CONSOLIDATION LOCOMOTIVE OF TABLE XXXIII, ON GIVEN GRADES AT GIVEN SPEEDS

Speed	Under	15	20	25	30	35	40
Grade	11 1111						
0.00	11430	7918	5400	3873	2908	2224	1718
.05	9234	6468	4467	3246	2464	1905	1487
.10	7736	5458	3800	2787	2131	1660	1305
.15	6650	4714	3300	2435	1872	1467	1159
.20	5825	4142	2911	2158	1665	1310	1039
.25	5177	3690	2600	1934	1495	1179	938
.30	4655	3323	2346	1748	1354	1070	853
-35	4225	3019	2134	1592	1235	977	779
.40	3866	2764	1954	1459	1132	896	715
-45	3560	2546	1800 1667	1345	1043	826	659
.50 -55	3297 3068	2358 2194	1550	1245 1158	966 897	764 709	609 565
.6o	2868	2050	1447	1080	836	660	525
.65	2691	1922	1356	1011	782	616	490
.70	2533	1808	1274	949	733	577	457
.75	2391	1706	1200	893	688	541	428
.80	2263	1613	1133	842	648	508	401
.85	2148	1529	1073	795	611	478	376
.90	2042	1453	1017	753	577	450	353
.95	1946	1382	967	714	546	425	332
1.00	1858	1318	920	678	517	401	313
.05	1776	1259	877	645	491	380	295
.10	1702	1204	837	615	466	359	278
.15	1632	1153	800	586	443	341	262
.20	1567	1106	765	559	422	323	247
.25	1507	1062	733	534	402	306	233
.30	1450	1020	703	511	383	291	220
-35	1398	982	675	489 469	365	276 262	208
.40 .45	1348 1302	946 911	649 624	409 449	348 333	249	197 186
.50	1258	879	600	449 43I	318	237	175
.55	1250	849	578	431	304	226	166
.60	1178	820	557	397	291	214	156
.65	1141	793	537	382	278	204	147
.70	1106	768	518	367	266	194	139
.75	1072	743	500	353	255	185	131
.80	1041	720	483	340	244	176	123
.85	1011	698	467	327	234	167	116
.90	982	677	451	315	224	159	109
.95	955	657	436	303	214	151	102
2.00	929	637	422	292	205	143	96

The average car weight for this table is 45 tons.

TABLE XXXV.—Relative Number of Trains to do the Same Business Tonnage on Different Grades, for Different Speeds. Computed from Table XXXIV

Speed	Under	15	20	25	30	35	40
0.00	0.34	0.49	0.72	1.00	1.33	1.74	2.25
0.05	0.42	0.60	0.87	1.19	1.57	2.03	2.60
0.10	0.50	0.71	1.02	1.39	1.81	2.33	2.96
0.15	0.58	0.82	1.17	1.59	2.07	2.64	3.34
0.20	0.66	0.93	1.33	1.79	2.32	2.95	3.72
0.25	0.75	1.05	1.49	2.00	2.59	3.29	4.12
0.30	0.83	1.16	1.65	2.21	2.86	3.61	4.53
0.35	0.92	1.28	1.81	2.43	3.13	3.96	4.96
0.40	1.00	1.40	1.98	2.65	3.42	4.31	5.41
0.45	1.09	I.52	2.15	2.87	3.71	4.68	5.87
0.50	1.17	1.64	2.32	3.11	4.00	5.06	6.35
0.55	1.26	1.76	2.49	3.34	4.31	5.45	6.84
0.60	1.35	1.89	2.67	3.58	4.62	5.86	7.36
0.65	I.44	2.01	2.85	3.82	4.94	6.28	7.89
0.70	1.53	2.14	3.03	4.07	5.27	6.70	8.46
0.75	1.62	2.27	3.22	4.33	5.62	7.15	9.03
0.80	1.71	2.40	3.41	4.59	5.97	7.61	9.64
0.85	1.80	2.53	3.60	4.86	6.33	8.09	10.28
0.90	1.89	2.66	3.80	5.13	6.70	8.59	10.95
0.95	1.99	2.80	4.00	5.41	7.08	9.10	11.64
1.00	2.08	2.93	4.20	5.70	7.48	9.64	12.35
1.05	2.18	3.07	4.41	5.99	7.87	10.17	13.10
1.10	2.27	3.21	4.62	6.29	8.30	10.77	13.91
1.15	2.37	3.35	4.83	6.60	8.73	11.34	14.76
1.20	2.47	3.50	5.05	6.92	9.16	11.97	15.65
1.25	2.57	3.64	5.27	7.24	9.62	12.63	16.59
1.30	2.67	3.79	5.50	7.57	10.09	13.29	17.57
1.35	2.77	3.94	5.73	7.91	10.59	14.01	18.59
1.40	2.87	4.09	5.96	8.24	II.II	14.76	19.63
1.45	2.97	4.24	6.20	8.61	11.61	15.53	20.79
1.50	3.07	4.40	6.44	8.97		16.31	22.09
1.55	3.18	4.55	6.69	9.34	12.72	17.11	23.29
1.60	3.28	4.71	6.94	9.74	13.29	18.07	24.78
1.65	3.39	4.87	7.20	10.12	13.91	18.95	26.30
1.70	3.50	5.03	7.46	10.53	14.53 15.16	19.93	27.82
1.75 1.80	3.61	5.20	7 · 73 8 · oo	10.95	15.10	20.90	29.51
1.85	3.7I 3.82	5.37	8.28	II.37 II.82	15.84	21.97	31.43
1.05		5.54 5.71	8.57	11.82	10.52	23.15	33.33
1.95	3.94	5.71	8.87	12.76	18.07	24.32 25.60	35.47
2.00	4.05 4.16	6.07	9.16	13.24	18.86	25.00	37.90 40.27
2.00	4.10	0.07	9.10	13.24	10.00	27.04	40.27

TABLE XXXVI. — Pusher Grades

The tabular quantities are pusher grades for the through grades indicated at the side and top of table. Computed for the Consolidation Engine of Table XXXIII.

Through grade	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.0 1.0 2.0	0.187 1.889 3.359	0.369 2.045	0.548	0.725 2.353	0.899	1.070	1.238 2.796	1.404	1.569 3.082	I.730 3.222

	-									-		
ı	Feet	Feet	Incli-	Feet	Feet	Incli-	Feet	Feet	Incli-	Feet	Feet	Incli-
١	per	per	nation.	per	per	nation,	per	per	nation,	per	per	nation.
1	sta-	mile	deg.	sta-	mile	deg.	sta-	mile	deg.	sta-	mile	deg.
ı	tion			tion			tion		8-	tion		acg.
	00	.000	,000	50	26.400	.286	1.00	52.800	.573	1.50	79.200	.859
	OI	.528	.006	51	26.928	.292	1.01	53.328	.579	1.51	79.728	.865
	02	1.056	.011	52	27.456	.298	1.02	53.856	. 584	1.52	80.256	.871
ı	03	1.584	.017	53	27.984	.304	1.03	54.384	.590	1.53	80.784	.877
	04	2.112	.023	54	28.512	.309	1.04	54.912	.596	1.54	81.312	.882
	05	2.640	.029	55	29.040	.315	1.05	55.440		1.55	81.840	.888
ı	06	3.168	.034	56	29.568	.321	1.06	55.968	.607	1.56	82.368	.894
	07	3.696	.040	57	30.096	.327	1.07	56.496	.613	1.57	82.896	.899
ı	08	4.224	.046	58	30.624	.332	1.08	57.024	.619	1.58	83.424	.905
ı	09	4.752	.052	59	31.152	.338	1.09	57.552	.624	1.59	83.952	.911
ľ	10	5.280	.057	60	31.680	.344	1.10	58.080	.630	1.60	84.480	.917
ı	11	5.808	.063	61	32.208	.349	I.II	58.608		1.61	85.008	.922
		6.336	.069	62	32.736		1.12	59.136		1.62	85.536	
	12	6.864	.074	63	32.730	.361	1.12	59.130	.648	1.63	86.064	.928
	13	7.392	.080	64	33.792		1.13	60.192		1.64	86.592	.934
				65				60.720	.659	1.65	87.120	
ı	15	7.920 8.448	.080	66	34.320 34.848	.372	1.15	61.248	.665	1.66	87.120	-945
ı	17	8.976	.092	67	35.376		1.17	61.776	.670	1.67	88.176	.951
ı												.957
	18	9.504	.103	68	35.904		1.18	62.304	.676	1.68	88.704	.962
ı	19	10.032	.109	69	36.432	-395	1.19	62.832 63.360	.688	1.69	89.232	.968
	20	10.560	.115	70	36.960		1.20)	1.70	89.760	.974
ı	21	11.088	.120	71	37.488		1.21	63.888	.693	1.71	90.288	.980
ı	22	11.616	.126	72	38.016		I.22	64.416	.699	1.72	90.816	.985
	23	12.144	.132	73	38.544	.418	1.23	64.944	. 705	1.73	91.344	.991
ı	24	12.672	.138	74	39.072		1.24	65.472	.710	1.74	91.872	.997
	25	13.200	.143	75	39.600		1.25	66.000	.716	1.75	92.400	1.002
	26	13.728	.149	76	40.128	.436	1.26	66.528	.722	1.76	92.928	1.008
	27	14.256	.155	77	40.656	.441	1.27	67.056	.728	1.77	93.456	1.014
	28	14.784	.160	78	41.184		1.28	67.584	.733	1.78	93.984	1.020
	29	15.312	.166	79	41.712	.452	1.29	68.112	.739	1.79	94.512	1.026
ı	30	15.840	.172	8o	42.240		1.30	68.640	.745	1.80	95.040	1.031
ı	31	16.368	.178	81	42.768	.464	1.31	69.168	.751	1.81	95.568	1.037
1	32	16.896	.183	82	43.296	.470	1.32	69.696	.756	1.82	96.096	1.043
ı	33	17.424	.189	83	43.824	.476	1.33	70.224	. 762	1.83	96.624	1.048
ı	34	17.952	.195	84	44.352	.481	1.34	70.752	.768	1.84	97.152	1.054
1	35	18.480	.200	85	44.880	.487	1.35	71.280		1.85	97.680	1.060
1	36	19.008	.206	86	45.408		1.36	71.808	.779	1.86	98.208	1.066
1	37	19.536	.212	87	45.936		1.37	72.336		1.87	98.736	1.071
1	38	20.064	.218	88	46.464	.504	1.38	72.864	.791	1.88	99.264	1.077
1	39	20.592	.223	89	46.992		1.39	73.392	. 796	1.89	99.792	1.083
	40	21.120	.229	90	47.520		1.40	73.920	.802	1.90	100.320	1.089
	41	21.648	.235	91	48.048	.521	1.41	74.448		1.91	100.848	1.094
	42	22.176	.240	92	48.576	.527	1.42	74.976	.814	1.92	101.376	1.100
	43	22.704	.246	93	49.104	.533	1.43	75 504	.819	1.93	101.904	1.106
1	44	23.232	.252	94	49.632	-539	I.44	76.032	.825	1.94	102.432	I.III
	45	23.760	.258	95	50.160	.544	1.45	76.560	.831	1.95	102.960	1.117
	46	24.288	. 264	96	50.688	. 550	1.46	77.088	.836	1.96	103.488	1.123
	47	24.816	. 269	97	51.216	. 556	1.47	77.616	.842	1.97	104.016	1.129
1	48	25.344	. 275	98	51.744	.561	1.48	78.144	.848	1.98	104.544	1.134
	49	25.872	.281	99	52.272	. 567	1.49	78.672	.854	1.99	105.072	1.140
	50	26.400	. 286	1.00	52.800	-573	1.50	79.200	.859	2.00	105.600	1.146
			•									

CHAPTER V

ESTIMATING AND CONSTRUCTION TABLES

TABLE XXXVIII

Relative prices in place that can be paid for articles for the same purpose lasting N and N' years. The article lasting N years is assumed to cost \$1.00 or one unit. Interest 4 per cent.

Example. — If a lasts 10 years and costs 50 cents, there may be paid for b lasting 7 years 50 \times 0.74 = 37 cents.

N' N	5	6	7	8	9	10	11	12	13	14	N N'	Amount \$1.00 at comp'd int.
5	I.00	0.85	0.74	0.66	0.60	0.55	0.51	0.47	0.45	0.42		1.21665
6	1.18	1.00	0.87	0.78	0.70	0.65	0.60	0.56	0.52	0.50		1.26532
7	1.35	1.14	I.00	0.89	0.81	0.74	0.69	0.64	0.60	0.57	7 8	1.31593
8	1.51	1.28	1.12	1.00	0.91	0.83	0.77	0.72	0.67	0.64		1.36857
9	1.67	I.42	1.24	1.10	1.00	0.92	0.85	0.79	0.74	0.70	9	1.42331
10	1.82	1.55	1.35	1.20	1.09	1.00	0.93	0.86		0.77		1.48024
11	1.97	1.67	1.46	1.30	1.18	1.08	1.00	0.93	0.88	0.83		I.53945
12	2.11	1.79	1.56	1.39	1.26	1.16	1.07	1.00	0.94	0.89	12	1.60103
13	2.43	1.90	1.66	1.48	1.34	1.23	1.14	1.06	1.00	0.95		1.66507
14	2.37	2.01	1.76	1.57	1.42	1.30	1.21	1.13				1.73167
15	2.50	2.12	1.85	1.65	1.50	1.37	1.27	1.18		1.05	_	1.80094
16	2.62	2.22	1.94	1.73	1.57	1.44	1.33	1.24		1.10		1.87297
17	2.73	2.32	2.03	1.81	1.64					1.15		1.94790
18	2.84	2.41	2.11	1.88	1.70					1.20		2.02581
19	2.95	2.50				1.62				1.24	_	2.10685
20	3.05	2.59	2.26	2.02	1.83					1.29		2.19112
21	3.15	2.68		2.08						1.33		2.27876
22	3.25	2.76								1.37		2.36991
23	3.34	2.83			2.00					1.41	_	2.46471
24	3.42	2.91			2.05							2.56330 2.66583
25	3.51	2.98	2.60	2.32	2.10	1.93	1.78	1.66	1.56	1.48	25	2.00583

TABLE XXXVIII. — (Continued)

N' N	15	16	17	18	19	20	21	22	23	24	25	$N_{N'}$
5	0.40	0.38	0.37	0.35	0.34	0.33	0.32	0.31	0.30	0.29	0.28	5
6	0.47	0.45	0.43	0.41	0.40	0.39	0.37	0.36	0.35	0.34	0.34	6
7	0.54	0.52	0.49	0.47	0.46	0.44	0.43	0.42	0.40	0.39	0.38	7 8
7 8	0.61	0.58	0.55	0.53	0.51	0.50	0.48	0.47	0.45	0.44	0.43	8
9	0.67	0.64	0.61	0.59	0.57	0.55	0.53	0.51	0.50	0.49	0.48	9
10	0.73	0.70	0.67	0.64	0.62	0.60	0.58	0.56	0.55	0.53	0.52	10
II	0.79	0.75	0.72	0.69	0.67	0.64	0.62	0.61	0.59	0.57	0.56	II
12	0.84	0.81	0.77	0.74	0.71	0.69	0.67	0.65	0.63	0.62	0.60	12
13	0.90	0.86	0.82	0.79	0.76	0.73	0.71	0.69	0.67	0.65	0.64	13
14	0.95	0.91	0.87	0.83	0.80	0.78	0.75	0.73	0.71	0.69	0.68	14
15	1.00	0.95	0.91	0.88	0.85	0.82	0.79	0.77	0.75	0.73	0.71	15
16	1.05	1.00	0.96	0.92	0.89	0.86	0.83	0.81	0.78	0.76	0.75	16
17	1.09	1.04	1.00	0.96	0.93	0.90	0.87	0.84	0.82	0.80	0.78	17
18	1.14	1.09	1.04	1.00	0.96	0.93	0.90	0.88	0.85	0.83	0.81	18
19	1.18	1.13	1.08	1.04	1.00	0.97	0.94	0.91	0.88	0.86	0.84	19
20	1.22	1.17	1.12	1.07	1.03	1.00	0.97	0.94	0.91	0.89	0.87	20
21	1.26	1.20	1.15	I.II	1.07	1.03	1.00	0.97	0.94	0.92	0.90	21
22	1.30	1.24	1.19	1.14	1.10	1.06	1.03	1.00	0.97	0.95	0.92	22
23	1.34	1.27	1.22	1.17	1.13	1.09	1.06	1.03	1.00	0.97	0.95	23
24	1.37	1.31	1.25	1.20	1.16	1.12	1.08	1.06	1.03	1.00	0.98	24
25	1.41	1.34	1.28	1.23	1.19	1.15	1.11	1.08	1.05	1.02	1.00	25

TABLE XXXIX

Relative prices in place that can be paid for articles for the same purpose lasting N and N' years. The article lasting N years is assumed to cost \$1.00 or one unit. Interest 5 per cent.

Example. — If a lasts 10 years and costs 60 cents, there may be paid for b lasting 12 years, $60 \times 1.15 = 70$ cents.

N' N	5	6	7	8	9	10	11	12	13	14	N N'	Amount \$1.00 at comp'd int.
5 6	1.00	0.85	0.75	0.67		0.56		0.49			5	1.27628
7	1.17	I.00	0.88	0.79	0.71	0.66	0.61	0.57	0.54	0.51	6	1.34009
	I.34			0.90		0.75		-	- 1	0.58	7	1.40710
8	1.49	I.27	1.12	1.00	0.91	0.84	0.78	0.73	0.69	0.65	8	1.47745
9	1.64	1.40	1.23	I.IO	I.00	0.92	0.86	0.80	0.76	0.72	9	1.55132
10	1.78	1.52	1.33	1.19	1.09	1.00	0.93	0.87	0.82	0.78	10	1.62889
II	1.92	1.64	I.44	1.29	1.17	1.08		0.94	0.88	0.84	II	1.71034
12	2.05	1.75	1.53	1.37	I.25	1.15		1.00	0.94	0.90	12	1.79585
13	2.17	1.85	1.62	1.45	I.32	I.22	1.13	1.06	1.00	0.95	13	1.88564
14	2.29	1.95	1.71	1.53	1.39	1.28	1.19	I.I2	I.05	1.00	14	1.97993
15	2.40	2.04	1.79	1.61	1.46	1.34	1.25	1.17	1.10	1.05	15	2.07892
16	2.50	2.14	1.87	1.68	1.52	1.40	1.30	I.22	1.15	1.09	16	2.18287
17	2.60	2.22	1.95	1.74	1.59	1.46	1.36	1.27	1.20	1.14	17	2.29202
18	2.70	2.30	2.02	1.81	1.64	1.51	1.41	I.32	I.24	1.18	18	2.40662
19	2.79	2.38	2.09	1.87	1.70	1.56	1.45	1.36	1.29	I.22	19	2.52695
20	2.88	2.46	2.15	1.93	1.75	1.61	1.50	1.41	1.33	1.25	20	2.65330
21	2.96	2.53	2.22	1.98	1.80	1.66	1.54	1.45	1.36	1.29	21	2.78596
22	3.04	2.59	2.27	2.04	1.85	1.70	1.58	1.49	1.40	1.33	22	2.92526
23	3.12	2.66	2.33	2.09	1.90	1.75	1.62	I.52	I.44	1.36	23	3.07152
24	3.19	2.72	2.38					1.56	I.47	I.39	24	3.22510
25	3.26	2.78	2 44	2.18	1.98	1.83	I.70	I.59	1.50	I.42	25	3.38635

TABLE XXXIX. — (Continued)

N' N	15	16	17	18	19	20	21	22	23	24	25	$N_{N'}$
5	0.42	0.40	0.38	0.37	0.36	0.35	0.34	0.33	0.32	0.31	0.31	5
6	0.49	0.47	0.45	0.43	0.42	0.41	0.40	0.39	0.38	0.37	0.36	6
7	0.56	0.53	0.51	0.49	0.48	0.46	0.45	0.44	0.43	0.42	0.41	7
8	0.62	0.60	0.57	0.55	0.53	0.52	0.50	0.49	0.48	0.47	0.46	8
9	0.68	0.66	0.63	0.61	0.59	0.57	0.55	0.54	0.53	0.52	0.50	9
10	0.74	0.71	0.68	0.66	0.64	0.62	0.60	0.59	0.57	0.56	0.55	10
11	0.80	0.77	0.74	0.71	0.69	0.67	0.65	0.63	0.62	0.60	0.59	11
12	0.85	0.82	0.79	0.76	0.73	0.71	0.69	0.67	0.66	0.64	0.63	12
13	0.90	0.87	0.83	0.80	0.78	0.75	0.73	0.71	0.70	0.68	0.67	13
14	0.95	0.91	0.88	0.85	0.82	0.79	0.77	0.75	0.73	0.72	0.70	14
15	1.00	0.96	0.92	0.89	0.86	0.83	0.81	0.79	0.77	0.75	0.74	15
16	1.04	1.00	0.96	0.93	0.90	0.87	0.85	0.82	0.80	0.79	0.77	16
17	1.09	1.04	1.00	0.96	0.93	0.90	0.88	0.86	0.84	0.82	0.80	17
18	1.13	1.08	1.04	1.00	0.97	0.94	0.91	0.89	0.87	0.85	0.83	18
19	1.16	1.12	1.07	1.03	1.00	0.97	0.94	0.92	0.90	0.88	0.86	19
20	1.20	1.15	1.11	1.07	1.03	1.00	0.97	0.95	0.92	0.90	0.88	20
21	I.24	1.18	1.14	1.10	1.06	1.03	1.00	0.97	0.95	0.93	0.91	21
22	1.27	1.21	1.17	1.13	1.09	1.06	1.03	1.00	0.98	0.95	0.93	22
23	1.30	I.24	I.20	1.15	I.I2	1.08	1.05	I.02	I.00	0.98	0.96	23
24	I.33	1.27	1.22	1.18	1.12	1.11	1.08	1.02	I.02	1.00	0.98	24
25	1.36	I.30	1.25	I.2I	1.17	1.13	I.10	1.03	1.04	I.02	I.00	25
3	30	2.,,0	1.23	1.21	4.1/	4.13	1.10	1.07	1.04	1.02	2.30	-3

Volumes of Triangular Prisms. — Table XL. In railroad earth-work the volume of a given length of cut or fill is given by the average end area method as $l \times \frac{A_1 + A_2}{2}$ in which l is the length, usually 100 feet, and A_1 and A_2 are the cross-section areas at the two ends. This is equivalent to $\frac{l}{2}A_1 + \frac{l}{2}A_2$ and Table XL is made on this basis with 100 for l. Hence the volumes are for 50-foot lengths and are to be used twice, once on one side of a station section for the part of the station

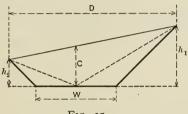


FIG. 25.

volume on that side, and once on the other side as part of the station volume on that side.

The commonest formula for the cross-section area of a 3-level section is $A = \frac{c}{2}D + \frac{w}{4}$ $(h_1 + h_2)$. This is equivalent to the area of two triangles of bases c and $\frac{w}{2}$ and altitudes D and $h_1 + h_2$ or it may be taken as three triangles of bases D and $\frac{w}{2}$ and altitudes c, h_1 and h_2 .

Whence the volume in cubic yards for a 50-foot length is

$$V_{50} = 50 \frac{c}{2 \times 27} D + 50 \frac{w}{4 \times 27} (h_1 + h_2)$$
$$= \frac{25}{27} cD + \frac{25}{27} \frac{w}{2} (h_1 + h_2).$$

D is the sum of the slope stake distances. The table is made to give the quantity $\frac{2}{2}\frac{\pi}{7} \cdot x \cdot y$, in which x is the base or altitude and y is the altitude or base of the triangular base or end of a triangular prism.

In using the table for such work the x numbers at the side of the page should be used for heights c and $\frac{w}{2}$ and the y numbers at the top for D and $h_1 + h_2$. The quantities are given for only whole numbers of y

from I to 9 inclusive, but are given to hundredths so that for y = 50 or 70, etc., ten times the tabular values for 5 or 7, etc., are taken and for y = 0.5 and 0.7, etc., one-tenth the tabular values for 5 and 7 are taken.

Example. — The cross-section notes of two stations show

Sta.
 L
 C
 R

 762

$$\frac{-3.6}{13.6}$$
 -4.2
 $\frac{-5.3}{15.3}$

 763
 $\frac{-4.8}{14.8}$
 -5.7
 $\frac{-6.4}{16.4}$

the minus sign indicating a cut. The volume between stations 762 and 763 is had from the tables as follows:

For 762.
$$D = 13.6 + 15.3 = 28.9$$
, done mentally,
 $c = 4.2$,
 $w = 20$, $\frac{w}{2} = 10$,
 $h_1 + h_2 = 8.9$.

From Table XL opposite x = 4.2 under 2 take 10 \times 7.78 = 77.8

under 8
$$I \times 31.11 = 31.11$$

under 9 $\frac{1}{10} \times 35.00 = 3.5$

$$\frac{w}{2} = 10$$
 : opposite $x = 10.0$ under 8 take $1 \times 74.00 = 74.00$

under 9
$$\frac{1}{10} \times 83.33 = \frac{8.33}{194.8} = 194.8$$

For 763.
$$D = 14.8 + 16.4 = 31.2$$
.
 $c = 5.7$,
 $w = 20$, $\frac{w}{2} = 10$,
 $h_1 + h_2 = 11.2$.

Opposite
$$x = 5.7$$
 take $10 \times 15.83 = 158.3$
 $1 \times 5.28 = 5.3$
 $\frac{1}{10} \times 10.56 = 1.1$
 $\frac{w}{2} = 10$.

∴ opposite
$$x = 10$$
 take $10 \times 9.72 = 97.2$

$$1 \times 9.72 = 9.7$$

$$\frac{1}{10} \times 19.44 = 1.9$$

$$\frac{1}{273.5}$$
Total

Total for sta. 468.3

If the length between two sections is 50 feet, take $\frac{1}{2}$ the result from the tables; if 40 feet, take $\frac{4}{10}$ the result, and so on. For a single right

prism of any length take that portion of the tabular quantity that the

length is of 50.

Prismoidal Correction. — Table XLI. To get the volume of a station of earthwork by the prismoidal formula, get it by the average end area method and subtract the prismoidal correction. That is, get the volume from Table XL, and subtract the correction of Table XLI. The correction is for full stations of 100 feet; for shorter lengths use proportional parts of the tabular quantities. The arguments of the table $C_1 - C_0$ and $D_1 - D_0$ are the differences in center heights and total widths respectively of the two end sections.

Level Section Volumes. — Table XLII. This table is used only in preliminary estimates and gives the volumes in cubic yards for 100-foot lengths for varying center heights. Its use will be evident.

TABLE XL. — Volumes of Triangular Prisms 50 Feet in Length

Y										V /
X	1	2	3	4	5	6	7	8	9	
.1	.09	.19	.28	.37	.46	.56	.65	.74	.83	.1
.2	.19	.37	. 56	.74	.93	I.II	1.30	1.48	1.67	.2
.3	.28	.56	.83	I.II	1.39	1.67	1.94	2.22	2.50	-3
-4	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	-4
.5 .6	.46 .56	.93 I.II	1.39 1.67	1.85	2.3I 2.78	2.78	3.24	3.70	4.17	.5 .6
	.65					3.33 3.89		4.44	5.00	
.7 .8	.05	I.30 I.48	1.94 2.22	2.59	3.24 3.70	4.44	4.54 5.19	5.19 5.93	6.67	.7 .8
.9	.83	1.67	2.50	3.33	4.17	5.00	5.83	6.67	7.50	.9
1.0	-93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	1.0
.I	I.02	2.04	3.06	4.07	5.09	6.11	7.13	8.15	9.17	.I
.2	I.II	2.22	3.33	4.44	5.56	6.67	7.78	8.89	10.00	.2
.3	1.20	2.41	3.61	4.81	6.02	7.22	8.43	9.63	10.83	-3
.4	1.30	2.59	3.89	5.19	6.48	7.78	9.07	10.37	11.67	-4
.5	1.39	2.78	4.17	5.56	6.94	8.33	9.72	II.II	12.50	-5
.6	1.48	2.96	4.44	5.93	7.41	8.89	10.37	11.85	13.33	.6
.7 .8	I.57 I.67	3.15	4.72 5.00	6.30	7.87 8.33	9.44 10.00	11.02 11.67	12.59	14.17 15.00	-7 .8
.9	1.76	3.33 3.52	5.28	7.04	8.80	10.56	12.31	13.33 14.07	15.83	.9
2.0	1.85	3.70	5.56	7.41	9.26	II.II	12.96	14.81	16.67	2.0
.1	1.94	3.89	5.83	7.78	9.72	11.67	13.61	15.56	17.50	.1
.2	2.04	4.07	6.11	8.15	10.19	12.22	14.26	16.30	18.33	.2
.3	2.13	4.26	6.39	8.52	10.65	12.78	14.91	17.04	19.17	.3
.4	2.22	4.44	6.67	8.89	II.II	13.33	15.56	17.78	20.00	-4
-5	2.31	4.63	6.94	9.26	11.57	13.89	16.20	18.52	20.83	.5
.6	2.41	4.81	7.22	9.63	12.04	14.44	16.85	19.26	21.67	.6
.7	2.50	5.00	7.50	10.00	12.50	15.00	17.50	20.00	22.50	.7
.8 .9	2.59	5.19	7.78 8.06	10.37	12.96	15.56 16.11	18.15 18.80	20.74 21.48	23.33	.8 .9
3.0	2.78	5.56	8.33	11.11	13.89	16.67	19.44	22.22	25.00	3.0
. I	2.87	5.74	8.61	11.48	14.35	17.22	20.09	22.96	25.83	.I
.2	2.96	5.74	8.89	11.40	14.35	17.22	20.09	23.70	25.63	.2
.3	3.06	6.11	9.17	12.22	15.28	18.33	21.39	24.44	27.50	-3
.4	3.15	6.30	9.44	12.59	15.74	18.89	22.04	25.19	28.33	.4
.5	3.24	6.48	9.72	12.96	16.20	19.44	22.69	25.93	29.17	-5
.6	3.33	6.67	10.00	13.33	16.67	20.00	23.33	26.67	30.00	.6
.7	3.43	6.85	10.28	13.70	17.13	20.56	23.98	27.41	30.83	.7
.8	3.52 3.61	7.04	10.56	14.07	17.59 18.06	2I.II 2I.67	24.63	28.15 28.89	31.67	.8
4.0		7.22		14.44		22.22	25.28		32.50	.9 4.0
	3.70	7.41	II.II	14.81	18.52		25.93	29.63	33.33	
.I	3.80	7.59 7.78	11.39	15.19 15.56	18.98 19.44	22.78 23.33	26.57 27.22	30.37 31.11	34.17 35.00	. I . 2
-3	3.98	7.96	11.94	15.93	19.44	23.89	27.87	31.85	35.83	.3
.4	4.07	8.15	12.22	16.30	20.37	24.44	28.52	32.59	36.67	.4
.5	4.17	8.33	12.50	16.67	20.83	25.00	29.17	33.33	37.50	-5
.6	4.26	8.52	12.78	17.04	21.30	25.56	29.81	34.07	38.33	.6
.7	4.35	8.70	13.06	17.41	21.76	26.11	30.46	34.81	39.17	.7
.8 .9	4.44	8.89	13.33	17.78	22.22	26.67	31.11	35.56	40.00	.8
5.0	4.54	9.07	13.61	18.15	22.69	27.22	31.76	36.30	40.83	.9 5 .0
3.0	4.63	9.26	13.89	18.52	23.15	27.78	32.41	37.04	41.67	3.0

Y	I	2	3	4	5	6	7	8	9	Y / X
				-0.00		-0				
5.1	4.72	9.44	14.17 14.44	18.89	23.61 24.07	28.33 28.89	33.06 33.70	37.78 38.52	42.50	5.1
.2	4.91	9.81	14.72	19.63	24.54	29.44	34.35	39.26	43.33 44.17	.2
	5.00	10.00	15.00	20.00	25.00	30.00	35.00	40.00	45.00	.4
.4	5.09	10.19	15.28	20.37	25.46	30.56	35.65	40.74	45.83	.5
.5 .6	5.19	10.37	15.56	20.74	25.93	31.11	36.30	41.48	46.67	.6
.7	5.28	10.56	15.83	21.11	26.39	31.67	36.94	42.22	47.50	.7
.8	5.37	10.74	16.11	21.48	26.85	32.22	37.59	42.96	48.33	.8
.9	5.46	10.93	16.39	21.85	27.31	32.78	38.24	43.70	49.17	.9
6.0	5.56	11.11	16.67	22.22	27.78	33.33	_38.89	44.44	50.00	6.0
.I	5.65	11.30	16.94	22.59	28.24	33.89	39.54	45.19	50.83	. І
.2	5.74	11.48	17.22	22.96	28.70	34.44	40.19	45.93	51.67	.2
.3	5.83	11.67	17.50	23.33	29.17	35.00	40.83	46.67	52.50	.3
.4	5.93	11.85	17.78	23.70	29.63	35.56	41.48	47.41	53.33	-4
.5 .6	6.02 6.11	12.04 12.22	18.06	24.07	30.09 30.56	36.11 36.67	42.13 42.78	48.15 48.89	54.17	.5 .6
	6.20		18.33	24.44 24.81	31.02	37.22		49.63	55.00	
.7 .8	6.30	12.41	18.89	25.19	31.02	37.22	43.43	50.37	55.83 56.67	.7 .8
.9	6.39	12.78	19.17	25.56	31.40	38.33	44.72	51.11	57.50	.9
7.0	6.48	12.96	19.44	25.93	32.41	38.89	45.37	51.85	58.33	7.0
Ι,	6.57	13.15	19.72	26.30	32.87	39.44	46.02	52.59	59.17	.1
.2	6.67	13.33	20.00	26.67	33.33	40.00	46.67	53.33	60.00	.2
.3	6.76	13.52	20.28	27.04	33.80	40.56	47.31	54.07	60.83	.3
.4	6.85	13.70	20.56	27.41	34.26	41.11	47.96	54.81	61.67	.4
.5	6.94	13.89	20.83	27.78	34.72	41.67	48.61	55.56	62.50	.5
.6	7.04	14.07	21.11	28.15	35.19	42.22	49.26	56.30	63.33	.6
.7	7.13	14.26	21.39	28.52	35.65	42.78	49.91	57.04	64.17	.7
.8	7.22	14.44	21.67	28.89	36.11	43.33	50.56	57.78	65.00	.8
.9	7.31	14.63	21.94	29.26	36.57	43.89	51.20	58.52	65.83	.9
8.0	7.41	14.81	22.22	29.63	37.04	44.44	51.85	59.26	66.67	8.0
.I	7.50 7.59	15.00	22.50 22.78	30.00	37.50 37.96	45.00 45.56	52.50 53.15	60.00	67.50 68.33	.I
.2	7.69	15.19	23.06	30.37	38.43	45.50	53.15	61.48	69.17	.3
.4	7.78	15.56	23.33	31.11	38.89	46.67	54.44	62,22	70.00	.4
.5	7.87	15.74	23.61	31.48	39.35	47.22	55.09	62.96	70.83	.5
.6	7.96	15.93	23.89	31.85	39.81	47.78	55.74	63.70	71.67	.6
.7	8.06	16.11	24.17	32.22	40.28	48.33	56.39	64.44	72.50	.7
.8	8.15	16.30	24.44	32.59	40.74	48.89	57.04	65.19	73.33	.8
.9	8.24	16.48	24.72	32.96	41.20	49.44	57.69	65.93	74.17	.9
9.0	8.33	16.67	25.00	33.33	41.67	50.00	58.33	66.67	75.00	9.0
.I	8.43	16.85	25.28	33.70	42.13	50.56	58.98	67.41	75.83	ı,
.2	8.52	17.04	25.56	34.07	42.59	51.11	59.63	68.15	76.67	.2
.3	8.61	17.22	25.83	34.44	43.06	51.67	60.28	68.89	77.50	.3
-4	8.70 8.80	17.41	26.11 26.39	34.81	43.52 43.98	52.22 52.78	60.93	69.63	78.33 79.17	.4
.5 .6	8.89	17.59	26.67	35.19	44.44	53.78	62.22	71.11	80.00	.5 .6
.7	8.98	17.96	26.94	35.93	44.91	53.89	62.87	71.85	80.83	.7
.8	9.07	18.15	27.22	36.30	45.37	54.44	63.52	72.59	81.67	.8
.9	9.17	18.33	27.50	36.67	45.83	55.00	64.17	73.33	82.50	.9
10.0	9.26	18.52	27.78	37.04	46.30	55.56	64.81	74.07	83.33	10.0

Y										Y /
X	I	2	3	4	5	6	7	8	9	$/_X$
10.1	9.35	18.70	28.06	37.41	46.76	56.11	65.46	74.81	84.17	10.1
.2	9.44	18.89	28.33	37.78	47.22	56.67	66.11	75.56	85.00	.2
-3	9.54	19.07	28.61	38.15	47.69	57.22	66.76	76.30	85.83	.3
.4	9.63	19.26	28.89	38.52	48.15	57.78	67.41	77.04	86.67	-4
.5	9.72	19.44	29.17	38.89	48.61	58.33	68.06	77.78	87.50	-5
.6	9.81	19.63	29.44	39.26	49.07	58.89	68.70	78.52	88.33	.6
.7	9.91	19.81	29.72 30.00	39.63	49.54	59.44 60.00	69.35	79.26	89.17	.7
.8	10.00	20.19	30.28	40.00	50.00	60.56	70.00	80.00	90.00	.8
11.0	10.19	20.37	30.56	40.74	50.93	61.11	71.30	81.48	91.67	11.0
.1	10.28	20.56	30.83	41.11	51.39	61.67	71.94	82.22	92.50	.1
.2	10.37	20.74	31.11	41.48	51.85	62.22	72.59	82.96	93.33	.2
.3	10.46	20.93	31.39	41.85	52.31	62.78	73.24	83.70	94.17	.3
-4	10.56	21.11	31.67	42.22	52.78	63.33	73.89	84.44	95.00	.4
-5	10.65	21.30	31.94	42.59	53.24	63.89	74.54	85.19	95.83	-5
.6	10.74	21.48	32.22	42.96	53.70	64.44	75.19	85.93	96.67	.6
.7	10.83	21.67	32.50	43.33	54.17	65.00	75.83	86.67	97.50	.7
.8	10.93 11.02	21.85	32.78 33.06	43.70	54.63 55.09	65.56 66.11	76.48 77.13	87.41 88.15	98.33 99.17	.8
12.0	II.II	22.22		44.44	55.56	66.67		88.89	100.00	.9 12.0
	II.20	22.41	33.33	44.44	56.02	67.22	77.78	89.63	100.83	1
.I .2	11.30	22.41	33.89	45.19	56.48	67.78	78.43 79.07	90.37	100.83	.I
-3	11.39	22.78	34.17	45.56	56.94	68.33	79.72	91.11	102.50	-3
.4	11.48	22.96	34.44	45.93	57.41	68.89	80.37	91.85	103.33	-4
5	11.57	23.15	34.72	46.30	57.87	69.44	81.02	92.59	104.17	-5
.6	11.67	23.33	35.00	46.67	58.33	70.00	81.67	93.33	105.00	.6
.7	11.76	23.52	35.28	47.04	58.80	70.56	82.31	94.07	105.83	.7
.8	11.85	23.70	35.56	47.41	59.26	71.11 71.67	82.96	94.81	106.67	.8
.9 13.0	12.04	23.89	35.83	47.78	59.72		83.61	95.56	107.50	.9
		24.07	36.11	48.15	60.19	72.22	84.26	96.30	108.33	13.0
.I .2	12.13 12.22	24.26	36.39 36.67	48.52 48.89	60.65	72.78 73.33	84.91 85.56	97.04 97.78	109.17	.I .2
-3	12.31	24.63	36.94	49.26	61.57	73.89	86.20	98.52	110.83	-3
-4	12.41	24.81	37.22	49.63	62.04	74.44	86.85	99.26	111.67	-4
.5	12.50	25.00	37.50	50.00	62.50	75.00	87.50	100.00	112.50	-5
.6	12.59	25.19	37.78	50.37	62.96	75.56	88.15	100.74	113.33	.6
.7	12.69	25.37	38.06	50.74	63.43	76.11	88.80	101.48	114.17	.7
.8	12.78	25.56	38.33	51.11	63.89	76.67	89.44	102.22	115.00	.8
.9		25.74	38.61	51.48	64.35	77.22	90.09	102.96	115.83	.9
14.0	12.96	25.93	38.89	51.85	64.81	77.78	90.74	103.70	116.67	14.0
.I .2	13.06	26.11 26.30	39.17	52.22 52.59	65.28 65.74	78.32 78.89	91.39 92.04	104.44	117.50	. I . 2
.3	13.24	26.48	39.44	52.96	66.20	79.44	92.69	105.19	119.17	.3
.4	13.33	26.67	40.00	53.33	66.67	80.00	93.33	106.67	120.00	-4
.5	13.43	26.85	40.28	53.70	67.13	80.56	93.98	107.41	120.83	.5
.6	13.52	27.04	40.56	54.07	67.59	81.11	94.63	108.15	121.67	.6
.7	13.61	27.22	40.83	54.44	68.06	81.67	95.28	108.89	122.50	.7
.8	13.70	27.41	41.11	54.81	68.52	82.22	95.93	109.63	123.33	.8
.9 15.0	13.80	27.59	41.39	55.19	68.98	82.78	96.57	110.37	124.17	.9
10.0	13.89	27.78	41.67	55.56	69.44	83.33	97.22	III.II	125.00	15.0
		1	1		1			1		

											T /
	Y	I	2	3	4	5	6	7	8	9	X_{X}
1	15.1	13.98	27.96	41.94	55.93	69.91	83.89	97.87	111.85	125.83	15.1
ı	.2	14.07	28.15	42.22	56.30	70.37	84.44	98.52	112.59	126.67	.2
ı	.3	14.17	28.33	42.50	56.67	70.83	85.00	99.17	113.33	127.50	.3
п	.4	14.26	28.52	42.78	57.04	71.30	85.56	99.81	114.07	128.33	.4
н	.5	14.35	28.70	43.06	57.41	71.76	86.11	100.46	114.81	129.17	-5
ı	.6	14.44	28.89	43.33	57.78	72.22	86.67	101.11	115.56	130.00	.6
ı		ı						1		_	1 1
ı	.7	14.54	29.07	43.61	58.15	72.69	87.22	101.76	116.30	130.83	.7
ı	.8	14.63	29.26	43.89	58.52	73.15	87.78	102.41	117.04	131.67	.8
ı	.9	14.72	29.44	44.17	58.89	73.61	88.33	103.06	117.78	132.50	.9
ı	16.0	14.81	29.63	44.44	59.26	74.07	88.89	103.70	118.52	133.33	16.0
ı	.I	14.91	29.81	44.72	59.63	74.54	89.44	104.35	119.26	134.17	1.
ı	.2	15.00	30.00	45.00	60.00	75.00	90.00	105.00	120.00	135.00	.2
ı	.3	15.09	30.19	45.28	60.37	75.46	90.56	105.65	120.74	135.83	-3
ı			1					1			
ı	-4	15.19	30.37	45.56	60.74	75.93	91.11	106.30	121.48	136.67	-4
П	-5	15.28	30.56	45.83	61.11	76.39	91.67	106.94	122.22	137.50	.5
	.6	15.37	30.74	46.11		76.85	92.22	107.59	122.96	138.33	.6
ı	.7	15.46	30.93	46.39	61.85	77.31	92.78	108.24	123.70	139.17	.7
ı	.8	15.56	31.11	46.67	62.22	77.78	93.33	108.89	124.44	140.00	.8
ı	.9	15.65	31.30	46.94	62.59	78.24	93.89	109.54	125.19	140.83	.9
ı	17.0	15.74	31.48	47.22	62.96	78.70	94.44	110.19	125.93	141.67	17.0
ı	.r	15.83	31.67	47.50	63.33	79.17	95.00	110.83	126.67	142.50	.т
ı	.2	15.93	31.85	47.78	63.70	79.63	95.56	111.48	127.41	143.33	.2
١	-3	16.02	32.04	48.06	64.07	80.09	96.11	112.13	128.15	144.17	.3
ı						_		_	-		
п	-4	16.11	32.22	48.33	64.44	80.56	96.67	112.78	128.89	145.00	-4
п	-5	16.20	32.41	48.61	64.81	81.02	97.22	113.43	129.63	145.83	.5
ı	.6	16.30	32.59	48.89	65.19	81.48	97.78	114.07	130.37	146.67	.6
п	.7	16.39	32.78	49.17	65.56	81.94	98.33	114.72	131.11	147.50	.7
п	.8	16.48	32.96	49.44	65.93	82.41	98.89	115.37	131.85	148.33	.8
п	.9	16.57	33.15	49.72	66.30	82.87	99.44	116.02	132.59	149.17	.9
Н	18.0	16.67	33-33	50.00	66.67	83.33	100.00	116.67	133.33	150.00	18.0
ı	. т	16.76	33.52	50.28	67.04	83.80	100.56	117.31	134.07	150.83	.1
ı	.2	16.85	33.70	50.56	67.41	84.26	101.11	117.96	134.81	151.67	.2
ı	.3	16.94	33.89	50.83	67.78	84.72	101.67	118.61	135.56	152.50	.3
ı		17.04			68.15	85.19	102,22	119.26			
ı	.4 .5	17.13	34.07 34.26	51.11	68.52	85.65	102.22	119.20	136.30	153.33	-4
1	.6	17.13	34.44	51.39 51.67	68.89	86.11	103.33	120.56	137.04	154.17	.5 .6
ı								_			
1	.7	17.31	34.63	51.94	69.26	86.57	103.89	121.20	138.52	155.83	.7
ı	.8	17.41	34.81	52.22	69.63	87.04	104.44	121.85	139.26	156.67	.8
ı	.9	17.50	35.00	52.50	70.00	87.50	105.00	122.50	140.00	157.50	.9
ŀ	19.0	17.59	35.19	52.78	70.37	87.96	105.56	123.15	140.74	158.33	19.0
ı	.ı	17.69	35.37	53.06	70.74	88.43	106.11	123.80	141.48	159.17	ı.
Н	.2	17.78	35.56	53.33	71.11	88.89	106.67	124.44	142.22	160.00	.2
ı	.3	17.87	35.74	53.61	71.48	89.35	107.22	125.09	142.96	160.83	-3
	.4	17.96	35.93	53.89	71.85	89.81	107.78	125.74	143.70	161.67	.4
	-5	18.06	36.11	54.17	72.22	90.28	108.33	126.39	144.44	162.50	-5
I	.6	18.15	36.30	54.44	72.59	90.74	108.89	127.04	145.19	163.33	.6
I	.7	18.24	36.48	54.72	72.96	91.20	109.44	127.69	145.93	164.17	.7
	.8	18.33	36.67	55.00	73.33	91.67	110.00	128.33	146.67	165.00	.8
1	.9	18.43	36.85	55.28	73.70	92.13	110.56	128.98	147.41	165.83	.9
1	20.0	18.52	37.04	55.56	74.07	92.59	III.II	129.63	148.15	166.67	20.0

_	_						-			
X	I	2	3	4	5	6	7	8	9	Y X
20.1	18.61	37.22	55.83	74.44	93.06	111.67	130.28	148.89	167.50	20.1
.2	18.70	37.41	56.11	74.81	93.52	112.22	130.93	149.63	168.33	.2
-3	18.80	37.59	56.39	75.19	93.98	112.78	131.57	150.37	169.17	.3
-4	18.89	37.78	56.67	75.56	94.44	113.33	132.22	151.11	170.00	.4
.5	18.98	37.96	56.94	75.93	94.91	113.89	132.87	151.85	170.83	-5
.6	19.07	38.15	57.22	76.30	95.37	114.44	133.52	152.59	171.67	.6
.7	19.17	38.33	57.50	76.67	95.83	115.00	134.17	153.33	172.50	-7
.8	19.26	38.52	57.78	77.04	96.30	115.56	134.81	154.07	173.33	.8
.9	19.35	38.70	58.06	77.41	96.76	116.11	135.46	154.81	174.17	.9
21.0	19.44	38.89	58.33	77.78	97.22	116.67	136.11	155.56	175.00	21.0
.I	19.54	39.07	58.61	78.15	97.69	117.22	136.76	156.30	175.83	.I
.2	19.63	39.26	58.89	78.52 78.89	98.15 98.61	117.78	137.41	157.04	176.67	.2
.3	19.72	39.44	59.17		-		_	157.78	177.50	.3
.4	19.81	39.63	59.44	79.26	99.07	118.89	138.70	158.52	178.33	-4
-5	19.91	39.81	59.72	79.63	99.54	119.44	139.35	159.26	179.17	-5
.6	20.00	40.00	60.00	80.00	100.00	120.00	140.00	160.00	180.00	.6
.7	20.09	40.19	60.28	80.37	100.46	120.56	140.65	160.74	180.83	-7
.8	20.19	40.37	60.56	80.74	100.93	121.11	141.30	161.48	181.67	.8
.9	20.28	40.56	60.83	81.11	101.39	121.67	141.94	162.22	182.50	.9
22.0	20.37	40.74	61.11	81.48	101.85	122.22	142.59	162.96	183.33	22.0
	20.46		61.39	81.85	102.31	122.78	143.24	163.70	184.17	. I
.I .2	20.40	40.93	61.67	82.22	102.31	123.33	143.24	164.44	185.00	.1
	20.65	41.30	61.94	82.59	103.24	123.89	144.54	165.19	185.83	
-3								-		.3
.4	20.74	41.48	62.22	82.96	103.70	124.44	145.19	165.93	186.67	.4
.5	20.83	41.67	62.50	83.33	104.17	125.00	145.83	166.67	187.50	.5
.6	20.93	41.85	62.78	83.70	104.63	125.56	146.48	167.41	188.33	.6
.7	21.02	42.04	63.06	84.07	105.09	126.11	147.13	168.15	189.17	.7
.8	21.11	42.22	63.33	84.44	105.56	126.67	147.78	168.89	190.00	.8
.9	21.20	42.4I	63.61	84.81	106.02	127.22	148.43	169.63	190.83	.9
23.0	21.30	42.59	63.89	85.19	106.48	127.78	149.07	170.37	191.67	23.0
.r	21.39	42.78	64.17	85.56	106.94	128.33	149.72	171.11	192.50	. г
.2	21.48	42.96	64.44	85.93	107.41	128.89	150.37	171.85	193.33	.2
.3	21.57	43.15	64.72	86.30	107.87	129.44	151.02	172.59	194.17	.3
							-			
-4	21.67	43.33	65.00	86.67	108.33	130.00	151.67	173.33	195.00	-4
.5 .6	21.76	43.52	65.28	87.04		130.56	152.31	174.07	195.83	.5 .6
	21.85	43.70	65.56	87.41	109.26	131.11	152.96	174.81	196.67	
.7	21.94	43.89	65.83	87.78	109.72	131.67	153.61	175.56	197.50	.7
.8	22.04	44.07	66.11	88.15	110.19	132.22	154.26	176.30	198.33	.8
.9	22.13	44.26	66.39	88.52	110.65	132.78	154.91	177.04	199.17	.9
24.0	22.22	44.44	66.67	88.89	III.II	133.33	155.56	177.78	200.00	24.0
.I	22.31	44.63	66.94	89.26	111.57	133.89	156.20	178.52	200.83	.ī
.2	22.41	44.81	67.22	89.63	112.04	134.44	156.85	179.26	201.67	.2
.3	22.50	45.00	67.50	90.00	112.50	135.00	157.50	180.00	202.50	.3
.4	22.59	45.19	67.78	90.37	112.96	135.56	158.15	180.74	203.33	.4
.5	22.69	45.37	68.06	90.74	113.43	136.11	158.80	181.48	204.17	.5
.6	22.78	45.56	68.33	91.11	113.89	136.67	159.44	182.22	205.00	.6
.7	22.87	45.74	68.61	91.48	114.35	137.22	160.09	182.96	205.83	.7
.8	22.96	45.93	68.89	91.46	114.81	137.78	160.74	183.70	206.67	.8
.9	23.06	46.11	69.17	92.22	115.28	138.33	161.39	184.44	207.50	.9
25.0	23.15	46.30	69.44	92.59	115.74	138.89	162.04	185.19	208.33	25.0
20.0	23.13	40.30	9.44	92.39	113.74	230.09	102.04	103.19	200.33	20.0

Table Tabl	_											
2	X	Y	1	2	3	4	5	6 .	7	8	9	X X
	25.	1	23.24	46.48	69.72	92.96	116.20	139.44	162.69	185.93	209.17	25.1
3							116.67					.2
		_									210.83	
1.											6-	
6										_		
1,			-									.5
8		٥l	23.70	47.41	71.11	94.81	118.52	142.22	105.93	189.03	213.33	.0
26.0 24.07 48.15 72.22 96.30 120.37 143.89 167.87 191.85 215.83 9.9 26.0 124.07 48.15 72.22 96.30 120.37 144.44 168.52 192.59 216.67 26.0 1.1 24.17 48.33 72.50 96.67 120.83 145.50 169.17 193.33 217.50 12.2 24.26 48.52 72.78 97.04 121.30 145.56 169.81 194.07 218.33 .2 17.50 144.54 48.89 73.33 97.78 122.22 146.67 171.11 195.56 220.00 14.5 1.5 122.69 147.22 171.76 196.30 220.83 .5 1.5 122.69 147.22 171.76 196.30 220.83 .5 1.5 12.69 147.22 171.76 196.30 220.83 .5 1.5 12.69 147.22 171.76 196.30 220.83 .5 1.5 12.5 12.5 147.78 172.41 197.04 121.67 1.6 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	١.	7	23.80	47.59	71.39	95.19	118.98	142.78	166.57	190.37	214.17	.7
26.0 24.07 48.15 72.22 96.30 120.37 1.44.44 168.52 192.59 216.67 26.0 1 24.17 48.33 72.50 96.67 120.83 145.00 169.81 194.07 218.33 217.50 1.1 2 24.26 48.52 72.78 97.04 121.30 145.56 169.81 194.07 218.33 217.50 1.1 3 24.35 48.70 73.36 98.15 122.69 147.22 171.76 196.38 220.00 .4 5 24.54 49.07 73.61 98.52 123.15 147.78 172.41 197.04 221.67 6 6 24.51 49.44 74.17 98.89 123.61 148.33 173.06 197.78 222.50 7 8 24.81 49.63 74.44 99.63 124.54 149.44 174.37 199.26 224.57 19.75.00 190.00 125.00 190.00 175.00	١.	8	23.89	47.78	71.67	95.56	119.44	143.33	167.22	191.11	215.00	.8
1	١.	9	23.98	47.96	71.99	95.93	119.91	143.89	167.87	191.85	215.83	.9
1	26	0	24.07	48.15	72.22	96.30	120.37	144.44	168.52	102.50	216.67	26.0
2 2.4.26 48.52 72.78 97.04 121.30 145.56 169.81 194.07 218.33 2.2 3 24.35 48.70 73.06 97.41 121.76 1.46.11 170.46 194.81 219.17 3 4 24.44 48.89 73.33 97.78 122.22 146.67 171.11 195.56 220.00 4 5 24.53 49.26 73.89 98.52 123.51 147.78 172.41 197.94 221.67 6 6 24.63 49.26 74.72 99.63 123.61 148.33 173.06 197.78 222.50 7 8 24.81 49.63 74.72 99.63 124.07 148.89 173.70 198.52 223.33 8 9 24.91 49.81 74.72 99.63 124.07 148.89 173.70 198.52 223.33 8 20 25.95 50.37 75.56 100.00 125.00 <th< th=""><th></th><th>- 1-</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<>		- 1-										
3 24.35 48.70 73.66 97.41 121.76 146.11 170.46 194.81 219.17 3 .4 24.44 48.89 73.33 97.78 122.22 146.67 171.11 195.56 220.00 .4 .5 24.54 49.07 73.61 98.52 123.69 147.22 171.76 196.30 220.83 .5 .7 24.72 49.44 74.17 98.89 123.61 148.83 173.70 198.52 223.33 .8 .9 24.91 49.81 74.72 99.63 124.54 149.44 174.35 199.26 224.17 .9 27.0 25.09 50.00 75.00 100.00 125.00 150.00 175.00 200.00 225.00 275.00 200.00 225.00 275.00 200.00 225.00 275.00 275.00 270.00 225.03 3 .9 24.017 29.00 225.00 270.00 227.00 227.00 227.00		_										
.4 24.44 48.89 73.33 97.78 122.22 146.67 171.11 195.56 220.00 .4 .5 24.54 49.07 73.61 98.15 122.69 147.22 171.76 196.30 220.83 .5 .7 24.72 49.44 74.17 98.89 123.61 148.33 173.06 197.78 222.50 .7 .8 24.81 49.63 74.44 99.26 124.07 148.89 173.70 198.52 223.33 8 .9 24.91 49.81 74.72 99.63 124.54 149.44 174.35 199.26 224.17 .9 27.0 25.00 50.00 75.00 100.00 125.00 155.00 175.00 200.00 225.00 27.0 27.0 25.09 50.77 75.28 100.37 125.06 155.00 175.00 200.00 225.00 27.0 28.1 25.19 50.37 75.81 101.11 12												
1. 1. 1. 1. 1. 1. 1. 1.	1	3	24.35	40.70	73.00	97.41	121.70		170.40	194.01	219.17	.3
.5 24.54 49.07 73.61 98.52 122.69 147.22 171.76 196.30 220.83 .5 .7 24.72 49.44 74.17 98.89 123.61 148.33 173.06 197.78 222.50 .6 .8 24.81 49.63 74.44 99.26 124.07 148.89 173.70 198.52 223.33 .8 .9 24.91 49.81 74.72 99.63 124.54 149.44 174.35 199.26 224.17 .9 27.0 25.00 50.00 75.00 100.00 125.00 150.00 175.00 200.00 225.00 27.0 .1 25.09 50.17 75.28 100.37 125.00 150.00 175.00 200.00 225.00 27.0 .2 25.19 50.37 75.56 100.37 125.90 151.07 176.04 202.22 227.50 .3 .4 25.37 50.74 76.11 101.48 126.		4	24.44									-4
6			24.54	49.07	73.61	98.15	122.69	147.22	171.76	196.30	220.83	
8			24.63	49.26	73.89	98.52	123.15	147.78	172.41	197.04	221.67	.6
8		7	24.72	49.44	74 17	08.80	123 6T	148 32	173 06	197 78	222 50	77
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.1 28.80 57.59 86.39 115.19 143.98 172.78 201.57 230.37 259.11 .2 28.89 57.78 86.67 115.56 144.44 173.33 202.22 231.11 260.8 .3 28.98 57.96 86.94 115.93 144.91 173.89 202.87 231.85 260.8 .4 29.07 58.15 87.22 116.30 145.37 174.44 203.52 232.59 261.6 .5 29.17 58.33 87.50 116.67 145.83 175.00 204.17 233.33 262.5 .6 29.26 58.52 87.78 117.04 146.30 175.56 204.81 234.07 263.3 .7 29.35 58.70 88.06 117.41 146.76 176.11 205.46 234.81 264.1 .8 29.44 58.89 88.33 117.78 147.22 176.67 206.16 235.56 265.0 225.56 225.66 <th>.9</th>	.9
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.7 29.35 58.70 88.06 117.41 146.76 176.11 205.46 234.81 264.1 8 29.44 58.89 88.33 117.78 147.22 176.67 226.11 235.56 265.0 29.00 29.63 59.26 88.89 118.75 147.69 177.22 206.76 236.30 265.8 265.0 29.00 29.63 59.26 88.89 118.52 148.15 177.78 207.41 237.04 266.6 11 29.72 59.44 89.17 118.89 148.61 178.33 208.06 237.78 267.5 2 29.81 59.63 89.44 119.26 149.07 178.89 208.70 238.52 268.3 3 29.91 59.81 89.72 119.63 149.07 178.89 208.70 238.52 268.3 3 29.91 59.81 89.72 119.63 149.07 178.89 208.70 238.52 268.3 3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.00 5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	.5
.8 29.44 58.89 88.33 117.78 147.22 176.67 206.11 235.56 265.0 .9 29.54 59.07 88.61 118.15 147.69 177.22 206.76 236.30 265.8 32.0 29.63 59.26 88.89 118.52 148.15 177.78 207.41 237.04 266.6 .1 29.72 59.44 89.17 118.89 148.61 178.33 208.06 237.78 267.5 .2 29.81 59.63 89.44 119.26 149.07 178.89 208.70 238.52 268.3 .3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 .4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 .5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	.6
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.9 29.54 59.07 88.61 I18.15 147.69 177.22 206.76 236.30 265.8 32.0 29.63 59.26 88.89 I18.52 148.15 177.78 207.41 237.04 266.6 x 29.72 59.44 89.17 118.89 148.61 178.33 208.06 237.78 267.5 2 29.81 59.63 89.44 119.63 149.07 178.89 208.70 238.52 268.3 3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	.8
32.0 29.63 59.26 88.89 118.52 148.15 177.78 207.41 237.04 266.6 .1 29.72 59.44 89.17 118.89 148.61 178.33 208.06 237.78 267.5 .2 29.81 59.63 89.44 119.26 149.07 178.89 208.70 238.52 268.3 .3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 .4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 .5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	.9
.1 29.72 59.44 89.17 118.89 148.61 178.33 208.06 237.78 267.5 .2 29.81 59.63 89.44 119.26 149.07 178.89 208.70 238.52 268.3 .3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 .4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 .5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	32.0
.2 29.81 59.63 89.44 119.26 149.07 178.89 208.70 238.52 268.3 .3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 .4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 .5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	32.0
.3 29.91 59.81 89.72 119.63 149.54 179.44 209.35 239.26 269.1 .4 30.00 60.00 90.00 120.00 150.00 180.00 210.00 240.00 270.0 .5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	I.
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.5 30.09 60.19 90.28 120.37 150.46 180.56 210.65 240.74 270.8	.4
	.5
.6 30.19 60.37 90.56 120.74 150.93 181.11 211.30 241.48 271.6	.6
	1
7 30.28 60.56 90.83 121.11 151.39 181.67 211.94 242.22 272.5	-7
.8 30.37 60.74 91.11 121.48 151.85 182.22 212.59 242.96 273.3	.8
.9 30.46 60.93 91.39 121.85 152.31 182.78 213.24 243.70 274.1	.9
33.0 30.56 61.11 91.67 122.22 152.78 183.33 213.89 244.44 275.0	33.0
.1 30.65 61.30 91.94 122.59 153.24 183.89 214.54 245.19 275.8	I.
.2 30.74 61.48 92.22 122.96 153.70 184.44 215.19 245.93 276.6	.2
3 30.83 61.67 92.50 123.33 154.17 185.00 215.83 246.67 277.5	.3
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.7 31.20 62.41 93.61 124.81 156.02 187.22 218.43 249.63 280.8	.7
.8 31.30 62.59 93.89 125.19 156.48 187.78 219.07 250.37 281.6	.8
.9 31.39 62.78 94.17 125.56 156.94 188.33 219.72 251.11 282.5	.9
34.0 31.48 62.96 94.44 125.93 157.41 188.89 220.37 251.85 283.3	34.0
.1 31.57 63.15 94.72 126.30 157.87 189.44 221.02 252.59 284.1	ı.
2 31.67 63.33 95.00 126.67 158.33 190.00 221.67 253.33 285.0	.2
.3 31.76 63.52 95.28 127.04 158.80 190.56 222.31 254.07 285.8	.3
	1
.4 31.85 63.70 95.56 127.41 159.26 191.11 222.96 254.81 286.6	-4
.5 31.94 63.89 95.83 127.78 159.72 191.67 223.61 255.56 287.5	-5
.6 32.04 64.07 96.11 128.15 160.19 192.22 224.26 256.30 288.3	.6
.7 32.13 64.26 96.39 128.52 160.65 192.78 224.91 257.04 289.1	.7
8 32.22 64.44 96.67 128.89 161.11 193.33 225.56 257.78 290.0	.8
.9 32.31 64.63 96.94 129.26 161.57 193.89 226.20 258.52 290.8	.9
35.0 32.41 64.81 97.22 129.63 162.04 194.44 226.85 259.26 291.6	35.0
7,11,11,11,11,11,11,11,11,11,11,11,11,11	

X	I	2	3	4	5	6	7	8	9	Y/X
35.1	32.50	65.00	97.50	130.00	162.50	195.00	227.50	260.00	292.50	35.1
.2	32.59	65.19	97.78	130.37	162.96	195.56	228.15	260.74	293.33	.3
.3	32.69	65.37	98.06	130.74	163.43	196.11	228.80	261.48	294.17	.3
										.3
-4	32.78	65.56	98.33	131.11	163.89	196.67	229.44	262.22	295.00	.4
-5	32.87	65.74	98.61	131.48	164.35	197.22	230.09	262.96	295.83	-5
.6	32.96	65.93	98.89	131.85	164.81	197.78	230.74	263.70	296.67	.6
-7	33.06	66.11	99.17	132.22	165.28	198.33	231.39	264.44	297.50	.7
.8	33.15	66.30	99.44	132.59	165.74	198.89	232.04	265.19	298.33	.8
.9	33.24	66.48	99.72	132.96	166.20	199.44	232.69	265.93	299.17	.9
36.0	33.33	66.67	100,00	133.33	166.67	200.00	233.33	266.67	300.00	36.0
I.	33.43	66.85	100.28	133.70	167.13	200.56	233.98	267.41	300.83	I.
.2	33.52	67.04	100.56	134.07	167.59	201.11	234.63	268.15	301.67	.2
.3	33.61	67.22	100.83	134.44	168.06	201.67	235.28	268.89	302.50	.3
-4	33.70	67.41	101.11	134.81	168.52	202.22	235.93	269.63	303.33	.4
-5	33.80	67.59	101.39	135.19	168.98	202.78	236.57	270.37	304.17	.5
.6	33.89	67.78	101.67	135.56	169.44	203.33	237.22	271.11	305.00	.6
.7	33.98	67.96	101.94	135.93	169.91	203.89	237.87	271.85	305.83	.7
.8	34.07	68.15	102.22	136.30	170.37	204.44	238.52	272.59	306.67	.8
.9	34.17	68.33	102.50	136.67	170.83	205.00	239.17	273.33	307.50	.9
37.0										
	34.26	68.52	102.78	137.04	171.30	205.56	239.81	274.07	308.33	37.0
.I	34.35	68.70	103.06	137.41	171.76	206.11	240.46	274.81	309.17	.I
.2	34 - 44	68.89	103.33	137.78	172.22	206.67	241.11	275.56	310.00	.2
.3	34.54	69.07	103.61	138.15	172.69	207.22	241.76	276.30	310.83	.3
-4	34.63	69.26	103.89	138.52	173.15	207.78	242.41	277.04	311.67	.4
-5	34.72	69.44	104.17	138.89	173.61	208.33	243.06	277.78	312.50	.5
.6	34.81	69.63	104.44	139.26	174.07	208.89	243.70	278.52	313.33	.6
7	34.91	69.81	104.72	139.63	174.54	209.44	244.35	279.26	314.17	.7
.8	35.00	70.00	105.00	140.00	175.00	210.00	245.00	280.00	315.00	.8
.9	35.09	70.19	105.28	140.37	175.46	210.56	245.65	280.74	315.83	.9
38.0			105.56							38.0
	35.19	70.37		140.74	175.93	211.11	246.30	281.48	316.67	
ı.I	35.28	70.56	105.83	141.11	176.39	211.67	246.94	282.22	317.50	I.
.2	35 - 37	70.74	106.11	141.48	176.85	212.22	247.59	282.96	318.33	.2
-3	35.46	70.93	106.39	141.85	177.31	212.78	248.24	283.70	319.17	.3
.4	35.56	71.11	106.67	142.22	177.78	213.33	248.89	284.44	320.00	.4
-5	35.65	71.30	106.94	142.59	178.24	213.89	249.54	285.19	320.83	-5
.6	35.74	71.48	107.22	142.96	178.70	214.44	250.19	285.93	321.67	.6
.7	35.83	71.67	107.50	143.33	179.17	215.00	250.83	286.67	322.50	.7
.8	35.93	71.85	107.78	143.70	179.63	215.56	251.48	287.41	323.33	.8
.9	36.02	72.04	108.06	144.07	180.09	216.11	252.13	288.15	324.17	.9
39.0	36.11	72.22	108.33		180.56	216.67	252.78	288.89		39.0
				144.44					325.00	
.I	36.20	72.41	108.61	144.81	181.02	217.22	253.43	289.63	325.83	ı.
.2	36.30	72.59	108.89	145.19	181.48	217.78	254.07	290.37	326.67	.2
.3	36.39	72.78	109.17	145.56	181.94	218.33	254.72	291.11	327.50	.3
.4	36.48	72.96	109.44	145.93	182.41	218.89	255.37	291.85	328.33	-4
-5	36.57	73.15	109.72	146.30	182.87	219.44	256.02	292.59	329.17	-5
.6	36.67	73.33	110.00	146.67	183.33	220.00	256.67	293.33	330.00	.6
.7	36.76	73.52	110.28	147.04	183.80	220.56	257.31	294.07	330.83	.7
.8	36.85	73.70	110.56	147.41	184.26	221.11	257.96	294.81	331.67	.8
.9	36.94	73.89	110.83	147.78	184.72	221.67	258.61	295.56	332.50	.9
40.0	37.04	74.07	III.II	148.15	185.19	222.22	259.26	296.30	333.33	40.0
	J	,,,,,,		43				-5	303.33	

TABLE XLI

Prismoidal Corrections to be subtracted from average end area volumes 100 feet long. $D-D_1=$ difference in total width; $C-C_1=$ difference in center height. Corrections in cubic yards.

- differ	ence i	n cen	ver 1161	gir.	COLLE	CUOIIS	in cu	Die ya	uus.	
$D-D_1$ $C-C_1$	ı	2	3	4	5	6	7	8	9	$D-D_1$ $C-C_1$
.2	0.06	0.12	0.19	0.25	0.31	0.37	0.43	0.49	0.56	.2
-4	0.12	0.25	0.37	0.49	0.62	0.74	0.86	0.99	1.11	.4
.6	0.19	0.37	0.56	0.74	0.93	1.11	1.30	1.48	1.67	.6
			- 1							
.8	0.25	0.49	0.74	0.99	1.23	1.48	1.73	1.98	2.22	.8
1.0	0.31	0.62	0.93	1.23	I.54	1.85	2.16	2.47	2.78	1.0
.2	0.37	0.74	I.II	1.48	1.85	2.22	2.59	2.96	3.33	.2
-4	0.43	0.86	1.30	1.73	2.16	2.59	3.02	3.46	3.89	.4
.6	0.49	0.99	1.48	1.98	2.47	2.96	3.46	3.95	4.44	.6
.8	0.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	.8
2.0	0.62	1.23	1.85	2.47	3.09	3.70	4.32	4.94	5.56	2.0
.2	0.68	1.36	2.04	2.72	3.40	4.07	4.75	5.43	6.11	.2
.4	0.74	1.48	2.22	2.96	3.70	4.44	5.19	5.93	6.67	-4
.6	0.80	1.60	2.41	3.21	4.01	4.81	5.62	6.42	7.22	.6
.8	0.86	1.73	2.59	3.46	4.32	5.19	6.05	6.91	7.78	.8
3.0	0.93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	3.0
.2	0.99	1.98	2.96	3.95	4.94	5.93	6.91	7.90	8.89	.2
.4	1.05	2.10	3.15	4.20	5.25	6.30	7.35	8.40	9.44	-4
.6	1.11	2,22	3.33	4.44	5.56	6.67	7.78	8.89	10.00	.6
.8	1.17	2.35	3.52	4.69	5.86	7.04	8.21	9.38	10.56	.8
							8.64			
4.0	1.23	2.47	3.70	4.94	6.17	7.41		9.88	II.II	4.0
.2	1.30	2.59	3.89	5.19	6.48	7.78	9.07	10.37	11.67	.2
.4	1.36	2.72	4.07	5.43	6.79	8.15	9.51	10.86	12.22	.4
.6	1.42	2.84	4.26	5.68	7.10	8.52	9.94	11.36	12.78	.6
.8	1.48	2.96	4.44	5.93	7.41	8.89	10.37	11.85	13.33	.8
5.0	1.54	3.09	4.63	6.17	7.72	9.26	10.80	12.35	13.89	5.0
.2	1.60	3.21	4.81	6.42	8.02	9.63	11.23	12.84	14.44	.2
-4	1.67	3.33	5.00	6.67	8.33	10.00	11.67	13.33	15.00	1.0
.6	1.73	3.46	5.19	6.91	8.64	10.37	12.10	13.83	15.56	·4 .6
.8	1.79	3.58	5.37	7.16	8.95	10.74	12.53	14.32	16.11	.8
6.0	1.85	3.70	5.56	7.41	9.26	II.II	12.96	14.81	16.67	6.0
.2	1.91	3.83	5.74	7.65	9.57	11.48	13.40	15.31	17.22	.2
.4	1.98	3.95	5.93	7.90	9.88	11.85	13.83	15.80	17.78	-4
.6	2.04	4.07	6.11	8.15	10.19	12.22	14.26	16.30	18.33	.6
.8	2.10	4.20	6.30	8.40	10.49	12.59	14.69	16.79	18.89	.8
7.0	2.16	4.32	6.48	8.64	10.80	12.96	15.12	17.28	19.44	7.0
.2	2,22	4.44	6.67	8.89	11.11	13.33	15.56	17.78	20.00	.2
-4	2.28	4.57	6.85	9.14	11.42	13.70	15.99	18.27	20.56	.4
.6	2.35	4.69	7.04	9.38	11.73	14.07	16.42	18.77	21.11	.6
.8	2.41	4.81	7.22	9.63	12.04	14.44	16.85	19.26	21.67	.8
8.0										i
	2.47	4.94	7.41	9.88	12.35	14.81	17.28	19.75	22.22	8.0
.2	2.53	5.06	7.59	IO. 12	12.65	15.19	17.72	20.25	22.78	.2
-4	2.59	5.19	7.78	10.37	12.96	15.56	18.15	20.74	23.33	-4
.6	2.65	5.31	7.96	10.62	13.27	15.93	18.58	21.23	23.89	.6
.8	2.72	5.43	8.15	10.86	13.58	16.30	19.01	21.73	24.44	.8
9.0	2.78	5.56	8.33	11.11	13.89	16.67	19.44	22.22	25.00	9.0
.2	2.84	5.68	8.52	11.36	14.20	17.04	19.88	22.72	25.56	. 2
.4	2.90	5.80	8.70	11.60	14.51	17.41	20.31	23.21	26.11	.4
.6	2.96	5.93	8.89	11.85	14.81	17.78	20.74	23.70	26.67	.6
.8	3.02	6.05	9.07	12.10	15.12	18.15	21.17	24.20	27.22	1 .8
10.0	3.09	6.17	9.26	12.35	15.43	18.52	21.60	24.69	27.78	10.0
10.0	3.09	0.17	9.20	12.33	13.43	10.52	21.00	24.09	27.70	10.0

$D-D_1$	I	2	3	4	5	6	7	8	9	$D-D_1$
$C-C_1$										C-C
		6		12.59		18.89	22.04		-0	
10.2	3.15	6.30	9.44 9.63	12.59	15.74 16.05	19.26	22.47	25.19 25.68	28.33	10.2
.4 .6	3.2I 3.27	6.54	9.81	13.09	16.36	19.63	22.47	25.00	29.44	.6
.8		6.67	10.00	13.33	16.67	20.00		26.67	30.00	.8
0.11	3.33	6.79	10.00	13.58	16.07	20.37	23.33	27.16	30.56	11.0
.2	3.46	6.91	10.37	13.83	17.28	20.74	24.20	27.65	31.11	.2
	3.52	7.04	10.56	14.07	17.59	21.11	24.63	28.15	31.67	4
.6	3.58	7.16	10.74	14.32	17.90	21.48	25.06	28.64	32.22	.6
.8	3.64	7.28	10.93	14.57	18.21	21.85	25.49	29.14	32.78	.8
12.0	3.70	7.41	II.II	14.81	18.52	22.22	25.93	29.63	33.33	12.0
,2	3.77	7.53	11.30	15.06	18.83	22.59	26.36	30.12	33.89	.2
.4	3.83	7.65	11.48	15.31	19.14	22.96	26.79	30.62	34.44	.4
.6	3.89	7.78	11.67	15.56	19.44	23.33	27.22	31.11	35.00	.6
.8	3.95	7.90	11.85	15.80	19.75	23.70	27.65	31.60	35.56	.8
13.0	4.01	8.02	12.04	16.05	20.06	24.07	28.09	32.10	36.11	13.0
.2	4.07	8.15	12.22	16.30	20.37	24.44	28.52	32.59	36.67	.2
.4	4.14	8.27	12.41	16.54	20.68	24.81	28.95	33.09	37.22	.4
.6	4.20	8.40	12.59	16.79	20.99	25.19	29.38	33.58	37.78	.6
.8	4.26	8.52	12.78	17.04	21.30	25.56	29.81	34.07	38.33	.8
14.0	4.32	8.64	12.96	17.28	21.60	25.93	30.25	34.57	38.89	14.0
.2	4.38	8.77	13.15	17.53	21.91	26.30	30.68	35.06	39.44	.2
.4	4.44	8.89	13.33	17.78	22.22	26.67	31.11	35.56	40.00	.4
.6	4.51	9.01	13.52	18.02	22.53	27.04	31.54	36.05	40.56	.6
.8	4.57	9.14	13.70	18.27	22.84	27.41	31.98	36.54	41.11	.8
15.0	4.63	9.26	13.89	18.52	23.15	27.78	32.41	37.04	41.67	15.0
.2	4.69	9.38	14.07	18.77	23.46	28.15	32.84	37.53	42.22	.2
-4	4.75	9.51	14.26	19.01	23.77	28.52	33.27	38.02	42.78	-4
6	4.81	9.63	14.44	19.26	24.07	28.89	33.70	38.52	43.33	.6
.8	4.88	9.75	14.63	19.51	24.38	29.26	34.14	39.01	43.89	.8
16.0	4.94	9.88	14.81	19.75	24.69	29.63	34.57	39.51	44 · 44	16.0
.2	5.00	10.00	15.00	20.00	25.00	30.00	35.00	40.00	45.00	.2
.4	5.06	10.12	15.19	20.25	25.31	30.37	35.43	40.49	45.56	.4
.6	5.12	10.25	15.37	20.49	25.62	30.74	35.86	40.99	46.11	6
.8	5.19	10.37	15.56	20.74	25.93	31.11	36.30	41.48	46.67	.8
17.0	5.25	10.49	15.74 15.93	20.99	26.23	31.48	36.73	41.98	47.22	17.0
	5.31	1		_				42.47		
.4	5.37 5.43	10.74	16.11	21.48	26.85	32.22 32.59	37.59 38.02	42.96	48.33	.4 .6
.8	5.49	10.80	16.48	21.73	27.47	32.59	38.46	43.40	49.44	.8
18.0	5.56	11.11	16.67	22.22	27.78	33.33	38.89	44.44	50.00	18.0
.2	5.62	II.23	16.85	22.47	28.09	33.70	39.32	44.44	50.56	.2
.4	5.68	11.23	17.04	22.47	28.40	33.70	39.32	44.94	51.11	.4
.6	5.74	11.48	17.22	22.96	28.70	34.44	40.19	45.93	51.67	.6
.8	5.80	11.60	17.41	23.21	29.01	34.81	40.62	46.42	52.22	.8
19.0	5.86	11.73	17.59	23.46	29.32	35.19	41.05	46.91	52.78	19.0
.2	5.93	11.85	17.78	23.70	29.63	35.56	41.48	47.4I	53.33	.2
.4	5.99	11.98	17.96	23.95	29.94	35.93	41.91	47.90	53.89	.4
.6	6.05	12.10	18.15	24.20	30.25	36.30	42.35	48.40	54.44	.6
.8	6.11	12.22	18.33	24.44	30.56	36.67	42.78	48.89	55.00	.8
20.0	6.17	12.35	18.52	24.69	30.86	37.04	43.21	49.38	55.56	20.0

TABLE XLII. — LEVEL SECTION VOLUMES 100 feet long. Roadbed 14 feet. Slope 1½:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	57 126 206 296 398 511 635 770 917 1074 1243 1422 1613 1815 2028 2252 2487 2733 2991	5 64 133 214 306 409 523 648 785 932 1090 1260 1441 1633 1836 2050 2275 2511 2759 3017	111 70 141 223 316 420 535 661 799 947 1107 1278 1459 1652 1857 2072 2298 2535 2784 3044	16 77 149 232 326 431 547 675 813 963 1123 1295 1478 2094 2321 2560 2809 3070	22 83 156 241 336 442 559 688 828 1140 1313 1497 1692 1899 2116 2345 2584 2835 3097	27 90 164 250 346 453 572 701 842 994 1157 1331 1516 1713 1920 2138 2368 2609 2861 3124	33 97 172 259 356 465 584 715 857 1010 1174 1349 1535 1733 1941 2161 2392 2633 2886 3151	39 104 181 268 366 476 597 729 872 1026 1191 1367 1555 1753 1963 2183 2415 2658 2912 3178	45 111 189 277 377 488 609 742 1208 1385 1574 1774 1984 2206 2439 2683 2938 3205	51 119 197 287 387 499 622 756 902 1058 1225 1404 1593 1794 2006 2229 2463 2708 2965 3232	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.o	7.0	8.0	9.0	Center height
20 30 40	3259 6556 10963	3539 6946 11465	3830 7348 11978	4131 7761 12502	4444 8185 1303 7	4769 8620 13583	5104 9067 1414 1	5450 9524 147 0 9	5807 9993 15289	6176 10472 25880	20 30 40

TABLE XLIII. — Level Section Volumes 100 feet long. Roadbed 16 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	65 141 228 326 435 556 687 830 983 1148 1324 1511 1709 1919 2139 2370 2613 2867 3131	6 72 149 237 336 447 568 701 845 999 1165 1342 1530 1730 1940 2162 2394 2638 2893 3159	12 79 157 247 347 458 581 715 859 1015 1182 1361 1550 1750 1962 2184 2418 2663 2919 3186	18 86 166 256 358 470 594 729 875 1032 1200 1379 1569 1771 1983 2207 2442 2688 2945 3213	25 94 174 266 368 482 607 743 890 1048 1217 1398 1589 1792 2005 2230 2466 2713 2971 3241	31 101 183 275 379 494 620 757 905 1064 1235 1416 1609 1813 2027 2253 2490 2738 2998 3268	38 109 192 285 390 506 633 771 1081 1252 1435 1629 1833 2049 2276 2515 2764 3024	44 117 201 295 401 518 646 786 1098 1270 1454 1649 1855 2072 2300 2539 2789 3051 3323	51 125 209 305 412 531 660 800 952 1114 1288 1473 1669 1876 2094 2323 2564 2815 3078	58 133 219 316 424 543 673 815 967 1131 1306 1492 1689 1897 2116 2347 2588 2841 3105 3379	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3407 6778 11259	3694 7176 11769	3993 7585 12289	4302 8006 12820	4622 8437 13363	4954 8880 13917	5296 9333 14481	5650 9798 15057	6015 10274 15644	6391 10761 16243	20 30 40

TABLE XLIV. — LEVEL SECTION VOLUMES 100 feet long. Roadbed 20 feet. Slope 1½:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	a.8	0.9	Center height
0 1 2 3 4 6 6 7 8 9 10 11 12 13 14 15 16 17 18	80 170 272 385 509 644 791 1487 1689 1902 2126 2361 2607 2865 3133 3413	7 88 180 283 397 522 659 806 1134 1315 1507 1710 1924 2149 2385 2633 2891 3161	15 97 190 294 409 535 673 821 1152 1334 1527 1731 1946 2172 2409 2658 2918 3188 3470	23 106 200 305 421 549 687 837 998 1159 1356 1752 1968 2195 2435 2683 2944 3216	31 115 210 316 433 562 702 852 1014 1187 1371 1566 1773 1990 2219 2458 2709 2971 3244 3528	38 124 220 327 446 575 716 868 1031 1205 1390 1587 1794 2012 2242 2483 2735 2998 3272 3557	46 133 230 339 458 589 731 884 1048 1223 1409 1607 1815 2035 2266 2508 2761 3025 3305 3586	55 142 240 350 471 603 746 900 1065 1241 1429 1627 1837 2058 2289 2532 2786 3052 3328 3615	63 151 251 362 484 617 761 916 1082 1259 1448 1648 2080 2313 2557 2812 3079 3356	71 161 262 373 496 630 776 932 1099 1278 1461 1668 1880 2103 2337 2582 2839 3106 3384 3674	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.o	9.0	Center height
20 30 40	3704 7222 11852	4006 7635 12376	4319 8059 12911	4643 8494 13457	4979 8941 14015	5324 9398 14583	5681 9867 15163	6050 10346 15754	6430 10837 16356	6820 11339 16969	20 30 40

TABLE XLV. — LEVEL SECTION VOLUMES 100 feet long. Roadbed 20 feet. Slope 1:1.

			_								
Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		7	15	23	30	38	46	54	62	70	0
ī	78	86	94	103	111	114	128	137	145	154	I
2	163	172	181	190	199	208	218	227	236	246	2
	256	265	275	285	295	305	315	325	335	345	
4	356	366	376	387	398	408	419	430	441	452	ا م
5	463	474	485	497	508	519	531	543	554	566	5
3 4 5 6 7 8 9	578	590	602	614	626	638	650	663	675	687	3 4 5 6
7	700	713	725	738	751	764	777	790	803	816	
8	830	843	856	870	884	897	911	925	939	953	7 8 9
9	967	981	995	1009	1024	1038	1052	1067	1082	1096	9
	IIII	1126	1141	1156	1171	1186	1201	1217	1232	1247	10
II	1263	1279	1294	1310	1326	1342	1358	1374	1390	1406	II
12	1422	1439	1455	1471	1488	1505	1521	1538	1555	1572	12
13	1589	1606	1623	1640	1658	1675	1692	1710	1728	1745	13
14	1763	1781	1799	1817	1835	1853	1871	1889	1908	1926	14
15 16	1944	1963	1982	2000	2019	2038	2057	2076	2095	2114	15 16
10	2133	2153	2172	2191	2211	2231	2250	2270	2290	2310	
17 18	2330	2350	2370	2390	2410	2431	2451	247I 2680	2492	2513	17
19	2533	2554 2766	2575 2788	2596 2809	2831	2638	2659		2702	2723	18
19	2744	2/00	2/00	2009	2031	2853	2875	2897	2919	2941	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.o	9.0	Center height
20	2963	3189	3422	3663	3991	4167	4430	4700	4978	5263	20
30	5556	5856	6163	6478	6800	7130	7467	7811	8163	8522	30
40	8889	9263	9644	10033	10430	10833	11244	11663	12089	12522	40

TABLE XLVI. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 3 4 5 6 7 8 9 10 11 13 14 15 16 17 18	94 200 317 444 583 733 894 1067 1250 1444 1650 1867 2094 2333 2583 2583 2583 3117 3400	9 105 211 329 458 598 749 911 1085 1269 1465 1671 1889 2118 2358 2609 2871 3145 3429	18 115 222 341 471 612 765 928 1102 1288 1485 1692 1911 2141 2382 2635 2898 3172 3458	27 125 234 354 485 627 780 945 1121 1307 1505 1714 1934 2165 2407 2661 2925 3201 3487 3785	36 135 245 366 499 642 796 962 1139 1326 1525 1735 1956 2189 2432 2686 2952 3229 3219 3815	46 146 257 379 512 657 812 979 1157 1346 1546 1757 1979 2213 2457 2713 2979 3257 3546	55 156 269 392 526 672 829 996 1175 1365 1566 1779 2002 2236 2482 2739 3006 3285 3575	65 167 280 405 540 687 845 1014 1194 1385 1587 2025 2261 2507 2765 3034 3314 33097	75 178 292 418 555 702 861 1031 1212 1405 1608 1822 2048 2285 2532 2791 3061 3342 3635 3938	85 189 304 431 569 718 878 1049 1231 1425 1629 1845 2071 2309 2558 389 3371 3665 3969	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	4000 7667 12444	4317 8004 12983	4644 8533 13533	4983 8983 14094	5333 9444 14667	5694 9917 15250	6067 10400 15844	6450 10894 16450	6844 11400 17067	7250 11917 17694	20 30 40

TABLE XLVII. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	o.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 13 14 15 16 17 18	93 193 300 415 537 667 804 1100 1259 1426 1600 1782 1970 2167 2370 2582 2800 3026	9 102 203 311 427 550 680 818 963 1116 1276 1618 1618 1800 1990 2187 2391 2603 2822 3049	18 112 214 322 439 562 694 832 1131 1292 1460 1636 1819 2009 2207 2412 2625 2845 3072	27 122 224 334 451 575 707 846 993 1147 1308 1477 1654 1837 2028 2227 2433 2646 2867 3095	36 132 235 345 463 588 721 1008 1163 1325 1495 1672 1856 2048 2247 2454 2668 2889 3118	45 142 245 356 475 601 734 875 1023 1179 1342 1690 1875 2068 2475 2690 2912	55 152 256 368 487 614 748 890 1038 1195 1358 1530 1708 1894 2087 2288 2496 2712 2935 3165	64 162 267 380 500 627 762 904 1054 1211 1375 1547 1726 1913 2107 2308 2517 2734 2957 3188	74 172 278 391 510 640 756 919 1069 1226 1392 1565 1745 1932 2127 2329 2539 2756 2980	83 182 289 403 524 653 790 933 1084 1243 1409 1582 1763 1951 2147 2350 2560 2778 3003 3236	0 1 2 3 4 5 6 7 8 9 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3259 6000 9481	3500 6315 9870	3748 6637 10267	4004 6967 10670	4267 7304 11081	4537 7648 11500	4815 8000 11926	5100 8359 12359	5393 8726 12800	5692 9100 13248	20 30 40

TABLE XLVIII. — Level Section Volumes 100 feet long. Roadbed 26 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		10	19	29	39	50	60	70	81	91	0
ī	102	113	124	135	146	157	168	180	191	203	I
2	215	227	239	251	263	275	288	301	313	326	2
3	339	352	365	378	392	405	419	432	446	460	
A	474	488	502	517	531	546	561	575	590	605	3 4 56 78 9
5	620	636	651	666	682	698	713	729	745	762	5
ĕ	778	794	811	827	844	861	878	895	912	929	6
4 5 6 7 8 9	946	964	981	999	1017	1035	1053	1071	1089	1107	7
8	1126	1144	1163	1182	1201	1220	1239	1258	1278	1297	8
9	1317	1333	1356	1376	1396	1416	1436	1457	1477	1498	
10	1519	1539	1560	1581	1602	1624	1645	1666	1688	1710	10
II	1731	1753	1775	1798	1820	1842	1865	1887	1910	1933	II
12	1956	1979	2002	2025	2048	2072	2095	2119	2143	2167	12
13	2191	2215	2239	2263	2288	2312	2337	2362	2387	2412	13
14	2437	2462	2488	2513	2539	2564	2590	2616	2642	2668	14
15 16	2694	2721	2747	2774	2800	2827	2854	2881	2908	2936	15 16
10	2963	2990	3018	3046	3073	3101	3129	3158	3186	3214	
17 18	3243	3271	3300	3329	3358	3387	3416	3445	3474	3504	17 18
18	3533	3563	3593	3623	3653	3683	3713	3743	3774	3804	
19	3835	3866	3897	3928	3959	3990	4022	4053	4085	4116	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20	4148	4472	4807	5154	5511	5880	6259	6650	7052	7465	20
30	7889	8324	8770	9228	9696	10176	10667	11168	11681	12205	30
40	12741	13287	13844	14413	14992	15583	16185	16798	17422	18057	40
40	12/41	10007	13044	*44*3	-4992	-5505	20103	20190	-,455	1 31	

TABLE XLIX. — Level Section Volumes 100 feet long. Roadbed 26 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 56 7 8 9 10 11 12 13 14 15 16 17	 100 207 322 444 574 571 856 1007 1167 1333 1507 1689 2074 2278 2489 2707 2933	10 110 219 334 457 725 870 1023 1183 1350 1525 1707 1897 2094 2299 2510 2730 2956	19 121 230 346 470 601 739 885 1039 1199 1368 1543 1726 1916 2114 2319 2532 2752 2979	29 131 241 358 483 614 900 1054 1216 1385 1561 1745 1936 2134 2340 2554 3003	39 142 252 370 495 628 768 915 1070 1232 1402 1579 1764 1955 2155 2361 2575 2797 3026	49 153 264 382 508 642 782 931 1086 1249 1419 1597 1782 2175 2382 2597 2819 3049	59 164 275 395 521 655 797 946 1102 1266 1437 1615 1801 1995 2195 2404 2619 2842 3072	69 174 287 407 534 669 811 961 1118 1283 1454 1634 1820 2014 2216 2425 2641 2865 3096	79 185 299 419 548 683 826 976 1134 1299 1472 1652 1839 2034 2236 2446 2663 2888 3119	90 196 310 432 561 697 841 992 1150 1316 1490 1670 1859 2054 2257 2467 2685 2910 3143	0 1 2 3 4 56 7 7 8 9 10 11 12 13 14 15 16 17
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.o	7.0	3359 8.o	9.0	Center height
20 30 40	3407 6222 9778	3656 6544 10174	3911 6874 10578	4174 7211 10989	4444 7556 11407	4722 7907 11833	5007 8267 12267	5300 8633 12707	5600 9007 13156	5907 9389 13611	20 30 40

TABLE L. — Level Section Volumes 100 feet long. Roadbed 28 feet. Slope $1\frac{1}{2}:1$.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 3 4 5 6 7 8 9 10 11 13 14 15 17 18	109 230 361 504 656 822 998 1185 1383 1592 1812 2044 2287 2541 2806 3081 3368 3667 3976	10 121 242 375 519 673 839 1016 1204 1403 1614 1835 2312 2567 2833 3109 3397 3697 4007	21 132 255 389 534 690 856 1035 1224 1424 1635 1858 2092 2337 2593 2860 3138 3427 3728 4039	32 144 268 403 549 706 874 1053 1243 1445 1657 1881 2116 2362 2619 2887 3166 3456 3758	42 156 281 417 564 722 891 1072 1263 1465 1679 1904 2140 2387 2645 2915 3195 3486 3789 4102	53 168 294 431 579 738 909 1090 1283 1486 1701 1927 2164 2413 2672 2942 3223 3516 3820 4134	64 180 307 445 595 755 926 1109 1303 1507 1723 1950 2189 2438 2698 2970 3252 3546 3851 4166	75 192 320 460 610 772 944 1128 1322 1528 1745 1973 2213 2464 2725 2997 3281 3576 3882 4198	86 205 334 474 626 788 962 1147 1343 1549 1767 2238 2489 2752 3025 3310 3606 3913 4231	98 217 348 489 642 805 980 1166 1363 1571 1790 2020 2262 2515 2779 3053 3339 3636 3944 4263	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	4296 8111 13037	4627 8554 13591	4970 9007 14156	5324 9472 14731	5689 9948 15318	6065 10435 15917	6451 10933 16526	6850 11443 17146	7259 11963 17778	7680 12494 18420	20 30 40

TABLE LI. — LEVEL SECTION VOLUMES 100 feet long. Roadbed 28 feet. Slope 1:1

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 3 4 5 6 7 8 9 10 11 12 13 14 15 17 18	107 222 344 474 611 656 908 1067 1233 1407 1589 1778 1974 2178 2389 2607 2833 3067 3307	10 119 234 357 487 625 770 923 1083 1250 1425 1607 1797 1994 2199 2410 2630 2856 3090 3332	21 130 246 370 501 639 785 939 1099 1267 1443 1626 1816 2014 2219 2432 2652 2879 3114 3356	31 141 258 383 514 654 800 954 1116 1285 1461 1645 1836 2034 2240 2454 2674 2903 3138 3381	42 152 270 395 528 668 816 970 1132 1302 1479 1664 1855 2055 2261 2475 2697 2926 3162 3406	53 164 282 408 542 682 831 149 1319 1497 1682 1875 2075 2282 2497 2719 2949 3186 3431	64 175 295 421 555 697 846 1002 1166 1337 1515 1701 1895 2095 2304 2519 2742 2972 3210 3455	74 167 307 434 569 711 861 1018 1182 1354 1720 1914 2116 2325 2941 2765 2996 3234 3480	85 199 319 448 583 726 876 1034 1199 1372 1552 1739 1934 2136 2346 2346 2346 2788 3019 3259 3505	96 210 332 461 597 741 892 1050 1216 1390 1570 1954 2157 2367 2367 2585 2810 3043 30283 3530	0 1 2 3 4 56 78 9 10 11 12 13 14 15 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3556 6444 10074	3811 6774 10478	4074 7111 10889	4344 7456 11307	4622 7807 11733	4907 8167 1216 7	5200 8533 12607	5500 8907 13056	5807 9289 13511	6122 9678 13974	20 30 40

TABLE LII. — Level Section Volumes 100 feet long. Roadbed 30 feet. Slope $1\frac{1}{2}:1$.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		11	22	34	45	57	69	80	92	104	0
ĭ	117	129	141	154	166	179	192	205	218	231	I
	244	258	271	285	299	312	326	340	355	369	2
2 3 4 5 6 7 8 9	383	398	412	427	442	457	472	487	502	518	3
4	533	549	565	580	596	612	629	645	661	678	4
5	694	711	728	745	762	779	796	814	831	849	4 56 7 8
6	867	884	902	920	939	957	975	994	1012	1031	6
7	1050	1069	1088	1107	1126	1146	1165	1185	1205	1224	7
8	1244	1264	1285	1305	1325	1346	1366	1387	1408	1429	8
9	1450	1471	1492	1514	1535	1557	1579	1600	1622	1644	9
	1667	1689	1711	1734	1756	1779	1802	1825	1848	1871	10
11	1894	1918	1941	1965	1981	2012	2036	2060	2085	2109	II
12	2133	2158	2182	2207	2232	2257	2282	2307	2332	2358	12
13	2383	2409	2435	2460	2486	2512	2539	2565	2591	2618	13
14	2644	2671	2698	2725	2752	2779	2806	2834	2861	2889	14
15 16	2917	2944	2972	3000 3287	3029	3057	3085	3114	3142	3171	15 16
10	3200	3229	3258	3585	3316 3615	3346 3646	3375	3405	3435	3464	10
17 18	3494 3800	3525 3831	3555 3862	3894		3957	3676 3989	3707 4020	3738	3769 4084	17 18
19	4117		4181	4214	3925 4246	4279	4312	4345	4052 4378		19
19	4117	4149	4101	4214	4240	4219	4312	4343	4370	4411	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20	4444	4783	5133	5494	5867	6250	6644	7050	7467	7894	20
30	8333	8783	9244	9717	10200	10694	11200	11717	12244	12783	30
40	13333	13894	14467	15050	15644	16250	16867	17494	18133	18783	40
						1		. 151	-00	, -0	

TABLE LIII. — Level Section Volumes 100 feet long. Roadbed 30 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 56 7 8 9 10 11 12 14 15 16 17	115 237 367 504 648 800 959 1126 1300 1481 1670 1867 2070 2281 2500 2726 2959 3200	11 127 250 380 518 663 816 976 1143 1318 1500 1690 1887 2091 2303 2522 2749 2983 3224	22 139 262 393 532 678 831 992 1166 1336 1519 1709 1907 2112 2325 2545 2772 3007 3249	34 151 275 407 546 693 847 1008 1177 1354 1537 1728 1927 2133 2346 2567 2795 3031	45 163 288 421 561 708 863 1025 1372 1556 1748 1947 2154 2368 2589 2818 3055 3298	56 175 301 434 575 723 879 1042 1212 1390 1575 1768 1968 2175 2390 2612 2842 3079 3323	68 187 314 448 589 738 895 1058 1229 1408 1594 1787 1988 2412 2635 2865 3103 3348	80 200 327 462 604 754 911 1075 1247 1426 1613 1807 2008 2217 2434 2657 2888 3127 3373	91 212 340 476 619 769 927 1092 1265 1445 1632 1827 2029 2239 2456 2680 2912 3151 3399	103 224 353 490 633 784 943 1109 1282 1463 1651 1847 2050 2260 2478 2703 2936 3176 3176	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
Center height	3448 0.0	3473	3499 2.0	3524	3549 4.0	3575 5.0	360I 6.0	3626 7.0	3652 8.0	3678 9.0	Center height
20 30 40	3704 6667 10370	3967 7004 10781	4237 7348 11200	4515 7700 11626	4800 8059 12059	5093 8426 12500	5393 8800 12948	5700 9181 13404	6015 9570 13867	6337 9967 14337	20 30 40

TABLE LIV. — Level Section Volumes 100 feet long. Roadbed 32 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	124 259 406 563 731 911 1102 1304 1517 1741 1976 2222 248 3028 3319 3620 3933	12 137 273 421 579 930 1122 1324 1539 1764 2000 2247 2506 2776 3056 3348 3651 3965	24 150 288 436 596 767 948 1141 1345 1561 1787 2024 2273 2803 3085 3378 3682 3997	36 163 302 452 612 784 967 1161 1366 1583 1810 2049 2298 2559 2831 3114 3408 4029	48 177 316 467 629 862 986 1181 1388 1605 1833 2073 2324 2586 2859 3143 3438 3744 4062	61 190 331 483 646 820 1005 1201 1409 1627 1857 2099 2350 2612 2887 3172 3468 3775 4094	73 204 346 499 663 838 1024 1222 1430 1650 1881 2122 2375 2639 2915 3201 3498 3807 4126	86 218 360 515 680 856 1043 1242 1472 1904 2147 2401 2666 2943 3230 3529 3888 4159	98 231 375 531 697 874 1063 1262 1473 1695 1928 2172 2427 2694 2971 3259 3359 3870 4192	111 245 390 547 714 893 1082 1283 1495 1718 1952 2197 2453 2721 2999 3289 3590 3902 4224	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
Center height	0.0	1.0	2.0	3.0	4.0	5.0	4457 6.o	7.0	4525 8.0	4559 9.0	Center height
20 30 40	4593 8556 13630	4939 9013 14198	5296 9482 14778	5665 9962 15369	6044 10452 15970	6435 10954 16583	6837 11467 17207	7250 11991 17843	7674 12526 18489	8109 13072 19146	20 30 40

TABLE LV. — Level Section Volumes 100 feet long. Roadbed 32 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	122 252 389 533 685 844 1011 1185 1367 1556 2167 2385 2611 2844 3085 3333 3389	12 135 265 403 548 701 861 1028 1203 1385 1575 1772 1976 2188 2407 2634 2868 3110 3359 3615	24 148 279 417 563 716 877 1045 1221 1404 1594 1792 1997 2210 2657 2892 3134 3384 3641	36 160 292 431 578 894 1063 1239 1423 1614 1812 2018 2231 2452 2680 2916 3159 3409 3667	48 173 306 446 593 748 910 1080 1257 1441 1633 1832 2039 2253 2475 2704 2940 3184 3435 3693	60 186 319 460 608 764 927 1097 1275 1460 1653 1853 2060 2275 2497 2727 2964 3208 3460 3719	72 199 333 475 624 780 944 1115 1293 1479 1672 1873 2081 2297 2520 2750 2988 3233 3486 3746	85 212 347 489 639 796 960 1132 1311 1498 1692 1894 2103 2319 2543 2774 3012 3258 3511 3772	97 225 361 504 812 977 1150 1330 1517 1712 1914 2124 2341 2565 2797 3036 3283 3537 3799	110 239 375 519 670 828 994 1167 1348 1536 1732 2145 2363 2245 2363 308 3363 3363 3363 3825	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0 9	9.0	Center height
20 30 40	3852 6889 10667	4122 7233 11085	4400 7585 11511	4685 7944 11944	4978 8311 12385	5278 8685 12833	5585 9067 13289	5900 9456 13752	6222 9852 14222	6552 10256 14700	20 30 40

TABLE LVI. — Level Section Volumes 100 feet long. Roadbed 20 feet. Slope $\frac{1}{4}$: 1.

I	Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
ſ	0		7 83	15 90	22 98	30 106	37 113	45 121	52	60 136	67	0 I
ı	I	75 152	160	167	175	183	191	199	129 207	214	144 223.	
ı	2	231	238	246	254	263	271	279	287	295	303	3
ı	2 3 4 5 6 7 8 9	311	319	327	336	344	352	360	369	377	385	2 3 4 5 6 7 8 9
ł	5	394	402	410	419	427	435	444	452	461	469	5
1	ĕ	478	486	495	503	512	521	529	538	546	555	6
ı	7	564	573	581	590	599	608	616	625	634	643	7
ı	8	652	661	670	679	688	696	706	714	724	733	8
ı	9	742	751	760	769	778	787	796	806	815	824	9
ı	10	833	843	852	861	870	880	889	899	908	917	10
ı	II	927	936	946	955	965	974	984	993	1003	1013	II
ı	12	1022	1032	1042	1051	1061	1071	1080	1090	1100	IIIO	12
ı	13	1119	1129	1139	1149	1159	1269	1179	1289	1199	1209 1309	13
ı	14	1319	1330	1340	1350	1360	1371	1381	1391	1402	1412	14
ı	15 16	1422	1433	1443	1453	1464	1474	1485	1495	1506	1516	15 16
ı	17	1527	1537	1548	1559	1569	1580	1591	1601	1612	1623	17
ı	17 18	1633	1644	1655	1666	1676	1687	1698	1709	1720	1731	18
ı	19	1742	1753	1764	1774	1785	1796	1808	1819	1830	1841	19
I	Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.o	9.0	Center height
	20 30 40	1852 3056 4444	1964 3186 4593	2078 3319 4744	2194 3453 4897	2311 3589 5052	2431 3727 5208	2552 3867 5367	2675 4008 5527	2800 4152 5689	2927 4297 5853	20 30 40

TABLE LVII. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope $\frac{1}{4}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		9	18	27	36	45	54	63	72	81	0
	90	99	108	117	126	135	145	154	163	172	I
1 2	181	191	200	209	219	228	237	247	256	266	2
3	275	284	294	303	313	322	332	342	351	361	3
4	370	380	390	399	409	419	428	438	448	458	
5	468	477	487	497	507	517	527	537	547	557	4 5 6
3 4 5 6 7 8 9	567	577	587	597	607	617	627	637	647	657	6
7	668	678	688	698	708	719	729	739	750	760	7 8
8	770	781	791	802	812	822	833	843	854	864	8
9	875	886	896	907	917	928	939	949	960	971	9
10	981	992	1003	1014	1025	1035	1046	1057	1068	1079	10
11	1090	IIOI	1112	1123	1134	1145	1156	1167	1178	1189	II
12	1200	1211	1222	1233	1245	1256	1267	1278	1289	1301	12
13	1312	1323	1335	1346	1357	1369	1380	1392	1403	1414	13
14	1426	1437	1449	1460	1472	1484	1495	1507	1518	1530	14
15 16	1542	1553	1565 1683	1577	1588	1600	1612	1624	1636	1647	15 16
	1659	1671	1803	1695	1707	1719	1731	1743	1755 1876	1888	
17	1779	1791	1924	1815	1949	1839 1961	1851	1986	1998	2011	17
19	2023	2036	2048	2060	2073	2085	2098	2110	2123	2136	19
19	2023	2030	2040	2000	20/3	2003	2090	2110	2123	2130	19
Center	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center
height		1.0	2.0	3.0	4.0	3.0		7.0		9.0	height
20	2148	2275	2404	2534	2667	2801	2937	3075	3215	3356	20
30	3500	3645	3793	3942	4093	4245	4400	4556	4715	4875	30
40	5037	5201	5367	5534	5704	5875	6048	6223	6400	6579	40

TABLE LVIII. — MIDDLE ORDINATES FOR CURVING RAILS Ordinate given in inches

From Roberts' "Track Formulæ and Tables."

Degree					Le	ngth of	rails in	n feet				
curve	10	12	14	16	18	20	22	24	26	28	30	33
0.5° 1° 1.5°					 ½	 ½	1/8	1/8 1/8	78 14	1/8 1/8 1/4	1/8 1/4 3/8	1/8 1/4 3/8
2° 2.5° 3°			1/8 1/8 1/8	1/8 1/8 1/8	1/8 1/4 1/4	1/8 1/4 1/4	1/4 1/4 3/8	14 38 12	38 38 12	3/8 1/2 5/8	3/8 1/2 5/8	58 34 78
3.5° 4° 4.5°	 1/8 1/8	1/8 1/8 1/8	1/8 1/8 1/4	1/4 1/4 1/4	1/4 3/8 3/8	3/8 3/8 1/2	3/8 1/2 1/2	1/2 5/8 5/8	58 34 34	34 78 78	7/8 I I	1 158 154
5° 5.5° 6°	1/8 1/8 1/8	1/8 1/4 1/4	1/4 1/4 3/8	3/8 3/8 3/8	3/8 1/2 1/2	7.2 5.8 5.8	5/8 3/4 3/4	34 78 78	78 I I148	I I½8 I¼	1½ 1¼ 1¾ 1¾	138 158 134
6.5° 7° 7.5°	1/8 1/8 1/8	1/4 1/4 1/4	3/8 3/8 3/8	1,6 1,6 1,6	1/2 5/8 5/8	3/4 3/4 3/4	7/8 7/8 I	I I I½8	178 174 138	138 112 112	1½ 158 134	17/8 2 21/8
8° 8.5° 9°	1/4 1/4 1/4	1/4 3/8 3/8	38 38 12	1/2 5/8 5/8	3/4 3/4 3/4	7/8 7/8 7/8	I I½ I½	114 114 138	138 112 158	158 134 178	17/8 2 21/8	2½ 2¾ 2¾ 2½
9.5° 10° 10.5°	1/4 1/4 1/4	3/8 3/8 3/8	1/2 1/2 5/8	58 58 34	34 76 78	I I I½8	11/4 11/4 13/8	138 112 138	134 134 178	2 2 2½8	2½ 2¾ 2¾ 2½	234 27/8 3
11° 11.5° 12°	1/4 3/8 3/8	38 1/2 1/2	58 58 58	3/4 3/4 3/4	I I	11/8 11/4 11/4	138 132 132	158 134 178	2 2½8 2½8	2 ¹ / ₄ 2 ³ / ₈ 2 ¹ / ₂	258 234 278	3½ 3½ 3½ 3¾
12.5° 13° 13.5°	38 38 38	1/2 1/2 1/2	58 58 34	7/8 7/8 I	11/8 11/8 11/4	138 138 112	158 158 134	2 2 2 ¹ /8	2½ 2½ 2½ 2¾ 2¾	25/8 25/8 23/4	3 3 3½	35/8 33/4 37/8
14° 14.5° 15°	3/8 3/8 3/8	1/2 5/8 5/8	34 34 34	I	11/4 11/4 11/4	13/2 13/8 15/8	134 178 178	21/8 21/4 21/4	2½ 25/8 25/8	27/8 3 31/8	3½ 3¾ 3½ 3½	4 4½ 4½ 4½
15.5° 16°	38 38	5/8 5/8	7/8 7/8	11/8	138 138	158 158	2 2	23/8 23/8	27/8 27/8	3 ¹ / ₄ 3 ¹ / ₄	35/8 33/4	438 458

TABLE LVIIIa. - GAGE ON CURVES

Degree of curve	Gage	Degree of curve	Gage
8° and under 9°-10° 11°-12° 13°-14°	4' 8½" 4' 856" 4' 834" 4' 878"	15°-16° 17°-18° 19°-20°	4' 9" 4' 9½6" 4' 9¼4"

CANTING THE TRACK

Using the gage for the base, if R = radius, S = speed in miles per hour and e is the difference in level of the two rails in feet,

$$e = \frac{4.708}{\sqrt{1 + 223.5 \frac{R^2}{S^4}}}.$$

Using gage plus one rail head which the author recommends for use with the common track level,

$$e = \frac{4.9}{\sqrt{1 + 223.5 \frac{R^2}{S^4}}}$$

The corresponding approximate formulas are $e = \frac{0.3149 \text{ } S^2}{R}$ and $e = \frac{0.3278 \text{ } S^2}{R}$. In inches $E = 0.00066 \text{ } S^2D$ and $E = 0.000686 \text{ } S^2D$.

The formula of the American Railway Engineering Association for difference of level measured at the gage lines is

$$E = 0.00066 S^2 D$$
,

but the author recommends $E = 0.000686 S^2D$. Both formulas are tabulated in Tables LIX and LIXa.

TABLE LIX

Difference of level in inches of the two rails of a standard gage track on curves of various degrees for various speeds.

Formula: $E = 0.00066 S^2D$

(Nearest ½ inch)

Degree					Sp	eed i	n mile	s per	hour					Degree of
curve	10	15	20	25	30	35	40	45	50	55	60	65	70	curve
I	_	1/8	1/4	3/8	5/8	3/4	11/8	13/8	15%	2	23/8	23/4	31/4	I
2	1/8	3/8	1/2	7/8	11/8	158	21/8	25/8	31/4	4	434	51/2	61/2	2
3	1/4	1/2	34	11/4	134	23/8	31/8	4	47/8	6	71/8	83/8	934	3
	1/4	5,8	I	15/8	23/8	31/4	41/4	53/8	65/8	8	91/2			4
4 5 6	1/4 3/8 3/8	3/4	11/4	2	3	4	51/4	658	81/4					5 6
6	3/8	I	15/8	21/2	31/2	47/8	61/4	8						6
7 8	1/2	11/8	17/8	27/8	41/8	55/8	73/8							7 8
8	1/2	11/4	21/8	31/4	43/4	61/2	83/8							
9	5/8	13/8	23/8	33/4	538	71/4								9
10	34	11/2	25/8	41/8	57/8	81/8								10
II	3/4	$1\frac{3}{4}$	27/8	41/2	61/2	87/8								11
12	7/8 7/8	17/8	31/8	47/8	71/8									12
13	7/8	2	33/8	53/8	734									13
14	I	21/8	35/8	53/4	83.8									14
15	Ι	21/4	37/8	61/4	87/8									15
16	11/8	21/2	41/4	65/8										16
17	11/4	25/8	41/2	7										17
18	11/4	23/4	43/4	71/2										18
19	138	27/8	5	73/4										19
20	138	3	51/4	81/8										20

TABLE LIXa

From Formula $E = 0.000686 S^2D$ (Nearest $\frac{1}{16}$ inch)

Degree					Spe	ed in	miles	per	hour					Degree
curve	10	15	20	25	30	35	40	45	50	55	60	65	70	curve
0.5	1/16	1/16	1/8	3/16	5/16	7/16	9/16	11/16	7/8	11/16	11/4	17/16	111/16	0.5
I	1/16	1/8	1/4	7/16	5/8	13/16	11/16	13/8	111/16	21/16	21/2	27/8	338	1
2	1/8	5/16	9/16	7/8	11/4	111/16	23/16	23/4	37/16	41/8	415/16	513/16	634	2
3	³ ⁄16	716	13/16	15/16	17/8	21/2	35/16	41/8	51/8	63/16	738	81 1/16		3
4	1/4	5/8	11/16	111/16	21/2	33/8	43/8	5%16	613/16					4
4 5 6	38	3/4	13/8	21/8	31/16	43/16	57/16	67/8						5 6
	7/16	15/16	15/8	29/16	31 1/16	5.0	6916							6
7 8	1/2	11/16	115/16	3.0	45/16	513/16	75/8							7
	%16	11/4	23/16	33/8	47/8	6916								8
9	5/8	13/8	21/2	313/16	51/2	71/2								9
10	¹ / ₁₆	1916	23/4	41/4	61/8									10
II	$\frac{3}{4}$	111/16	3.0	41 1/16	634									11
12	13/16	17/8	35/16	51/8	75/16									12
14	15/16	23/16												14
	11/16	21/2	43/8	613/16						".				16
	11/4	234	415/16	75/8										18
20	13/8	31/16	57/16											20

TABLE LX

From Roberts' "Track Formulæ and Tables."

		20	-	-	~	~	~	~~		~~	~	~	10	10	10	10	10	10	10	10	_	7	7	7	7	7
olts	%.!	keg	102	_	148			_														247				247
Track bolts	ä	Size	1×434"	1X434"	78×4½"	78×4½"	78×4½"	78×4½"	78×4½"	78×4½"	78×4½"	78×4½"	34×41/8"	34×41/8"	34×438"	34×418"	34×41,8"	34×438"	34×436"	34×438"	34×3½"	34×3½"	34×3½"	34×3½"	3/4×3/5"	34×31/5"
Wt. in	I pair	bars	99.5	99.5	87.0	87.0	74.0	74.0	1.89	68.I	63.1	63.I	58.5	58.5	54.0	24.6	37.8	34.0	35.6	32.4	32.4	34.0	34.0	28.9	27.2	25.5
Lgth.	of angle	bars	34"	34"	34,		34"								34"	34″	24"	24,,	24"	24"	24"					24"
ų l	ck ts	Kgs.	0.399	0.366	0.275	0.252	0.266	0.244	0.266	0.244	0.266	0.244	0.181	0.166	0.181	0.181	12 0.121	0.121	0.121	0.121	O.IIO	0.110	.12 0.110	0.110	O.IIO	0.110
trac!	Track bolts	No.	40.68	37.29	40.68	37.29	40.68	37.29	40.68	37.29	40.68	37.29	40.68	37.29	40.68	40.68	27	27.12	27.12 0.121	27.12 0.121	27.12	27.12	27.12	27.12	27. IZ	27.12
feet o	bars	Tons	0.30I	0.276	0.263	0.241	0.224	0.205	0.206	0.144	161.0	0.180	0.177	0.162	0.163	0.165	0.114	0.163	901.0	O. IOI	O.IOI	0.103	0.103	0.087	0.082	0.077
Material per 100 linear feet of track	Angle bars	No. prs.	6.780	6.215	6.780	6.215	6.780	6.215	6.780	6.215	6.780	6.215	6.780	6.215	6.780	6.780		6.780	6.780	6.780	6.780	6.780	6.780	6.780	6.780	6.780
per 10c	Spk.	Kgs.			0.64				0.64			0.65				0.64	0.64			0.64				0.64	0.64	0.64
terial	Ties	No.	0.09	9.09	0.09	9.09	0.09	9.09	0.09	9.09	0.09	9.09	0.09	9.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09
Ma	Rail	Tons	3.274	3.274	2.976	2.976	2.678	2.678	2.530	2.530	2.381	2.381	2.232	2.232	2.143	2.083	I.994	I.964	I.933	1.830	I.786	I.734	I.667	I.607	I.548	1.488
	ts tr	Kgs.	2I.I	19.3	14.5	13.2	14.0	12.8	14.0	12.8	14.0	12.8	9.6	8.7	9.6	9.6	6.4	6.4	6.4	6.4	5.8	5.8	5.8	5.8	5.8	5.8
74	Track bolts	No.	2148	8961	2148	8961	2148	8961	2148	896I	2148	8961	2148	896I	2148	2148	1432	1432	1432	1432	1432	1432	1432	1432	1432	1432
Material per mile of track	bars	Tons	15.90	14.57	13.90	12.74	11.83	10.83	10.88	9.93	10.08	9.24	9.35	8.57	8.63	8.73	6.04	5.43	5.69	5.18	5.18	5.43	5.43	4.62	4.35	4.08
r mile	Angle bars	No. prs.	358	328	358	328	358	328	328	328	358	328	328	328	358	358	358	358	358	358	358	358	358	358	358	358
rial pe	Spk.	Kgs.	33.8	34.I	33.8	34.I	33.8	34.I	33.8	34.I	33.8	34.I	33.8	34.I	33.8	33.8	38.8	38.8	33.8	33.8	33.8	33.8	33.8	33.8	33.8	33.8
Mate	Ties	No.	3168	3200	3168	3200	3168	3200	3168	3200	3168	3200	3168	3200	3168	3168				3168	3168	3168		3168	3168	3168
	Rail /	Tons	172.86	172.86	157.14	157.14	141.43	141.43	133.57	133.57	125.71	125.71	117.86	117.86	113.14	110.00	105.29	0.295 103.71	102.14	96.64	94.29		88.00	84.86	81.71	78.57
Wt.	rail	Tons	0.491	0.540	0.446	0.49I	0.402	0.442	0.379 I33.57	0.417 133.57	0.357 125.71	0.393 125.71	0.335 117.86	0.368	0.321 113.14	0.312 110.00	0.299	0.295	0.290	0.275	0.268	0.260	0.250	0.241	0.232	0.223
Lgth.	rail	Ft.	30	33	30	33	30	33	30	33	30	33	30	33	30	30	30	30	30	30	8	30	30	30	30	30
One		Lin. ft.	30.5	30.5	33.6	33.6	37.3	37.3	39.5	39.5	42.0	42.0	44.8	44.8	41.7	48.0	50.2	50.9	51.7	54.6	56.0	57.7	0.09	62.2	64.6	67.2
Wt.	yd.	Lbs.	OII	IIO	100	100	96	96	85	85	80	8	75	75	72	20	29	99	65	611/2	9	581/4	26	54	52	20

Note. — Data for angle bars and track bolts computed on basis of using 10 per cent of 24', 26' and 28' rails with 30' rails and 10 per cent of 24', 26', 28' and 30' rails with 33' rails. The data computed on basis of using 18 ties per 30' rail and 20 ties per 33' rail. Spike 375 to keg of 200 pounds. One ton = 2240 pounds.

TABLE LXI
Conversion of linear feet of 100 ft. wide right-of-way into acres
From Roberts' "Track Formulæ and Tables."

	Acres	Lin. R. of		Acres	Lin. ft. R. of W.	Acres	Lin. R. of		Acı		in. ft. of W.
ſ	1.0	435 - 871 -		II.0 I2.0	4791.6 5227.2	2I.0 22.0	914 958		31. 32.		13503.6
ı	3.0	1306.		13.0	5662.8	23.0	1001		33	.0 1	14374.8
ı	4.0 5.0	1742. 2178.		14.0	6098.4 6534.0	24.0	1045		34 ·		14810.4 15246.0
ı	6.0	2613.		16.0	6969.6	26.0	1132	5.6	36.	.0	15681.6
ı	7.0 8.0	3049 3484		17.0	7405.2 7840.8	27.0 28.0	1176	6.8	37 38		16117.2 16552.8
ı	9.0	3920. 4356.		19.0	8276.4 8712.0	30.0	1263		39		16988.4 17424.0
ŀ	10.0	1		1	1				1		
ı	Acres	Lin. ft.	Acres	Lin. ft	. Acres	Lin. ft.	Acres	Lin.	ft.	Acres	Lin. ft.
ı	0.01	2.2	0.21	89.3	0.41	176.4	0.61	263	.5	0.81	350.7
ł	0.02	6.5	0.22	93.7		180.8	0.62	267	.9	0.82	355.0
ı		10.9		98.0		185.1		272	.3		359 - 4
ı	0.03	15.2	0.23	102.4	0.43	189.5	0.63	276	.6	0.83	363.7
ı	0.04	19.6	0.24	106.7	0.44	193.8	0.64	281	.0	0.84	368.I
ı	0.05	24.0	0.25	111.1	0.45	198.2	0.65	285	.3	0.85	372.4
ı	0.06	28.3	0.26	1	0.46	202.6	0.66	289		0.86	376.8
ı	0.07		0.27	115.4	0.47		0.67			0.87	
ı	0.08	32.7	0.28	119.8	0.48	206.9	0.68	294		0.88	381.2
ı	0.09	37.0	0.29	124.1	0.49	211.3	0.69	298	-4	0.89	385.5
ı	0.10	41.4	0.30	128.5	0.50	215.6	0.70	302	-7	0.90	389.9
ı	0.11	45.7	0.31	132.9		220.0	0.71	307	I.	0.91	394.2
ı		50.I		137.2	:	224.3		311	.5	Ť	398.6
	0.12	54.5	0.32	141.6		228.7	0.72	315	.8	0.92	402.9
	0.13	58.8	0.33	145.9	0.53	233.0	0.73	320	.2	0.93	407.3
	0.14	63.2	0.34	150.3	0.54	237.4	0.74	324	.5	0.94	411.6
	0.15	67.5	0.35	154.6	0.55	241.8	0.75	328	1	0.95	416.0
	0.16		0.36		0.56	246.1	0.76			0.96	420.4
	0.17	71.9	0.37	159.0	0.57		0.77	333		0.97	
	0.18	76.2	0.38	163.4	0.58	250.5	0.78	337		0.98	424.7
	0.19	80.6	0.39	167.7	0.59	254.8	0.79	341	.9	0.99	429.1
	0.20	84.9	0.40	172.1		259.2	0.80	346	.3	1.00	433-4
	3.20	89.3	0.40	176.4		263.5		350	.7		437.8

TABLE LXII. - Drainage Areas

Sq. ft. opening = $C\sqrt[4]{(\text{drainage area, in acres})^3}$ From Roberts' "Track Formulæ and Tables."

Acres	Steep slopes $C = I$	Moderately steep slopes $C = \frac{2}{3}$	Rolling land $C = \frac{1}{3}$	Flat farm lands $C = \frac{1}{5}$
drained		Sq. ft. open	ing required	- 70
10	5.6	2.7	1.9	I.I
20	9.5	6.3	3.2	1.9
30	12.8	8.5	4.3	2.6
• 40	15.9	10.6	5.3	3.2
50	18.8	12.5	6.3	3.8
60	21.5	14.3	7.2	4.3
70	24.2	16.1	8.1	4.8
80	26.7	17.8	8.9	5.3
90	29.2	19.5	9.7	5.8
100	31.6	21.1	10.5	6.3
150	42.9	28.6	14.3	8.6
160	44.9	29.9	15.0	9.0
200	53.2	35.5	17.7	10.6
240	60.9	40.6	20.3	12.2
300	72.1	48.1	24.0	14.4
320	75.9	50.6	25.3	15.2
400	89.4	59.6	29.8	17.9
480	102.5	68.3	34.2	20.5
500	105.7	70.5	35.2	21.1
560	115.1	76.7	38.4	23.0
600	121.2	80.8	40.4	24.2
640	127.2	84.8	42.4	25.4
800	150.4	100.3	50.1	30.1
1000	177.8	118.5	59.3	35.6
2000	299.0	199.3	99.7	59.8
2500	353.5	235.7	117.8	70.7
3600	464.8	309.9	154.9	93.0
5000	594.6	396.4	198.2	118.9
6000	681.7	454.5	227.2	136.3
7000	765.3	510.2	255.1	153.1
8000	845.9	563.9	282.0	169.2
9000	924.4	616.3	308.1	184.9
10 000	1000.0	666.7	333.3	200.0

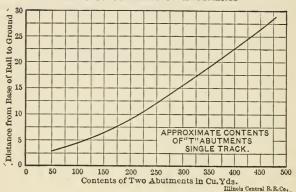
I. C. R.R. Co., 1906.

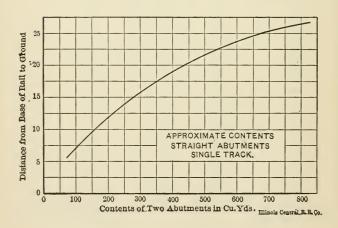
Extended, 1909, by S. S. R.

TABLE LXIII

From Roberts' "Track Formulæ and Tables."

CURVES OF CONTENTS OF ABUTMENTS





\$55.00 per M. Ft. B.M.

0.05 per pound.

TABLE LXIV. — Cost Curves Timber Trestles From Roberts' "Track Formulæ and Tables."

Unit Prices.

Material in Place.

Stringers	55.00 pci m. i t. b.m.
Other material	43.00 per M. Ft. B.M.
Piles	0.37 per linear foot.
Untreated Material:	
Caps	\$42.00 per M. Ft. B.M.
Stringers	42.00 per M. Ft. B.M.
Other Material	30.00 per M. Ft. B.M.
Piles	0.24 per M. Ft. B.M.

To the cost of the trestle obtained from the following curves by multiplying the cost per foot by the length, add for single track:

\$25.00 for two bulkheads in all cases.

Creosoted Material:

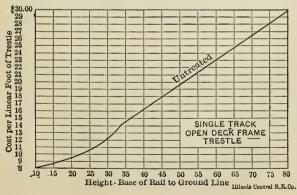
0.70 per linear foot for ties and ballast for ballast floors only.
For double track add:

\$50.00 for two bulkheads in all cases.

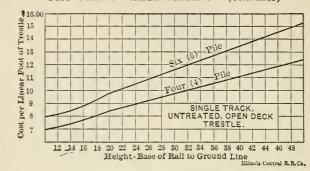
1.40 per linear foot for ties and ballast for ballast floors only.

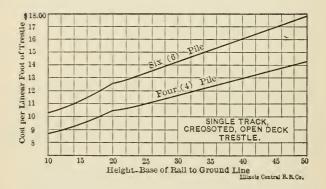
Creosoted open deck trestles have piles, caps and braces creosoted. Ballast floor trestles have all material creosoted.

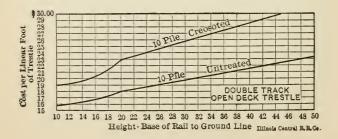
The cost per linear foot given by the following curves does *not* include longitudinal bracing. This should be figured separately for each trestle as the conditions at the opening may require.

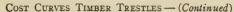


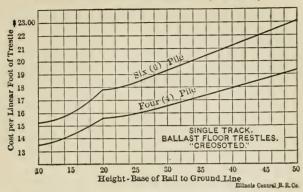
COST CURVES TIMBER TRESTLES - (Continued)











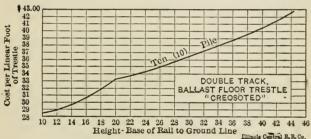


TABLE LXV. — Preliminary Culvert Estimates and Bridge
Weights

Diam-		Iron pipe		Concrete arch							
eter, inches	Area, sq. ft.			Dimen- sions, feet	Area, sq. ft.	Cu. yds. per ft. length	Cu. yds., two ends				
12 16 18 20 24 30 36 42 48	0.79 1.40 1.77 2.18 3.14 4.91 7.07 9.62 12.57	72.5 107.8 127.7 165.7 200.6 290.2 391.6 512.2 665.2	4.0 5.0 5.7 6.5 7.8 10.8 13.2 17.8 22.3	2× 2 3× 4 4× 6 6× 6 8× 8 10×10 12×12 15×15 20×18	3.5 10.9 22.0 30.4 54.4 85.4 123.3 193.2 306.2	0.57 1.06 1.63 3.10 3.99 5.57 6.89 8.81 12.08	8.0* 26.1* 60.9* 42.5† 76.2† 109.0† 168.4† 278.5† 499.0†				

[·] Square end walls.

[†] Thirty-degree wing walls.

BRIDGE WEIGHTS*

W = weight of steel in pounds. l = span in feet for truss bridges and length overall for girder bridges.

Plate Girders:

Plate	e Girders:					
	Deck plate girder	W	= 1	2 12 +	- 150 l	
	Through plate girder, iron floor system	W	= 1	12 12 -	- 500 l	
	Through plate girder, large ties on shelf					
	or flange angles	W	= 9) 1 l2 +	- 150 l	
	Through plate girder, solid iron floor	W	= 1	12 12 +	- 800 <i>l</i>	
Rive	eted Lattice Bridges:					
	Deck bridge, cross-ties on top chord	W	=	7 12 +	- 200 l	
	Through bridge, iron floor system	W	=	7 12 -	- 300 l	
Pin	Connected Bridges:					
	Deck span, cross-ties on top chord	W	=	5 l2 +	- 250 l	
	Deck span, iron floor system	W	=	5 l2 -	- 475 l	

Through span, iron floor system..... $W = 7 l^2 + 650 l$ TABLE LXVI. — Preliminary Ballast Estimates

Ties $6'' \times 8'' \times 8'$.

18 ties to a 33-ft. rail.

Tabular quantities are in cubic yards per mile.

Depth under tie	Gravel 3" a		Broken stone level with top of ties I ft. outside slopes I½-I			
in inches	Single	Double track	Single	Double track		
	track	14' C. to C.	track	14' C. to C.		
6	1400	4159	1965	4418		
8	1737	4952	2396	5306		
10	2095	5767	2845	6210		
12	2476	6603	3309	7131		

^{*} From "Modern Framed Structures" by Johnson, Bryan and Turneaure.

CHAPTER VI

TURNOUTS AND CROSSOVERS

Let F = frog angle.

S =switch angle.

f =toe length of frog from theoretic point.

T = heel spread of switch.

t = point thickness of switch rail.

t' = point thickness of actual frog point.

N = number of frog.

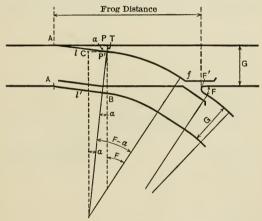


Fig. 26.

l = length of switch rail.

R = radius of turnout curve.

G = gage of track.

$$N = \frac{1}{2}\cot\frac{1}{2}F, \quad \sin S = \frac{T-t}{I}.$$

Frog distance = $I + [G - (T + f \sin F)] \cot \frac{1}{2} (F + S) + f \cos F + t'N$

$$R + \frac{1}{2}G = \frac{G - (T + f\sin F)}{2\sin\frac{1}{2}(F - S)\sin\frac{1}{2}(F + S)}.$$

Values for F, R, frog distance, S, and other quantities for varying values of N and l are given in Tables XLVII and XLVIII, and for spring rail frogs in Table XLIX.

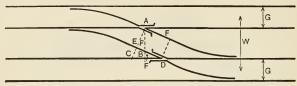


FIG. 27.

$$BD = (W - G) \cot F - \frac{G}{\sin F},$$

$$ED = \frac{W - G}{\sin F} - G \cot F.$$

Total length = $BD + 2 \times frog$ distance to theoretic point.

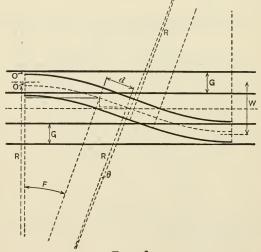


FIG. 28.

$$O = T - (R + \frac{1}{2}G) \text{ vers } S,$$

$$\text{Vers } (F + \theta) = \frac{\frac{W}{2} - d \sin F - O}{R}$$

$$\theta = (F + \theta) - F,$$

$$p = l - (R + \frac{1}{2}G)\sin S,$$

$$L = \text{length of crossover} = 2 \left\{ R\sin (F + \theta) + d\cos F \mp p \right\}.$$

Distance between frogs = $L - 2 \times$ frog distance.

Length of connecting rail = $2R \frac{\theta}{57.3}$.

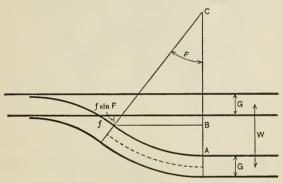


FIG. 29.

$$R = \frac{W - G - f' \sin F}{\text{vers } F} + \frac{1}{2}G.$$

Curve length is $R \frac{F}{57.3}$.

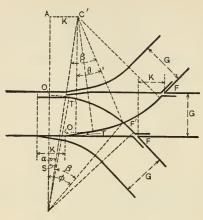


FIG. 30

K and the elements for both turnouts with equal frog angles F are known. To find F'' and the crotch frog distance.

$$O = T - (R + \frac{1}{2}G) \text{ vers } S,$$

$$AC = 2(R + O),$$

$$\frac{K}{AC} = \tan \alpha, \qquad CC' = \frac{K}{\sin \alpha} \quad \text{or} \quad \frac{AC}{\cos \alpha},$$

$$\frac{AC}{2(R + \frac{1}{2}G)} = \cos \beta, \qquad F'' = 2\beta,$$

$$\phi = \alpha + \beta,$$

$$\theta = \beta - \alpha.$$

Crotch frog distance from first point is

$$L = (R + \frac{1}{2}G) (\sin \phi - \sin S) + l + \frac{N''}{32}.$$

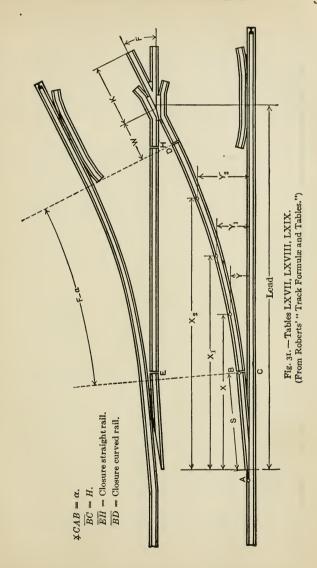


TABLE LXVII. — PROPERTIES OF FROGS AND SWITCHES AND THEORETICAL SWITCH LEADS In all cases gage is considered 4 ft. 8½ in.

		Closure curved rail	VIX	Feet	23.29 28.55 33.38 41.24 46.42 49.92 52.58 55.17 68.96 92.46 92.46 92.46 113.76
	Ø	Closure straight rail	XIII	Feet	22.88 28.19 33.11 41.02 46.72 49.74 55.01 64.05 68.83 92.36 94.95 113.66
	Theoretical leads	Distance point is in interpretation to theoretical goal to thought of the control	XII	Feet	37.05 42.77 48.11 61.94 67.47 72.24 77.51 92.05 97.25 133.02 133.02 146.38 160.38
	Ţ	D = degree besd to v evrue	XI	Degrees	52.899 31.673 31.673 15.789 11.744 9.308 8.192 7.255 6.097 5.044 2.2857 2.214 1.756 1.756
		R = radius of center line	×	Feet	112.26 183.22 273.95 364.88 488.71 616.27 699.97 790.25 940.25 1136.34 1744.38 2587.66 3262.98
	Properties of switches for all switches Thickness of point $=0.4$ " and heel distance $=H=61$ ".	dotiwe = a	IX	Degrees	2.605 2.605 2.605 1.736 1.736 1.736 1.736 1.736 1.302 1.302 0.868 0.868 0.868
-0.0	Properties of so for all swite Thickness of =0¼" and distance=H=	fignel = 2 fortiwe to list	VIII	Ft. In.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		ts bserq2 leed	VII	Feet	1.38 1.16 1.16 1.09 1.05 1.05 1.05 1.05 1.05 1.05 0.99
ı	474	Spread at 50t	IA	Feet	0.79 0.63 0.63 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65
ı	ogs points o!	Total length	Λ	Ft. In.	8 11 11 12 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
l	Properties of frogs mess of all frog poi	K = length theoretical point to heel	IV	Ft. In.	5 5 6 7 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
	Properties of frogs Thickness of all frog points 0).5"	W = length theoretical point to toe	III	Ft. ln.	8 8 4 4 4 6 6 6 6 6 7 8 8 9 H
	Th	F = frog	II	Degrees	14.250 11.421 9.527 8.171 7.153 6.360 6.026 5.725 5.725 5.725 5.725 5.725 3.888 3.580 3.882 2.387
-		gorì = V. rədmun	I	202)	4

TABLE LXVIII. — PRACTICAL SWITCH LEADS In all cases gage is considered 4 ft. 8½ in.

1-28 1-26 2-33 1-33 I-16.60 I-30 I-33 I-27 XXVIII Closure for curved I-14.II 1-16.59 1-26 1-27. 3-27 1-33 1-25.9 2-27 -33 1-28 1-33 2-24 2-33 3-26 Closure for straight rail -32.85 -23.601-27.68 1-32.73 I-13.89 1-16.40 -16.41 1-25.82 1-23.88 1-29.90 1-25.9392 1-26. -27 Lead = distance act-ual point of switch rail to actual point of frog 67.98 100.80 133.28 146.51 137.57 75.71 77.93 94.31 Feet point of frog 75.32 77.51 93.85 100.30 42.26 47.73 5I.8I 67.65 16.17 8 Feet rail to theoretical 36. .26. ual point of switch = distance act-99.0 8.0 0.0 0.0 0.0 0.0 8 gori to sot of frog Feet 8 9 T = tangent adla-T_s = tangent and cent to switch rail 8 0.0 8.0 0.0 8.0 0.44 Practical leads 2.82 2.62 2.91 2.87 2.91 2.87 2.93 Rectangular coördinates to the quarter and center points on gage side of curved rail, referred to point of switch rail as 1.97 eet 0.97 I.02 I.02 90'1 90.1 I.88 I.o. I.04 1.04 1.08 I.OI Peet 56.37 57.81 72.19 100.41 105.35 59 47.II (IO, IO Peet 77 46 36.93 S 56.47 65 77.95 81.76 39.9140.98 2Iġ. 28.75 55.49 58.73 61.84 67.82 6.07 30.28 10.74 13.99 Feet 30.3I Degrees 8.246 15.875 6.213 5.216 3.284 21.718 7.255 lead curve $D_1 = \text{degree of}$ 487.48 605.18 695.45 790.25 922.65 265.39 362.08 1098.73 2546.31 3257.26 4886.16 1993.24 110.69 Feet center line $K_1 = \text{radius of}$ 93/2 number 20 786 112 115 118 120 24 gori = N

Thickness of switch rail at point and bluntness of point of frog not considered. TABLE LXIX. — TABLE OF SWITCH LEADS FOR SPRING FROGS

Frog	ber,	9	7	∞	6	975	IO	12	15
leads	Rails required	2-30	2-27 2-10	2-30 2-15	2-27 2-26	2-30 2-24	2-33 2-27	2-30 2-27 2-15	2-33 4-27
Practical leads	Degree of curve	24.150°	16.750°	12.600°	9.533°	8.583°	7.500°	5.083°	3.033°
	Length in feet	47.00	26.00	67.00	73.00	77.50	80.50	97.00	114.50
Theoretical leads	Degree of curve,	24.583°	16.283° 16.750° 17.133°	12.100° 12.533°	9.467°	8.333° 8.450°	7.383°	4.867°	2.950° 3.033°
Theore	Length in feet,	46.89	52.61 56.02 60.55	66.68	72.48	75.31 77.84	78.07 80.70	91.81 94.67	109.91
5	G G	4' 8\\\\\4' 8\\\\\\\\\\\\\\\\\\\\\\\\\\\	4' 8½" 4' 8½" 4' 8½"	4' 8½"	4' 81/2"	4' 8½"	4' 81/2" 4' 81/2"	4' 8½" 4' 8½"	4' 8!5"
Switch	angle,	2.388° 1.990°	2.388° I.990° I.592°	1.990° 1.592°	1.592°	1.592° 1.448°	1.592° 1.448°	I.448° I.326°	1.326° 1.194°
Heel dis-	tance,	2,"5	ณ์ ณ์	າ້ ດ້	2,,	2, 2,	`.'s	מ"מ"	2,,,
Length	switch rail, S	10, 0,,	10' 0'' 12' 0'' 15' 0''	12' 0"	15, 0,,	15, 0,,	15' o'' . 16' 6''	,,o ,81 18, o,,	18' 0"
Dis- tance	point to heel, K	8, 0,,	% %	8,0,1	8, 0,,	% o'%	8, 0,,	% o''	8, 0,,
Dis- tance		7, 0,,	7, 0,1	1,0,1	1, 0,,	7, 0,,	1,0,1	7, 0,,	1,0,1
Frog	angle, F	9.533°	8.167°	7.150°	6.367°	6.033°	5.733°	4.767°	3.817°
Frog	ber,	9	7	∞	6	\$46	Q.	12	15

From Roberts' "Track Formulæ and Tables."

CHAPTER VII

AZIMUTH, LATITUDE, AND TIME

Meridian Determinations. I. By an Observation on Polaris at Elongation. — Find the time of elongation from Table LXXI. Just before the time of elongation set the transit over a point and with the alidade clamped turn the telescope on the star, clamp the limb and follow the star with the slow motion till it seems to stop traveling east or west as the case may be. Plunge the telescope and range out a stake in line. If the observer is quick he may transit the telescope and take a second observation with the telescope reversed before the star moves in azimuth appreciably. Compute the azimuth of the star at elongation from the formula

$$Sin Z = \frac{\sin \text{ pole distance}}{\cos \text{ latitude}}.$$

The pole distance is found in Table LXX. The latitude may be taken to the nearest minute from a good map or determined as in the next article. Next morning set again over the transit point and from the established line set off Z and range out the meridian.

2. By an Observation on Polaris at Any Time. — This is not so good as the preceding method but is often more convenient and sufficiently precise for practically all field purposes.

Set the transit over a point and at any instant set the intersection of the wires on the star by clamps and slow motions. Range out a line in the azimuth plane of the star. Compute the azimuth of this line from the equation

$$\operatorname{Sin} \frac{1}{2} Z = \pm \sqrt{\frac{\sin(s-a)\sin(s-l)}{\sin a \sin l}},$$

in which $s = \frac{1}{2}(d + a + l)$, d being the pole distance, a the co-altitude, and l the co-latitude.

Since there are two equal azimuth angles — one east, the other west — for any given altitude, and four positions of the star that will give the same Z angle — two east and two west of the meridian — the observer must know from the observed motion of the star in which quadrant of its apparent revolution the star is, or he may know from the

times of observation and culmination, the latter taken from Table LXXI.

3. By Equal Altitudes of a Star. — In the southern hemisphere or elsewhere when not convenient to use Polaris, use equal altitudes of any star that may be observed on both sides of the meridian at reasonable altitudes of between 20° and 40°.

Select a star; set up the instrument over a fixed point; clamp one horizontal motion, and with the other and the vertical motion of the telescope bring the intersection of the wires approximately on the star; clamp both motions; set the vertical circle to read a whole minute or 0.01° such that the star is approaching the horizontal wire: follow with the azimuth motion so that when the star is on the horizontal wire it shall be also on the vertical wire, i.e., at the intersection of the wires. Plunge the telescope and range out a stake some distance ahead. Repeat once or twice at intervals of from ten to twenty minutes and range out other points, numbering the points 1, 2, 3, etc. Set the vertical circle to read the last measured altitude and wait till the star again reaches it when an exact setting is made and a stake ranged out; set at the next altitude and repeat the operation until as many stakes are set on one side of the meridian as on the other, numbering them 3, 2, 1. The extra stakes are for checks on the work. In the morning bisect the angles 1-instrument-1, 2-instrument-2, etc., and set points which should coincide but may not. If they do not coincide set a point to average them unless there is enough variation to indicate an error. To average them select the most east or west of the middle points as an origin and measure the distance to each of the other middle points, add and divide by the number of middle points. The result is the distance of the average point from the origin. Use this and the instrument point to define the meridian. The times should be at least from one and one-half to two hours either side of the meridian. reaching culmination early in the night should be chosen. Approximate north and south will be known by the needle or the daytime position of the sun.

4. By a Transit Observation on the Sun. — Measure the altitude of the sun and its azimuth from any fixed line at the same instant; substitute the altitude, the latitude of the place determined from a good map to the nearest minute or by one of the methods of the next article, and the declination of the sun (explained later) in the formula.

$$\sin \frac{1}{2}Z = \pm \sqrt{\frac{\sin (s' - \phi) \sin (s' - h)}{\cos \phi \cos h}},$$

in which Z is the azimuth of the sun measured from the meridian, ϕ is the latitude, h is the altitude, and $s' = \frac{1}{2} (90 - \delta + \phi + h)$, δ being the declination taken with its proper sign, + when north and - when south. The difference between Z and the observed azimuth from the fixed line gives the azimuth of that line from which the meridian may be run out.

To make the observation, set the transit over a point at least one and one-half hours before or after noon and as long after sunrise or before sunset, and use any fixed distant point for zero azimuth. Use a piece of colored or smoked glass in the eyepiece cap or before the object glass, and bring the cross wires tangent to the sun's disc, approximately by hand motion of the alidade and telescope and clamps and precisely by both slow motions together; read the vertical circle and the azimuth. Subtract the refraction correction of Table LXX for the measured altitude from the vertical circle reading.

If the horizontal wire has been made tangent to the lower limb (edge) of the sun, add the sun's semi-diameter, 16^m or 0.26667°, to the corrected vertical circle reading; if the upper limb has been observed subtract the semi-diameter. The result is the correct altitude of the sun at the instant of observation. The sun's semi-diameter is not exactly 16^m but varies during the year and may be had from the Nautical Almanac mentioned later if greater precision is desired.

The measured azimuth from the reference line is increased or diminished according as the edge nearest or farthest from the reference line is observed, by $16' \times \sec h$ or $0.27^{\circ} \sec h$. If the observer is satisfied to quarter the sun's image with the cross wires no semi-diameter correction is required either for altitude or azimuth.

Explanation of Astronomical Terms. — Celestial bodies are located on the celestial sphere by coördinates corresponding to latitude and longitude of the terrestrial sphere. The celestial equator is a circle cut from the celestial sphere by the terrestrial equatorial plane extended, and angular distances north or south of the celestial equator are called declinations, corresponding to terrestrial latitude. An arbitrary meridian of the celestial sphere is chosen as the reference for what is called right ascension, corresponding to longitude. Right ascension is not used in the methods of this chapter.

The declination of the sun changes constantly. The Nautical Almanac or American Ephemeris, published by the Government annually, gives the hourly change. Several instrument makers distribute gratis in pocket form reprints of that part of the Nautical Almanac relating to the sun and useful to surveyors. Every surveyor should have one of these reprints.

To determine the declination at a given place and hour on a given day the approximate Greenwich time of the observation must be known. In North America if standard time is carried by the observer, he will know what meridian time he carries and hence how many hours slow he is of Greenwich time; Eastern time is 5 hours, Central time 6 hours, Mountain time 7 hours, and Pacific time 8 hours slow of Greenwich time. The Almanac gives the coördinates of the sun for Greenwich apparent and mean noon, and some reprints give the coördinates for one and some for the other.

Noon. — The sun does not appear to move at a uniform rate around the earth. Apparent noon is the instant the sun appears to cross the meridian. Mean noon is the instant that an imaginary sun, moving at a uniform rate and making the same number of revolutions in a year as the real sun, appears to cross the meridian. Mean time is time according to the mean sun and is what is carried by clocks and watches. The difference between apparent and mean time is called the equation of time and is found in the Nautical Almanac and reprints. It is sometimes to be added and sometimes subtracted to convert one time into the other. The sign to be used is given with the equation.

Assuming standard time at any place where central time is used, 9 o'clock in the morning, being 3 hours before noon, would be (6-3) hours = 3 hours after noon at Greenwich, and the declination of the table for a given day must be corrected for 3 hours change. In the table — means south and + north. If the change is marked — the sun is going south, and north or + declination is decreasing, while south or — declination is increasing.

If local mean time is carried by the observer he must know his approximate longitude and must convert this into time, 15° to the hour, to find the difference between Greenwich and local time. In either case if his reprint gives the position of the sun for apparent noon, he must apply the equation of time to his mean time to find the local or standard apparent time.

The positions of heavenly bodies are figured from the center of the earth. With a body as near as the sun this gives rise to a correction to altitudes measured at the surface known as the correction for parallax. It is but a few seconds and is neglected in this discussion. The methods of this chapter are such as are suited to field instruments reading to minutes or 0.01 of a degree and many refinements necessary in astronomical work are omitted.

Latitude. I. By Polaris. — The altitude of the north pole equals the latitude of the place of observation. Measure the altitude of Polaris

at upper or lower culmination, subtract the refraction correction found in Table LXX. Add or subtract the pole distance of the star as found in Table LXX, according as lower or upper culmination is observed. The result is the latitude.

TABLE LXX. — POLAR DISTANCE OF POLARIS

For January 1 of years named

1915	1918	1921	1924	1927	1930	1933	1936	1939	1942
1.149°	1.133°	1.118°	1.102°	1.087°	1.071°	1.056°	1.041°	1.026°	1.011°

Sin of azimuth at elongation = $\frac{\sin \text{ polar distance}}{\cos \text{in latitude}}$.

Latitude = altitude of Polaris at culmination ± polar distance - refraction correction given below.

Latitude altitude		Latitude or altitude	Correction
20° 30° 40°	0.043° 0.027°	50° 60°	0.013° 0.009°

To observe, set up a little before the time of culmination found in Table LXXI; set the horizontal wire on the star and follow with the slow motions till the star's motion seems to be wholly in azimuth and not at all in altitude. Read the vertical angle.

2. By a Noon Observation of the Sun.— Measure the altitude of the sun when at its highest point; subtract the refraction correction of Table LXX for the altitude found; subtract the sun's declination if north or add if south; the result is the co-latitude.

To observe set up the transit a little before noon; set the horizontal wire on the upper or lower limb (edge) of the sun's disc and keep it there as the sun rises and until it has ceased to rise and its motion seems to be wholly in azimuth; read the vertical circle very carefully and subtract or add the sun's semi-diameter according as the upper or lower limb was observed. Colored or smoked glass must be used, preferably in the eyepiece cap rather than before the object glass, but either may answer. The sun's semi-diameter is an average of 16 minutes or

0.26667°. It varies during the year and may be had from the Nautical Almanac or makers' reprint (see previous article) if desired to greater precision.

TABLE LXXI*

Approximate local mean times (counting from noon 24 hours) of the elongations and culminations of polaris in the year 1915 for latitude 40° N.; longitude 6^H W. from Greenwich.

Date	East elongation		West elongation		Upper culmination		Lower culmination	
	h.	m.	h.	m.	h.	m.	h.	m.
Jan. 1	0	52.I	12	42.I	6	47.I	18	45.2
15	23	53.0	11	46.8	5	51.8	17	49.9
Feb. I	22	45.9	10	39.7	4	44.7	16	42.8
15	21	50.6	9	44.2	3	49 · 4	15	47.5
Mar. I	20	55.4	8	49.2	2	54.2	14	52.3
15	20	00.2	7	54.0	I	59.0	13	57.1
Apr. I	18	53.3	6	47.I	0	52.1	12	50.2
15	17	58.1	5	51.9	23	43.I	II	55.0
May I	16	55.3	4	49.1	22	50.3	10	52.2
15	16	00.4	3	54.2	21	55.4	9	57.3
June I	14	53.8	2	47.6	20	48.8	8	50.7
15	13	58.9	I	52.7	19	53.9	7	55.8
July I	12	56.3	0	50.I	18	51.3	6	53.2
15	12	01.5	23	51.5	17	56.5	5	58.4
Aug. I	10	55.0	22	45.0	16	50.0	4	51.9
15	10	00.I	21	50.I	15	55.I	3	57.0
Sept. I	8	53.5	20	43.5	14	48.5	2	50.4
15	7	58.6	19	48.6	13	53.6	I	55.5
Oct. 1	6	55.8	18	45.8	12	50.8	0	52.7
15	6	00.8	17	50.8	II	55.8	23	53.9
Nov. I	4	54.0	16	44.0	10	49.0	22	47.I
15	3	58.9	15	48.9	9	53.9	21	52.0
Dec. 1	2	55.8	14	45.8	8	50.8	20	48.9
15	2	∞.6	13	50.6	7	55.6	19	53.7

^{*} From data furnished by the U.S. Coast and Geodetic Survey.

Approximate Determination of Time. 1. To Find the Error of a Watch. — The observation for azimuth on the sun may be utilized. The instant of the observation should be noted on the watch. Then

$$\sin t = \frac{\sin Z \cos h}{\cos \delta},$$

in which t is the hour angle in degrees before or after apparent local noon. Reduce t to hours by dividing by 15 and find the apparent local time; apply the equation of time for the day from the Nautical Almanac, and the result is mean local time. The longitude of the place must in general be had from a map, if possible to the nearest minute. The difference between local longitude and the standard meridian whose time is carried reduced to time is applied to the determined mean local time to get the mean standard time. The difference between this and the observed time of the observation is the error of the watch. If the watch carries local time, longitude is needed only to compute change in declination and need not be so precisely determined.

To refer to any calendar day other than the first and fifteenth of each month, subtract 3.94^m for every day between it and the preceding tabular day, or add 3.94^m for every day between it and the succeeding tabular day.

To find the times for the tabular dates after 1915, to the tabular value add 1.36^m for each year after 1915 less 3.9^m for each leap year. In any leap year deduction for that year is not made until March 1.

To find the time of western elongation for Jan. 18, 1919:

For January 15, 1915, western elongation, tabular time is 11^h 46.8^m. 1919 - 1915 = 4; $4 \times 1.36 = 5.4$. One leap year has intervened, and, therefore, $5.4 - 3.9 = 1.5^m$ to be added. 11^h 46.8^m + 1.5^m = 11^h 48.3^m for January 15, 1919. For January 18 subtract 38 - 15 = $3 \times 3 \times 3.94^m = 11.8^m$ getting 11^h 36.5^m.

To refer to any other than the tabular latitude between the limits of 25° and 50° north add to the time of west elongation 0.13^m for every degree south of latitude 40°, and subtract from the time of west elongation 0.18^m for every degree north of 40°. Reverse these signs for corrections to the times of east elongation. For latitudes as high as 60° diminish the times of west elongation and increase the times of east elongation by 0.23^m for every degree north of latitude 40°.

To refer to other longitudes, add 0.16^m for each hour east of 6 hours and subtract 0.16^m for each hour west of 6 hours.

TABLE LXXII

Length of o.or° of latitude and o.or° of longitude to the nearest whole foot

Latitude	Length o.or° latitude	Length o.or° longitude	Latitude	Length o.or° latitude	Length o.or° longitude
° 1 2 3 4 5 6	3628	3652	31	3637	3133
	3628	3650	32	3638	3100
	3628	3647	33	3638	3066
	3628	3643	34	3639	3031
	3628	3638	35	3640	2995
	3628	3632	36	3641	2958
7 8 9 10 11 12	3628 3628 3628 3629 3629 3629	3625 3617 3608 3597 3586 3573 3559	37 38 39 40 41 42 43	3641 3641 3642 3643 3643 3644 3645	2920 2882 2842 2802 2761 2719 2675
14 15 16 17 18	3630 3630 3631 3631 3631 3631 3632	3545 3529 3512 3494 3475 3455 3433	44 45 46 47 48 49 50	3646 3646 3647 3647 3648 3649	2632 2587 2542 2495 2449 2401 2353
21	3632	3411	51	3650	2303
22	3633	3388	52	3650	2254
23	3633	3364	53	3651	2203
24	3634	3338	54	3652	2152
25	3634	3312	55	3652	2099
26	3635	3285	56	3653	2047
27	3635	3256	57	3653	1994
28	3635	3227	58	3654	1940
29	3636	3197	59	3655	1886
30	3637	3166	60	3655	1831

TABLE LXXIII. — Convergence of Meridians

Latitude	Angular convergence per mile, degrees	Distance for convergence of o.oi°, feet	Latitude	Angular convergence per mile, degrees	Distance for convergence of o.o1°, feet
0			0		
1	0.000	209,240	31	0.009	6084
2	.001	104,588	32	.009	5851
3	.001	69,690	33	.009	5629
4	.001	52,231	34	.010	5420
5	.001	41,747	35	.010	5222
5 6	.002	34,750	36	.010	5032
7	.002	29,747	37	110.	4852
8	.002	26,002	38	.011	4681
9	.002	23,062	39	.012	4516
10	.003	20,715	40	.012	4359
11	.003	18,792	41	.013	4339
12	.003	17,185	42	.013	4062
13	.003	15,823	43	,013	3922
14.	.003	14,651	44	.014	3788
15	.004	13,634	45	.014	3658
16	.004	12,740	46	.015	3533
17	,004	11,950	47	.015	3412
18	.005	11,244	48	.016	3295
19	.005	10,611	49	.017	3181
20	.005	10,039	50	.017	3071
21	.006	9,518	51	.018	2964
22	.006	9,044	52	.018	2860
23	.006	8,609	53	,019	2758
24	.006	8,208	54	.020	2660
25	,007	7,837	55	.021	2563
26	.007	7,493	56	.021	2469
27	.007	7,173	57	.022	2377
28	,008	6,874	58	.023	2288
29	.008	6,594	59	.024	2200
30	.008	6,331	60	.025	2114

CHAPTER VIII

TABLES FOR METRIC CURVES

METRIC curves are used in Latin-American countries. The "degree" is the angle subtended by a chord of 20 meters. Practically all usually tabulated curve functions may be converted from feet values in tables for curves used in the United States to meter values for metric curves by dividing by five.

The more commonly used functions have been tabulated in the three following tables. The tabular values are in meters.

TABLE LXXIV. — RADII, TANGENT OFFSETS AND MIDDLE ORDINATES FOR METRIC CURVES

Degree = angle subtended by chord of 20 meters

Deg.,	Radius	Logarithm.	Tan.	Mid.	Deg.	Radius.	Logarithm,	Tan.	Mid.
D	R	$\log R$	off., t	ord., m	D	R	$\log R$	off., t	ord., m
0.0	- 00		.000	.000	10.0	114.74	2.05970	1.743	.437
.2	5729.57	3.75812	.035	.009	.2	112.49	2.05113	1.778	. 445
.4	2864.80	3.45709	.070	.017	.4	110.34	2.04272	1.813	-454
.6	1909.87	3.28100	. 105	.026	.6	108.26	2.03447	1.847	. 463
.8	1432.41	3.15607	.140	.035	.8	106.26	2.02637	1.882	.472
I.0	1145.93	3.05916	.175	.044	II.O	104.33	2.01843	1.917	. 480
.2	954.95	2.97998	. 209	.052	.2	102.48	2.01063	1.952	. 489
.4	818.53	2.91304	.244	.061	.4	100.68	2.00296	1.986	. 498
.6 .8	716.22 636.65	2.85505	.279	.070	.6 .8	98.95 97.28	1.99544	2.021	.507
		2.80390			12.0				.515
2.0	572.99	2.75814	-349	. 087		95.67	1.98077	2.091	.524
.2	520.90	2.71676	.384	.096	.2	94.11	1.97361	2.125	-533
.4 .6	477 · 50 440 · 77	2.67897	.419	.105	.4 .6	92.59 91.13	1.96658	2.160	.542
.8		2.61204	.489	.122	.8	89.71	1.95285	2.229	
3.0	409.30 382.02	2.01204	.524	.131	13.0	88.34	1.95265	2.229	· 559 · 568
,2	358.15	2.55406	.558	.140	.2	87.00	1.93954	2.299	.577
.4	337.08	2.52774	-593	.148	.4	85.71	1.93304	2.333	.585
.6	318.36	2.50292	.628	.157	.6	84.46	1.92663	2.368	.594
.8	301.61	2.47945	.663	. 166	.8	83.24	1.92032	2.403	.603
4.0	286.54	2.45718	.698	.175	14.0	82.06	1.91411	2.437	.612
.2	272.90	2.43600	-733	. 183	.2	80.91	1.90798	2.472	.620
-4	260.50	2.41581	. 768	.192	.4	79.79	1.90193	2.507	.629
.6	249.18	2.39651	.803	.201	.6	78.70	1.89598	2.541	. 638
.8	238.80	2.37804	.838	. 209	. 8	77.64	1.89010	2.576	.647
5.0	229.26	2.36032	.872	.218	15.0	76.61	1.88430	2.611	.655
.2	220.44	2.34330	.907	.227	.2	75.61	1.87858	2.645	.664
.4	212.29	2.32692	.942	.236	.4 .6	74.63	1.87294	2.680	.673
.6 .8	204.71 197.66	2.31114 2.29591	.977	.244	.8	73.68 72.76	1.86737	2.714	.682 .690
6.0		2.28120	1.047	.262	16.0	71.85			
	191.07		1.047				1.85644	2.783	.699
.2 .4	184.92 179.14	2.26697	1.082	.271	.2	70.97 70.11	1.85109	2.853	.708
.6	173.72	2.23985	1.151	.288	.6	69.27	1.84056	2.887	.726
.8	168.62	2,22690	1.186	.297	.8	68.45	1.83540	2.922	.734
7.0	163.80	2.21432	1.221	.306	17.0	67.65	1.83030	2.956	.743
.2	159.26	2.20211	1.256	.314	.2	66.87	1.82526	2.991	.752
.4	154.96	2.19022	1.291	.323	.4	66.11	1.82027	3.025	.761
.6	150.89	2.17866	1.325	.332	.6	65.37	1.81535	3.060	. 769
.8	147.03	2.16739	1.360	.340	.8	64.64	1.81048	3.094	.778
8.0	143.36	2.15642	1.395	.349	18.0	63.92	1.80567	3.129	. 787
.2	139.87	2.14571	1.430	.358	.2	63.23	1.80091	3.163	. 796
.4	136.54	2.13526	1.465	.367	.4	62.55	1.79620	3.198	.805
.6	133.37	2.12506	1.500	-375	.6	61.88	1.79155	3.232	.813
.8	130.35	2.11510	1.534	.384	.8	61.23	1.78694	3.267	.822
9.0	127.45	2.10536 2.09583	1.569	.393	19.0	60.59 59.96	1.78239	3.301	.831 .840
							į	1	
.4	122.04	2.08651	1.639	.410	.4	59.35 58.75	1.77343	3.370	.849 .857
.8	119.51	2.07739	1.708	.419	.8	58.16	1.76465	3.439	.866
10.0	114.74	2.05970	I.743	.437	20.0	57.59	1.76033	3.473	.875
	2-4.74	. 2.0,,970	1.143	1437	,	31.73	1 2 1 7 2 - 1 1 1	3.470	

TABLE LXXV. - METRIC CURVES

Degree	Actual arc,		Long chords									
of curve	one station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of curve			
0.2	20.000 m.	40.00	60.00	80.00	100.00	120.00	139.99	159.99	0.2			
.4	.000	0.00	0.00	0.00	0.00	119.99	9.98	9.98	.4			
.6 .8	.000	0.00	0.00	79.99	99.99	9.98	9.97	9.95	.6 .8			
.o I.0	20.000	40.00	59.99	9.99 79.99	9.98	9.97	9.95	9.92	I.0			
.2	.000	0.00	9.99	9.98	9.96	9.92	9.88	9.82	.2			
-4	.000	0.00	9.99	9.97	9.94	9.90	9.83	9.75	.4			
.6 .8	.001	0.00	9.98	9.96	9.92	9.86	9.78	9.67	.6			
2.0	20.001	39.99	9.98	9.95	9.90	9.83	9.72	9.59	2.0			
.2	.001	9.99	9.97	9.93	9.85	9.74	9.59	9.38	.2			
-4	.001	9.99	9.97	9.93	9.82	9.74	9.51	9.36	.4			
.6	.002	9.99	9.96	9.90	9.80	9.64	9.42	9.14	.6			
.8	.002	9.99	9.95	9.88	9.76	9.58	9.33	9.00	.8			
3.0	20.002	39.99 9.98	59.94 9.94	79.86 9.84	99.73	119.52 9.45	139.23	158.85	3.0			
.4	.003	9.98	9.94	9.82	9.65	9.45	9.13	8.53	.4			
.6	.003	9.98	9.93	9.80	9.60	9.39	8.90	8.35	.6			
.8	.004	9.98	9.91	9.78	9.56	9.23	8.77	8.16	.8			
4.0	20.004	39.98	59.90	79.76	99.51	119.15	138.64	157.96	4.0			
.2	.004	9.97	9.89	9.73	9.46	9.06	8.50	7.75	.2			
.4 .6	.005	9.97 9.97	9.88	9.71	9.41	8.97	8.36	7.54	.4			
.8	.006	9.97	9.86	9.65	9.30	8.78	8.04	7.07	.8			
5.0	20.006	39.96	59.85	79.62	99.24	118.67	137.88	156.82	5.0			
.2	.007	9.96	9.84	9.59	9.18	8.56	7.71	6.56	.2			
.4	.007	9.96	9.82	9.56	9.12	8.45	7.52	6.29	-4			
.6 .8	.008	9.95	9.81	9.52	9.05	8.34	7.34	6.02	.6			
6.0	20.009	39.94	59.78	79.45	98.91	118.09	136.95	155.43	6.0			
.2	.010	9.94	9.77	9.41	8.83	7.96	6.74	5.12	.2			
-4	.010	9.94	9.75	9.38	8.76	7.83	6.53	4.81	-4			
.6	.011	9.93	9.74	9.34	8.68	7.69	6.31	4.48	.6			
.8	.012	9.93	9.72	9.30	8.60	7.55	6.09	4.15	.8			
7.0	20.012 .013	39.92 9.92	59.70	79.26	98.51	7.25	135.86	153.80	7.0			
.4	.014	9.92	9.67	9.17	8.34	7.10	5.37	3.08	.4			
.6	.015	9.91	9.65	9.12	8.25	6.94	5.12	2.71	.6			
.8	.015	9.91	9.63	9.08	8.16	6.78	4.87	2.32	.8			
8.0	20.016	39.90	59.61	79.03	98.06	116.62	134.60	151.94	8.0			
.2	.017	9.90	9.59	8.98	7.96	6.45	4.33	I.53 I.12	.2			
.6	.019	9.89	9.55	8.88	7.76	6.09	3.77	0.70	.6			
.8	.020	9.88	9.53	8.83	7.66	5.91	3.49	0.27	.8			
9.0	20.021	39.88	59.51	78.77	97.55	115.73	133.19	149.83	9.0			
.2	.022	9.87	9.49	8.72	7.44	5.54	2.89	9.38	.2			
.4 .6	.022	9.87	9.46	8.60	7.33 7.21	5.34	2.58	8.93 8.46	.6			
.8	.024	9.85	9.44	8.55	7.10	4.94	1.95	7.99	.8			
10.0	20.025	39.85	59.39	78.48	96.98	114.74	131.62	147.50	10.0			
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree			

TABLE LXXV. — (Continued)

Degree	Actual arc,			Lo	ng chor	de			Degree
of curve	one station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of
10.0	20.025 m.	39.85		78.48	96.98		131.62		curve 10.0
	.026	9.84	59.39	8.42	6.86	114.74		147.50	
.2	.020	9.84	9.37 9.34	8.36	6.74	4.53 4.31	0.95	7.01 6.51	.2
.6	.029	9.83	9.32	8.30	6.61	4.10	0.61	6.00	.6
.8	.030	9.82	9.29	8.23	6.48	3.87	0.25	5.48	.8
11.0	20.031	39.82	59.27	78.17	96.35	113.65	129.90	144.95	11.0
.2	.032	9.81	9.24	8.10	6.22	3.42	9.54	4.42	.2
.4	.033	9.80	9.21	8.03	6.08	3.19	9.17	3.87	.4
.6 .8	.034	9.80	9.18	7.97	5.95 5.81	2.95 2.71	8.80 8.42	3.32 2.76	.6 .8
12.0	20.037	39.78	59.13	77.82	95.67	112.47	128.03	142.19	12.0
.2	.038	9.77	9.10	7.75	5.52	2.21	7.64	1.61	.2
.4	.039	9.77	9.10	7.68	5.38	1.96	7.24	1.01	.4
.6	.040	9.76	9.04	7.60	5.23	1.71	6.84	0.43	.6
.8	.042	9.75	9.01	7.53	5.08	1.45	6.43	139.83	.8
13.0	20.043	39.74	58.98	77 - 45	94.93	111.18	126.01	139.22	13.0
.2	.044	9.73	8.94	7.37	4.77	0.92	5.59	8.60	.2
.4 .6	.046	9.73	8.91	7.29	4.61	0.65	5.17	7.98	-4
.0 .8	.047 .048	9.72 9.71	8.88	7.21	4.45 4.29	0.37	4.73	7.34 6.70	.6 .8
14.0	20.050	39.70	58.81	77.05	94.13	109.81	123.86	136.05	14.0
.2	.051	9.69	8.78	6.96	3.96	9.53	3.41	5.40	.2
.4	.053	9.68	8.74	6.88	3.80	9.33	2.95	4.73	.4
.6	.054	9.68	8.71	6.79	3.63	8.95	2.50	4.06	.6
.8	.056	9.67	8.67	6.70	3.45	8.65	2.03	3.38	.8
15.0	20.057	39.66	58.64	76.61	93.28	108.35	121.56	132.70	15.0
.2	.059	9.65	8.60	6.52	3.10	8.04	1.09	2.00	.2
.4 .6	. 060 . 062	9.64	8.56	6.43	2.92	7.74	0.61	1.30	.4
.8	.002	9.63	8.53	6.34	2.74	7.43	0.12	0.60	.6 .8
16.0	20.065	39.61	58.45	76.15	92.37	106.79	119.14	129.16	16.0
.2	.067	9.60	8.41	6.06	2.18	6.48	8.64	8.44	.2
.4	.068	9.59	8.37	5.96	1.99	6.15	8.13	7.70	.4
.6	.070	9.58	8.33	5.86	1.80	5.82	7.62	6.96	.6
.8	.072	9.57	8.29	5.76	1.61	5.49	7.11	6.21	.8
17.0	20.074	39.56	58.25	75.66	91.41	105.16	116.59	125.46	17.0
.2	.075	9.55	8.21	5.56	I.22	4.82	6.06	4.70	.2
.4 .6	.077 .079	9.54 9.53	8.17	5.46	0.81	4.47	5.53	3.93 3.16	.4 .6
.8	.081	9.52	8.08	5.25	0.61	3.78	4.46	2.38	.8
18.0	20.082	39.51	58.04	75.15	90.40	103.43	113.91	121.59	18.0
.2	.084	9.50	8.00	5.04	0.19	3.08	3.36	0.80	.2
.4	.086	9.48	7.95	4.93	89.98	2.72	2.81	0.00	.4
.6	.088	9.47	7.91	4.83	9.77	2.36	2.26	119.20	.6
.8	.090	9.46	7.87	4.71	9.56	1.99	1.69	8.39	.8
19.0	20.092 .094	39·45 9·44	57.82 7.78	74.60	89.34 9.12	1.26	0.56	6.76	19.0
.4	.094	9.44	7.73	4.49	8.90	0.88	109.98	5.93	
.6	.090	9.43	7.68	4.30	8.68	0.51	9.40	5.10	.4
.8	.100	9.40	7.64	4.15	8.46	0.13	8.82	4.27	.8
20.0	20.102	39.39	57.59	74.03	88.23	99.74	108.23	113.43	20.0
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE LXXVI. — METRIC CURVES

Degree			1	Middle or	dinates				Degree
of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of curve
0.2	.009	.035	.079	.140	.218	.314	.428	.558	0.2
.4	.009	.070	.157	.279	.436	.628	.855	1.117	-4
.6	.026	.105	. 236	.419	.654	.942	1.283	1.675	.6
.8	.035	.140	.314	.558	.873	1.256	1.710	2.233	.8
1.0	.044	.175	-393	.698	1.091	1.570	2.137	2.791	1.0
.2	.052	. 209	.471	.838	1.309	1.884	2.565	3.349	.2
-4	.061	.244	.550	.977	1.527	2.198	2.992	3.907	-4
.6 .8	.070	. 279	.624	1.117	1.745	2.512	3.418	4.464 5.020	.6 .8
2.0	.087		.785	1.396	2.180				2.0
		-349				3.139	4.697	5.576	
.2	.096	.384	.864	1.535	2.398	3.452	5.122	6.132	.2
.6	.113	. 454	1.021	1.814	2.833	4.078	5.548	7.241	.6
.8	.122	. 489	1.099	1.953	3.051	4.391	5.973	7.795	.8
3.0	.131	.524	1.178	2.093	3.268	4.703	6.397	8.348	3.0
.2	.140	.558	1.256	2.232	3.485	5.015	6.821	8.900	.2
-4	.148	-593	1.335	2.371	3.703	5.327	7.244	9.451	-4
.6 .8	.157	.628	1.413	2.510	3.920	5.639	7.667	10.002	.6
	. 166	.663	1.491	2.650	4.136	5.950	8.090	10.551	.8
4.0	.175	.698	1.570	2.789	4.353	6.262	8.511	11.100	4.0
.2	.183	.733 .768	1.648	2.928 3.067	4.570 4.786	6.572	8.933	11.647	.2
.4 .6	.192	.803	1.726	3.205	5.002	7.193	9·353 9·773	12.194	.4
.8	,200	.838	1.883	3.344	5.218	7.502	10.192	13.283	.8
5.0	.218	.872	1.961	3.483	5.434	7.812	10.192	13.826	5.0
.2	.227	.907	2.040	3.622	5.650	8.121	11.028	14.367	.2
.4	.236	.942	2.118	3.760	5.865	8.429	11.445	14.907	.4
.6	.244	-977	2.196	3.899	6.081	8.737	11.862	15.446	.6
.8	.253	1.012	2.274	4.037	6.296	9.045	12.277	15.983	.8
6.0	.262	1.047	2.352	4.175	6.511	9.352	12.691	16.519	6.0
.2	.271	1.082	2.431	4.314	6.725	9.658	13.104	17.053	.2
.4 .6	.279	1.116 1.151	2.509 2.587	4.452	6.940 7.154	9.965	13.517	17.586	.4 .6
.8	.297	1.186	2.665	4.728	7.368	10.575	14.339	18.646	.8
7.0	.306	1.221	2.743	4.866	7.581	10.880	14.749	19.174	7.0
.2	.314	1.256	2.821	5.003	7.795	11.184	15.157	19.700	.2
-4	.323	1.291	2.899	5.141	8.008	11.487	15.565	20.223	-4
.6	.332	1.325	2.977	5.279	8.221	11.790	15.971	20.745	.6
.8	340	1.360	3.055	5.416	8.433	12.092	16.376	21.265	.8
8.0	-349	1.395	3.133	5.553	8.645	12.394	16.780	21.783	8.0
.2	.358	1.430	3.211	5.691 5.828	8.857	12.695	17.183	22.299	.2
·4 .6	-375	1.465	3.288 3.366	5.828	9.069	12.995 13.294	17.584	22.813	.4 .6
.8	.384	1.534	3.444	6.101	9.491	13.594	18.384	23.834	.8
9.0	.393	1.569	3.522	6.238	9.491	13.892	18.782	24.342	9.0
.2	. 402	1.604	3.599	6.375	9.912	14.189	19.178	24.847	.2
-4	.410	1.639	3.677	6.511	10.122	14.486	19.573	25.350	.4
.6	.419	1.674	3.754	6.647	10.332	14.782	19.967	25.850	.6
.8	.428	1.708	3.832	6.784	10.541	15.078	20.359	26.348	.8
10.0	-437	1.743	3.910	6.919	10.750	15.372	20.750	26.843	10.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE LXXVI. — (Continued)

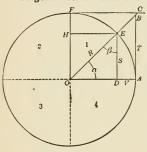
				Middle or	rdinates				D
Degree of curve	- C4-	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
10.0	ı Sta.			6.919	10.750	15.372	20.750	26.843	10.0
	-437	1.743	3.910			15.666			
.2	. 445 . 454	1.778	3.987 4.065	7.055	10.958 11.167	15.959	21.139 21.527	27.336	.2 .4
.6	.454	1.847	4.142	7.327	11.374	16.251	21.913	28.315	.6
.8	.472	1.882	4.219	7.462	11.582	16.542	22.298	28,800	.8
11.0	.480	1.917	4.297	7.597	11.789	16.832	22.681	29.282	11.0
.2	.489	1.952	4.374	7.732	11.995	17.122	23.063	29.762	.2
.4	.498	1.986	4.451	7.867	12.201	17.410	23.443	30.239	-4
.6	.507	2.021	4.539	8.002	12.407	17.698	23.821	30.714	.6
.8	.515	2.056	4.605	8.137	12.612	17.985	24.198	31.185	.8
12.0	.524	2.091	4.682	8.271	12.817	18.271	24.573	31.654	12.0
.2	.533	2.125	4.759	8.405	13.021	18.556	24.946	32.119	.2
-4	.542	2.160	4.836	8.539	13.225	18.840	25.317	32.582	.4 .6
.6	.550	2.195	4.913	8.673	13.429	19.123	25.687	33.041	
.8	.559	2.229	4.990	8.807	13.632	19.405 19.686	26.055	33.498 33.951	.8
13.0	.568 -577	2.264 2.299	5.067 5.144	8.940 9.074	13.834	19.000	26.42I 26.785	34.402	13.0
.4	.585	2.333	5.220	9.207	14.238	20.245	27.147	34.849	.4
.6	.594	2.368	5.297	9.339	14.439	20.523	27.507	35.292	.6
.8	.603	2.403	5.374	9.472	14.639	20.800	27.866	35 - 733	.8
14.0	.612	2.437	5.450	9.605	14.839	21.076	28.222	36.171	14.0
.2	.620	2.472	5.527	9.737	15.039	21.351	28.576	36.604	.2
.4	.629	2.507	5.603	9.870	15.238	21.625	28.929	37.035	-4
.6	.638	2.541	5.679	10.001	15.437	21.897	29.279	37.462	.6
.8	.647	2.576	5.756	10.133	15.634	22.169	29.628	37.886	.8
15.0	.655	2.611	5.832	10.264	15.832	22.439	29.974	38.306	15.0
.2	.664	2.645	5.908	10.395	16.028	22.709	30.318	38.723	.2
.4	.673	2.680	5.984	10.526	16.225	22.977	30.660	39.137	.4 .6
.6 .8	.682 .690	2.704 2.749	6.060	10.657	16.421 16.616	23.244	31.000 31.338	39.546 39.952	.8
16.0	.699	2.783	6.212	10.918	16.810	23.774	31.673	40.355	16.0
		2.818	6.288	11.048	17.005	24.037	32.007	40.753	.2
.2	.708 .717	2.853	6.364	11.178	17.198	24.299	32.338	41.148	.4
.6	.726	2.887	6.439	11.308	17.390	24.560	32.667	41.540	.6
.8	.734	2,922	6.515	11.437	17.583	24.820	32.993	41.927	.8
17.0	.743	2.956	6.591	11.566	17.774	25.078	33.317	42.311	17.0
.2	.752	2.991	6.666	11.696	17.966	25.335	33.639	42.691	.2
.4	.761	3.025	6.741	11.824	18.156	25.591	33.959	43.067	-4
.6 .8	.769	3.060	6.817	11.953	18.346	25.846 26.099	34.276	43.439 43.807	.6 .8
	.778	3.094	6.892		18.534		34.591		
18.0	787	3.129	6.967	12.208	18.723	26.351	34.903	44.171	18.0
.2	.796 .805	3.163	7.043 7.117	12.336	18.911	26.60I 26.850	35.213 35.52I	44.531 44.887	.2
.6	.813	3.198	7.117	12.404	19.098	27.098	35.826	45.239	.6
.8	.822	3.266	7.267	12.717	19.470	27.345	36.129	45.587	.8
19.0	.831	3.301	7.342	12.844	19.656	27.590	36.429	45.931	19.0
.2	.840	3.335	7.417	12.971	19.840	27.833	36.727	46.271	.2
.4	.849	3.370	7.492	13.097	20.024	28.076	37.022	46.606	.4
.6	.857	3.404	7.566	13.222	20.207	28.316	37.314	46.938	.6
.8	.866	3.439	7.641	13.348	20.389	28.556	37.604	47.265	.8
20.0	.875	3.473	7.715	13.473	20.571	28.794	37.892	47.588	20.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

CHAPTER IX

MISCELLANEOUS TABLES

TABLE LXXVII. - TRIGONOMETRIC FORMULAS, CIRCULAR MEASURE, ETC.

Trigonometric Functions and Formulas. Solution of Triangles



- I. $ED = R \sin \alpha$.
- 2. $OD = R \cos \alpha$.
- 3. $DA = R \operatorname{versin} \alpha$.
- 4. $HF = R \operatorname{coversin} \alpha$.

By definition, if R = 1,

 $ED = \sin \alpha$.

 $OD = cosine \alpha$. $DA = \text{versed sine } \alpha$.

 $HF = \text{coversed sine } \alpha.$

 $BA = \text{tangent } \alpha$.

 $FC = \text{cotangent } \alpha.$ $OB = \text{secant } \alpha.$

 $OC = \operatorname{cosecant} \alpha$. If R is other than I, it follows

from the above definitions and the proportionality of similar figures,

5. $BA = R \tan \alpha$.

6. $FC = R \cot \alpha$.

7. $OB = R \sec \alpha$.

8. $QC = R \csc \alpha$

from which also in any right triangle of angles α and β , if o be the side opposite the angle α , a the side adjacent thereto, and h the hypotenuse,

that

9.
$$\sin \alpha = \frac{o}{h} = \cos \beta$$
.

13.
$$\sec \alpha = \frac{h}{a} = \csc \beta$$
.

10.
$$\cos \alpha = \frac{a}{h} = \sin \beta$$
.

14.
$$\csc \alpha = \frac{h}{o} = \sec \beta$$
.

II.
$$\tan \alpha = \frac{o}{a} = \cot \beta$$
.

15.
$$\operatorname{vers} \alpha = \frac{h-a}{h} = \operatorname{covers} \beta.$$

12.
$$\cot \alpha = \frac{a}{o} = \tan \beta$$
.

16. covers
$$\alpha = \frac{h-o}{h} = \text{vers } \beta$$
.

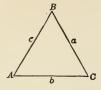
Hence,

17.
$$\begin{cases} o = h \sin \alpha = h \cos \beta. \\ h = \frac{o}{\sin \alpha} = \frac{o}{\cos \beta}. \end{cases}$$

18.
$$\begin{cases} a = h \cos \alpha = h \sin \beta. \\ h = \frac{a}{\cos \alpha} = \frac{a}{\sin \beta}. \end{cases}$$

19.
$$\begin{cases} o = a \tan \alpha = a \cot \beta. \\ a = \frac{o}{\tan \alpha} = \frac{o}{\cot \beta}. \end{cases}$$
22.
$$\begin{cases} h = o \csc \alpha = o \sec \beta. \\ o = \frac{h}{\csc \alpha} = \frac{h}{\sec \beta}. \end{cases}$$
20.
$$\begin{cases} a = o \cot \alpha = o \tan \beta. \\ o = \frac{a}{\cot \alpha} = \frac{a}{\tan \beta}. \end{cases}$$
23.
$$o = \sqrt{h^2 - a^2} = \sqrt{(h+a)(h-a)}.$$
24.
$$a = \sqrt{h^2 - o^2} = \sqrt{(h+o)(h-o)}.$$
25.
$$h = \sqrt{o^2 + a^2}.$$

21.
$$\begin{cases} h = a \sec \alpha = a \csc \beta. & 25. \ h = \sqrt{o^2 + a} \\ a = \frac{h}{\sec \alpha} = \frac{h}{\csc \beta}. & 26. \ \text{Area} = \frac{oa}{2}. \end{cases}$$



Oblique triangles may be solved by some one of the following formulas:

Given	Sought	Formulas
27. A, B, a,	C, b, c,	$C = 180^{\circ} - (A+B), b = \frac{a}{\sin A} \sin B,$
28. A, a, b,	B, C, c,	$c = \frac{a}{\sin A} \sin (A + B).$ $\sin B = \frac{\sin A}{a} b, C = 180^{\circ} - (A + B),$
29. \mathring{C} , a , b , 30. C , a , b ,	$\frac{1}{2}(A + B),$ $\frac{1}{2}(A - B),$	$c = \frac{a}{\sin A} \sin C.$ $\frac{1}{2} (A + B) = 90^{\circ} - \frac{1}{2} C.$ $\tan \frac{1}{2} (A - B) = \frac{a - b}{a + b} \tan \frac{1}{2} (A + B).$
31. C, a, b,	A, B,	$\begin{cases} A = \frac{1}{2}(A+B) + \frac{1}{2}(A-B); \\ B = \frac{1}{2}(A+B) - \frac{1}{2}(A-B). \end{cases}$
32. C, a, b,	с,	$c = (a+b)\frac{\cos\frac{1}{2}(A+B)}{\cos\frac{1}{2}(A-B)}$ $\sin\frac{1}{2}(A+B)$
33. <i>C</i> , <i>a</i> , <i>b</i> , 34. <i>a</i> , <i>b</i> , <i>c</i> ,	Area, A ,	$= (a - b) \frac{\sin \frac{1}{2} (A + B)}{\sin \frac{1}{2} (A - B)}.$ Area = $\frac{1}{2} ab \sin C$. If $s = \frac{1}{2} (a + b + c)$,
		$\sin \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{bc}},$
		$\cos \frac{1}{2}A = \sqrt{\frac{s(s-a)}{bc}},$ $\sqrt{(s-b)(s-c)}$
		$\tan \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}},$ $\sin A = \frac{2\sqrt{(s-a)(s-b)(s-c)}}{bc},$
		$\operatorname{vers} A = \frac{2(s-b)(s-c)}{bc}.$
35. a, b, c, 36. A, B, C, a,	Area,	Area = $\sqrt{s(s-a)(s-b)(s-c)}$. Area = $\frac{a^2 \sin B \sin C}{2 \sin A}$.
		2 sin A

From the definitions of the trigonometric functions, the geometrical properties of right triangles and in some cases algebraic transformations, it may be shown that if A is any angle and B any other angle,

37.
$$\sin^2 A + \cos^2 A = 1$$
.

38.
$$\sin A = \frac{I}{\csc A} = \sqrt{I - \cos^2 A} = \tan A \cos A$$

= $2 \sin \frac{1}{2} A \cos \frac{1}{2} A = \text{vers } A \cot \frac{1}{2} A$
= $\sqrt{\frac{1}{2} \text{vers } 2 A} = \sqrt{\frac{1}{2} (I - \cos 2 A)}$.

39.
$$\cos A = \frac{I}{\sec A} = \sqrt{I - \sin^2 A} = \cot A \sin A$$

 $= I - \text{vers } A = 2\cos^2 \frac{1}{2}A - I = I - 2\sin^2 \frac{1}{2}A$
 $= \cos^2 \frac{1}{2}A - \sin^2 \frac{1}{2}A = \sqrt{\frac{1}{2} + \frac{1}{2}\cos 2A}.$

40.
$$\tan A = \frac{\sin A}{\cos A} = \frac{I}{\cot A} = \sqrt{\sec^2 A - I}$$

$$= \sqrt{\frac{I}{\cos^2 A} - I} = \frac{\sqrt{I - \cos^2 A}}{\cos A} = \frac{\sin 2A}{I + \cos 2A}$$

$$= \frac{I - \cos 2A}{\sin 2A} = \frac{\text{vers } 2A}{\sin 2A} = \cot \frac{1}{2}A \text{ (sec } A - I).$$

41. cot
$$A = \frac{\cos A}{\sin A} = \frac{1}{\tan A} = \sqrt{\csc^2 A - 1}$$

= $\frac{\sin 2A}{1 - \cos 2A} = \frac{\sin 2A}{\text{vers } 2A} = \frac{1 + \cos 2A}{\sin 2A} = \frac{\tan \frac{1}{2}A}{\sec A - 1}$

42. vers
$$A = I - \cos A = \sin A \tan \frac{1}{2} A = 2 \sin^2 \frac{1}{2} A = \cos A (\sec A - I)$$
.

43.
$$\sin (A \pm B) = \sin A \cos B \pm \sin B \cos A$$
.

44.
$$\cos (A \pm B) = \cos A \cos B \mp \sin A \sin B$$
.

45.
$$\sin \frac{1}{2}A = \sqrt{\frac{1 - \cos A}{2}} = \sqrt{\frac{\text{vers } A}{2}}$$
.

46.
$$\sin 2A = 2 \sin A \cos A$$
.

47.
$$\cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$
.

48.
$$\cos 2A = 2\cos^2 A - I = \cos^2 A - \sin^2 A = I - 2\sin^2 A$$
.

49.
$$\tan \frac{1}{2}A = \frac{\tan A}{1 + \sec A} = \csc A - \cot A = \frac{1 - \cos A}{\sin A} = \sqrt{\frac{1 - \cos A}{1 + \cos A}}$$

50.
$$\tan 2A = \frac{2 \tan A}{1 - \tan^2 A}$$
.

51.
$$\cot \frac{1}{2}A = \frac{\sin A}{\text{vers }A} = \frac{1 + \cos A}{\sin A} = \frac{1}{\csc A - \cot A}$$

52.
$$\cot 2A = \frac{\cot^2 A - 1}{2 \cot A}$$

53.
$$\operatorname{vers} \frac{1}{2} A = \frac{\frac{1}{2} \operatorname{vers} A}{1 + \sqrt{1 - \frac{1}{2} \operatorname{vers} A}} = \frac{1 - \cos A}{2 + \sqrt{2 (1 + \cos A)}}$$

54. $vers 2A = 2 sin^2 A$

55. $\sin A + \sin B = 2 \sin \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$.

56. $\sin A - \sin B = 2 \cos \frac{1}{2} (A + B) \sin \frac{1}{2} (A - B)$.

57. $\cos A + \cos B = 2 \cos \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$.

58. $\cos B - \cos A = 2 \sin \frac{1}{2} (A + B) \sin \frac{1}{2} (A - B)$.

59. $\sin^2 A - \sin^2 B = \cos^2 B - \cos^2 A = \sin (A + B) \sin (A - B)$.

60. $\cos^2 A - \sin^2 B = \cos (A + B) \cos (A - B)$.

61. $\tan A + \tan B = \frac{\sin (A+B)}{\cos A \cos B}$

62. $\tan A - \tan B = \frac{\sin (A - B)}{\cos A \cos B}$

LENGTH OF CIRCULAR ARCS TO RADIUS I

Deg.	Length	Deg.	Length	Deg.	Length	Deg.	Length	Deg.	Length
10 20 30 40	0.1745329 0.3490659 0.5235988 0.6981317	60 . 70	0.8726646 1.0471976 1.2217305 1.3962634	100	1.5707963 1.7453293 1.9198622 2.0943951	140 150	2.2689280 2.4434610 2.6179939 2.7925268	180 190	2.9670597 3.1415927 3.3161256 3.4906585

$$\pi = 3.14159$$

 $\log \pi = 0.497150$

Degrees in arc of length equal to radius, 57.295780. Degrees in arc of length equal to π , 180.

Circumference = $2 \pi r$ =

Area

If l = length of circular arc

d = number of degrees in same

r = radius of same

c =chord of same

m = middle ordinate

$$\begin{cases} d = \frac{l}{r} \cdot \frac{180^{\circ}}{\pi} = \frac{l}{r} 57.3^{\circ} \text{ approx.} \\ r = \frac{l}{d} \cdot \frac{180^{\circ}}{\pi} = \frac{l}{d} 57.3^{\circ} \text{ approx.} \end{cases}$$

$$l = \frac{d}{180} \pi r = \frac{d}{57.3^{\circ}} r \text{ approx.}$$
Area of sector = $\frac{1}{2} lr$.
Area of sector = $\frac{d}{360} \pi r^2$.
Approx. area of segment = $\frac{2}{3} cm$.

$$\frac{1}{\pi} = 0.31831.$$

Volume of sphere = $\frac{4}{3}\pi r^3$.

Square feet in I acre = 43,560.

Cubic feet in I cubic meter = 35.3145.

TABLE LXXVIII. — STADIA FUNCTIONS

Differences of elevation for 100 feet rod reading

Deg.	0	I	2	3	4	5	6 '	7	8	9	Deg.
.00 .05 .1 .15 .2 .25 .3 .35 .4 .45	0.00 0.09 0.17 0.26 0.35 0.42 0.52 0.61 0.70 0.79 0.87	1.74 1.83 1.92 2.01 2.09 2.18 2.27 2.36 2.44 2.53 2.62	3.49 3.57 3.66 3.75 3.84 3.92 4.01 4.10 4.18 4.27 4.36	5.23 5.31 5.40 5.49 5.57 5.66 5.75 5.83 5.92 6.01 6.09	6.96 7.05 7.13 7.22 7.30 7.39 7.48 7.56 7.65 7.73 7.82	8.68 8.77 8.85 8.94 9.03 9.11 9.20 9.28 9.37 9.46	IO.40 IO.48 IO.57 IO.65 IO.74 IO.82 IO.91 IO.99 II.08 II.16 II.25	12.10 12.18 12.26 12.35 12.43 12.52 12.60 12.69 12.77 12.86 12.94	13.78 13.87 13.95 14.03 14.12 14.20 14.28 14.37 14.45 14.54	15.45 15.53 15.62 15.70 15.78 15.87 15.95 16.03 16.11 16.20 16.28	.00 .05 .1 .15 .2 .25 .3 .35 .4 .45
.55 .6 .65 .7 .75 .8 .85 .9	0.96 1.05 1.13 1.22 1.31 1.40 1.48 1.57 1.66 1.74	2.70 2.79 2.88 2.97 3.05 3.14 3.23 3.31 3.40 3.49	4.44 4.53 4.62 4.71 4.79 4.88 4.97 5.05 5.14 5.23	6.18 6.27 6.35 6.44 6.53 6.61 6.70 6.79 6.87 6.96	7.91 7.99 8.08 8.17 8.25 8.34 8.42 8.51 8.60 8.68	9.34 9.63 9.71 9.80 9.88 9.97 10.05 10.14 10.22 10.31	11.33 11.42 11.50 11.59 11.67 11.76 11.84 11.93 12.01	13.03 13.11 13.19 13.28 13.36 13.45 13.53 13.61 13.70	14.70 14.79 14.87 14.95 15.04 15.12 15.20 15.28 15.37 15.45	16.36 16.44 16.52 16.61 16.69 16.77 16.86 16.94 17.02	.55 .6 .65 .7 .75 .8 .85

Corrections to rod readings for horizontal distance

Rod	o°	ı°	2°	3°	4°	5°	6°	7°	8°	9°	Rođ
100 200 300 400 500 600 700 800 900	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.1 0.1 0.2 0.2 0.2 0.2 0.3	0.1 0.2 0.4 0.5 0.6 0.7 0.8 1.0 1.1	0.3 0.5 0.8 1.1 1.4 1.6 1.9 2.2 2.4 2.7	0.5 1.0 1.5 2.0 2.5 2.9 3.4 3.9 4.4 4.9	0.8 1.5 2.3 3.0 3.8 4.6 5.3 6.1 6.8 7.6	1.1 2.2 3.3 4.4 5.5 6.5 7.6 8.7 9.8	1.5 3.0 4.5 6.0 7.5 8.9 10.4 11.9 13.4	1.9 3.9 5.8 7.8 9.7 11.6 13.6 15.5 17.5	2.5 4.9 7.4 9.8 12.3 14.7 17.2 19.6 22.1	100 200 300 400 500 600 700 800 900

TABLE LXXVIII. — (Continued)

Deg.	10	11	12	13	14	15	16	17	18	19	Deg.
.00 .05 .1 .15 .2 .25 .3 .35 .4 .45 .5 .55 .6 .65 .7	17.10 17.18 17.26 17.35 17.43 17.51 17.59 17.67 17.76 17.84 17.92 18.00 18.08 18.16 18.24 18.33 18.41 18.49	18.73 18.81 18.89 18.97 19.05 19.13 19.21 19.30 19.38 19.46 19.54 19.62 19.70 19.78 19.86	20.34 20.42 20.50 20.58 20.66 20.73 20.81 20.89 20.97 21.05 21.13 21.21 21.29 21.37 21.45	21.92 22.08 22.15 22.23 22.31 22.39 22.47 22.54 22.62 22.70 22.78 22.85 22.93 23.01 23.09 23.16	23.47 23.55 23.63 23.70 23.78 23.86 23.93 24.01 24.09 24.16 24.24 24.32 24.39 24.47 24.55 24.62	25.00 25.08 25.15 25.23 25.30 25.38 25.45 25.60 25.68 25.75 25.83 25.90 25.98 26.03 26.20 26.27	26.50 26.57 26.64 26.79 26.79 26.87 26.94 27.01 27.09 27.16 27.23 27.31 27.38 27.45 27.52 27.67 27.67	27.96 28.03 28.10 28.12 28.32 28.32 28.39 28.46 28.54 28.68 28.75 28.89 28.96 29.04	29.39 29.46 29.53 29.60 29.67 29.74 29.81 29.88 29.95 30.09 30.16 30.23 30.30 30.37 30.41 30.51 30.58	30.78 30.85 30.92 30.99 31.06 31.13 31.19 31.26 31.47 31.53 31.40 31.47 31.53 31.60 31.67 31.74 31.87	.00 .05 .1 .15 .2 .25 .3 .35 .4 .45 .5 .55 .6 .65 .7
.9 .95 1.00	18.57 18.65 18.73		21.76 21.84 21.92	23.40	24.85 24.92 25.00	26.35 26.42 26.50	27.81 27.89 27.96	29.25 29.32 29.39	30.65 30.71 30.78	32.01 32.07 32.14	.9 .95 1.00

Corrections to rod readings for horizontal distance

Rod	10°	110	12°	13°	14°	15°	16°	17°	18°	19°	Rod
100 200 300 400 500 600 700 800 900	3.0 6.0 9.1 12.1 15.1 18.1 21.1 24.2 27.2 30.2	3.6 7.3 10.9 14.6 18.2 21.8 25.5 29.1 32.8 36.4	4.3 8.6 13.0 17.3 21.6 25.9 30.2 34.6 38.9 43.2	5.I 10.I 15.2 20.2 25.3 30.4 35.4 40.5 45.5 50.6	5.9 11.7 17.6 23.4 29.3 35.1 41.0 46.8 52.7 58.5	6.7 13.4 20.1 26.8 33.5 40.2 46.9 53.6 60.3 67.0	7.6 15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4 76.0	8.5 17.1 25.6 34.2 42.7 51.3 59.8 68.4 76.9 85.5	9.5 19.1 28.6 38.2 47.7 57.3 66.8 76.4 85.9	10.6 21.2 31.8 42.4 53.0 63.6 74.2 84.8 95.4 106.0	100 200 300 400 500 600 700 800 900

TABLE LXXVIII. — (Continued)

Deg.	20	21	22	23	24	25	26	27	28	29	Deg.
.00	32.14	33.46		35.97	37.16	38.30	39.40	40.45	41.45	42.40	.00
.05	32.21	33.52		36.03	37.22	38.36	39.45	40.50	41.50	42.45	.05
.I	32.27	33.59		36.09	37.27	38.41	39.51	40.55	41.55	42.49	.I
.15	32.34 32.41	33.65 33.72	34.92 34.98	36.15 36.21	37 · 33 37 · 39	38.47 38.53	39.56 39.61	40.60	41.60	42.54	.15
.25	32.47	33.78	35.05	36.27	37.45	38.58	39.67	40.71	41.69	42.63	.25
.3	32.54	33.84		36.33		38.64	39.72	40.76	41.74	42.68	.3
-35	32.61	33.91	35.17	36.39			39.77	40.81	41.79	42.72	-35
-4	32.67	33.97	35.23	36.45	37.62	38.75	39.83	40.86	41.84	42.77	-4
-45	32.74	34.04	35.29	36.51		38.80	39.88	40.91	41.89	42.81	.45
-5	32.80	34.10	35.36	36.57	37.74	38.86	39.93	40.96	41.93	42.86	-5
.55	32.87	34.16	35.42	36.63		38.91	39.98	41.01	41.98	42.90	-55
.6 .65	32.93	34.23	35.48	36.69	37.85	38.97	40.04	41.06	42.03	42.95	.6
.7	33.00	34.29 34.35	35.54 35.60	36.75 36.80	37.91 37.96	39.02 39.08	40.09	41.11	42.08	42.99	.65
.75	33.13	34.42	35.66	36.86	38.02	39.13	40.19	41.21	42.17	43.08	.75
.8	33.20	34.48	35.72	36.92	38.08	39.18	40.19	41.26	42.22	43.13	.8
.85	33.26	34 - 54	35.78	36.98	38.13	39.24	40.30	41.31	42.26	43.17	.85
.9	33.33	34.61	35.85	37.04	38.19	39.29	40.35	41.35	42.31	43.21	.9
.95	33.39	34.67	35.91	37.10	38.25	39 - 35	40.40	41.40	42.36	43.26	.95
1.00	33.46	34.73	35.97	37.16	38.30	39.40	40.45	41.45	42.40	43.30	1.00

Corrections to rod readings for horizontal distance

Rod	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	Rod
100 200 300 400 500 600 700 800 900	11.7 23.4 35.1 46.8 58.5 70.2 81.9 93.6 105.3	12.8 25.7 38.5 51.4 64.2 77.0 89.9 102.7 115.6 128.4	14.0 28.1 42.1 56.1 70.2 84.2 98.2 112.2 126.3	15.3 30.5 45.8 61.1 76.4 91.6 106.9 122.2 137.4	16.5 33.1 49.6 66.2 82.7 99.2 115.8 132.3 148.9 165.4	17.9 35.7 53.6 71.4 89.3 107.2 125.0 142.9 160.7 178.6	19.2 38.4 57.7 76.9 96.1 115.3 134.5 153.8 173.0	20.6 41.2 61.8 82.4 103.1 123.7 144.3 164.9 185.5	22.0 44.1 66.1 88.2 110.2 132.2 154.3 176.3 198.4	23.5 47.0 70.5 94.0 117.5 141.0 164.5 188.0 211.5	100 200 300 400 500 600 700 800 900

TABLE LXXIX. - BAROMETRIC ELEVATIONS

Giving altitudes above arbitrary sea level (barometer reading 30 inches) for various barometer readings B.

To determine difference of elevation of two points having barometer readings B and B_1 , take from the table the altitudes corresponding to B and B_1 , and correct their difference by Table LXXX. The corrected difference is the quantity required.

В	A	Diff. for o.oi	В	A	Diff. for c.oi	В	A	Diff. for 0.01
Inches II.0 II.1 II.2 II.3 II.4 II.5 II.6 II.7 II.8 II.9 I2.0 I2.1 I2.2 I2.3 I2.4 I2.5 I2.6 I2.7 I2.8 I2.9 I3.0 I3.1 I3.2 I3.3 I3.4 I3.5 I3.6 I3.7 I3.8 I3.9	Feet 27,336 27,090 26,846 26,846 26,364 26,364 25,890 25,656 25,424 25,194 24,946 24,740 24,516 24,294 23,637 23,421 23,297 22,785 22,785 22,785 22,152 21,558 21,1557 21,358 21,160 20,962 20,765	Feet -24.6 24.4 24.2 24.0 23.8 23.6 23.4 23.2 23.0 22.8 22.6 22.4 22.2 22.1 21.7 21.6 21.4 21.2 21.0 20.9 20.8 20.6 20.4 20.1 20.0 19.9 19.8 19.8 19.8 19.8 19.8 19.8	Inches 14.0 14.1 14.2 14.3 14.4 14.5 14.6 14.7 14.8 14.9 15.0 15.1 15.2 15.3 15.4 15.5 15.6 16.7 16.8 16.9	Feet 20,765 20,570 20,570 20,377 19,809 19,623 19,437 19,252 19,068 18,705 18,525 18,346 18,705 17,127 16,958 16,789 16,621 16,454 16,288 16,124 15,961 15,798 15,636	Feet -19.5 19.3 19.1 18.9 18.8 18.6 18.6 18.5 18.4 18.2 18.1 17.6 17.8 17.4 17.3 17.2 17.1 16.9 16.8 16.7 16.6 16.4 16.3 16.3 16.3 16.2 16.0	Inches 17.0 17.1 17.2 17.3 17.4 17.5 17.6 17.7 17.8 17.9 18.0 18.1 18.2 18.3 18.4 18.5 18.6 18.7 19.0 19.1 19.2 19.3 19.4 19.5 19.6 19.7 19.8 19.9 20.0	Feet 15.476 15.316 15.157 14.999 14.842 14.686 14.531 14.377 14.223 14.070 13.918 13.767 13.468 13.319 13.172 13.025 12.879 12.130 12.733 12.589 12.445 12.302 12.160 12.018 11.877 11.7598 11.459 11.459 11.459 11.459 11.459 11.459	Feet -16.0 15.9 15.8 15.7 15.6 15.5 15.4 15.3 15.2 15.1 15.0 14.9 14.7 14.6 14.6 14.4 14.3 14.2 14.1 14.0 13.9 13.9 13.8 13.7 -13.7

Taken from Appendix 10, "U.S. Coast and Geodetic Survey Report" for 1881.

TABLE LXXIX. — (Continued)

В	A	Diff.	В	A	Diff. for o.oɪ	В	A	Diff. for 0.01
Inches	Feet	Feet	Inches	Feet	Feet	Inches	Feet	Feet
20.0	11,047	-13.6	23.7	6,423	-11.5	27.4	2,470	-9.9
20. I	10,911	13.5	23.8	6,308	11.4	27.5	2,371	9.9
20.2	10,776	13.4	23.9	6,194	11.4	27.6	2,272	9.9
20.3	10,642	13.4	24.0	6,080	11.3	27.7	2,173	9.8
20.4	10,508	13.3	24. I	5,967	11.3	27.8	2,075	9.8
20.5	10,375	13.3	24.2	5,854	11.3	27.9	1,977	9.7
20.6	10,242	13.2	24.3	5,741	11.2	28.0	1,880	9.7
20.7	10,110	13.1	24.4	5,629	II.I	28.1 28.2	1,783	9.7
20.8	9,979	13.1	24.5	5,518	II.I		1,686	9.7
20.9	9,848	13.0	24.6	5,407	II.I	28.3	1,589	9.6
21.0	9,718	12.9	24.7 24.8	5,296 5,186	II.O	28.4 28.5	1,493	9.6
21.1	9,589	12.9			10.9	_	1,397	9.5
21.2	9,460	12.8	24.9	5,077 4,968	10.9	28.6 28.7	1,302 1,207	9.5
2I.3 2I.4	9,332 9,204	12.8	25.0 25.1	4,859	10.9	28.8	1,112	9.5
	-	12.7			10.8	,	ł	9.4
21.5 21.6	9,077 8,951	12.6	25.2 25.3	4,751 4,643	10.8	28.9 29.0	1,018 924	9.4
21.0	8,825	12.6	25.4	4,535	10.8	29.0 29.1	830	9.4
	8,700	12.5			10.7		736	9.4
21.8 21.9	8,575	12.5	25.5 25.6	4,428 4,321	10.7	29.2 29.3	643	9 3
22.0	8,451	12.4	25.7	4,215	10.6	29.4	550	9.3
22.I	8,327	12.4	25.8	4,109	10.6	29.5	458	9.2
22.1	8,204	12.3	25.0	4,004	10.5	29.5	366	9.2
22.3	8,082	12.2	26.0	3,899	10.5	29.7	274	9.2
22.4	7,960	12.2	26.1	3,794	10.5	29.8	182	9.2
22.4	7,838	12.2	26.2	3,794	10.4	29.0	91	9.1
22.6	7,717	12.1	26.3	3,586	10.4	30.0	00	9.1
22.7	7,597	12.0	26.4	3,483	10.3	30.1	-91	9.1
22.8	7,477	12.0	26.5	3,380	10.3	30.2	181	9.0
22.9	7,358	11.9	26.6	3,277	10.3	30.3	271	9.0
23.0	7,239	11.9	26.7	3,175	10.2	30.4	361	9.0
23.I	7,121	11.8	26.8	3,073	10.2	30.5	451	9.0
23.2	7,004	11.7	26.9	2,972	10.1	30.6	540	8.9
23.3	6,887	11.7	27.0	2,871	10.1	30.7	629	8.9
23.4	6,770	11.7	27.I	2,770	10.1	30.8	717	8.8
23.5	6,654	11.6	27.2	2,670	10.0	30.9	805	8.8 -8.8
23.6	6,538		27.3	2,570		31.0	-893	-0.0
23.7	6,423	-11.5	27.4	2,470	-10.0			
		!	1					

TABLE LXXX. — Correction Coefficient for Temperature AND Hygrometric Conditions

This correction is used when no hygrometric observations have been made. To the difference in altitude found in Table LXXIX for the given barometer readings is added algebraically the product of that difference and the correction below given, according to the formula, diff. alt. = (diff. by Table LXXIX) (r + c).

Sum O. T.1	Corr. coeff.	Sum O. T.	Corr. Coeff.	Sum O. T.	Corr. coeff.
0° 10 20 30 40 50	-0.1024 -0.0915 -0.0806 -0.0698 -0.0592 -0.0486 -0.0380	70° 80 90 100 110 120	-0.0273 -0.0166 -0.0058 +0.0049 +0.0156 +0.0262 +0.0368	140° 150 160 170 180	+0.047I +0.0575 +0.0677 +0.0779 +0.0879

¹ Computed from Tables I and IV, Appendix 10, "U.S. Coast Survey Report" for 1881.

TABLE LXXXI.¹—Volume in cubic feet per second discharging over a thin plate weir one foot in length without end contractions² according to Francis' Formula $Q = 3.33 L \sqrt{H^3}$.

Head,	Cu. ft.	Head,	Cu. ft.	Head,	Cu. ft.	Head,	Cu. ft.	Head,	Cu. ft.
H, in ft.	per sec.	H, in ft.	per sec.	H, in ft.	per sec.	H, in ft.	per sec.	H, in ft.	per sec.
							-		- 0
.01	0.003	.51	1.213	1.01	3.380	1.51	6.179	2.01	9.489
.02	0.009	.52	I.249 I.285	I.02	3.430	1.52	6.240	2.02	9.560
.03	0.017	-53	1.321	I.03 I.04	3.481	I.53 I.54	6.302 6.364	2.03	9.631 9.703
.05	0.027	.54 .55	1.358	1.04	3.532 3.583	1.54	6.426	2.04	9.703
.06	0.049	.56	1.395	1.06	3.634	1.56	6.488	2.06	9.846
.07	0.062	.57	1.433	1.07	3.686	1.57	6.551	2.07	9.917
.08	0.075	.58	1.471	1.08	3.737	1.58	6.613	2.08	9.989
.09	0.090	.59	1.509	1.09	3.790	1.59	6.676	2.09	10.062
. 10	0.105	.60	1.548	1.10	3.842	1.60	6.739	2.10	10.134
.II	0.121	.61	1.586	I.II	3.894	1.61	6.803	2.11	10.206
. 12	0.138	.62	1.626	I.12	3.947	1.62	6.866	2.12	10.279
.13	0.156	.63	1.665	1.13	4.000	1.63	6.930	2.13	10.352
.14	0.174	.64	1.705	1.14	4.053	1.64	6.994	2.14	10.425
.15	0.193	.65	1.745	1.15	4.107	1.65	7.058	2.15	10.498
.16	0.213	.66	1.786	1.16	4.160	1.66	7.122	2.16	10.571
.17	0.233	.67	1.826	1.17	4.214	1.67	7.187	2.17	10.645
.18	0.254	.68	1.867	1.18	4.268	1.68	7.251	2.18	10.718
.19	0.276	.69	1.909	1.19	4.323	1.69	7.316	2.19	10.792
.20	0.298	.70 .71	1.950	I.20 I.21	4.377	I.70 I.71	7.381	2.20 2.2I	10.940
.21	0.344	.72	2.034	I.21	4.432	1.71	7.446	2.21	11.015
.23	0.367	.73	2.077	1.23	4.467	1.72	7.577	2.23	11.089
.24	0.392	-74	2.120	1.24	4.598	1.74	7.643	2.24	11.164
.25	0.416	.75	2.163	1.25	4.654	1.75	7.709	2.25	11.239
.26	0.441	.76	2.206	1.26	4.710	1.76	7.775	2.26	11.314
.27	0.467	.77	2.250	1.27	4.766	1.77	7.842	2.27	11.389
.28	0.493	.78	2.294	1.28	4.822	1.78	7.908	2.28	11.464
.29	0.520	.79	2.338	1.29	4.879	1.79	7.975	2.29	11.540
.30	0.547	.80	2.383	1.30	4.936	1.80	8.042	2.30	11.615
.31	0.575	.81	2.428	1.31	4.993	1.81	8.109	2.31	11.691
.32	0.603	.82	2.473	1.32	5.050	1.82	8.176	2.32	11.767
+33	0.631	.83	2.518	1.33	5.108	1.83	8.244	2.33	11.843
.34	0.660	.84	2.564	1.34	5.165	1.84	8.311	2.34	11.920
·35	0.690	.85	2.610	1.35	5.223	1.85	8.379	2.35	11.996
.36	0.719 0.749	.86 .87	2.656	1.36	5.281	1.86	8.447	2.36	12.073
.37 .38	0.749	.88	2.702 2.749	1.37	5.340	1.87 1.88	8.515 8.584	2.37 2.38	12.150
.39	0.780	.89	2.749	1.38 1.39	5.398	1.89	8.652	2.30	12.304
.40	0.842	.90	2.843	I.40	5.516	1.90	8.721	2.40	12.381
.41	0.874	.91	2.891	1.41	5.575	1.91	8.790	2.41	12.459
.42	0.906	.92	2.939	1.42	5.635	1.92	8.859	2.42	12.536
.43	0.939	.93	2.987	1.43	5.694	1.93	8.929	2.43	12.614
-44	0.972	.94	3.035	1.44	5.754	1.94	8.998	2.44	12.692
.45	1.005	95	3.083	1.45	5.814	1.95	9.068	2.45	12.770
.46	1.039	.96	3.132	1.46	5.875	1.96	9.138	2.46	12.848
.47	1.073	-97	3.181	1.47	5.935	1.97	9.208	2.47	12.927
.48	1.107	.98	3.231	1.48	5.996	1.98	9.278	2.48	13.005
.49	1.142	.99	3.280	1.49	6.057	1.99	9.348	2.49	13.084
.50	1.177	1.00	3.330	1.50	6.118	2.00	9.419	2.50	13.163

¹ From Trautwine's Engineers' Pocketbook.

² The table values are not seriously in error when there are end contractions provided L is at least 10 H. The original formula was limited to heads, H, between ½ foot and 2 feet. The tabular values are probably not seriously in error for the range given. For any weir of length L feet multiply the tabular values by L.

TABLE LXXXII Feet to Meters

	0	I	2	3	4	5	6	7	8	9
Feet	Meters									
0	0.000	0.305	0.610	0.914	1.219	1.524	1.829	2.134	2.438	2.743
10	3.048			3.962	4.267	4.572	4.877	5.182	5.486	
20	6.036	6.401	6.706	7.010	7.315	7.620	7.925	8.229	8.534	8.839
30	9.144	9.449	9.753	10.058	10.363	10.668	10.972	11.277	11.582	11.887
40	12.192	12.496	12.801	13.106	13.411	13.716	14.020	14.325	14.630	14.935
50	15.239	15.544	15.849	16.154	16.459	16.763	17.068	17.373	17.678	17.983
60	18.287	18.592	18.897	19.202	19.507	19.811			20.726	21.031
70	21.335			22.250	22.555	22.859				24.079
80	24.383	24.688	24.993	25.298	25.602	25.907	26.212	26.517	26.822	27.126
90	27.431	27.736	28.041	28.346	28.651	28.955	29.260			
100	30.479	30.784	31.089	31.394	31.698	32.003	32.308	32.613	32.918	33.222

Meters to Feet

Veter	0	I	2	3	4	5	6	7	8	9
Meters	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet
0	0.00	3.28	6.56	9.84	13.12	16.40	19.69	22.97	26.25	29.53
10	32.81	36.09	39.37	42.65	45.93	49.21		55.78	59.06	62.34
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.15
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.96
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.76
50	164.04	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.57
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.38
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63		259.19
80	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.00
90	295.28	298.56	391.84	305.12	308.40	311.69	314.97	318.25	321.53	324.81
100	328.09	331.37	334.65	337.93	341.21	344 - 49	347.78	351.06	354 · 34	357.62

¹ statute mile = 1.6093 kilometers.

¹ kilometer = 0.6214 statute mile.

CHAPTER X

ADJUSTMENT OF INSTRUMENTS

The Transit. — The adjustments in order are:

- I. Axis of plate bubbles perpendicular to vertical axis of instrument.
- II. Line of sight perpendicular to and presumably coincident with horizontal axis of telescope.
 - I. Parallax.
 - 2. Vertical wire perpendicular to horizontal axis of telescope.
 - 3. Intersection of wires to axis of telescope.
 - 4. Objective slide coincident with axis of telescope.
 - 5. Line of sight perpendicular to horizontal axis of telescope.
 - 6. Eyepiece to center.
 - III. Horizontal axis of telescope truly horizontal (Standard).
 - IV. Axis of telescope bubble parallel to line of sight.
 - V. Error of vernier of vertical circle.

To test for and make the adjustments:

- I. Set up; turn the alidade through 180°; if the plate bubbles depart from the centers of their tubes, bring them halfway back with the adjusting pin, and relevel. Repeat test and adjustment until complete.
- II. I. Carefully focus the eyepiece on the wires until they are sharp and there is no apparent motion over an object sighted as the eye is moved a little sidewise or up and down.
- 2. Sight a minute distant point and note whether the vertical wire remains on the point as the telescope is slightly revolved on its horizontal axis. If not, loosen two adjacent capstan screws carrying the wire ring, and turn the ring slightly until by further trial the adjustment is complete.
- 3. Construct a pair of Y standards of wood, as two notches cut in opposite sides of a box, that will support the telescope near the two ends after it has been removed from the standards. Remove the telescope and place it in the Y's; direct the line of sight to any minute distant point and revolve the telescope in the Y's 180°; notice if the intersection of the wires remains on the point; if not, bring the wires halfway back to the point by opposite capstan screws, moving first

one set and then the other. Repeat the test and adjustment until complete. This adjustment is not often made but should be made if careful leveling is to be done with the transit.

- 4. Not all object slides are adjustable. If the slide may be adjusted, its adjustment may be tested by making a test for 3 on a very near object; if an error appears, the slide may be moved by moving the ring carrying it. The ring is often concealed by a band around the telescope. After adjusting the slide a test should be made again for 3, and both tests and adjustments repeated until complete.
- 5. Set up; sight a minute distant point, or set a pin some 200 to 400 feet away; transit the telescope and find a distant point in the line of sight or set a pin some 200 to 400 feet away; revolve in azimuth and sight the first point; transit and see whether the line of sight falls on the second point; if not, move the vertical wire one-fourth the apparent distance toward the second point; repeat the test and adjustment until complete. The same first point may be retained but new second points must be found or set for each test.
- 6. If the wires seem to be to one side of the field of view, the eyepiece is not centered. This need not cause error in work. To correct the condition, if the eyepiece is adjustable, move the ring carrying it between the eye end and the wire ring until the wires appear to be in the center of the field.
- III. (a) Hang a plumb line from a high point not far from the transit, turn the line of sight on the line near its top and plunge the telescope downward, noting if the intersection of the wires follows the line; if not, raise or lower one end of the horizontal axis until the required condition is met.
- (b) Sight a nearby high point, say, on a building, plunge the telescope and set a point near the level of the instrument or lower; reverse in azimuth, transit, and sight the high point; plunge again and note whether the line of sight cuts the first lower point set; if not, raise or lower one end of the horizontal axis until the required condition is met. A new lower point will be needed for each test.
 - IV. Adjust as described for the Y level, II 1 (b).
- V. After making IV, with the transit carefully leveled, bring the telescope bubble to the center of its tube and note the reading of the vertical arc vernier. If it is not zero, either move the vernier till it does read zero or note the error as an index error to be applied to all vertical angle readings. Care must be taken to note whether the error is such as to diminish or increase angles of elevation; angles of depression will be affected in the opposite way.

The Y Level. - The adjustments are:

- I. Line of sight coincident with axis of telescope.
 - I. Parallax.
 - 2. Horizontal wire perpendicular to vertical axis of instrument.
 - 3. Intersection of wires to axis of telescope.
 - 4. Objective slide coincident with axis of telescope.
 - 5. Eyepiece to center.
- II. Bubble axis parallel to line of sight.
 - 1. Vertical adjustment.
 - 2. Lateral adjustment.
- III. Y adjustment bubble axis perpendicular to vertical axis of level.

To Make the Adjustment:

- I. I. Set up; focus the eyepiece on the wires until they appear sharp and there is no apparent motion over the field as the eye is moved a little sidewise or vertically.
- 2. Sight a distant point near one end of the horizontal wire; turn the telescope a little on the vertical axis and note if the point remains covered by the wire from one end to the other; if not, loosen two adjacent screws carrying the wire ring and turn the ring until by trial the required condition is met.
- 3. Loosen the clips over the Y's and sight a distant point, clamping the azimuth motion; revolve the telescope in the Y's upside down, and note whether the intersection of the wires remains on the point; if not, move the wire ring first sidewise and then vertically about half the apparent error until the intersection of the wires will remain on a point through a complete revolution of the telescope.
- 4. If the object slide is adjustable, perform the same test on a very near point and adjust the object slide. The ring carrying the object slide when it is adjustable is likely to be concealed beneath a band around the telescope between the object focusing screw and the wire adjusting screws.
- 5. When the instrument is adjusted the wires may appear to be out of the center of the field of view; if so, the eyepiece is out of center and may be centered by moving the ring between the eye end and the wire ring until the wires appear to center the field.
- II. I (a) Set up carefully, loosen the clips over the Y's, remove the telescope and replace it end for end; if the bubble does not return to the center of the tube bring it halfway back by the bubble adjusting screws, relevel, and test and adjust again, until the required condition is met. A better method is the following:

- (b) Set up midway between two stakes about 200 feet apart; read a rod on the two stakes and get their difference of elevation; set up beyond one of the stakes about $\frac{1}{10}$ the distance between them; read the rod on the near stake, apply the difference in level and add a correction for curvature, = 0.001 ft. for 220 feet, for a trial reading on the distant stake; read the rod on the distant stake and if the reading is not the same as the trial reading, move the target up or down $\frac{1}{10}$ of the apparent error according as the instrument is pointing low or high; set the line of sight on the target and bring the bubble to the center by its adjusting screws. Without moving the instrument make another complete test on near and far rod and continue until the required condition is met. If the level is set outside one stake one-fourth of the distance between the stakes the apparent error will be multiplied by $\frac{1}{4}$ instead of $\frac{1}{10}$, and similarly for other proportions.
- 2. With the level set up and the clips loose, turn the telescope a little in the Y's and note whether the bubble remains centered; if not, adjust it by the lateral adjusting screws at one end until it will so remain when the telescope is turned from side to side.
- III. Set up and level with particular care over one set of leveling screws; turn on the vertical axis 180° and note whether the bubble remains in the center of the tube; if not, bring it halfway back by raising or lowering one Y by the capstan nuts through which its stem passes; relevel and repeat until the required condition is met.

The Dumpy Level. - The adjustments are:

- I. Bubble axis perpendicular to vertical axis of level.
- II. Line of sight parallel to bubble axis.
 - I. Parallax.
 - 2. Horizontal wire perpendicular to vertical axis of instrument.
 - 3. Line of sight.

The adjustments are made as follows:

- I. Set up with telescope leveled with particular care over one set of screws; reverse in azimuth and note whether the bubble remains in the center of its tube; if not, bring it halfway back by the bubble adjusting screws; relevel and repeat until the condition is met.
 - II. I and 2 are made as for the Y level.
- 3 is made as for Y level II I (b), adjusting the wires to the bubble rather than the bubble to the wires; i.e., centering the bubble and moving the horizontal wire to the computed correct reading on the distant rod.

CHAPTER XI

SEXAGESIMAL TRIGONOMETRIC FUNCTIONS

TABLE LXXXIII.—Logarithmic Sines, Cosines, Tangents, and Cotangents for Each Minute of Arc

To interpolate when the angles are less than 3°, the quantities S and T as found in the 5th and 6th columns of the first three pages are used as follows:

Log sine
$$\alpha = \text{Log } \alpha' - S$$
,
Log tangent $\alpha = \text{Log } \alpha' - T$,
Log $\alpha' = \text{Log sine } \alpha + S = \text{Log tangent } \alpha + T$.

For cosine and cotangent of angles near 90° use the sine and tangent of the complements.

	0 °								179°	
1	′	L Sin	d	S	Т	L Tan	c d	L Cot	L Cos	
0	0								0.00 000	60
1	I	6.46 373	30103	3.53 627	3.53 627	6.46 373 6.76 476	30103	3.53 627	0.00 000	59 58
3	3	6.76 476 6.94 0 85	17609	3.53 627	3.53 627 3.53 627	6.94 085	17609	3.23 524 3.05 915	0.00 000	58
4	4	7.06 579	9691	3.53 627	3.53 627	7.06 579	12494 9691	2.93 421	0.00 000	56
5 6	5	7.16 270 7.24 188	7918	3.53 627 3.53 627	3.53 627 3.53 627	7.16 270	7918	2.83 730 2.75 812	0.00 000	55
	7	7.30 882	6694 5800	3.53 627	3.53 627	7.30 882	6694 5800	2.69 118	0.00 000	54 53
7 8	8	7.36 682	5115	3.53 627	3.53 627	7.36 682	5115	2.63 318 2.58 203	0.00 000	52
9	9 10	7.41 797	4576	3.53 627	3.53 627	7.41 797	4576	2.53 627	0.00 000	51 50
II	II	7.50 512	4139	3.53 627	3.53 627	7.50 512	4139	2.49 488	0.00 000	49
12	12	7.54 291	3779 3476	3.53 627	3.53 627	7.54 291	3779 3476	2.45 709	0.00 000	48
13	13	7.57 767 7.60 985	3218	3.53 627	3.53 627 3.53 627	7.57 767	3219	2.42 233	0.00 000	47
14	14 15	7.63 982	2997	3.53 628	3.53 627	7.63 982	2996 2803	2.39 01 4 2.36 01 8	0.00 000	46 45
16	16	7.66 784	2802 2633	3.53 628	3.53 627	7.66 785	2633	2.33 215	0.00 000	44
17	17	7.69 417	2483	3.53 628 3.53 628	3.53 627 3.53 627	7.69 418	2482	2.30 582	9.99 999	43
19	19	7.74 248	2348	3.53 628	3.53 627	7.74 248	2348	2.25 752	9.99 999	41
20	20	7.76 475	2119	3.53 628	3.53 627	7.76 476	2119	2.23 524	9.99 999	40
21	2I 22	7.78 594	2021	3.53 628	3.53 627	7.78 595	2020	2.21 405	9.99 999	39
22 23	23	7.80 615	1930	3.53 628 3.53 628	3.53 627 3.53 627	7.82 546	1931	2.19 385	9.99 999	38
24	24	7.84 393	1848	3.53 628	3.53 627	7.84 394	1848	2.15 606	9.99 999	36
25 26	25 26	7.86 166	1704	3.53 628 3.53 628	3.53 627 3.53 627	7.86 167	1704	2.13 833	9.99 999	35
27	27	7.89 509	1639	3.53 628	3.53 626	7.89 510	1639	2.10 490	9.99 999	33
28	28	7.91 088	1579 1524	3.53 628	3.53 626	7.91 089	1579	2.08 911	9.99 999	32
29	29 30	7.92 612	1472	3.53 628	3.53 626	7.92 613	1473	2.07 387	9.99 998	31 30
30	31	7.94 084	1424	3.53 628	3.53 626	7.95 510	1424	2.05 914	9.99 998	29
32	32	7.96 887	1379 1336	13,53 628	3.53 626	7.96 889	1379 1336	2.03 111	9.99 998	28
33	33	7.98 223	1297	3.53 028	3.53 020	7.98 225	1297	2.01 775	9.99 998	27
34	34 35	7.99 520 8.00 779	1259	3.53 628 3.53 628	3.53 626 3.53 626	7.99 522 8.00 781	1259	1.99 219	9.99 998	26
36	36	8.02 002	1223	3.53 628	3.53 626	8.02 004	1223	1.97 996	9.99 998	24
37 38	37 38	8.03 192 8.04 350	1158	3.53 628 3.53 628	3.53 626 3.53 626	8.03 194 8.04 353	1159	1.96 806	9.99 997	23
39	39	8.05 478	1128	3.53 628	3.53 626	8.05 481	1128	1.94 519	9.99 997	21
40	40	8.06 578	1072	3.53 628	3.53 625	8.06 581	1072	1.93 419	9.99 997	20
41	41	8.07 650 8.08 696	1046	3.53 628	3.53 625	8.07 653	1047	1.92 347	9.99 997	19
42	42	8.09 718	1022	3.53 628	3.53 625 3.53 625	8.09 722	1022	1.91 300	9.99 997	17
44	44	8.10 717	999	3.53 629	3.53 625	8.10 720	998	1.89 280	9.99 996	16
45 46	45 46	8.11 693 8.12 647	954	3.53 629 3.53 629	3.53 625 3.53 625	8.11 696	955	1.88 304	9.99 996	15
47	47	8.13 581	934	3.53 629	3.53 625	8.13 585	934	1.86 415	9.99 996	13
48	48	8.14.495	896	3.53 629	3.53 625	8.14 500	895	1.85 500	9.99 996	I2 II
50	49 50	8.15 391	877	3.53 629 3.53 629	3.53 624	8.15 395 8.16 273	878	1.84 605	9.99 996	10
51	51	8.17 128	860	3.53 629	3.53 624	8.17 133	860	1.82 867	9.99 995	
52	52	8.17 971	843 827	3.53 629	3.53 624	8.17 976	843 828	1.82 024	9.99 995	8
53 54	53 54	8.18 798 8.19 610	812	3.53 629	3.53 624	8.18 804	812	1.81 196	9.99 995	7 6
55	55	8.20 407	797 782	3.53 629	3.53 624	8.20 413	797 782	1.79 587	9.99 995	5
56	56	8.21 189	769	3.53 629	3.53 624	8.21 195	769	1.78 805	9.99 994	4
57 58	57 58	8.21 958	755	3.53 629	3.53 623	8.21 964	756	1.78 036	9.99 994	3 2
59	59	8.23 456	743	3.53 630	3.53 623	8.23 462	742	1.76 538	9.99 994	I
60	60	8.24 186		3.53 630	3.53 623	8.24 192	l	1.75 808	9.99 993	0
	000	L Cos	d		(229	L Cot	c d	L Tan	L Sin	,

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,	,	L Sin	d	S	Т	L Tan	c d	L Cot	L Cos	
60	0	8.24 186		3.53 630	3.53 623	8.24 192		1.75 808	9.99 993	60
61	I	8.24 903	717	3.53 630	3.53 623	8.24 910	718	1.75 090	9.99 993	59
62	2	8.25 609	706 695	3.53 630	3.53 623	8.25 616	706 696	1.74 384	9.99 993	58
63	3	8.26 304 8.26 988	684	3.53 630	3.53 623	8.26 312	684	1.73 688	9.99 993	57 56
64 65	4 5	8.27 661	673	3.53 630	3.53 622	8.27 669	673	1.72 331	9.99 992	55
65	5	8.28 324	663	3.53 630	3.53 622	8.28 332	663	1.71 668	9.99 992	54
67	7 8	8.28 977	644	3.53 630	3.53 622	8.28 986	643	1.71 014	9.99 992	53
68 69	9	8.29 621 8.30 255	634	3.53 630	3.53 622 3.53 622	8.29 629 8.30 263	634	1.70 371	9.99 992 9.99 991	52 51
70	10	8.30 879	624	3.53 630	3.53 621	8.30 888	625	1.69 112	9.99 991	50
71	11	8.31 495	616	3.53 630	3.53 621	8.31 505	617	1.68 495	9.99 991	49
72	12	8.32 103	608 599	3.53 631	3.53 621	8.32 112	607 599	1.67 888	9.99 990	48
73	13 14	8.32 702 8.33 292	590	3.53 631 3.53 631	3.53 621	8.32 711	591	1.66 698	9.99 990	47 46
74 75	15	8.33 875	583	3.53 631	3.53 620	8.33 302 8.33 886	584	1.66 114	9.99 990	45
76	16	8.34 450	575 568	3.53 631	3.53 620	8.34 461	575 568	1.65 539	9.99 989	44
77 78	17	8.35 o18 8.35 578	560	3.53 631 3.53 631	3.53 620 3.53 620	8.35 029	561	1.64 971	9.99 989 9.99 989	43
79	19	8.36 131	553	3.53 631	3.53 620	8.36 143	553	1.63 857	9.99 989	42 41
80	20	8.36 678	547	3.53 631	3.53 620	8.36 689	546	1.63 311	9.99 988	40
81	21	8.37 217	539	3.53 631	3.53 619	8.37 229	540	1.62 771	9.99 988	39
82	22	8.37 750	533 526	3.53 632	3.53 619	8.37 762	533 527	1.62 238	9.99 988	38
83 84	23 24	8.38 276 8.38 796	520	3.53 632	3.53 619	8.38 289 8.38 809	520	1.61 711	9.99 987 9.99 987	37 36
85	25	8.39 310	514	3.53 632	3.53 619	8.39 323	514	1.60 677	9.99 987	35
80	26	8.39 818	508	3.53 632	3.53 618	8.39832	509 502	1.60 168	9.99 986	34
8 ₇ 88	27	8.40 320	496	3.53 632	3.53 618	8.40 334	496	1.59 666	9.99 986	33
89	28 29	8.40 816	49I	3.53 632 3.53 632	3.53 618	8.40 830	491	1.59 170	9.99 986 9.99 985	32 31
90	30	8.41 792	485	3.53 632	3.53 617	8.41 807	486	1.58 193	9.99 985	30
91	31	8.42 272	480	3.53 632	3.53 617	8.42 287	480	1.57 713	9.99 985	29
92	32	8.42 746	474 470	3.53 633	3 53 617	8.42 762	475 470	1.57 238	9.99 984	28
93	33	8.43 216 8.43 680	464	3.53 633	3.53 617	8.43 232 8.43 696	464	1.56 768 1.56 304	9.99 984	27 26
94 95	34 35	8.44 139	459	3.53 633	3.53 616	8.44 156	460	1.55 844	9.99 983	25
96	36	8.44 594	455	3.53 633	3.53 010	8.44 611	455 450	1.55 389	9.99 983	24
97 98	37 38	8.45 044 8.45 489	445	3.53 633	3.53 616	8.45 of 1 8.45 507	446	1.54 939	9.99 983	23
99	39	8.45 930	441	3.53 633 3.53 633	3.53 616 3.53 615	8.45 948	441	1.54 493	9.99 982	21
100	40	8.46 366	436	3.53 634	3.53 615	8.46 385	437	1.53 615	9.99 982	20
IOI	41	8.46 799	433	3.53 634	3.53 615	8.46 817	432	1.53 183	9.99 981	19
102	42	8.47 226	427 424	3.53 634	3.53 615	8.47 245	428	1.52 755	9.99 981	18
103	43	8.47 650 8.48 069	419	3.53 634	3.53 614	8.47 669 8.48 089	420	1.52 331	9.99 981	17
104	44	8.48 485	416	3.53 634	3.53 614	8.48 505	416	1.51 495	9.99 980	15
106	46	8.48 896	411	3.53 634	3.53 614	8.48 917	412	1.51 083	9.99 979	14
107	47 48	8.49 304 8.49 708	404	3.53 634	3.53 613	8.49 325	404	1.50 675	9.99 979	13
100	49	8.50 108	400	3.53 635	3.53 613	8.50 130	401	1.49 870	9.99 978	11
IIO	50	8.50 504	396	3.53 635	3.53 613	8.50 527	397	1.49 473	9.99 978	10
III	51	8.50 897	393	3.53 635	3.53 612	8.50 920	393	1.49 080	9.99 977	9
112	52	8.51 287	390 386	3.53 635	3.53 612	8.51 310	390 386	1.48 690	9.99 977	
113	53	8.51 673 8.52 055	382	3.53 635	3.53 611	8.51 696 8.52 079	383	1.48 304	9.99 977	7 6
115	55	8.52 434	379	3.53 635	3.53 611	8.52 459	380	1.47 541	9.99 976	5
116	56	8.52 810	376	3.53 636	3.53 611	8.52 835	376	1.47 165	9.99 975	4
117	57 58	8.53 183 8.53 552	369	3.53 636	3.53 611	8.53 208 8.53 578	370	1.46 792	9.99 975	3 2
110	59	8.53 919	367	3.53 636	3.53 610	8.53 945	367	1.46 055	9.99 974	ī
120	60	8.54 282	363	3.53 636	3.53 610	8.54 308	363	1.45 692	9.99 974	0
		L Cos	d			L Cot	cd	L Tan	L Sin	,

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,	, 1	I Sim	الم	S	T	1 Tan	0 4	L Cot	I Coo	
		L Sin	d			L Tan	c d		L Cos	
120	0	8.54 282	360	3.53 636	3.53 610	8.54 308	361	1.45 692	9.99 974	60
121	1 2	8.54 999	357	3.53 636 3.53 637	3.53 609 3.53 609	8.55 027	358	1.45 331	9.99 973 9.99 973	59 58
123	3	8.55 354	355 351	3.53 637	3.53 609	8.55 382	355 352	1.44 618	9.99 972	57
124	4	8.55 705	349	3.53 637	3.53 609	8.55 734	349	1.44 266	9.99 972	56
125	5 6	8.56 o54 8.56 400	346	3.53 637 3.53 637	3.53 608 3.53 608	8.56 0 83 8.56 4 29	346	1.43 917	9.99 971	55 54
127	7 8	8.56 743	343	3.53 637	3.53 608	8.56 773	344	1.43 227	9.99 970	53
128		8.57 084	341	3.53 637	3.53 607	8.57 114	34I 338	1.42 886	9.99 970	52
129	9	8.57 421	336	3.53 638	3.53 607	8.57 452	336	1.42 548	9.99 969	51
130	10	8.57 757	332	3.53 638	3.53 607	8.57 788	333	1.42 212	9.99 969	50
131	II I2	8.58 089	330	3.53 638 3.53 638	3.53 606	8.58 451	330	1.41 879	9.99 968	49 48
133	13	8.58 747	328	3.53 638	3.53 606	8.58 779	328	1.41 221	9.99 967	47
134	14	8.59 072	325	3.53 638	3.53 605	8.59 105	326 323	1.40 895	9.99 967	46
135	15	8.59 395	323	3.53 639	3.53 605	8.59 428	321	1.40 572	9.99 967	45
137	17	8.59 715 8.60 033	318	3.53 639 3.53 639	3.53 605 3.53 604	8,60 068	319	1.39 932	9.99 966	44 43
138	18	8.60 349	316	3.53 639	3.53 604	8.60 384	316	1.39616	9.99 965	42
139	19	8.60 662	313	3.53 639	3.53 604	8.60 698	314	1.39 302	9.99 964	41
140	20	8.60 973	309	3.53 639	3.53 603	8.61 009	310	1.38 991	9.99 964	40
141	2I 22	8.61 282	307	3.53 640	3.53 603	8.61 319	307	1.38 681	9.99 963	39
I42 I43	23	8.61 589 8.61 894	305	3.53 640 3.53 640	3.53 603 3.53 602	8.61 931	305	1.38 374	9.99 963	38
144	24	8.62 196	302	3.53 640	3.53 602	8.62 234	303	1.37 766	9.99 962	36
145	25	8.62 497	301	3.53 640	3.53 602	8.62 535	30I 299	1.37 465	9.99 961	35
146	26	8.62 795	296	3.53 640	3.53 601	8.62 834	297	1.37 166	9.99 961	34
147 148	27 28	8.63 o91 8.63 385	294	3.53 641	3.53 601 3.53 601	8.63 131	295	1.36 869	9.99 960	33
149	29	8.63 678	293	3.53 641	3.53 600	8.63 718	292 291	1.36 282	9.99 959	31
150	30	8.63 968	290	3.53 641	3.53 600	8.64 009	289	1.35 991	9.99 959	30
151	3 I	8.64 256	287	3.53 641	3.53 599	8.64 298	287	1.35 702	9.99 958	29
152	32 33	8.64 543 8.64 827	284	3.53 642	3.53 599	8.64 585	285	1.35 415	9.99 958	28
153	34	8.65 110	283	3.53 642	3.53 599 3.53 598	8.65 154	284	1.34 846	9.99 956	26
155	35	8.65 391	281	3.53 642	3.53 598	8.65 435	281	1.34 565	9.99 956	25
156	36	8.65 670	279 277	3.53 642	3.53 598	8.65 715	278	1.34 285	9.99 955	24
157	37 38	8.65 947 8.66 223	276	3.53 642 3.53 643	3.53 597 3.53 597	8.65 993	276	1.34 007	9.99 955	23
159	39	8.66 497	274	3.53 643	3.53 596	8.66 543	274	1.33 457	9.99 954	21
160	40	8.66 769	272	3.53 643	3.53 596	8.66 816	273	1.33 184	9.99 953	20
161	41	8.67 039	270	3.53 643	3.53 596	8.67 087	271	1.32 913	9.99 952	19
162	42	8.67 308	269 267	3.53 643	3.53 595	8.67 356	269	1.32 644	9.99 952	18
163	43	8.67 575 8.67 841	266	3.53 644	3.53 595	8.67 624	266	1.32 376	9.99 951	17
165	44	8.68 104	263	3.53 644 3.53 644	3.53 594 3.53 594	8.68 154	264	1.31 846	9.99 950	15
166	46	8.68 367	263 260	3.53 644	3.53 594	8.68 417	263	1.31 583	9.99 949	14
167	47	8.68 627	259	3.53 644	3.53 593	8.68 678	260	1.31 322	9.99 949	13
168	48 49	8.68 886 8.69 144	258	3.53 645	3.53 593 3.53 592	8.68 938 8.69 196	258	1.31 062	9.99 948	II
170	50	8.69 400	256	3.53 645	3.53 592	8.69 453	257	1.30 547	9.99 947	10
171	51	8.69 654	254	3.53 645	3.53 592	8.69 708	255	1.30 292	9.99 946	-1
172	52	8.69 907	253	3.53 646	3.53 591	8.69 962	254	1.30 038	9.99 946	8
173	53	8.70 159	252 250	3.53 646	3.53 591	8.70 214	252 251	1.29 786	9.99 945	7
174	54 55	8.70 409 8.70 658	249	3.53 646 3.53 646	3.53 590	8.70 465	249	1.29 535	9.99 944	6 5
176	56	8.70 905	247	3.53 646	3.53 589	8.70 962	248	1.29 038	9.99 944	4
177	57 58	8.71 151	246	3.53 647	3.53 589	8.71 208	246	1.28 792	9.99 942	3
178	58	8.71 395	244	3.53 647	3.53 589	8.71 453	245	1.28 547	9.99 942	2 I
179	59 60	8.71 638	242	3.53 647	3.53 588	8.71.697	243	1.28 303	9.99 941	0
100	00	L Cos	d	3-53 647	3.53 588	8.71 940 L Cot	c d	L Tan	L Sin	,
	1	L Cos	u	1		L Cot	Ca	Lian	Lom	

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_	8° 176°													
Ľ	L Sin	d	L Tan	c d	L Cot	L Cos				1	PP			
1	8.71 88	240	8.71 940	241	1.28 060	9.99 940	60		241	239	237	236	234	
	8.72 120	239	8 72 181 8.72 420	239	1.27 819	9.99 940 9.99 939	59 58	1 2	24.I 48.2	23.9 47.8	23.7 47.4	23.6 47.2	23.4 46.8	
3	8.72 59	230	8.72 659	239	1.27 341	9.99 938	57	3· 4	72.3 96.4	71.7 95.6	71.1 94.8	70.8 94.4	70.2 93.6	
1 3	8.73 06	233	8.72 896 8.73 132	236	1.27 104	9.99 938 9.99 937	56 55	5	120.5	119.5	118.5	118.0	117.0	
		232	8.73 300	234	1.26 634	9.99 936 9.99 936	54	7 8	168.7	167.3	165.9 189.6	165.2 188.8	163.8 187.2	
		232	8.73 832 8.74 063	232 231	1.26 168	9.99 935 9.99 934	52 51	9	216.9	215.1	213.3	212.4	210.6	
10		220	8.74 292	229	1.25 708	9.99 934	50	T I	232 23.2	231 23.I	229 22.9	227	226 22.6	
1:	8.74.45	228	8.74 521	229	1.25 479	9.99 933	49	3	46.4 69.6	46.2 69.3	45.8 68.7	45.4 68.1	45.2 67.8	
1;		5 220	8 74 748 8.74 974	227	I.25 252 I.25 026	9.99 932 9.99 932	48	4	92.8	92.4	91.6 114.5	90.8	90.4 113.0	
1.	8 75 13	0 224	8.75 199	225	1.24 801	9.99 931	46	5 6 7	139.2	115.5 138.6 161.7	137.4	136.2 158.9	135.6 158.2	
I,		3 000	8.75 423 8.75 645	222	1.24 577 1.24 355	9.99 930 9.99 929	45 44	7 8 9	185.6 208.8	184.8	183.2 206.1	181.6	180.8	
I	8.75 79 8.76 or	220	8.75 867 8.76 087	220	1.24 133	9.99 929 9.99 928	43 42	,	224	222	220	219	217	
1	8.76 23	4 219	8.76 306	219	1.23 694	9.99 927	41	I 2	22.4 44.8	22.2	22.0	21.9 43.8	21.7 43.4	
2	0.70 43	216	8.76 525	217	1.23 475	9.99 926	40	3 4	67.2 89.6	66.6 88.8	66.0 88.0	65.7 87.6	65.1 86.8	
2 2		7 216	8.76 742 8.76 958	216	1.23 258	9.99 926	39 38	5	112.0	0.111	110.0	109.5	108.5	
2	8.77 09	7 214	8.77 173	215	1.22 827	9.99 924	37	7 8	134.4	133.2	132.0 154.0	131.4	130.2	
2.	8.77 52	2 212	8.77 387 8.77 600	213	1.22 613	9.99 923 9.99 923	36 35	9	179.2 201.6	177.6 199.8	176.0 198.0	175.2 197 I	173.6 195.3	
2 2	1 11 10	210	8.77 811	211	1.22 189	9.99 922	34		216	214	213	211	209	
2 2	8.78 15	209	8.78 232 8.78 441	210	1-21 768	9.99 920 9.99 920	32	1 2	21.6 43.2	42.8	21.3 42.6	21.1 42.2	20.9 41.8	
3		- 208	8.78 649	208	1.21 559	9.99 919	30	3 4	64.8 86.4	64.2 85.6	63.9 85.2	63.3 84.4	62.7 83.6	
3	8.78 77	206	8.78 855	206	1.21 145	9.99 918	29	5	108.0	107.0	106.5	105.5	104.5	
3	8.78 97	9 205	8.79 of 1 8.79 266	206	1.20 939	9.99 917	28	8	151.2	149.8	149.1 170.4	147.7 168.8	146.3 167.2	
3	1 8.70 18	6 203	8.79 470	204	1.20 530	9.99 916	26	9	194.4	192.6	191.7	189.9	188.1	
3	8.79 58 8.79 78	9 201	8.79 673 8.79 875	202	I.20 327 I.20 I25	9.99 915	25 24	1	206	206	203	201 20.I	199 19.9	
3	8.79 99 8 8.80 18	0 199	8.80 076 8.80 277	201	1.19 924	9.99 913	23	3	41.6 62.4	41.2 61.8	40.6 60.9	40.2 60.3	39.8 59.7	
3	8.80 38	8 199	8.80 476	199	1.19 723 1.19 524	9.99 912	21	4	83.2	82.4	81.2	80.4	79.6 99.5	
4	8.80 58	5 197	8.80 674	198	1,19 326	9.99 911	20	5 6 7	124.8	123.6	121.8	120.6	119.4	
4	2 8.80 97	8 196	8.80 872 8.81 068	196	1.19 128	9.99 910	19	7 8 9	166.4	164.8 185.4	162.4	160.8	159.2 179.1	
4	8.81 17	3 195	8.81 264	196	1.18 736	9.99 909	17	Ľ	198	196	194	192	190	
4	8.81 56	7 0 193	8.81 459 8.81 653	194	1.18 541 1.18 347 1.18 154	9.99 908	16	I 2	19.8	19.6 39.2	19.4 38.8	19.2 38.4	19.0 38.0	
4		4 192	8.81 846 8.82 038	193	1.18 154	9.99 905	14	3 4	59.4 79.2	58.8 78.4	58.2 77.6	57.6	57.0 76.0	
4	8 8.82 13	4 190	8.82 230 8.82 420	192	1-17 770	9.99 904	12	5 6	99.0	98.0	97.0	96.0 115.2	95.0 114.0	
5	_	780	8.82 610	190	1.17 390	9.99 904	10	7 8	138.6	137.2	135.8	134.4	133.0 152.0	
5	-		8.82 799	189	1.17 201	9.99 902	9 8	9	178.2	176.4	174.6	172.8	171.Q	
5		E 187	8.82 987 8.83 175	188	1.17 013	9.99 900	8 7	1	188 18.8	186 18.6	184 18.4	182	181 18.1	
5	4 8.83 20	1 100	8.83 361	186	1.16 639	9.99 899	6	2	37.6 56.4	37.2 55.8	36.8 55.2	36.4 54.6	36.2 54.3	
5	5 8.83 44 6 8.83 6	0 184	8.83 547 8.83 732	185	1.16 453	9.99 898	5 4	3 4	75.2 94.0	74.4 93.0	73.6 92.0	72.8	72.4 90.5	
9	8 8.83 90	6 183	8.83 916 8.84 100	184	1.16 084	9.99 897	3 2	6	112.8	111.6	110.4	109.2	108.6	
5	9 8.84 1	7 181	8.84 282	182	1.15 718	9.99 895	1	8 9	131.0 150.4 169.2	130.2 148.8 167.4	147.2 165.6	145.6 163.8	144.8 162.0	
6	8.84 3	8 181	8.84 464	102	1.15 836	9.99 894	0	9	1 109.2	107.4	105.0	103.8	102.9	
L	L Co	s d	L Cot	c d	L Tan	L Sin	90				PP			

		4 °						175°	,				
	1	L Sin	d	L Tan	c d	L Cot	L Cos				PP		
ı	0	8.84 358	181	8.84 464	182	1.15 536	9.99 894	60	182	181	180	179	178
ı	1 2	8.84 539 8.84 718	179	8.84 646 8.84 826	180	1.15 354	9.99 893 9.99 892	59 58	1 18.2 2 36.4	18.1 36.2	18.0 36.0	17.9 35.8	17.8 35.6
ı	3	8.84 897	179	8.85 000	180	1.14 994	9.99 891	57	3 54.6 4 72.8	54-3 72.4	54.0	53.7	53.4
ı	4 5 6	8.85 075 8.85 252	177	8.85 185 8.85 363	178	1 14 815	9.99 891 9.99 890	56 55	5 91.0 6 109.2	90.5	90.0	89.5	71.2 89.0 106.8
ı		8.85 429 8.85 605	176	8.85 540	177	1.14 460	9.99 889 9.99 888	54	7 127.4 8 145.6	126.7	126.0	125.3	124.6
ı	7 8 9	8.85 780 8.85 955	175	8.85 717 8.85 893 8.86 069	176	1.14 107	9.99 887 9.99 886	52 51	9 163.8	162.9	162.0	161.1	160.2
ı	10	8.86 128	173	8.86 243	174	1.13 757	9.99 885	50	177	176 17.6	175 17.5	174	178 17.3
ı	11	8.86 301	173 173	8.86 417	174	1.13 583	9.99 884	49	2 35.4 3 53.1	35.2 52.8	35.0 52.5	34.8	34.6
ı	12 13	8.86 474 8.86 645	171	8.86 591 8.86 763	172	I.I3 409 I.I3 237	9.99 883 9.99 882	48 47	4 70.8 5 88.5	70.4 88.0	70.0 87.5	69.6 87.0	51. 9 69.2 86.5
	14	8.86 816	171	8.86 935	172	1.13 065	9.99 881 9.99 880	46	6 106.2	105.6	105.0	104.4	86.5 103.8 121.1
ı	16	8.86 987 8.87 156	169	8.87 106 8.87 277	171	1-12 894	9.99 879	45 44	7 123.9 8 141.6 9 159.3	140.8	140.0	139.2 156 6	138.4 155.7
	17	8.87 325 8.87 494	169	8.87 447 8.87 616	169	1.12 553	9.99 879 9.99 878	43 42	172	171	170	169	166
	19	8.87 001	168	0.07 705	168	1.12 215	9.99 877	41	1 17.2	17.1 34.2	17.0 34.0	16.9 33.8	16.8 33.6
ı	20	8.87 829	166	8.87 953	167	1.12 047	9.99 876	40	3 51.6 4 68.8	51.3	51.0	50.7 67.6	50.4 67.2
ı	2 I 2 2	8.87 995 8.88 161	166 165	8.88 120 8.88 287	167	1.11 880	9.99 875 9.99 874	39 38	5 86.0 6 103.2	85.5	85.0 102.0	84.5	84.0 100.8
ı	23	8.88 326	164	8.88 453 8.88 618	165	1.11 547	9.99 873	37 36	7 120.4 8 137.6	119.7	119.0	118.3	117.6
ı	25 26	8.88 490 8.88 654 8.88 817	164 163	8.88 783 8.88 948	165	1.11 217 1.11 052	9.99 871	35	9 154.8	153.9	153.0	135.2 152.1	134.4
ı	27	8.88 980	163 162	8.89 111	163	1.10 889	9.99 869	34	167 1 16.7	166 16.6	165 16.5	164 16.4	163 16.3
ı	28	8.89 142 8.89 304	162	8.89 274 8.89 437	163	1.10 726	9.99 868 9.99 867	32 31	2 33.4 3 50.1	33.2 49.8	33.0 49.5	32.8	32.6 48.9
ı	30	8.89 464	160	8.89 598	161	1.10 402	9.99 866	30	4 66.8 5 83.5	66.4 83.0	66.0 82.5	65.6 82.0	65.2 81.5
ı	31	8.89 625 8.89 784	161	8.89 760 8.89 920	162	1.10 240	9.99 865	29 28	6 100.2	99.6	99.0	98.4	97.8 114.1
ı	32 33	8.89 943	159 159	8.90 080	160	1.09 920	9.99 863	27	8 133.6 9 150.3	132.8	132.0	131.2	130.4
ı	34 35	8.90 102 8.90 260	158	8.90 240	159	1.09 760	9.99 862	26 25	162	161	160	159	158
ı	36	8.90 417	157	8.90 557	158	1.09 443	9.99 860	24	1 16.2	16.1 32.2	16.0	15.9 31.8	15.8 31.6
ı	37 38	8.90 574 8.90 730	156 155	8.90 715 8.90 872	157	1.09 285	9.99 859 9.99 858	23	3 48.6 4 64.8	48.3	48.0 64.0	47.7 63.6	47.4 63.2
	39 40	8.90 885	155	8.91 029	156	1.08 971	9.99 857	21	5 81.0 6 97-2	80.5	80.0 96.0	79.5 95.4	79.0 94.8
ı	41	8.91 040	155	8.91 185	155	1.08 815	9.99 856	19	7 113.4 8 129.6	112.7	112.0	111.3	110.6
ı	42	8.91 349	154	8.91 495 8.91 650	155	1.08 505	9.99 854	18	9 145.8	144.9	144.0	143.1	142.2
	43	8.91 502 8.91 655	153 152	8.91 803	153	1.08 350	9.99 852	17	157 1 15.7	156 15.6	155 15.5	154 15.4	153
	45 46	8.91 807 8.91 959	152	8.91 957 8.92 110	154	1.08 043	9.99 851	15	2 31.4	31.2 46.8	31.0 46.5	30.8 46.2	30.6
	47 48	8.92 110 8.92 261	151	8.92 262	152	1.07 738	9.99 848 9.99 847	13	3 47 1 4 62.8 5 78 5	62.4 78.0	62.0	61.6 77.0	45.9 61.2
	49	8.92 411	150	8.92 414 8.92 565	151	1.07 586	9.99 846	11	6 94.2	93.6	77.5 93.0 108.5	92.4 107.8	76.5 91.8 107.1
	50	8.92 561	149	8.92 716	151	1.07 284	9.99 845	10	8 125.6	124.8	124.0	107.8 123.2 138.6	122.4
	51 52	8.92 710 8.92 859	149	8.92 866 8.93 01 6	150	1.07 134	9.99 844 9.99 843	9 8	9 141.3	140.4	139.5 150	149	137.7 143
	53	8.93 007	148	8.93 165	149	1.06 835	9.99 842	7	1 15.2	15.1	15.0	14.9	14.8
	54 55	8.93 154	147	8.93 313 8.93 462	149	1.06 687	9.99 841	6 5	2 30.4 3 45.6 4 60.8	30.2 45.3 60.4	30.0 45.0 60.0	29.8 44.7 59.6	29.6 44.4
	56	8.93 448 8.93 594	146	8.93 6 0 9 8.93 756	147	1.06 391	9.99 839	3	5 76.0	75.5	75.0	74.5	59.2 74.0 88.8
	57 58 59	8.93 740 8.93 885	146	8.93 903 8.94 049	147	1.06 097	9.99 837 9.99 836	2	7 106.4	90.6 105.7 120.8	90.0	89.4	103.6
	60	8.94 030	145	8.94 195	146	1.05 805	9.99 834	0	8 121.6 9 136.8	135.9	135.0	119.2	133.2
		L Cos	d	L Cot	c d	L Tan	L Sin	,			PP		
-		94°					(242)	850					

94°

		5°						174°						
I	,	L Sin	d	L Tan	c d	L Cot	L Cos				Р	•		
ı	0	8.94 030	144	8.94 195	145	1.05 805	9.99 834	60		147	146	145	144	
ı	I	8.94 174	143	8.94 340	145	1.05 660	9.99 833	59	1 2	14.7	14.6	14.5	14.4	
ı	3	8.94 317 8.94 461	144	8.94 485 8.94 630	145	1.05 515	9.99 832 9.99 831	58	3	44.1	29.2 43.8	43.5	43.2	
ı	4	8.94 603	143	8.94 773	144	1.05 227	9.99 830	56	4 5	58.8 73.5 88.2	58.4 73.0 87.6	58.0 72.5	57.6 72.0	
ı	5	8.94 746 8.94 887	141	8.94 917 8.95 060	143	1.05 083	9.99 829 9.99 828	55 54	5 6 7	88.2 102.9	87.6	87.0 101.5	86.4 100.8	
ı	7	8.95 029	142	8.95 202	142	1.04 798	9.99 827	53	8	117.6	116.8	116.0	115.2	
ı	8	8.95 170	140	8.95 344 8.95 486	142	1.04 656	9.99 825 9.99 824	52 51	9	132.3	131.4	130.5	129.6	
ı	10	8.95 450	140	8.95 627	141	1.04 373	9.99 823	50	1	14.3 14.3 28.6	14.2 14.2 28.4	141 14.1 28.2	140 14.0 28.0	
ı	11	8.95 589	139	8.95 767	140	1.04 233	9.99 822	49	3	28.6 42.9	28.4 42.6	28.2 42.3	28.0 42.0	
1	12 13	8.95 728 8.95 867	139	8.95 908 8.96 047	141	1.04 092	9.99 821 9.99 820	48	4 5	57.2	56.8	56.4 70.5	56.0	
ı	14	8,96 005	138	8.96 187	140	1.03 933	9.99 819	46	6	71.5 85.8	71.0 85.2	84.6	70.0 84.0	
ı	15	8.96 143 8.96 280	138	8.96 325 8.96 464	138	1.03 675	9.99 817	45	7 8	100.I 114.4	99.4 113.6	98.7 112.8	98.0 112.0	
I	17	8.96 417	137	8.06.602	138	1.03 536	9.99 816	44	9	128.7	127.8	126.9	126.0	
	18	8.96 553 8.96 689	136	8.96 739 8.96 877	137	1.03 261	9.99 814	42		139	138	137	136	
	19		136		136	1.03 123	9.99 813	41	1 2	13.9 27.8	13.8 27.6	13.7 27.4	13.6 27.2	
1	20	8.96 825	135	8.97 013	137	1.02 987	9.99 812	40	3	41.7 55.6	41.4 55.2	41.1	40.8	
1	21	8.96 960 8.97 095	135	8.97 150 8.97 285	135	1.02 850	9.99 810	39 38	5 6	69.5 83.4	69.0 82.8	68.5 82.2	54.4 68.0 81.6	
ı	23	8.97 229	134	8.97 421	136	1.02 579	9.99 808	37	7 8	97-3	96.6	95.9	95.2 108.8	
ı	24 25	8.97 363 8.97 496	133	8.97 556 8.97 691	135	1.02 444	9.99 807 9.99 806	36 35	9	111.2 125.1	110.4	109.6	108.8	
1	26	8.97 629	133	8.97 825	134	1.02 175	9.99 804	34		135	134	133	132	
ı	27 28	8.97 762 8.97 894	132	8.97 959 8.98 092	133	1.02 041	9.99 803	33	1	13.5	13.4	13.3	13.2	
ı	29	8.98 026	132	8.98 225	133	1.01 775	9.99 801	32 31	3	27.0 40.5	40.2	26.6 39.9	26.4 39.6	
1	30	8.98 157	131	8.98 358	133	1.01 642	9.99 800	30	4 5	54.0 67.5	53.6 67.0	53.2 66.5	52.8 66.0	
ı	31	8.98 288	131	8.98 490	132 132	1.01 510	9.99 798	29	6	81.0	80.4 93.8	79.8	79.2 92.4	
	32	8.98 419 8.98 549	130	8.98 622 8.98 753	131	1.01 378	9.99 797 9.99 796	28 27	7 8	94.5 108.0	107.2	93.1 106.4	105.6	
	34	8.98 679	130	8.98 884	131	1.01 116	9.99 795	26	9	121.5	120.6	119.7	118.8	
ı	35 36	8.98 808 8.98 937	129	8.99 015 8.99 145	130	1.00 985	9.99 793 9.99 792	25 24	1	131 13.1	130 13.0	129	128 12.8	
и	37	8.99 066	129	8.99 275	130	1.00 725	9.99 791	23	2	26.2	26.0	25.8	25.6	
ı	38 39	8.99 194 8.99 322	128	8.99 405 8.99 534	130	1.00 595	9.99 790 9.99 788	22 21	3 4	39.3 52.4	39.0 52.0	38.7 51.6	38.4 51.2	
	40		128	8.99 662	128				5 6	65.5 78.6	65.0 78.0	64.5 77.4	64.0 76.8	
Ł	-	8.99 450	127		129	1.00 338	9.99 787	20	7 8	91.7	91.0	90.3	89.6 102.4	
	41 42	8.99 577 8.99 704	127	8.99 791 8.99 919	128	1.00 209	9.99 786	19 18	9	104.8	104.0	103.2 116.1	115.2	
1	43	8 99 830	126	9.00 046	128	0.99 954	9.99 783	17		127	126	125	124	
Ł	44 45	8.99 956 9.00 082	126	9.00 174	127	0.99 826	9.99 782	16	1 2	12.7 25.4	12.6	12.5 25.0	12.4	
	46	9.00 207	125	9.00 427	126	0 99 573	9.99 780	14	3	38.1	37.8	37.5	37.2 49.6	
1	47 48	9.00 332 9.00 456	124	9.00 553 9.00 679	126 126	0.99 447 0.99 321	9.99 778 9.99 777	13	5	50.8 63.5	50.4 63.0	50.0 62.5	62.0	
	49	9.00 581	123	9.00 805	125	0.99 195	9.99 776	11	6	76.2 88.9	75.6 88.2	75.0 87.5	74.4 86.8	
1	50	9.00 704	124	9.00 930	125	0.99 070	9.99 775	10	7 8 9	101.6	100.8	100.0	99.2 111.6	
	51 52	9.00 828 9.00 951	123	9.01 055	124	0.98 945	9.99 773 9.99 772	9	,	123	122	121	120	
	53	9.01 074	123	9.01 303	124	0.98 697	9.99 771	7	1	12.3	12.2	12.1	12.0	
	54 55	9.01 196 9.01 318	I 2 2	9.01 427 9.01 550	123	0.98 573	9.99 769 9.99 768	6 5	3	24.6 36.9	24.4 36.6	24.2 36.3	24.0 36.0	
1	56	9.01 440	122	9.01 673	123	0.98 327	9.99 767	5 4	4	49.2	48.8	48.4 60.5	48.0 60.0	
1	57	9.01 561	121	9.01 796 9.01 918	122	0.98 204	9.99 765 9.99 764	3 2	5 6	61.5 73.8 86.1	73.2	72.6 84.7	72.0 84.0	
1	59	9.01 803	IZI	9.02 040	122	0.98 082	9.99 763	1	7 8	98.4	85.4 97.6	96.8	96.0	
1	80	9.01 923	120	9.02 162	122	0.97 838	9.99 761	0	9	110.7	109.8	108.9	108.0	
		L Cos	d	L Cot	c d	L Tan	L Sin	,			PF	,		

	6°											
1	LSin	d	L Tan	c d	L Cot	L Cos				PF		
0	9.01 923	120	9.02 162	121	0.97 838	9.99 761	60					
I	9.02 043	120	9.02 283	121	0.97717	9.99 760	59					
3	9.02 163	120	9.02 404 9.02 525	121	0.97 596	9.99 759 9.99 757	58 57		121	120	119	118
4	9.02 402	119	9.02 645	120	0.97 355	9.99 756	56	2	12.1	12.0	11.9	11.8
5 6	9.02 520	118	9.02 766	121	0.97 234	9.99 755	55	3	24.2 36.3	24.0 36.0	23.8 35.7	23.6 35.4
	9.02 639	118	9.02 885	120	0.97 115	9.99 753 9.99 752	54	4	48.4	48.0	47.6	47.2
7 8	9.02 757	117	9.03 003	119	0.96 876	9.99 751	52	5	60.5	60.0	59.5 71.4	59.0
9	9.02 992	118	9.03 242	118	0.96 758	9.99 749	51		72.6 84.7	72.0 84.0	83.3	70.8 82.6
10	9.03 109	117	9.03 361	118	0.96 639	9.99 748	50	7 8	96.8	96. o	95.2	94.4
11	9.03 226	116	9.03 479	118	0.96 521	9.99 747	49	9	108.9	108.0	107.1	106.2
12	9.03 342 9.03 458	116	9.03 597 9.03 714	117	0.96 403 0.96 286	9.99 745 9.99 744	48 47					
14	9.03 574	116	9.03 832	118	0.96 168	9.99 742	46		117	116	115	114
15	9.03 690	116	9.03 948	116	0.96 052	9.99741	45	r	11.7	11.6	11.5	11.4
16	9.03 805	115	9.04.065	116	0.95 935	9.99 740	44	2	23.4	23.2	23.0	22.8
17	9.03 920	114	9.04 181	116	0.95 703	9.99 737	43	3 4	35.I 46.8	34.8 46.4	34.5 46.0	34.2 45.6
19	9.04 149	115	9.04 413	116	0.95 587	9.99 736	41	5	58.5	58.o	57-5	57.0
20	9.04 262	114	9.04 528	115	0.95 472	9.99 734	40		70.2 81.9	69.6 81.2	69.0 80.5	68.4 79.8
21	9.04 376	114	9.04 643	115	0.95 357	9.99 733	39 38	7 8	93.6	92.8	92.0	91.2
22	9.04 490	113	9.04 758 9.04 873	115	0.95 242	9.99 731	37	9	105.3	104.4	103.5	102.6
24	9.04 715	112	9.04 987	114	0.95 013	9.99 728	36					
25	9.04828	113	9.05 101	114	0.94 899	9.99 727	35		113	112	111	110
26 27	9.04 940	II2	9.05 214	11.4	0.94 786	9.99 726	34	I	11.3	11.2	II.I	11.0
28		112	9.05 441	113	0.94 559	9.99 723	32	2	22.6	22.4	22.2	22.0
29		III	9.05 553	112	0.94 447	9.99 721	31	3 4	33.9 45.2	33.6 44.8	33·3 44·4	33.0 44.0
30		III	9.05 666	112	0.94 334	9.99 720	30	5 6	56.5	56.o	55-5	55.0
31	9.05 497	110	9.05 778	II2	0.94 222	9.99 718	29		67.8 79.1	67.2 78.4	66.6	66.0
32		110	9.05 002	112	0.93 998	9.99 716	27	7 8	90.4	89.6	77.7 88.8	77.0 88.0
34	9.05 827	110	9.06 113	III	0.93 887	9.99714	26	9	101.7	8.001	99.9	99.0
35 36		109	9.06 224	III	0.93 776	9.99 713	25					
37	9.06 155	109	9.06 445	110	0.93 555	9.99 710	23		109	108	107	106
38	9.06 264	109	9.06 556	III	0.93 444	9.99 708	22	1	10.9	10.8	10.7	10.6
39		100	9.06 666	109	0.93 334	9.99 707	21	2	21.8	21.6	21.4	21.2
40		108	9.06 775	110	0.93 225	9.99 705	20	3	32.7 43.6	32.4 43.2	32.I 42.8	31.8
41		107	9.06 885	109	0.93 115	9.99 704 9.99 702	19	4 5	54.5	54.0	53.5	53.0
43		108	9.07 103	109	0.92 897	9.99 701	17	5 6	65.4	64.8	64.2	63.6
44	9.06 911	107	9.07 211	108	0.92 789	9.99 699	16	7 8	76.3 87.2	75.6 86.4	74.9 85.6	74.2 84.8
45	9.07 018	106	9.07 320 9.07 428	108	0.92 680	9.99 698	15	9	98.1	97.2	96.3	95.4
47	9.07 231	107	9.07 536	108	0.92 372	9.99 695	13					
48	9.07 337	106	9.07 643	107	0.92 357	9.99 693	12		105	1	04	103
49	-	106	9.07 751	107	0.92 249	9.99 692	II			_	.4	10.3
50		105	9.07 858	106	0.92 142	9.99 690	10	2		20	.8	20.6
51 52		105	9.07 964	107	0.92 036	9.99 687	8	3	31.5		.2	30.9
53	9.07 863	105	9.08 177	106	0.91 823	9.99 686	7	4 5			.6 !.o	41.2 51.5
54		103	9.08 283	106	0.91 717	9.99 684	6	5	63.0	62	.4	61.8
55 56		104	9.08 389	106	0.91 505	9.99 683 9.99 681	5 4	7 8	73.5 84.0	72 81	2.8	72.I 82.4
57	9.08 280	104	9.08 600	105	0.91 400	9.99 680	3	9			.6	92.7
58		103	9.08 705	105	0.91 295	9.99 678	2 I					
59 60	-	103	9.08 914	104	0.91 190	9.99 675	0					
-				0.0		L Sin	1			PI		
L	L Cos	d	L Cot	c d	L Tan					Г		
	960					(211)	830					

	7°	•				1	72)			
7	L Sin	d	L Tan	cd	L Cot	L Cos				PP	
0	9.08 589		9.08 914		0.91 086	9.99 675	60				
1	9.08 692	103	9.09 019	105	0.90 981	9.99 674	59				
2	9.08 795 9.08 897	103	9.09 123	104	0.90 877	9.99 672	58		105	104	103
3 4	9.08 999	102	9.09 227	103	0.90 670	9.99 669	57	1	10.5	10.4	10.3
5 6	9.09 101	102	9.09 434	104	0.90 566	9.99 667	55	3	21.0 31.5	20.8 31.2	20.6 30.9
_	9.09 202	101	9.09 537	103	0.90 463	9.99 666	54	4	42.0	41.6	41.2
7 8	9.09 304	IOI	9.09 640	102	0.90 360	9.99 664	53 52	5 6	52.5	52.0	51.5 61.8
9	9.09 506	101	9.09 742 9.09 845	103	0.90 155	9.99 661	51	7	63.0 73.5	62.4 72.8	72.1
10	9.09 606	101	9.09 947	102	0.90 053	9.99 659	50	8	84.0	83.2	82.4
II	9.09 707	100	9.10 049	101	0.89 951	9.99 658	49	9	94.5	93.6	92.7
12	9.09 807	100	9.10 150 9.10 252	102	0.89 850	9.99 656	48 47				
14	9.10 006	99	9.10 353	101	0.89 647	9.99 653	46		102	101	99
15	9.10 106	99	9.10 454	101	0.89 546	9.99 651	45	1	10.2	10.1	9.9
16	9.10 205	99	9.10 555	101	0.89 445	9.99 650	44	3	20.4 30.6	20.2 30.3	19.8
17 18	9.10 304	98		100	0.89 244	9.99 647	43	4	4 0 .8	40.4	39.6
19	9.10 501	99 98	9.10 756 9.10 856	100	0.89 144	9.99 645	41	5	51.0	50.5	49.5
20	9.10 599	98	9.10 956	100	0.89 044	9.99 643	40	6	61.2 71.4	60.6 70.7	59.4 69.3
21	9.10 697	98	9.11 056	99	0.88 944	9.99 642	39	7 8	81.6	80.8	79.2
22	9.10 795	98	9.11 155 9.11 254	99	0.88 845	9.99 640	38	9	91.8	90.9	89.1
24	9.10 093	97	9.11 353	99	0.88 647	9.99 637	36				
25	9.11 087	97 97	9.11 452	99	0.88 548	9.99 635	35		98	97	96
26	9.11 184	97	9.11 551	99 98	0.88 449	9.99 633	34	1	9.8	9.7	9.6
27 28	9.11 281	96	9.11 649	98	0.88 351	9.99 632	33	2	19.6	19.4	19.2
29	9.11 474	97	9.11 845	98	0.88 155	9.99 629	31	3	29.4	29.1	28.8 38.4
30	9.11 570	96	9.11 943	98	0.88 057	9.99 627	30	4 5	39.2 49.0	38.8 48.5	48.0
31	9.11 666	96	9.12 040	97 98	0.87 960	9.99 625	29	5 6	58.8	58.2	57.6
32	9.11 761	95 96	9.12 138	97	0.87 862	9.99 624	28	7 8	68.6	67.9 77.6	67.2 76.8
33	9.11 057	95	9.12 233	97	0.87 668	9.99 620	26	9	88.2	87.3	86.4
35	9.12 047	95	9.12 428	96	0.87 572	9.99 618	25				
36	9.12 142	95	9.12 525	97	0.87 475	9.99 617	24				
37 38	9.12 236	95	9.12 621	96	0.87 379	9.99 613	23		95	94	93
39	9.12 425	94	9.12 813	96	0.87 187	9.99 612	21	I 2	9.5	9.4 18.8	9.3 18.6
40	9.12 519	94	9.12 909	96	0.87 091	9.99 610	20	3	28.5	28.2	27.9
41	9.12612	93	9.13 004	95	0.86 996	9.99 608	19	4	38.0	37.6	37.2
42	9.12 706	94	9.13 099	95	0.86 901	9.99 607	18	5 6	47.5 57.0	47.0 56.4	46.5 55.8
43	9.12 799	93	9.13 194	95	0.86 711	9.99 603	16	7 8	66.5	65.8	65.1
45	9.12 985	93	9.13 384	95	0.86 616	9.99 601	15	8	76.0	75.2 84.6	74.4
46	9.13 078	93	9.13 478	94 95	0.86 522	9.99 600	14	9	85.5	04.0	83.7
47 48	9.13 171 9.13 263	92	9.13 573 9.13 667	94	o.86 427 o.86 333	9.99 598	13				
49	9.13 355	92	9.13 761	94	0.86 239	9.99 595	II		92	91	90
50	9.13 447	92	9.13854	93	0.86 146	9.99 593	10	1	9.2	9.1	9.0
51	9.13 539	92	9.13 948	94	0.86 052	9.99 591	9 8	2	18.4	18.2 27.3	18.0 27.0
52	9.13 630 9.13 722	91	9.14 041	93	0.85 959	9.99 589 9.99 588		3 4	36.8	36.4	36.0
53 54	9.13 722 9.13 813	91	9.14 134	93	0.85 773	9.99 586	7 6	5 6	46.0	45.5	45.0
55	9.13 904	91	9.14 320	93	0.85 773	9.99 584	5		55.2	54.6 63.7	54.0 63.0
56	9.13 994	90	9.14 412	92	0.85 588	9.99 582	4	7 8	73.6 82.8	72.8	72.0
57 58	9.14 085	90	9.14 504 9.14 597	93	0.85 496	9.99 581	3	9	82.8	81.9	81.0
59	9.14 1/3	91	9.14 688	91	0.85 312	9.99 577	ī				
60	9.14 356	90	9.14 780	92	0.85 220	9.99 575	0				
	L Cos	d	L Cot	c d	L Tan	L Sin	1		8	PP	

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'	L Sin	d	L Tan	c d	L Cot	L Cos		PP
0	9.14 356	89	9.14 780	92	0.85 220	9.99 575	60	
1 2	9.14 445	90	9.14872	91	0.85 128	9.99 574 9.99 572	59 58	
3	9.14 535	89	9.14 903	91	0.84 946	9.99 570	57	
4	9.14 714	90 80	9.15 145	91	0.84 855	9.99 568	56	
5 6	9.14 803	88	9.15 236	91	0.84 764	9.99 566	55	
7 8	9.14 980	89	9.15 417	90	0.84 583	9.99 563	53	4 36.8 36.4 36.0
	9.15 069	89 88	9.15 508	91 90	0.84 492	9.99 561	52	
9 10	9.15 157	88	9.15 598	90	0.84 312	9.99 559 9.99 557	51 50	7 64.4 63.7 63.0
11	9.15 333	88	9.15 777	89	0.84 223	9.99 556	49	
12	9.15 421	88 87	9.15 867	90 89	0.84 133	9.99 554	48	3
13	9.15 508	88	9.15 956	90	0.84 044	9.99 552	47 46	20 00
14	9.15 683	87	9.16 135	89	0.83 865	9.99 548	45	
16	9.15 770	87 87	9.16 224	89 88	0.83 776	9.99 546	44	2 17.8 17.6
17	9.15 857	87	9.16 312	89	o.83 688 o.83 599	9.99 545 9.99 543	43	3 26.7 26.4
19	9.16 030	86 86	9.16 489	88 88	0.83 511	9.99 541	41	. 4 55.0
30	9.16116	87	9.16 577	88	0.83 423	9.99 539	40	6 53.4 52.8
21	9.16 203	86	9.16 665	88	0.83 335	9.99 537	39	7 62.3 61.6 8 71.2 70.4
22	9.16 289 9.16 374	85	9.16 753	88	0.83 247	9.99 535 9.99 533	38	0 0
24	9.16 460	86 85	9.16 928	87 88	0.83 072	9.99 532	36	
25 26	9.16 545	86	9.17 016	87	0.82 984	9.99 530 9.99 528	35	
27	9.16 716	85	9.17 190	87	0.82 810	9.99 526	34	
28	9.16 801	85 85	9.17 277	8 ₇	0.82 723	9.99 524	32	2 17.4 17.2 17.0
29 30	9.16 886	84	9.17 363	87	0.82 637	9.99 522	31 30	
31	9.16 970	85	9.17 450	86	0.82 550	9.99 520	29	5 43.5 43.0 42.5
32	9.17 139	84	9.17 622	86	0.82 378	9.99 517	28	
33	9.17 223	84	9.17 708	86 86	0.82 292	9.99 515	27	8 69.6 68.8 68.0
34 35	9.17 307 9.17 391	84	9.17 794 9.17 880	86	0.82 206	9.99 513	26	
36	9.17 474	83 84	9.17 965	85 86	0.82 035	9.99 509	24	
37	9.17 558	83	9.18 051	85	0.81 949	9.99 507	23	
38	9.17 641 9.17 724	83	9.18 136	85	0.81 779	9.99 505	21	1 8.4 8.3
40	9.17 807	83	9.18 306	85	0.81 694	9.99 501	20	2 16.8 16.6 24.9
41	9.17890	83 83	9.18 391	85	0.81 609	9.99 499	19	4 33.6 33.2
42	9.17 973 9.18 055	82	9.18 475 9.18 560	84 85	0.81 525	9.99 497 9.99 495	18	
44	9.18 137	82	9.18 644	84	0.81 356	9.99 493	16	7 58.8 58.I
45	9.18 220	8 ₃	9.18 728 9.18 812	84 84	0.81 272	9.99 492	15	7 - 1 - 1 - 2
46 47	9.18 302	81	9.18 812	84	0.81 188	9.99 490	14	1
48	9.18 465	8 ₂ 8 ₂	9.18 979	83	0.81 021	9.99 486	12	2
49	9.18 547	81	9.19 063	84	0.80 937	9.99 484	II	
50	9.18 628	81	9.19 146	83	0.80854	9.99 482	10	2 764 762 760
51 52	9.18 709 9.18 790	81	9.19 229	83	0.80 771	9.99 480 9.99 478	8	3 24.6 24.3 24.0
53	9.18871	81 81	9.19 395	83	0.80 605	9.99 476	7	4 32.8 32.4 32.0
54	9.18 952	81	9.19 478	83	o.8o 522 o.8o 439	9.99 474	6	6 49.2 48.6 48.0
55 56	9.19 033	80	9.19 561	82	0.80 357	9.99 472	4	. 1 / 1 3 / . 4 30 . 7 30 . 0
57	9.19 193	80 80	9.19 725	82	0.80 275	9.99 468	3	3 9 73.8 72.6 72.0
58 59	9.19 273 9.19 353	80	9.19 807	82	0.80 193	9.99 466	2 I	2
60	9.19 433	80	9.19 971	82	0.80 029	9.99 462	0	· ·
	L Cos	d	L Cot	c d	L Tan	L Sin	7	
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1	L Sin	d	LTan	c d	L Cot	L Cos			PP	
0	9.19 433	80	9.19 971	82	0.80 029	9.99 462	60			
1	9.19 513		9.20 053	81	0.79 947	9.99 460	59			
2	9.19 592.	79 80	9.20 134	82	0.79 866	9.99 458	58			
3	9.19 672	79	9.20 216	81	0.79 784	9.99 456	57	82	81	80
4 5	9.19 /31	79	9.20 378	81	0.79 622	9.99 454	55	1 8.2	8.1	8.0
6	9.19 909	79	9.20 459	81 81	0.79 541	9.99 450	54	2 16.4	16.2	16.0
7 8	9.19 988	79	9.20 540	81	0.79 460	9.99 448	53	3 24.6	24.3	24.0
	9.20 067	79 78	9.20 621	80	0.79 379	9.99 446	52	4 32.8	32.4	32.0
9	9.20 145	78	9.20 701	81	0.79 299	9.99 444	51 50	5 4I.0 6 49.2	40.5 48.6	40.0 48.0
10	9.20 223	79	9.20 782	80	0.79 218	9.99 442		7 57.4	56.7	56.0
11	9.20 302	78	9.20 862	80	0.79 138	9.99 440 9.99 438	49 48	8 65.6	64.8	64.0
13	9.20 458	78	9.20 942	80	0.78 978	9.99 436	47	9 73.8	72.9	72.0
14	9.20 535	77	9.21 102	80 80	0.78 898	9.99 434	46			
15	9.20613	78 78	9.21 182	79	0.78818	9.99 432	45			
16	9.20 691	77	9.21 261	80	0.78 739	9.99 429	44			
17	9.20 768	77	9.21 341 9.21 420	79	0.78 659	9.99 427 9.99 425	43			
19	9.20 922	77	9.21 420	79	0.78 501	9.99 423	41	79	78	77
20	9.20 999	77	9.21 578	79	0.78 422	9.99 421	40	I 7.9	7.8	7.7
21	9.21 076	77	9.21 657	79	0.78 343	9.99 419	39	2 15.8	15.6 23.4	15.4 23.1
22	9.21 153	77	9.21 736	79 78	0.78 264	9.99 417	38	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	31.2	30.8
23	9.21 229	76 77	9.21 814	79	0.78 186	9.99 415	37	5 39.5	39.0	38.5
24 25	9.21 306	76	9.21 893	78	0.78 107	9.99 413	36		46.8	46.2
26	9.21 352	76	9.21 9/1	78	0.77 951	9.99 411	34	7 55.3 8 63.2	54.6 62.4	53.9 61.6
27	9.21 534	76	9.22 127	78	0.77 873	9.99 407	33	9 71.1	70.2	69.3
28	9.21 610	76	9.22 205	78 78	0.77 795	9.99 404	32			
29	9.21 685	75 76	9.22 283	78	0.77 717	9.99 402	31			
30	9.21 761	75	9.22 361	77	0.77 639	9.99 400	30			
31	9.21 836	76	9.22 438	78	0.77 562	9.99 398	29			
32 33	9.21 912	75	9.22 516	77	0.77 484	9.99 396	28	76	75	74
34	9.22 062	75	9.22 570	77	0.77 330	9.99 392	26	1 7.6	7.5	7.4
35	9.22 137	75	9.22 747	77	0.77 253	9.99 390	25	2 15.2	15.0	14.8
36	9.22 211	74 75	9.22824	77 77	0.77 176	9.99 388	24	3 22.8	22.5	22.2
37	9.22 286	75	9.22 901	76	0.77 099	9.99 385	23	4 30.4 5 38.0	30.0 37.5	29.6 37.0
38 39	9.22 361 9.22 435	74	9.22 977	77	0.77 023	9.99 383	22 2I	6 45.6	45.0	44.4
40	9.22 509	74	9.23 130	76	0.76 870	9.99 379	20	7 53.2	52.5	51.8
41	9.22 583	74	9.23 206	76	0.76 794	9.99 377	19	8 60.8 9 68.4	60.0 67.5	59.2 66.6
42	9.22 657	74	9.23 283	77	0.76 717	9.99 375	18	9 1 00.4	07.3	30.0
43	9.22 731	74 74	9.23 359	76 76	0.76 641	9.99 372	17			
44	9.22 805	73	9.23 435	75	0.76 565	9.99 370	16			
45 46	9.22 878	74	9.23 510 9.23 586	76	0.76 490	9.99 368	15			
47	9.23 025	73	9.23 661	75	0.76 339	9.99 364	13	73	72	71
48	9.23 098	73	9.23 737	76	0.76 263	9.99 362	I 2			
49	9.23 171	73 73	9.23 812	75 75	0.76 188	9.99 359	II	1 7.3 2 14.6	7.2 I4.4	7.I 14.2
50	9.23 244	73	9.23 887	75	0.76 113	9.99 357	10	3 21.9	21.6	21.3
51	9.23 317	73	9.23 962	75	0.76 038	9.99 355	9	4 29.2	28.8	28.4
52 53	9.23 390	72	9.24 037	75	0.75 963	9.99 353	8 7	5 36.5 6 43.8	36.0 43.2	35.5 42.6
54	9.23 535	73	9.24 112	74	0.75 814	9.99 331	6		50.4	49.7
55	9.23 607	72	9.24 261	75	0.75 739	9.99 346	5	8 58.4	57.6	56.8
56	9.23 679	72	9.24 335	74	0.75 665	9.99 344	4	9 65.7	64.8	63.9
57	9.23 752	71	9.24 410	75 74	0.75 590	9.99 342	3			
58 59	9.23 823 9.23 895	72	9.24 484 9.24 558	74	0.75 516	9.99 340	2			
60	9.23 967	72	9.24 632	74	0.75 368	9.99 337	0			
-	L Cos	d	L Cot	c d	L Tan	L Sin	1		PP	
_		-	2 000	,	3 7 411	2 0.11	L			

_					_				
′	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.23 967	72	9.24 632	74	0.75 368	9.99 335	2	60	
1 2	9.24 039	71	9.24 706	73	0.75 294	9.99 333 9.99 331	2	59 58	
3	9.24 110 9.24 181	71	9.24 779	74	0.75 147	9.99 331	3	57	14
4	9.24 253	72 71	9.24 926	73	0.75 074	9.99 326	2	56	74 73 72
5 6	9.24 324 9.24 395	71	9.25 000	73	0.75 000	9.99 324 9.99 322	2	55 54	I 7.4 7.3 7.2
	9.24 466	71	9.25 146	73	0.74 854	9.99 319	3	53	2 14.8 14.6 14.4
7 8	9.24 536	70 71	9.25 219	73	0.74 781	9.99 317	2	52	3 22.2 21.9 21.6 4 29.6 29.2 28.8
9 10	9.24 607	70	9.25 292	73	0.74 708	9.99 315	2	51 50	5 37.0 36.5 36.0
11	9.24 677	71	9.25 365	72	0.74 635	9.99 313	3	49	
12	9.24818	70	9.25 510	73	0.74 490	9.99 308	2	48	8 59.2 58.4 57.6
13	9.24 888	70	9.25 582	72 73	0.74 418	9.99 306	2 2	47	9 66.6 65.7 64.8
14 15	9.24 958	70	9.25 655	72	0.74 345 0.74 273	9.99 3 0 4 9.99 3 0 1	3	46 45	
16	9.25 098	70 70	9.25 799	72	0.74 201	9.99 299	2 2	44	
17 18	9.25 168	69	9.25 871	72 72	0.74 129	9.99 297	3	43	
19	9.25 237 9.25 307	70	9.25 943 9.26 015	72	0.74 057 0.73 985	9.99 294 9.99 292	2	42 41	71 70 69
20	9.25 376	69	9.26 086	71	0.73 914	9.99 290	2	40	1 7.1 7.0 6.9
21	9.25 445	69 69	9.26 158	72	0.73 842	9.99 288	2	39	2 14.2 14.0 13.8 3 21.3 21.0 20.7
22	9.25 514	69	9.26 229	71 72	0.73 771	9.99 285	3	38	4 28.4 28.0 27.6
24	9.25 583	69	9.26 372	71	0.73 628	9.99 281	2	37 36	5 35.5 35.0 34.5 6 42.6 42.0 41.4
25	9.25 721	69 69	9.26 443	71	0.73 557	9.99 278	3 2	35	7 49.7 49.0 48.3
26 27	9.25 790	68	9.26 514	71	0.73 486	9.99 276	2	34	8 56.8 56.0 55.2 9 63.9 63.0 62.1
28	9.25 927	69	9.26 655	70	0.73 345	9.99 271	3	33	9 03.9 03.0 02.1
29	9.25 995	68 68	9.26 726	7I 7I	0.73 274	9.99 269	2 2	31	
30	9.26 063	68	9.26 797	70	0.73 203	9.99 267	3	30	
31 32	9.26 131	68	9.26 867	70	0.73 133	9.99 264	2	29	68 67 66
33	9.26 267	68 68	9.27 008	71	0.72 992	9.99 260	2	27	68 67 66 1 6.8 6.7 6.6
34	9.26 335	68	9.27 078	70	0.72 922	9.99 257	3 2	26	2 13.6 13.4 13.2
35 36	9.26 403	67	9.27 148	70	0.72 852	9.99 255	3	25 24	3 20.4 20.1 19.8
37	9.26 538	68 67	9.27 288	70 69	0.72 712	9.99 250	2 2	23	4 27.2 26.8 26.4 5 34.0 33.5 33.0
38	9.26 605	67	9.27 357 9.27 427	70	0.72 643	9.99 248	3	22	6 40.8 40.2 39.6
40	9.26 739	67	9.27 496	69	0.72 504	9.99 243	2	20	7 47.6 46.9 46.2 8 54.4 53.6 52.8
41	9.26 806	67	9.27 496	70	0.72 434	9.99 241	2	19	9 61.2 60.3 59.4
42	9.26 873	67 67	9.27 635	69	0.72 365	9.99 238	3	18	
43	9.26 940	67	9.27 704	69	0.72 296	9.99 236	3	17	
44 45	9.27 007	66	9.27 773 9.27 842	69	0.72 158	9.99 233	2	15	
46	9.27 140	66	9.27 911	69	0.72 089	9.99 229	3	14	65 3
47 48	9.27 206	67	9.27 980	69	0.72 020	9.99 226	2	13	I 6.5 0.3
49	9.27 339	66	9.28 117	68	0.71 883	9.99 221	3	II	2 13.0 0.6
50	9.27 405	66	9.28 186	68	0.71814	9.99 219	2	10	4 26.0 I.2
51	9.27 471	66	9.28 254	69	0.71 746	9.99 217	3	9	5 32.5 1.5
52 53	9.27 537 9.27 602	65	9.28 323	68	0.71 677	9.99 214	2	8 7	
54	9.27 668	66	9.28 459	68	0.71 541	9.99 209	3 2	6	8 52.0 2.4
55	9.27 734	65	9.28 527	68	0.71 473	9.99 207	3	5 4	9 58.5 2.7
56	9.27 799	65	9.28 595	67	0.71 405	9.99 204	2	3	
58	9.27 930	66	9.28 730	68	0.71 270	9.99 200	3	2	
59 60	9.27 995	65	9.28 798	67	0.71 202	9.99 197	2	0	
00	9.28 060	_	9.28 865	-	0.71 135	9.99 195		-	0.0
L	L Cos	d	L Cot	cd	L Tan	LSin	d	<u></u>	PP

	11°							68°	
1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.28 060	65	9.28 865	68	0.71 135	9.99 195	3	60	
1	9.28 125	65	9.28 933	67	0.71 067	9.99 192 9.99 190	2	59	
3	9.28 190 9.28 254	64	9.29 000	67	0.71 000	9.99 190	3	58 57	
4	9.28 319	65 65	9.29 134	67 67	0.70866	9.99 185	2	56	68 67 66
5	9.28 384 9.28 448	64	9.29 201 9.29 268	67	0.70 799	9.99 182 9.99 180	3 2	55	ı 6.8 6.7 6.6
7	9.28 512	64	9.29 335	67	0.70 665	9.99 177	3	53	2 13.6 13.4 13.2 3 20.4 20.1 19.8
8	9.28 577	65 64	9.29 402	67 66	0.70 598	9.99 175	3	52	4 27.2 26.8 26.4
9	9.28 641	64	9.29 468	67	0.70 532	9.99 172	2	51 50	5 34.0 33.5 33.0 6 40.8 40.2 39.6
	9.28 705	64	9.29 535	66	0.70 399	9.99 167	3	49	7 47.6 46.9 46.2
II I2	9.28 833	64	9.29 668	67 66	0.70 332	9.99 165	2	48	8 54.4 53.6 52.8 9 61.2 60.3 59.4
13	9.28 896	63	9.29 734	66	0.70 266	9.99 162	3 2	47	9 01.2 00.3 39.4
14	9.28 960	64	9.29 800	66	0.70 200	9.99 160	3	46 45	
16	9.29 087	63	9.29 932	66 66	0.70 068	9.99 155	2	44	
17	9.29 150	63 64	9.29 998	66	0.70 002	9.99 152	3 2	43	
18	9.29 214 9.29 277	63	9.30 064 9.30 130	66	0.69 936	9.99 150	3	42 41	65 64 63
20	9.29 340	03	9.30 195	65	0.69 805	9.99 145	2	40	1 6.5 6.4 6.3
21	9.29 403	63	9.30 261	66 65	0.69 739	9.99 142	3	39	2 13.0 12.8 12.6 3 19.5 19.2 18.9
22	9.29 466	63 63	9.30 326	65	0.69 674	9.99 140	3	38	4 26.0 25.6 25.2
23	9.29 529 9.29 591	62	9.30 391	66	0.69 543	9.99 135	2	37	5 32.5 32.0 31.5 6 39.0 38.4 37.8
25	9.29 654	63 62	9.30 522	65 65	0.69 478	9.99 132	3	35	7 45.5 44.8 44.I
26	9.29 716	63	9.30 587	65	0.69 413	9.99 130	3	34	
27	9.29 779 9.29 841	62	9.30 052	65	0.69 283	9.99 124	3	33	9 58.5 57.6 56.7
29	9.29 903	62 63	9.30 782	65 64	0.69 218	9.99 122	3	31	
30	9.29 966	62	9.30 846	65	0.69 154	9.99 119	2	30	
31 32	9.30 028 9.30 090	62	9.30 911	64	0.69 089	9.99 117	3	29	
33	9.30 151	61	9.30 9/3	65	0.68 960	9.99 112	2	27	62 61 60
34	9.30 213	62 62	9.31 104	64 64	0.68 896	9.99 109	3	26	1 6.2 6.1 6.0
35 36	9.30 275	61	9.31 168	65	0.68 832	9.99 106	2	25	2 12.4 12.2 12.0 3 18.6 18.3 18.0
37	9.30 398	62	9.31 297	64	0.68 703	9.99 101	3	23	4 24.8 24.4 24.0
38	9.30 459	61 62	9.31 361	64 64	0.68 639	9.99 099	3	22 21	5 31.0 30.5 30.0 6 37.2 36.6 36.0
39 40	9.30 521	61	9.31 425 9.31 489	64	0.68 575	9.99 096	3	20	7 43.4 42.7 42.0
41	9.30 643	61	9.31 552	63	0.68 448	9.99 091	2	19	
42	9.30 704	61 61	9.31 616	64 63	0.68 384	9.99 088	3	18	9 55.8 54.9 54.0
43	9.30 765	61	9.31 679	64	0.68 321	9.99 086	3	17	
44	9.30 826 9.30 887	61	9.31 743 9.31 806	63	0.68 257	9.99 o83 9.99 o8o	3	15	
46	9.30 947	60	9.31 870	64 63	0.68 130	9.99 078	3	14	
47 48	9.31 oo8 9.31 o68	60	9.31 933 9.31 996	63	0.68 067	9.99 075	3	13	59 3
49	9.31 129	61	9.31 990	63	0.67 941	9.99 072	2	II	1 5.9 0.3
50	9.31 189	60 61	9.32 122	63	0.67 878	9.99 067	3	10	2 11.8 0.6 3 17.7 0.9
51	9.31 250	60	9.32 185	63	0.67 815	9.99 064	3 2	9	4 23.6 1.2
52 53	9.31 310	60	9.32 248	63	0.67 752	9.99 062	3	8 7	5 29.5 I.5 6 35.4 I.8
54	9.31 430	60	9.32 373	02	0.67 627	9.99 056	3	6	7 41.3 2.1
55	9.31 490	60 59	9.32 436	63	0.67 564	9.99 054	3	5	8 47.2 2.4 9 53.1 2.7
56	9.31 549	60	9.32 498	63	0.67 502	9.99 051	3	3	9 33.1 2.1
58	9.31 669	60 59	9.32 623	62	0.67 377	9.99 046	3	2	
59	9.31 728	60	9.32 685	62	0.67 315	9.99 043	3	0	
60	9.31 788		9.32 747		0.67 253	9.99 040		.	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	1	PP

101° (349) **78°**

	_				_				01	
	'	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
ı	0	9.31 788		9.32 747	63	0.67 253	9.99 040	_	60	
ı	I	9.31 847	59 60	9.32810	62	0.67 190	9.99 038	2	59	
ı	3	9.31 907	59	9.32 872 9.32 933	61	0.67 128	9.99 035	3	58 57	
ı	4	9.32 025	59	9.32 933	62	0.67 005	9.99 032	2	56	63 62 61
ı	5	9.32 084	59	9.33 057	62 62	0.66 943	9.99 027	3	55	1 6.3 6.2 6.1
ı	6	9.32 143	59 59	9.33 119	61	0.66 881	9.99 024	3	54	2 12.6 12.4 12.2 3 18.9 18.6 18.3
ı	7 8	9.32 202 9.32 261	59	9.33 180	62	0.66 758	9.99 022	3	53 52	3 18.9 18.6 18.3 4 25.2 24.8 24.4
ı	9	9.32 319	58 59	9.33 303	61 62	0.66 697	9.99 016	3	51	5 31.5 31.0 30.5
ı	10	9.32 378	59	9.33 365	61	0.66 635	9.99 013	3 2	50	6 37.8 37.2 36.6 7 44.1 43.4 42.7
ı	II	9.32 437	58	9.33 426	61	0.66 574	9.99 011	3	49	8 50.4 49.6 48.8
ı	I2 I3	9.32 495	58	9.33 487 9.33 548	61	0.66 513	9.99 008	3	48 47	9 56.7 55.8 54.9
1	14	9.32 612	59	9.33 609	61	0.66 391	9.99 002	3	46	
ı	15	9.32 670	58 58	9.33 670	61	0.66 330	9.99 000	3	45	
1	16 17	9.32 728	58	9.33 73I 9.33 792	61	0.66 269	9.98 997	3	44 43	
I	18	9.32 844	58 58	9.33 853	61 60	0.66 147	9.98 991	3 2	43	60 59
	19	9.32 902	58	9.33 913	61	0.66 087	9.98 989	3	41	1 6.0 5.9
	20	9.32 960	58	9.33 974	60	0.66 026	9.98 986	3	40	2 12.0 11.8
ı	2I 22	9.33 018	57	9.34 034 9.34 095	6ı	0.65 966	9.98 983	3	39 38	3 18.0 17.7 4 24.0 23.6
ı	23	9.33 133	58	9.34 155	60 60	0.65 845	9.98 978	2	37	4 24.0 23.6 5 30.0 29.5
Ш	24	9.33 190	57 58	9.34 215	61	0.65 785	9.98 975	3	36	6 36.0 35.4
ı	25	9.33 248 9.33 305	57	9.34 276	60	0.65 724	9.98 972	3	35	7 42.0 4I.3 8 48.0 47.2
ı	27	9.33 362	57	9.34 396	60	0.65 604	9.98 967	2	33	9 54.0 53.1
ı	28	9.33 420	58 57	9.34 456	60 60	0.65 544	9.98 964	3	32	
-	29	9.33 477	57	9.34 516	60	0.65 484	9.98 961	3	31	
-1	30	9.33 534	57	9.34 576	59	0.65 424	9.98 958	3	30 29	
	31 32	9.33 591	56	9.34 635	60	0.65 365	9.98 953	2	28	
	33	9.33 704	57 57	9.34 755	60 59	0.65 245	9.98 950	3	27	58 57
	34	9.33 761 9.33 818	57	9.34 814	60	0.65 186	9.98 947	3	26	1 5.8 5.7 2 11.6 11.4
	35 36	9.33 874	56	9.34 933	59	0.65 067	9.98 941	3	25 24	3 17.4 17.1
ı	37	9.33 931	57 56	9.34 992	59 59	0.65 008	9.98 938	3 2	23	4 23.2 22.8 5 29.0 28.5
ı	38	9.33 987	56	9.35 051	60	0.64 949 0.64 889	9.98 936 9.98 933	3	22 2I	5 29.0 28.5 6 34.8 34.2
	39 40	9.34 043	57	9.35 111	59	0.64 830	9.98 930	3	20	7 40.6 39.9
	41	9.34 156	56	9.35 229	59	0.64 771	9.98 930	3	10	8 46.4 45.6 9 52.2 51.3
	42	9.34 212	56	9.35 288	59	0.64712	9.98 924	3	18	9 0-1- 0+10
-	43	9.34 268	56 56	9.35 347	59 58	0.64 653	9.98 921	3 2	17	
	44 45	9.34 324 9.34 380	56	9.35 405 9.35 464	59	0.64 595 0.64 536	9.98 919	3	16	
	46	9.34 436	56 55	9.35 523	59 58	0.64 477	9.98 913	3	14	
1	47	9.34 491	56	9.35 581	59	0.64 419	9.98 910	3	13	56 55 3
	48	9.34 547 9.34 602	55	9.35 640	58	0.64 360	9.98 907	3	II.	1 5.6 5.5 0.3
	50	9.34 658	56	9-35 757	59	0.64 243	9.98 901	3	10	2 11.2 11.0 0.6 3 16.8 16.5 0.9
1	51	9.34713	55	9.35 815	58 58	0.64 185	9.98 898	3	9	4 22.4 22.0 I.2
1	52	9.34 769	56 55	9.35 873	5.8	0.64 127	9.98 896 9.98 893	3	8	5 28.0 27.5 1.5 6 33.6 33.0 1.8
	53 54	9.34 824	55	9.35 931	58	0.64 069	9.98 890	3	7 6	
1	55	9.34 934	55	9.36 047	58 58	0.63 953	9.98 887	3	5	8 44.8 44.0 2.4
	56	9.34 989	55 55	9.36 105	58	0.63 895	9.98 884	3	4	9 50.4 49.5 2.7
1	57 58	9.35 044	55	9.36 163	58	0.63 837	9.98 881	3	3	
1	59	9.35 154	55	9.36 279	58	0.63 721	9.98 875	3	I	
	60	9.35 209	55	9.36 336	57	0.63 664	9.98 872	3	0	
		L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP
-	_	1000	_					-	BBO	

13° 166°

ı	1													
		L Sin	d	L Tan	c d	L Cot	L Cos	d				F	Р	
I	0	9.35 209	F.4	9.36 336	58	0.63 664	9.98 872	2	60					
ı	1	9.35 263	54 55	9.36 394	58	0.63 606	9.98 869	3 2	59					
ı	3	9.35 318 9.35 373	55	9.36 452 9.36 509	57	0.63 548	9.98 867	3	58					
1	4	9.35 427	54	9.36 566	57	0.63 434	9.98 861	3	56		E	i8	57	56
ı	5	9.35 481	54	9.36 624	58	0.63 376	9.98858	3	55	I	-	5.8	5.7	5.6
ı	6	9.35 536	55 54	9.36 681	57 57	0.63 319	9.98 855	3	54	2	1	1.6	11.4	11.2
ı	7	9.35 590	54	9.36 738	57	0.63 262	9.98 852	3	53 52	3		7·4 3.2	17.I 22.8	16.8 22.4
1	9	9.35 698	54	9.36 852	57	0.63 148	9.98 846	3	51	4 5		9.0	28.5	28.0
ľ	10	9.35 752	54	9.36 909	57	0.63 091	9.98 843	3	50	5	3.	4.8	34.2	33.6
	11	9.35 806	54	9.36 966	57	0.63 034	9.98 840	3	49	7 8		5.6 5.4	39.9 45.6	39.2 44.8
	12	9.35 860 9.35 914	54 54	9.37 023 9.37 080	57 57	0.62 977	9.98 837 9.98 834	3	48	9		2.2	51.3	50.4
•	14	9.35 914	54	9.37 137	57	0.62 863	9.98 831	3	47 46					
	15	9.36 022	54	9.37 193	56	0.62 807	9.98 828	3	45					
	16	9.36 075	53 54	9.37 250	57 56	0.62 750	9.98 825	3	44					
	17	9.36 129 9.36 182	53	9.37 306 9.37 363	57	0.62 694	9.98 822	3	43					
	19	9.36 236	54	9.37 419	56	0.62 581	9.98 816	3	42 4I		5	5	54	53
	20	9.36 289	53	9.37 476	57	0.62 524	9.98813	3	40	I		5.5	5.4	5.3
1	21	9.36 342	53	9.37 532	56	0.62 468	9.98 810	3	39	3		i.o	10.8	10.6
	22	9.36 395	53 54	9.37 588	56 56	0.62 412	9.98 807	3	38	4		2.0	21.6	21.2
	23	9.36 449	53	9.37 644	56	0.62 356	9.98 804 9.98 801	3	37	5		7.5	27.0	26.5
	24		53	9.37 756	56	0.62 244	9.98 798	3	36	6	33	3.0 3.5	32.4 37.8	31.8 37.1
	26	9.36 555 9.36 608	53	9.37 756 9.37 812	56 56	0.62 244 0.62 188	9.98 795	3	34	7 8		1.0	43.2	42.4
	27	9.36 660	52 53	9.37 868	56	0.62 132	9.98 792	3	33	9	49	-5	48.6	47.7
	28	9.36 713	53	9.37 924 9.37 980	56	0.62 076	9.98 789 9.98 786	3	32 31					
	80	9.36 819	53	9.38 035	55	0.61 965	9.98 783	3	30					
	31	9.36 871	52	9.38 091	56	0.61 909	9.98 780	3	29					
3	32	9.36 924	53	9.38 147	56	0.61 853	9.98 777	3	28			52		1
	33	9.36 976	52 52	9.38 202	55 55	0.61 798	9.98 774	3	27					
	34	9.37 028 9.37 081	53	9.38 257 9.38 313	56	0.61 743	9.98 771	3	26 25		1 2	5.2 10.4		.1 .2
	36	9.37 133	52	9.38 368	55	0.61 632	9.98 765	3	24		3	15.6	15	.3
3	37	9.37 185	52 52	9.38 423	55 56	0.61 577	9.98 762	3	23		4	20.8 26.0		0.4
	38	9.37 237 9.37 289	52	9.38 479 9.38 534	55	0.61 521	9.98 759 9.98 756	3	22 2I		5	31.2		.6
	10	9.37 341	52	9.38 589	55	0.61 411	9.98 753	3	20		7 8	36.4	35	-7
ш	ıı	9.37 341	52	9.38 644	55	0.61 356	9.98 750	3	19		9	41.6	40 45	
4	12	9.37 445	52	9.38 699	55	0.61 301	9.98 746	4	18		7	. 40.0	43	
	13	9.37 497	52 52	9.38 754	55	0.61 246	9.98 743	3 3	17					
	14 15	9.37 549 9.37 600	51	9.38 808 9.38 863	55	0.61 192	9.98 740	3	16					
	‡6	9.37 652	52	9.38 918	55	0.61 082	9.98 734	3	14					- 1
4	47	9.37 703	51 52	9.38 972	54	0.61 028	9.98 731	3	13			4		3
	18 19	9-37 755 9-37 806	52 51	9.39 027 9.39 082	55	0.60 973	9.98 728 9.98 725	3	12		I	0.4		-3
	50	9.37 858	52	9.39 136	54	0.60 864	9.98 722	3	10		2	0.8		.6
ı	51	9.37 909	51	9.39 190	54	0.60 810	9.98 719	3	9		3	1.6		.9
п	52	9.37 960	51	9.39 245	55	0.60 755	9.98 715	4	8		5	2.0		.5
	53	9.38 011	51 51	9.39 299	54 54	0.60 701	9.98712	3	7			2.4		.8 .1
	54	9.38 062	51	9.39 353	54	0.60 647	9.98 709	3	6		7 8	3.2		.4
	56 56	9.38 164	51	9.39 461	54	0.60 539	9.98 703	3	4		9	3.6		.7
	57 58	9.38 215	51	9.39 515	54	0.60 485	9.98 700	3	3					
ı	58 59	9.38 266 9.38 317	51 51	9.39 569	54 54	0.60 431	9.98 697 9.98 694	3	2 I					
	60	9.38 368	51	9.39 623	54	0.60 377	9.98 690	4	0					
I		L Cos	d	L Cot	c d	L Tan	L Sin	d	,			Р	Р	

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1 0 3.38 479 57 59 3.38 579 57 59 3.38 579	0	9.38 368		9.39 677	E 4	0.60 323		2	60	
3 9.38 9.39 9.55 9.38 9.3				9.39 731					59	
4 9,38 570 51 9,39 892 54 0,60 or 58 9,98 678 3 55 1 5,4 5.0 9,38 670 50 9,39 999 54 0,60 or 59 9,98 675 3 55 1 5,4 5.0 9,38 711 50 9,40 105 53 0,59 948 9,98 668 3 53 3 16,2 15,		9.38 409		0.39 785		0.60 162				
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9 9,38 821 50 9,40 212	8					0.59 940	9.98 665	3		
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TS 9.39 121 150 9.40 478 53 0.59 522 9.98 643 3 44 43 43 44 43 44 43 44 44 44 44 44 44 44 44 44 44 44 44 44 48 9.44 920 9.40 636 52 0.59 364 9.98 633 3 44 44 44 44 48 9.40 920 9.39 360 9.40 636 53 0.59 311 9.98 630 3 44 44 44 44 44 44 4										
17	15	9.39 121		9.40 478		0.59 522	9.98 643		45	
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20 9.39 309 49 9.40 745 50 9.98 5027 7 9.39 518 7 9.40 795 50 9.40 847 52 9.39 517 50 9.40 905 52 9.39 615 49 9.41 057 52 0.59 048 9.98 617 3 36 6 31.2 30.6 32.2 32.2 33.6 34 20.8 20.4 40.8 35 7 36.4 35.7										
21 9,39 418 7 9,40 795 70 9,98 623 3 38 4 20,8 20,4	20		-						40	
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38 9.40 249 49 9.41 081 52 0.58 319 9.98 565 3 221 6 29.4 28.8 3 32.2 3 5 24.5 24.5 24.5 24.5 24.5 24.5 24.5 24	36		49			0.58 422				3 14.7 14.4 14.I 1 19.6 19.2 18.8
39 9.40 297 49 48 9.41 733 51 0.58 216 9.98 565 3 42 20 7 83.43 33.6 42 9.40 442 48 9.41 836 52 0.58 216 9.98 551 3 18 9.40 940 48 9.41 939 52 0.58 601 9.98 551 3 18 9.40 940 48 9.42 940 51 0.58 213 9.98 551 4 17 9.42 501 51 9.40 823 48 9.42 941 51 0.57 959 9.98 541 4 14 9.40 538 48 9.42 941 51 0.57 959 9.98 541 4 14 9.40 538 48 9.42 941 51 0.57 959 9.98 541 4 14 9.40 538 48 9.42 941 51 0.57 959 9.98 541 4 14 9.40 538 48 9.42 941 51 0.57 959 9.98 541 4 14 9.40 538 48 9.42 941 51 0.57 959 9.98 531 3 15 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.40 825 48 9.42 941 51 0.57 959 9.98 531 3 12 9.80 825 51 0.57 949 9.98 511 4 8 5 2.0 11 0.4 0.57 959 9.98 541 4 1.6 11 0.4 0.57 959 9.98 511 4 11 0.4 0.57			49		- 1					5 24.5 24.0 23.5
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44 9.40 538 48 9.41 990 51 0.58 501 9.98 545 3 16 4 9.40 634 48 9.42 903 51 0.57 856 9.98 538 3 15 4 4 9.40 632 48 9.42 144 51 0.57 856 9.98 538 3 12 0.57 856 9			48			0.58 113	9.98 555			
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54 9.41 016 48 9.42 501 51 0.57 499 9.98 515 3 6 7 2.8 2.55 9.41 063 47 9.42 552 51 0.57 448 9.98 511 4 5 8 3.2 2.55 9.41 111 48 9.42 503 50 0.57 347 9.98 505 3 4 9 3.6 2.57 9.41 158 47 9.42 503 50 0.57 347 9.08 505 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	52	9.40 921		9.42 399		0.57 601	9.98 521			
34 9.42 552 51 0.57 499 9.98 508 3 4 9 3.6 22 55 9.41 111 48 9.42 603 51 0.57 347 9.98 508 3 4 9 3.6 22 55 9.41 111 48 9.42 603 50 0.57 347 9.98 508 3 4 9 3.6 22 55 9.41 205 47 9.42 705 51 0.57 347 9.98 505 3 5 9.41 205 47 9.42 705 51 0.57 246 9.98 501 4 2 5 9 9.41 205 47 9.42 705 51 0.57 246 9.98 501 4 2 5 9 9.41 205 47 9.42 705 51 0.57 246 9.98 501 4 2 5 9 9.41 205 48 9.42 705 51 0.57 245 9.98 498 3 1 1			48							
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58 9.41 205 47 9.42 755 51 0.57 245 9.98 498 3 1	56	9.41 111		9.42 603		0.57 397	9.98 508		4	9 3.6 2.7
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18 3 10 10 5 10 5 10			47		51	0.57 290		3		
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L Cos d L Cot cd L Tan L Sin d ' PP			d		c d			d	,	PP

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i	,	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
	0	9.41 300		9.42 805		0.57 195	9.98 494		60	
	r	9.41 347	47	9.42 856	51	0.57 144	9.98 491	3	59	
	2	9.41 394	47	9.42 906	50 51	0.57 094	9.98 488	3	58	
	3	9.41 441	47	9.42 957	50	0.57 043	9.98 484	3	57	51 50 49
	4 5	9.41 535	47	9.43 007	50	0.56 943	9.98 477	4	56 55	1 5.1 5.0 4.9
ı	5	9.41 582	47	9.43 108	5 I	0.56 892	9.98 474	3	54	2 10.2 10.0 9.8
	7 8	9.41 628	46	9.43 158	50	0.56842	9.98 471	3	53	3 15.3 15.0 14.7
ı	9	9.41 675	47	9.43 208	50	0.56 792	9.98 467	3	52	4 20.4 20.0 19.6
ı	10	9.41 768	46	9.43 258	50	0.56 692	9.98 464	4	51 50	5 25.5 25.0 24.5 6 30.6 30.0 29.4
ı	TT	9.41 700	47	9.43 358	50	0.56 642	9.98 457	3	49	7 35.7 35.0 34.3
ı	12	9.41 861	46	9.43 408	50	0.56 592	9.98 457	4	48	
ı	13	9.41 908	47 46	9.43 458	50	0.56 542	9.98 450	3	47	9 45.9 45.0 44.1
ı	14	9.41 954	47	9.43 508	50 50	0.56 492	9.98 447	3	46	
ı	15	9.42 001	46	9.43 558	49	0.56 442	9.98 443	3	45 44	
	17	9.42 093	46	9.43 657	50	0.56 343	9.98 436	4	43	
	18	9.42 140	47 46	9.43 707	50	0.56 293	9.98 433	3	42	48 47 46
1	19	9.42 186	46	9.43 756	49 50	0.56 244	9.98 429	4	41	I 4.8 4.7 4.6
	20	9.42 232	46	9.43 806	49	0.56 194	9.98 426	4	40	2 9.6 9.4 9.2
1	2I 22	9.42 278	46	9.43 855	50	0.56 145	9.98 422	3	39 38	3 14.4 14.1 13.8
	23	9.42 324	46	9.43 905 9.43 954	49	0.56 095	9.98 419	4	37	4 19.2 18.8 18.4 5 24.0 23.5 23.0
1	24	9.42 416	46	9.44 004	50	0.55 996	9.98 412	3	36	6 28.8 28.2 27.6
ı	25	9.42 461	45 46	9.44 053	49 49	0.55 947	9.98 409	3 4	35	7 33.6 32.9 32.2 8 38.4 37.6 36.8
ı	26	9.42 507	46	9.44 102	49	0.55 898	9.98 405	3	34	8 38.4 37.6 36.8 9 43.2 42.3 41.4
ı	27 28	9.42 553 9.42 599	46	9.44 151	50	0.55 849	9.98 402	4	33 32	9 43.2 42.3 41.4
ı	29	9.42 644	45	9.44 250	49	0.55 750	9.98 395	3	31	
1	30	9.42 690	46	9.44 299	49	0.55 701	9.98 391	4	30	
ı	31	9.42 735	45	9.44 348	49	0.55 652	9.98 388	3	29	
ı	32	9.42 781	46 45	9.44 397	49 49	0.55 603	9.98 384	4 3	28	45 44
ı	33	9.42 826	46	9.44 446	49	0.55 554	9.98 381	4	27	I 4.5 4.4
	34 35	9.42 917	45	9.44 495 9.44 544	49	0.55 505	9.98 377	4	25	2 9.0 8.8
ı	36	9.42 962	45	9.44 592	48	0.55 408	9.98 370	3	24	3 13.5 13.2
ı	37	9.43 008	46 45	9.44 641	49	0.55 359	9.98 366	4 3	23	4 18.0 17.6 5 22.5 22.0
	38 39	9.43 053 9.43 098	45	9.44 690	48	0.55 310	9.98 363 9.98 359	4	22 2I	5 22.5 22.0 6 27.0 26.4
_	39 40	9.43 143	45	9.44 738	49	0.55 213	9.98 356	3	20	7 31.5 30.8 8 36.0 35.2
-	41	9.43 188	45	9.44 836	49	0.55 164	9.98 352	4	19	8 36.0 35.2 9 40.5 39.6
	42	9.43 233	45	9.44 884	48	0.55 116	9.98 349	3	18	314-13 37.3
i	43	9.43 278	45 45	9.44 933	49 48	0.55 067	9.98 345	4 3	17	
	44	9.43 323	44	9.44 981	48	0.55 019	9.98 342	4	16	
1	45 46	9.43 367 9.43 412	45	9.45 029 9.45 078	49	0.54 971	9.98 338	4	15	
	47	9.43 457	45	9.45 126	48	0.54 874	9.98 331	3	13	4 3
	48	9.43 502	45 44	9.45 174	48 48	0.54 826	9.98 327	4 3	12	1 0.4 0.3
1	49 50	9.43 546	45	9.45 222	49	0.54 778	9.98 324	4	II	2 0.8 0.6
		9.43 591	44	9.45 271	48	0.54 729	9.98 320	3	10	3 I.2 0.9 4 I.6 I.2
	51 52	9.43 635 9.43 680	45	9.45 319	48	0.54 681	9.98 317	4	8	
	53	9.43 724	44	9.45 415	48	0.54 585	9.98 309	4	7	5 2.0 I.5 6 2.4 I.8
	54	9.43 769	45	9.45 463	48	0.54 537	9.98 306	3	6	7 2.8 2.1 8 3.2 2.4
	55 56	9.43 813	44	9.45 511	48 48	0.54 489	9.98 302	4	5	9 3.6 2.7
	57	9.43 857	44	9.45 559	47	0.54 441	9.98 299	4	3	
	58	9.43 946	45	9.45 654	48	0.54 346	9.98 291	4	2	
	59	9.43 990	44 44	9.45 702	48 48	0.54 298	9.98 288	3	I	
	60	9.44 034		9.45 750	40	0.54 250	9.98 284	-	0	
		L Cos	d	L Cot	cd	L Tan	L Sin	d	'	PP

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		16°						T.	63°	
	′	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
ı	0	9.44 034	44	9.45 750	47	0.54 205	9.98 284	3	60	
ı	1	9.44 078	44	9.45 797	48	0.54 203	9.98 281	4	59	
ı	3	9.44 122 9.44 166	44	9.45 845	47	0.54 155	9.98 277	4	58 57	
ı	4	9.44 210	44	9.45 940	48	0.54 060	9.98 270	3	56	48 47 46
ı	5	9.44 253	43	9.45 987	47 48	0.54 013	9.98 266	4	55	1 4.8 4.7 4.6
ı	6	9.44 297 9.44 341	44	9.46 0 35 9.46 0 82	47	0.53 965	9.98 262	3	54	2 9.6 9.4 9.2 3 14.4 14.1 13.8
ı	8	9.44 341	44	9.46 130	48	0.53 870	9.98 255	4	52	3 14.4 14.1 13.8 4 19.2 18.8 18.4
ı	9	9.44 428	43	9.46 177	47	0.53 823	9.98 251	4	51	5 24.0 23.5 23.0
ı	10	9.44 472	44	9.46 224	47	0.53 776	9.98 248	4	50	
ł	II I2	9.44 516 9.44 559	43	9.46 271	48	0.53 729	9.98 244 9.98 240	4	49 48	7 33.6 32.9 32.2 8 38.4 37.6 36.8
ı	13	9.44 602	43	9.46 366	47	0.53 634	9.98 237	3	47	9 43.2 42.3 41.4
ı	14	9.44 646	44	9.46 413	47	0.53 587	9.98 233	4	46	
ı	15 16	9.44 689	43 44	9.46 460	47	0.53 540	9.98 229	3	45	
ı	17		43	9.46 554	47	0.53 446	9.98 222	4	43	
	18	9.44 776	43	9.46 601	47 47	0.53 399	9.98 218	4	42	45 44 43
	19 20	9.44 862	43	9.46 648	46	0.53 352	9.98 215	4	41 40	
	21	9.44 905	43	9.46 741	47	0.53 306	9.98 211	4	39	2 9.0 8.8 8.6
ı	22	9.44 940	44	9.46 788	47	0.53 259	9.98 204	3	38	3 13.5 13.2 12.9 4 18.0 17.6 17.2
ı	23	9.45 035	43	9.46 835	47 46	0.53 165	9.98 200	4	37	5 22.5 22.0 21.5 6 27.0 26.4 25.8
ı	24 25	9.45 077 9.45 120	43	9.46 881	47	0.53 119	9.98 196 9.98 192	4	36	
ı	26	9.45 163	43	9.46 975	47	0.53 025	9.98 189	3	34	7 31.5 30.8 30.1 8 36.0 35.2 34.4
ı	27	9.45 206	43	9.47 021	46 47	0.52 979	9.98 185	4	33	9 40.5 39.6 38.7
ı	28	9.45 249 9.45 292	43	9.47 068	46	0.52 932 0.52 886	9.98 181 9.98 177	4	32 31	
ı	30	9.45 334	42	9.47 160	46	0.52 840	9.98 174	3	30	
ı	31	9.45 377	43	9.47 207	47	0.52 793	9.98 170	4	29	
ı	32	9.45 419	42	9.47 253	46 46	0.52 747	9.98 166	4	28	42 41
ł	33	9.45 462	43	9.47 299	47	0.52 701	9.98 162	3	27	I 4.2 4.1
ı	35	9.45 504 9.45 547	43	9.47 346	46	0.52 608	9.98 155	4	25	2 8.4 8.2
ı	36	9.45 589	42	9.47 438	46 46	0.52 562	9.98 151	4	24	3 12.6 12.3
ı	37 38	9.45 632	42	9.47 484 9.47 530	46	0.52 516	9.98 147 9.98 144	3	23	4 16.8 16.4 5 21.0 20.5
ı	39	9.45 716	42	9.47 576	46	0.52 424	9.98 140	4	2 I	6 25.2 24.6
	40	9.45 758	42	9.47 622	46	0.52 378	9.98 136	4	20	7 29.4 28.7 8 33.6 32.8
	4I	9.45 801	43	9.47 668	46 46	0.52 332	9.98 132	4	19	9 37.8 36.9
	42 43	9.45 843 9.45 885	42	9.47 714 9.47 760	46	0.52 286	9.98 129	4	18	
	44	9.45 927	42	9.47 700	46	0.52 194	9.98 121	4	16	
	45	9.45 969	42 42	9.47 852	46 45	0.52 148	9.98 117	4	15	
	46	9.46 011	42	9.47 897	46	0.52 103	9.98 113	3	14	
1	48	9.46 095	42	9.47 989	46	0.52 011	9.98 106	4	12	4 3
1	49	9.46 136	41 42	9.48 035	46 45	0.51 965	9.98 102	4	II	1 0.4 0.3 2 0.6
ı	50	9.46 178	42	9.48 080	46	0.51 920	9.98 098	4	10	3 1.2 0.9
1	51 52	9.46 220	42	9.48 126 9.48 171	45	0.51 874	9.98 094	4	9 8	4 I.6 I.2 5 2.0 I.5
1	53	9.46 303	41	9.48 217	46	0.51 783	9.98 090	3	7	6 2.4 1.8
1	54	9.46 345	42 41	9.48 262	45	0.51 738	9.98 083	4	6	7 2.8 2.1
ı	55 56	9.46 386	41	9.48 307 9.48 353	45 46	0.51 693	9.98 079	4 4	5 4	8 3.2 2.4 9 3.6 2.7
I	57	9.46 469	41	9.48 398	45	0.51 602	9.98 071	4	3	, , , , ,
1	58	9.46 511	42 41	9.48 443	45 46	0.51 557	9.98 067	4	2 I	
١	59 60	9.46 552	42	9.48 489	45	0.51 511	9.98 063	3	0	
ŀ	-	L Cos		L Cot	c d	L Tan	L Sin		,	PP
					- 4					

17	L Sin	d	L Tan	c d	L Cot	L Cos	d		РР
0	9.46 594	_	9.48 534	_	0.51 466	9.98 060	<u>u</u>	60	
1	9.46 635	41	9.48 579	45	0.51 421	9.98 056	4	59	
2	9.46 676	41	9.48 624	45	0.51 376	9.98 052	4	58	
3	9.46 717	4I 4I	9.48 669	45 45	0.51 331	9.98 048	4	57	
4	9.46 758 9.46 800	42	9.48 714	45	0.51 286	9.98 044	4	56	
5 6	9.46 841	41	9.48 759 9.48 804	45	0.51 241	9.98 0 40 9.98 0 36	4	55 54	
7	9.46 882	41	9.48 849	45	0.51 151	9.98 032	4	53	
8	9.46 923	41	9.48 894	45	0.51 106	9.98 029	3	52	45 44 43
9	9.46 964	4I 4I	9.48 939	45 45	0.51 061	9.98 025	4	51	
10	9.47 005	40	9.48 984	45	0.51 016	9.98 021	4	50	1 4.5 4.4 4.3 2 9.0 8.8 8.6
II	9.47 045	41	9.49 029	44	0.50 971	9.98 017	4	-49	3 13.5 13.2 12.9
12	9.47 086 9.47 127	41	9.49 073	45	0.50 927	9.98 o13 9.98 oo9	4	48 47	4 18.0 17.6 17.2 5 22.5 22.0 21.5
14	9.47 168	41	9.49 163	45	0.50 837	9.98 005	4	46	6 27.0 26.4 25.8
15	9.47 209	4I 40	9.49 207	44	0.50 793	9.98 001	4	45	7 31.5 30.8 30.1
16	9.47 249	41	9.49 252	45 44	0.50 748	9.97 997	4	44	8 36.0 35.2 34.4 9 40.5 39.6 38.7
17 18	9.47 290 9.47 330	40	9.49 296	45	0.50 704	9.97 993 9.97 989	4	43	9 1 40.5 39.0 30.7
19	9.47 371	41	9.49 385	44	0.50 615	9.97 986	3	41	
20	9.47 411	40	9.49 430	45	0.50 570	9.97 982	4	40	
21	9.47 452	41	9.49 474	44	0.50 526	9.97 978	4	39	
22	9.47 492	40	9.49 519	45	0.50 481	9.97 974	4	38	
23	9.47 533	4I 40	9.49 563	44 44	0.50 437	9.97 970	4	37	
24	9.47 573	40	9.49 607	45	0.50 393	9.97 966 9.97 962	4	36 35	42 41 40
26	9.47 654	41	9.49 696	44	0.50 340	9.97 958	4	34	
27	9.47 694	40	9.49 740	44	0.50 260	9.97 954	4	33	I 4.2 4.I 4.0 2 8.4 8.2 8.0
28	9.47 734	40 40	9.49 784	44 44	0.50 216	9.97 950	4	32	3 12.6 12.3 12.0
29	9.47 774	40	9.49 828	44	0.50 172	9.97 946	4	31	4 16.8 16.4 16.0
30	9.47 814	40	9.49 872	44	0.50 1 28	9.97 942	4	30	5 21.0 20.5 20.0 6 25.2 24.6 24.0
31 32	9.47 854	40	9.49 916	44	0.50 084	9.97 938 9.97 934	4	29 28	7 29.4 28.7 28.0
33	9.47 934	40	9.49 900	44	0.49 996	9.97 934	4	27	
34	9.47 974	40	9.50 048	44	0.49 952	9.97 926	4	26	9 37.8 36.9 36.0
35	9.48 014	40 40	9.50 092	44 44	0.49 908	9.97 922	4	25	
36	9.48 054	40	9.50 136	44	0.49 864	9.97 918	4	24 23	
37 38	9.48 133	39	9.50 223	43	0.49 777	9.97 914	4	23	
39	9.48 173	40	9.50 267	44	0.49 733	9.97 906	4	21	
40	9.48 213	40	9.50 311	44	0.49 689	9.97 902	4	20	
41	9.48 252	39	9.50 355	44	0.49 645	9.97 898	4	19	
42	9.48 292	40 40	9.50 398	43 44	0.49 602	9.97 894	4	18	39 5 4 3
43	9.48 332	39	9.50 442	43	0.49 558	9.97 890 9.97 886	4	17	I 3.9 0.5 0.4 0.3 2 7.8 1.0 0.8 0.6
44 45	9.48 411	40	9.50 405	44	0.49 313	9.97 882	4	15	2 7.8 1.0 0.8 0.6 3 11.7 1.5 1.2 0.9
46	9.48 450	39 40	9.50 572	43	0.49 428	9.97 878	4	14	4 15.6 2.0 1.6 1.2
47	9.48 490	39	9.50 616	44	0.49 384	9.97 874	4	13	5 19.5 2.5 2.0 1.5 6 23.4 3.0 2.4 1.8
48 49	9.48 529 9.48 568	39	9.50 659	44	0.49 341	9.97 870 9.97 866	4	12	
50	9.48 607	39	9.50 746	43	0.49 254	9.97 861	5	10	8 31.2 4.0 3.2 2.4
51	9.48 647	40	9.50 789	43	0.49 211	9.97 857	4	9	9 35.1 4.5 3.6 2.7
52	9.48 686	39	9.50 833	44	0.49 167	9.97 853	4	8	
53	9.48 725	39	9.50 876	43	0.49 124	9.97 849	4	7	
54	9.48 764	39	9.50 919	43	0.49 081	9.97 845	4	6	
55 56	9.48 803	39	9.50 962	43	0.49 038	9.97 841	4	5 4	
	9.48 881	39	9.51 048	43	0.48 952	9.97 833	4	3	
57 58	9.48 920	39	9.51 092	44	0.48 908	9.97 829	4	2	
59	9.48 959	39	9.51 135	43	0.48 865	9.97 825	4	I	
60	9.48 998	d	9.51 178		0.48 822	9.97 821	d	0	PP
	L Cos	u	L Cot	cd	L Tan	LSin	a	Ĺ	

1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.48 998		9.51 178	_	0.48 822	9.97 821		60	
I	9.49 037	39	9.51 221	43	0.48 779	9.97 817	4	59	
2	9.49 076	39	9.51 264	43 42	0.48 736	9.97 812	5 4	58	
3 4	9.49 115	38	9.51 306	43	0.48 694	9.97 808	4	57 56	
5	9.49 192	39	9.51 349	43	0.48 608	9.97 800	4	55	
6	9.49 231	39 38	9.51 435	43 43	0.48 565	9.97 796	4	54	
7 8	9.49 269 9.49 308	39	9.51 478	42	0.48 522 0.48 480	9.97 792 9.97 788	4	53	
9	9.49 347	39	9.51 563	43	0.48 437	9.97 784	4	52 51	43 42 41
10	9.49 385	38	9.51 606	43	0.48 394	9.97 779	5	50	I 4.3 4.2 4.1 2 8.6 8.4 8.2
11	9.49 424	39	9.51 648	42	0.48 352	9.97 775	4	49	3 12.9 12.6 12.3
12	9.49 462	38 38	9.51 691	43 43	0.48 309	9.97 771	4	48	4 17.2 16.8 16.4
13	9.49 500	39	9.51 734	42	0.48 266	9.97 767	4	47 46	5 21.5 21.0 20.5 6 25.8 25.2 24.6
15	9.49 577	38	9.51 819	43	0.48 181	9.97 759	4	45	7 30.1 29.4 28.7
16	9.49 615	38 39	9.51 861	42 42	0.48 139	9.97 754	5	44	8 34.4 33.6 32.8 9 38.7 37.8 36.9
17 18	9.49 654 9.49 692	38	9.51 903	43	0.48 097	9.97 750	4	43	9 30.7 37.0 30.9
19	9.49 730	38	9.51 988	42	0.48 012	9.97 740	4	42 4I	
20	9.49 768	38	9.52 031	43	0.47 969	9.97 738	4	40	
21	9.49 806	38	9.52 073	42	0.47 927	9.97 734	4	39	
22 23	9.49 844 9.49 882	38 38	9.52 115	42 42	0.47 885	9.97 729	5 4	38	
24	9.49 920	38	9.52 157	43	0.47 843	9.97 725 9.97 721	4	37 36	
25	9.49 958	38	9.52 242	42	0.47 758	9.97 717	4	35	
26	9.49 996	38 38	9.52 284	42	0.47 716	9.97713	5	34	39 38 37
27 28	9.50 034	38	9.52 326 9.52 368	42	0.47 674	9.97 708	4	33	1 3.9 3.8 3.7
29	9.50 110	38	9.52 410	42	0.47 590	9.97 704	4	32 31	2 7.8 7.6 7.4
30	9.50 148	38	9.52 452	42	0.47 548	9.97 696	4	30	4 15.6 15.2 14.8
31	9.50 185	37	9.52 494	42	0.47 506	9.97 691	5	29	5 19.5 19.0 18.5
32	9.50 223	38 38	9.52 536	42 42	0.47 464	9.97 687	4	28	6 23.4 22.8 22.2 7 27.3 26.6 25.9
33	9.50 261	37	9.52 578	42	0.47 422 0.47 380	9.97 683	4	27 26	8 31.2 30.4 29.6
35	9.50 336	38	9.52 661	41	0.47 339	9.97 674	5	25	9 35.1 34.2 33.3
36	9.50 374	38 37	9.52 703	42	0.47 297	9.97 670	4	24	
37 38	9.50 411	38	9.52 745 9.52 787	42 42	0.47 255	9.97 666 9.97 662	4	23	
39	9.50 486	37	9.52 829	42	0.47 213	9.97 657	5	21 2I	
40	9.50 523	37	9.52 870	41	0.47 130	9.97 653	4	20	
41	9.50 561	38	9.52 912	42	0.47 088	9.97 649	4	19	
42	9.50 598	37 37	9.52 953	4I 42	0.47 047	9.97 645	4 5	18	
43	9.50 635	38	9.52 995	42	0.47 005	9.97 640	4	17 16	36 5 4
45	9.50 710	37	9.53 037	41	0.46 922	9.97 632	4	15	1 3.6 0.5 0.4
46	9.50 747	37	9.53 120	42	0.46 880	9.97 628	4 5	14	2 7.2 1.0 0.8
47 48	9.50 784	37	9.53 161	4I 4I	0.46 839	9.97 623	4	13	3 10.8 1.5 1.2
49	9.50 858	37	9.53 202	42	o.46 798 o.46 756	9.97 619 9.97 615	4	12 11	4 14.4 2.0 1.6 5 18.0 2.5 2.0
50	9.50 896	38	9.53 285	41	0.46 715	9.97 610	5	10	6 21.6 3.0 2.4
51	9.50 933	37	9.53 327	42	0.46 673	9.97 606	4	9	7 25.2 3.5 2.8 8 28.8 4.0 3.2
52	9.50 970	37	9.53 368	41	0.46 632	9.97 602	4 5	8	9 32.4 4.5 3.6
53	9.51 007	37 36	9.53 409	41	0.46 591	9.97 597	4	7 6	
54	9.51 043	37	9.53 450	42	0.46 550	9.97 593 9.97 589	4	5	
56	9.51 117	37	9.53 533	4I	0.46 467	9.97 584	5	4	
57 58	9.51 154	37 37	9.53 574	4I 4I	0.46 426	9.97 580	4	3	
59	9.51 191 9.51 227	36	9.53 615 9.53 656	41	0.46 385	9.97 576 9.97 571	5	2 I	
60	9.51 264	37	9.53 697	41	0.46 303	9.97 567	4	0	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	7	PP

19° 160°

Column C	_	10						_	.00	
1	1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
1 9.51 338 37 9.53 379 41 0.46 221 9.97 538 5 58 74 74 75 75 75 75 75 75	0	9.51 264	25	9.53 697	47	0.46 303	9.97 567	,	60	
3 9.51 374 37 6 9.53 861 41 0.46 180 9.97 554 4 57 6 9.51 447 37 9.51 53 902 41 7 0.46 0.89 9.97 555 5 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1		1	9.53 738				i	59	
4 9.51 41 36 0.53 801 41 0.40 0.40 0.95 0.97 545 55 55 55 55 55 55			37	9.53 779		0.46 221				
4 9.51 447 36 9.53 992 41 0.46 0x6 9y7 9y7 545 45 55 58 79 9.51 557 37 9.54 0x5 41 0.46 0x6 9y7 9y7 536 58 58 58 79 9.51 557 37 9.54 0x5 41 0.46 0x6 9y7 528 45 51 1 4.1 4.0 4.1				9.53 820						
6 9.51 484 37 9.53 943 41 0.46 016 9 9.97 536 53 41 40 40 40 40 40 40 40				0.53 002		0.46 008		5		
7 9.51 520 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 36 9.54 905 905 36 9.54 905	6		37							
10 0.51 629 730	7			9.53 984						
10			37	9.54 025						41 40 39
11 9.51 666 37 9.54 147 40 0.45 853 9.97 519 4 40 40 41 16.0 61 62 62 62 62 62 62 62			36							
11 9.51 000 36 9.54 1487 40 0.45 873 9.97 515 4 48 48 16.4 16.1 17.5 17.5 18.1 17.5 18.1 17.5 18.1 17.5 18.1 17.5 18.1 17.5 18.1	10							1	50	2 8.2 8.0 7.8
13				9.54 147				1		3 12.3 12.0 11.7 4 16.4 16.0 15.6
15 9.51 847 36 9.54 359 40 0.45 650 9.97 500 5 45 7 28.7 28.0			36							
15			36					4		
17 9.51 883 36 9.54 390 36.		9.51 811				0.45 691				7 28.7 28.0 27.3
18 9.51 9.19 36 9.54 4.31 40 9.51 9.51 9.51 9.51 9.51 9.51 9.51 9.51 9.51 9.51 9.52 9.52 9.52 0.32 36 9.54 5.31 9.54 5.31 9.54 5.31 9.54 5.31 9.54 5.32 9.52 0.32 9.52 0.32 36 9.54 6.33 40 0.45 5.29 9.97 4.84 4 41 41 41 41 42 42 42	_									
10										9130.9 30.0 33.1
20									42	
21 9.52 063 36 9.54 552 40 0.45 448 9.97 475 5 38 38 25 9.52 171 36 9.54 633 41 0.45 269 9.97 457 42 9.52 217 36 9.54 754 40 0.45 269 9.97 457 40 0.45 269 9					41			5		
22			36		40			4	1 1	
24			36						38	
25 9.52 171 36 9.54 714 40 9.52 267 36 9.54 714 40 9.52 267 37 9.52 278 36 9.54 835 41 0.45 165 9.97 444 45 32 27 7.4 7.2 7.2 7.2 7.2 7.4 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2	23						9.97 466			
26 9.52 207 36 9.54 754 40 0.45 206 9.97 453 4 33 33 1 3.7 3.6 28 9.52 278 36 9.54 858 40 0.45 206 9.97 448 4 32 2 7.4 7.2 29 9.52 315 36 9.54 858 40 0.45 206 9.97 435 5 31 3 3 3 3 3 3 3 30 9.52 358 35 9.54 995 40 0.45 205 9.97 448 4 32 2 7.4 7.2 33 9.52 450 35 9.54 995 40 0.45 205 9.97 426 4 28 7 25.9 34 9.52 492 35 9.55 255 40 0.44 968 9.97 421 5 5 35 9.52 527 35 9.55 195 40 0.45 205 9.97 448 4 32 2 7.4 7.2 35 9.52 528 36 9.55 255 40 0.44 968 9.97 421 5 5 36 9.52 506 35 9.55 255 40 0.44 865 9.97 403 5 37 9.52 508 36 9.55 255 40 0.44 865 9.97 303 5 40 9.52 705 35 9.55 315 40 0.44 685 9.97 303 5 41 9.52 740 44 9.52 846 45 9.55 355 40 0.44 685 9.97 309 5 42 9.52 778 35 9.55 514 40 0.44 685 9.97 305 5 43 9.52 986 35 9.55 514 40 0.44 685 9.97 305 5 44 9.52 846 35 9.55 514 40 0.44 685 9.97 305 5 45 9.52 986 35 9.55 514 40 0.44 685 9.97 305 5 46 9.52 916 35 9.55 514 40 0.44 685 9.97 305 5 47 9.52 928 35 9.55 514 40 0.44 685 9.97 305 5 48 9.52 926 35 9.55 514 40 0.44 685 9.97 305 5 49 9.53 021 35 9.55 573 0.44 406 9.97 335 5 9.53 320 35 9.55 573 0.44 407 9.97 335 5 9.53 321 35 9.55 91 9.55 9										
28	25	9.52 171								37 36 35
28										
29	28			9.54 835						
31 9.52 358 35 9.54 955 35 9.54 955 36 9.55 955 36 9.55 955 37 9.52 598 38 9.52 956 35 9.55 275 35 9.52 276 36 9.52 276 37 9.52 278 37 9.52 278 38 9.52 264 38 9.52 264 38 9.52 264 38 9.52 278 38 9.52 264 38 9.52 264 38 9.52 264 38 9.52 278 38 9.52 264 38 9.52 264 38 9.52 264 38 9.52 278 38 9.52 264 38 9.52 278 38 9.52 27	29					0.45 125	9.97 439			
33 9.52 421 36 9.54 995 40 0.45 045 9.97 426 4 28 9.97 427 3 3 3 3 3 3 3 3 3	30	9.52 350		9.54 915		0.45 085	9.97 435		30	
33 9.52 492 36 34 9.52 973 36 9.55 935 40 0.44 985 9.97 421 5 27 7 25.9 28.8 32.4 26 29.5 27.5 36 29.5 27.5 36 29.5 27.5 36 29.5 27.5 36 29.5 27.5 36 29.5 27.5 36 29.5 27.5 37.5 36 29.5 27.5 37.5 36 29.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 36.5 27.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 37.5 36.5 27.5 36.		9.52 385			1 1			l .		
34										7 25.9 25.2 24.5
35			36							
36 9.52 563 35 9.55 195 40 0.44 865 9.97 408 4 224 33 9.952 669 35 9.55 235 40 0.44 765 9.97 399 4 222 22 22 22 22 22 22 22 22 22 22 22						0.44 885				9 33.3 32.4 31.5
38 9.52 659 36	36	9.52 563				0.44 845	9.97 408			
39 9.52 669 36 9.55 275 40 9.52 775 35 9.55 375 36 9.55 385 36 9.55 385 46 9.52 881 36 9.52 881 36 9.52 881 36 9.55 385 46 9.52 881 36 9.55 385 46 9.52 986 35 9.55 574 46 9.52 986 35 9.55 574 47 9.52 986 35 9.55 581 48 9.52 986 35 9.55 574 49 9.53 3021 35 9.55 593 49 9.53 3021 35 9.55 575 49 9.53 3021 35 9.55 575 49 9.53 3021 35 9.55 575 49 9.53 3021 35 9.55 575 49 9.53 3021 35 9.55 575 49 9.53 3021 35 9.55 573 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.53 301 35 9.55 575 49 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.55 752 9.	37	9.52 598								
40 9.52 755 740 741 741 742 742 743 744 745	30					0.44 705				
41 9.52 7.75 35 9.55 355 40 0.44 645 9.97 3.85 5 19 19 44 65 9.97 3.85 5 17 34 5 45 9.52 881 35 9.55 534 40 9.52 9.52 881 35 9.55 534 40 9.52 9.52 9.53 35 9.55 554 40 9.52 9.53 35 9.55 554 40 9.53 321 35 9.55 573 35 9.55 573 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357 35 9.55 357			36		40					
42 9.52 775 35 9.55 344 49.52 846 45 9.52 881 35 9.55 474 49.52 9.51 35 9.55 574 49 9.53 021 35 9.55 594 99.53 021 35 9.55 021 35 9.			35		40			5		
44 9.52 841 35 9.55 474 40 0.44 526 9.97 376 5 17 44 56 9.52 881 35 9.55 574 40 0.44 428 9.97 367 5 15 17 3.4 0.5 14 3.6 1.5 1.5 17 3.4 0.5 1.5 17 1.5 1.5 17 1.5 1.5 17 1.5 1.5 17 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5			35				9.97 381			
44 9.52 846 35 9.55 81 35 9.55 514 40 9.97 372 4 16 16 1 3.4 0.5 16 16 9.52 916 35 9.55 514 30 9.55 514 30 9.52 986 35 9.55 533 30 9.55 533 30 9.55 573 40 9.53 376 35 9.55 752 9.53 3126 34 9.55 752 9.53 3126 34 9.55 752 9.53 3126 34 9.55 752 9.53 3126 35 9.55 870 35 9.55 919 35 9.55 919 35 9.55 919 30.44 919 9.97 332 4 5 5 6 6 6 70 50 50 9.53 370 35 9.55 919 30 0.44 150 9.97 312 5 5 8 9.55 3370 35 9.55 919 30 0.44 919 9.97 317 5 4 9.55 919 30.40 9.97 317 5 9.55 919 30.40 9.97 317 5 9.55 919 30.40 9.97 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55 919 30.40 919 317 5 9.55		9.52 811				0.44 566				34 5 4
46 9.52 916 35 9.55 554 40 9.53 61 15 2 6.8 1.0 10.2 1.5 10.2 10.2 1.5 10.2 10.2 1.5 10.2 10.2 1.5 10.2 10.2 10.2 10.2 1.5 10.2 10.2 10.2 10.2 1.5 10.2 10.2 10.2 10.2 10.2 10.2 10.2 1		9.52 846				0.44 526				
47 9.52 951 35 9.55 593 39 0.44 407 9.97 358 5 13 31 0.2 1.5 48 9.52 951 35 9.55 593 40 0.44 367 9.97 353 5 12 5 17.0 2.5 50 9.53 021 35 9.55 752 39 0.44 288 9.97 344 4 11 6 20.43 30. 51 9.53 161 35 9.55 752 39 0.44 248 9.97 344 4 10 7 23.8 3.5 54 9.53 261 35 9.55 831 30 9.55 873 39 0.44 248 9.97 3345 5 8 27.2 4.0 55 9.53 266 35 9.55 910 30 0.44 290 9.97 335 5 8 27.2 4.0 56 9.53 266 35 9.55 910 30 0.44 130 9.97 326 5 6 6 0.44 90 9.97 331 5 4 7 2.3.8 3.5 9.55 910 9 0.44 90 9.97 337 5 4 4 <td< td=""><td></td><td>9.52 016</td><td></td><td></td><td></td><td>0.44 480</td><td></td><td></td><td></td><td>2 6.8 1.0 0.8</td></td<>		9.52 016				0.44 480				2 6.8 1.0 0.8
48 9.52 986 35 9.55 673 36 9.55 673 37 39 9.55 752 39 9.53 326 35 9.55 873 39 9.55 873 39 9.53 326 35 9.55 873 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 874 39 9.53 326 35 9.55 949 30 30 30 30 30 30 30 3					39					3 10.2 1.5 1.2
49 9.53 o21 35 9.55 712 9 9.53 75 5 9 9.53 370 60 9.53 340 5 9 9.53 370 60 9.53 370 60 9.53 370 60 9.53 340 5 9.55 607 3 9 9.53 370 60 9.53 340 5 9.55 607 3 9 9.53 370 60 9.53 340 5 9.55 607 3 9 9.53 370 60 9.53 340 5 9.55 607 3 9 9.53 370 60 9.53 340 5 9 9.53 370 60 9.	48			9.55 633						
50 0.53 056 51 36 9.53 026 9.53 161 35 35 9.55 712 40 9.55 791 0.44 288 9.97 344 9.97 344 9 9.97 335 40 9 8 9 9.73 315 3.5 8 27.2 4.5 4.5 53 9.53 161 35 9.55 831 9.55 831 40 9.55 90.55 40 9.52 90.55 910 0.44 288 9.97 344 9.97 344 9 9.97 331 4 7 7 7 23.8 8 27.2 3.5 9 9.55 831 56 9.53 206 9.53 306 35 9.55 959 9.53 370 35 9.56 288 9.56 28 39 9.56 028 0.44 130 9.97 317 9.97 317 5 9.44 051 5 9.97 317 9.44 051 5 9.97 317 9.44 051 4 9.97 317 9.97 317 9.97 308 4 4 9.97 317 5 4 9.43 933 9.97 303 5 4 9.43 933 9.97 303 5 5 8 9.43 939 9.97 299 4 9 10 7 2 3.8 8 27.2 3.5 6 9 30.6 4.5	49	9.53 021				0.44 327			II	
31 32 33 34 33 35 35 35 35 35	50	9.53 056		9.55 712		0.44 288	9.97 344		10	7 23.8 3.5 2.8
33 9.53 161 35 9.55 831 40 0.44 169 9.97 331 4 7 54 9.53 196 35 9.55 870 39 0.44 130 9.97 326 5 55 9.53 261 35 9.55 949 0.44 0.91 9.97 317 5 57 9.53 301 35 9.55 949 0.44 0.91 9.97 317 5 58 9.53 336 35 9.56 0.64 0.91 0.97 317 5 59 9.53 370 34 9.56 0.67 39 0.44 0.91 0.97 317 5 60 0.53 405 35 9.56 0.67 39 0.43 9.39 0.97 2.99 4 60 0.53 405 0.56 0.67 39 0.43 9.39 0.97 2.99 4 60 0.53 405 0.56		9.53 092			1				9	
54 0.53 196 35 0.55 870 39 0.44 130 9.97 326 5 6 55 9.53 266 35 9.55 949 40 0.44 900 9.97 322 4 5 57 9.53 336 35 9.55 989 40 0.44 901 9.97 317 5 4 58 9.53 370 35 9.56 028 39 0.43 91 9.97 312 5 3 59 9.53 370 34 9.56 067 39 0.43 933 9.97 303 5 1 60 9.53 405 35 9.56 107 40 0.43 933 9.97 299 4 0				9.55 791						9 30.0 4.3 3.0
55 9.53 231 35 9.55 910 40 0.44 090 9.07 322 4 5 5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5									6	
56 0.53 266 35 0.55 949 39 0.44 051 9.07 317 5 4 57 9.53 336 35 9.55 989 40 0.44 051 9.07 317 5 3 59 9.53 336 35 9.56 028 39 0.43 972 9.97 303 4 2 59 9.53 370 35 9.56 067 39 0.43 933 9.97 303 5 1 60 9.53 405 9.56 107 40 0.43 933 9.97 299 4 0	55	9.53 231								
57 9.53 336 35 9.56 028 39 0.43 972 9.97 303 4 2 2 3 3 4 0.56 07 40 0.43 933 9.97 303 5 1 0.43 933 9.97 303 5 1 0.43 933 9.97 299 4 0	56	9.53 266		9.55 949		0.44 051	9.97 317			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	57			9.55 989						
60 9.53 405 35 9.56 107 40 0.43 893 9.97 299 4 0				9.50 028						
L Cos d L Cot cd L Tan L Sin d ' P P		L Cos	d	L Cot	c d	L Tan	L Sin	d	7	PP

1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.53 405	25	9.56 107	39	0.43 893	9.97 299		60	
1		35	9.56 146	39	0.43 854	9.97 294	5	59	
3		34	9.56 185	39	0.43 815	9.97 289 9.97 285	4	58	
4	1	35	9.56 264	40	0.43 736	9.97 280	5	56	
5	9.53 578	34	9.56 303	39 39	0.43 697	9.97 276	5	55	
		34	9.56 342	39	0.43 658	9.97 271	5	54	
7 8	9.53 682	35	9.56 420	39	0.43 580	9.97 262	4	53	40 39 38
9	9.53 716	34	9.56 459	39	0.43 541	9.97 257	5	51	
10	200.0	34	9.56 498	39	0.43 502	9.97 252	5	50	1 4.0 3.9 3.8 2 8.0 7.8 7.6
II	9.53 785	34	9.56 537	39	0.43 463	9.97 248	5	49	3 12.0 11.7 11.4
13	9.53 819 9.53 854	35	9.56 576 9.56 615	39	0.43 424 0.43 385	9.97 243 9.97 238	5	48	
14		34	9.56 654	39	0.43 346	9.97 234	4	46	
15	9.53 922	34	9.56 693	39	0.43 307	9.97 229	5	45	7 28.0 27.3 20.0
16	9.53 957	34	9.56 732	39 39	0.43 268	9.97 224	5	44	0 260 257 242
17	9.53 991 9.54 025	34	9.56 771	39	0.43 229	9.97 220	5	43	
19	9.54 059	34	9.56 849	39	0.43 151	9.97 210	5	41	
20	9.54 093	34	9.56 887	38	0.43 113	9.97 206	4	40	
21	9.54 127	34	9.56 926	39	0.43 074	9.97 201	5	39	
22		34	9.56 965	39 39	0.43 035	9.97 196	5	38	
23 24	9.54 195	34	9.57 004	38	0.42 996	9.97 192	5	37	
25	9.54 263	34	9.57 081	39	0.42 930	9.97 182	5	35	
26	9.54 297	34	9.57 120	39	0.42 880	9.97 178	4	34	37 35 34
27 28	9.54 331	34	9.57 158	38	0.42 842	9.97 173	5 5	33	
29	9.54 365 9.54 399	34	9.57 197 9.57 235	38	0.42 803	9.97 168	5	32 31	
30	9.54 433	34	9.57 274	39	0.42 726	9.97 159	4	30	4 14.8 14.0 13.6
31	9.54 466	33	9.57 312	38	0.42 688	9.97 154	5	20	5 18.5 17.5 17.0
32		34 34	9.57 351	39	0.42 649	9.97 149	5	28	
33	9.54 534	33	9.57 389	38	0.42 611	9.97 145	5	27	8 29.6 28.0 27.2
34 35	9.54 567 9.54 601	34	9.57 428 9.57 466	38	0.42 572	9.97 I40 9.97 I35	5	26	7 7 33.3 34.3
36	9.54 635	34	9.57 504	38	0.42 496	9.97 130	5	24	
37	9.54 668	34	9.57 543	39	0.42 457	9.97 126	4	23	1
38	9.54 702	33	9.57 581	38 38	0.42 419	9.97 121	5	22 2I	
40	9.54 735	34	9.57 658	39	0.42 381		5	20	
41	9.54 802	33	9.57 696	38	0.42 342	9.97 111	4	19	
42	9.54 836	34	9.57 734	38	0.42 304	9.97 107	5	18	
43	9.54 869	34	9.57 772	38 38	0.42 228	9.97 097	5 5	17	33 5 4
44 45	9.54 903	33	9.57 810	39	0.42 190	9.97 092 9.97 087	5	16	1 3.3 0.5 0.4
45	9.54 969	33	9.57 887	38	0.42 151	9.97 083	4	15	2 6.6 1.0 0.8
47	9.55 003	34	9.57 925	38	0.42 075	9.97 078	5	13	3 9.9 1.5 1.2 4 13.2 2.0 1.6
48	9.55 036	33	9.57 963	38 38	0.42 037	9.97 073	5	12	5 16.5 2.5 2.0
49 50	9.55 069	33	9.58 001	38	0.41 999	9.97 068	5	11 10	
51	9.55 102	34	9.58 077	38	0.41 961	9.97 063	4		7 23.I 3.5 2.8 8 26.4 4.0 3.2
52	9.55 169	33	9.58 115	38	0.41 923	9.97 059	5	9	9 29.7 4.5 3.6
53	9.55 202	33 33	9.58 153	38 38	0.41 847	9.97 049	5	7	
54	9.55 235	33	9.58 191	38	0.41 809	9.97 044	5	6	
55 56	9.55 268 9.55 301	33	9.58 229 9.58 267	38	0.41 771	9.97 039 9.97 035	4	5 4	
57	9.55 334	33	9.58 304	37	0.41 696	9.97 030	5	3	
58	9.55 367	33	9.58 342	38 38	0.41 658	9.97 025	5 5	2	
59 60	9.55 400	33	9.58 380	38	0.41 620	9.97 020	5	I	
٣	9-55 433 L Cos		9.58 418 L Cot	c d	0.41 582 L Tan	9.97 015 L Sin		,	РР
	- 003	u	_ 001	o u	- I all	- OIII	u		

110° (358) **69°**

21° 158°

	1 0:				1.0.	1.0.	, l		0.0
Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	_d_	_	PP
0	9.55 433	33	9.58 418	37	0.41 582	9.97 015	5	60	
1 2	9.55 466	33	9.58 455 9.58 493	38	0.41 545	9.97 010	5	59 58	
3	9.55 499 9.55 532	33	9.58 531	38	0.41 469	9.97 003	4	57	
4	9.55 564	32	9.58 569	38	0.41 431	9.96 996	5	56	
5	9.55 597	33	9.58 606	37 38	0.41 394	9.96 991	5 5	55	
6	9.55 630	33	9.58 644 9.58 681	37	0.41 356	9.96 986	5	54	
7 8	9.55 663	32	9.58 719	38	0.41 319	9.96 976	5	53	_
9	9.55 728	33	9.58 757	38	0.41 243	9.96 971	5	51	38 37 36
10	9.55 761	33	9.58 794	37 38	0.41 206	9.96 966	5	50	1 3.8 3.7 3.6
11	9.55 793	32	9.58 832	37	0.41 168	9.96 962	4 5	49	2 7.6 7.4 7.2 3 11.4 11.1 10.8
12	9.55 820	32	9.58 869 9.58 907	38	0.41 131	9.96 957	5:	48	4 15.2 14.8 14.4
13	9.55 858 9.55 891	33	9.58 944	37	0.41 056	9.96 932	5	47	5 19.0 18.5 18.0 6 22.8 22.2 21.6
15	9.55 923	32	9.58 981	37 38	0.41 019	9.96 942	5	45	
16	9.55 956	33 32	9.59 019	38	0.40 981	9.96 937	5	44	8 30.4 29.6 28.8
17	9.55 988	33	9.59 056	38	0.40 944	9.96 932	5	43	9 34.2 33.3 32.4
10	9.56 o21 9.56 o53	32	9.59 094 9.59 131	37	0.40 960	9.96 927	5	42 41	
20	9.56 085	32	9.59 168	37	0.40 832	9.96 917	5	40	
21	9.56 118	33	9.59 205	37	0.40 795	9.96 912	5	39	
22	9.56 150	32	9.59 243	38	0.40 757	9.96 907	5	38	
23	9.56 182	32	9.59 280	37 37	0.40 720	9.96 903	4 5	37	
24 25	9.56 215 9.56 247	32	9.59 317	37	0.40 683	9.96 898	5	36 35	
26	9.56 279	32	9.59 391	37	0.40 609	9.96 888	5	34	33 32 31
27	9.56 311	32	9.59 429	38	0.40 571	9.96 883	5	33	, 1 3.3 3.2 3.1
28	9.56 343	32 32	9.59 466	37 37	0.40 534	9.96 878	5	32	2 6.6 6.4 6.2
29 30	9.56 375	33	9.59 503	37	0.40 497	9.96 873	5	31 30	3 9.9 9.6 9.3 4 13.2 12.8 12.4
	9.56 408	32	9.59 540	37	0.40 460	9.96 863	5	29	
31 32	9.56 472	32	9.59 614	37	0.40 386	9.96 858	5	28	0 19.8 19.2 18.0
33	9.56 504	32 32	9.59 651	37	0.40 349	9.96 853	5	27	7 23.I 22.4 2I.7 8 26.4 25.6 24.8
34	9.56 536	32	9.59 688	37 37	0.40 312	9.96 848	5	26	9 29.7 28.8 27.9
35 36	9.56 568 9.56 599	31	9.59 725 9.59 762	37	0.40 275	9.96 843 9.96 838	5	25 24	
37	9.56 631	32	9.59 799	37	0.40 201	9.96 833	5	23	
38	9.56 663	32 32	9.59 835	36	0.40 165	9.96 828	5 5	22	
39	9.56 695	32	9.59872	37 37	0.40 128	9.96 823	5	21	
40	9.56 727	32	9.59 909	37	0.40 091	9.96 818	5	20	
41 42	9.56 759	31	9.59 946 9.59 983	37	0.40 054	9.96 813 9.96 808	5	19	
43	9.56 790 9.56 822	32	9.59 903	36	0.39 981	9.96 803	5	17	
44	9.56 854	32	9.60 056	37	0.39 944	9.96 798	. 5	16	6 5 4
45	9.56 886	32 31	9.60 093	37 37	0.39 907	9.96 793	5	15	1 0.6 0.5 0.4
46 47	9.56 917	32	9.60 130 9.60 166	36	0.39870	9.96 788	5	14	3 1.8 1.5 1.2
48	9.56 980	31	9.60 203	37	0.39 797	9.96 778	5	12	4 2.4 2.0 1.6
49	9.57 012	32 32	9.60 240	37 36	0.39 760	9.96 772	6 5	II	5 3.0 2.5 2.0 6 3.6 3.0 2.4
50	9.57 044	31	9.60 276	37	0.39 724	9.96 767	5	10	7 4.2 3.5 2.8
51	9.57 075	32	9.60 313	36	0.39 687	9.96 762	5	9	8 4.8 4.0 3.2
52 53	9.57 107 9.57 138	31	9.60 349 9.60 386	37	0.39 651	9.96 757 9.96 752	5	8 7	9 5.4 4.5 3.6
54	9.57 169	31	9.60 422	36	0.39 578	9.96 747	5	6	
55	9.57 201	32 31	9.60 459	37	0.39 541	9.96 742	5	5	
56	9.57 232	32	9.60 495	36	0.39 505	9.96 737	5	4	
57 58	9.57 264 9.57 295	31	9.60 532 9.60 568	36	0.39 468	9.96 732	5	3 2	
59	9.57 326	31	9.60 605	37	0.39 395	9.96 722	5	ī	
60	9.57 358	32	9.60 641	36	0.39 359	9.96 717	5	0	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	′	PP

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-	22							UI	
	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.57 358	31	9.60 641	36	0.39 359	9.96 717	6	60	
1	9.57 389	31	9.60 677	37	0.39 323	9.96 711	5	59	
2	9.57 420	31	9.60 714	36	0.39 286	9.96 706	5	58	
3	9.57 451	31	9.60 786	36	0.39 214	9.96 696	5	57 56	
4 5	9.57 514	32	9.60 823	37	0.39 177	9.96 691	5	55	
ő	9.57 545	31	9.60 859	36	0.39 141	9.96 686	5	54	
7 8	9.57 576	31 31	9.60 895	36 36	0.39 105	9.96 681	5	53	07 96 95
8	9.57 607 9.57 638	31	9.60 931	36	0.39 069	9.96 676	5 6	52 51	37 36 35
10	9.57 669	31	9.61 004	37	0.38 996	9.96 665	5	50	I 3.7 3.6 3.5 2 7.4 7.2 7.0
II	9.57 700	31	9.61 040	36	0.38 960	9.96 660	5	1	3 11.1 10.8 10.5
12	9.57 731	31	9.61 076	36	0.38 924	9.96 655	5	49 48	4 14.8 14.4 14.0
13	9.57 762	31	9.61 112	36	0.38 888	9.96 650	5	47	3 10.5 10.0 17.5
14	9.57 793	31	9.61 148	36 36	0.38 852	9.96 645	5	46	
15 16	9.57 824	31	9.61 184	36	0.38 816	9.96 640	5	45	7 25.9 25.2 24.5 8 29.6 28.8 28.0
17	9.57 885	30	9.61 256	36	0.38 744	9.96 629	5	44	9 33.3 32.4 31.5
18	9.57 916	31	9.61 292	36	0.38 708	9.96 624	5	43	
19	9.57 947	3I 3I	9.61 328	36 36	0.38 672	9.96619	5	41	
20	9.57 978	30	9.61 364	36	0.38 636	9.96 614	6	40	
21	9.58 008	31	9.61 400	36	0.38 600	9.96 608	5	39	
22	9.58 039	31	9.61 436	36	0.38 564	9.96 603	5	38	
23	9.58 101	31	9.61 472	36	0.38 492	9.96 593	5	37	
25	9.58 131	30	9.61 544	36	0.38 456	9.96 588	5 6	36	
26	9.58 162	31	9.61 579	35 36	0.38 421	9.96 582		34	32 31 30
27	9.58 192	30	9.61 615	36	0.38 385	9.96 577	5 5	33	
28 29	9.58 223 9.58 253	30	9.61 651	36	0.38 349	9.96 572 9.96 567	5	32	3 9.6 9.3 9.0
30	9.58 284	31	9.61 722	35	0.38 278	9.96 562	5	31	4 12.8 12.4 12.0
	9.58 314	30	9.61 758	36	0.38 242	9.96 556	6	1	5 10.0 15.5 15.0
31 32	9.58 345	31	9.61 794	36	0.38 206	9.96 551	5	29	
33	9.58 375	30	9.61 830	36	0.38 170	9.96 546	5	27	8 25.6 24.8 24.0
34	9.58 406	3 I 30	9.61 865	35	0.38 135	9.96 541	5	26	
35 36	9.58 436	31	9.61 901	35	0.38 099	9.96 535	5	25	
37	9.58 497	30	9.61 930	36	0.38 004	9.96 525	5	24	
38	9.58 527	30	9.62 008	36	0.37 992	9.96 520	5 6	23	
39	9.58 557	30 31	9.62 043	35 36	0.37 957	9.96 514	5	21	
40	9.58 588	30	9.62 079	35	0.37 921	9.96 509	5	20	
41	9.58618	30	9.62 114	36	0.37 886	9.96 504	6	19	
42	9.58 648 9.58 678	30	9.62 150	35	0.37 850	9.96 498	5	18	
43	9.58 709	31	9.62 221	36	0.37 779	9.96 488	5	17	
44	9.58 739	30	9.62 256	35	0.37 744	9.96 483	5 6	15	1 2.9 0.0 0.3
46	9.58 769	30	9.62 292	36	0.37 708	9.96 477	5	14	
47	9.58 799	30	9.62 327	35	0.37 673	9.96 472		13	4 11.6 2.4 2.0
48	9.58 829 9.58 859	30	9.62 362 9.62 398	36	0.37 638	9.96 461	5 6	12	3 -4.3
50	9.58 889	30	9.62 433	35	0.37 567	9.96 456	5	10	
51	9.58 919	30	9.62 468	35	0.37 532	9.96 451	5		8 23.2 4.8 4.0
52	9.58 949	30	9.62 504	36	0.37 496	9.96 445	6	8	0 267 54 45
53	9.58 979	30	9.62 539	35	0.37 461	9.96 440	5	7	
54	9.59 009	30	9.62 574	35	0.37 426	9.96 435	5	6	
55 56	9.59 039	30	9.62 609	36	0.37 391	9.96 429	. 5	5	
	9.59 098	29	9.62 680	35	0.37 333	9.96 419	5	4	
57 58	9.59 128	30	9.62 715	35	0.37 285	9.96 413	6	3 2	
59	9.59 158	30	9.62 750	35	0.37 250	9.96 408	5	I	
60	9.59 188	-30	9.62 785	33	0.37 215	9.96 403		0	
L	L Cos	d	L Cot	cd	L Tan	L Sin	d	1	PP

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		23	-						56	
Г	,	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
ſ	0	9.59 188	30	9.62 785	35	0.37 215	9.96 403	6	60	
ı	I	9.59 218	29	9.62 820	35	0.37 180	9.96 397	5	59	
ı	3	9.59 247 9.59 277	30	9.62 855 9.62 890	35	0.37 145	9.96 392	5 6	58	
ı	4	9.59 307	30	9.62 926	36	0.37 074	9.96 381		56	• •
L	5	9.59 336	30	9.62 961	35 35	0.37 039	9.96 376	5	55	
ı	6	9.59 366	30	9.62 996	35	0.37 004	9.96 370	5	54	
ı	78	9.59 425	29	9.63 066	35	0.36 934	9.96 360	5	53 52	36 35 34
L	9	9.59 455	30	9.63 101	35	0.36 899	9.96 354	5	51	1 3.6 3.5 3.4
1	0	9.59 484	30	9.63 135	35	0.36 865	9.96 349	6	50	2 7.2 7.0 6.8 3 10.8 10.5 10.2
	2	9.59 514	29	9.63 170	35	0.36 830	9.96 343 9.96 338	5	49 48	4 14.4 14.0 13.6
	3	9.59 543 9.59 573	30	9.63 205	35	0.36 795	9.96 333	5	47	5 18.0 17.5 17.0 6 21.6 21.0 20.4
1	4	9.59 602	29	9.63 275	35	0.36 725	9.96 327		46	
I	5	9.59 632	30 29	9.63 310	35 35	0.36 690	9.96 322	5	45	7 25.2 24.5 23.8 8 28.8 28.0 27.2
	7	9.59 661	29	9.63 345	34	0.36 621	9.96 316	5	44	9 32.4 31.5 30.6
I	8	9.59 720	30	9.63 414	35	0.36 586	9.96 305	6	42	
	9	9.59 749	29	9.63 449	35	0.36 551	9.96 300	5	41	
ı	0	9.59 778	30	9.63 484	35	0.36 516	9.96 294	5	40	
	1 2	9.59 808	29	9.63 519	34	0.36 481	9.96 289	5	39 38	
	3	9.59 866	29	9.63 588	35	0.36 412	9.96 278		37	
	4	9.59 895	29	9.63 623	35 34	0.36 377	9.96 273	5	36	
2	5	9.59 924 9.59 954	30	9.63 657	35	o.36 343 o.36 308	9.96 267 9.96 262	5 6	35	30 29 28
2	7	9.59 983	29	9.63 726	34	0.36 274	9.96 256		34	I 3.0 2.9 2.8 2 6.0 5.8 5.6
2	8	9.60 012	29 29	9.63 761	35	0.36 239	9.96 251	5	32	2 6.0 5.8 5.6 3 9.0 8.7 8.4
	9	9.60 041	29	9.63 796	35 34	0.36 204	9.96 245	5	31	4 12.0 11.6 11.2
3	~ I	9.60 070	29	9.63 830	35	0.36 170	9.96 240	6	30	5 15.0 14.5 14.0 6 18.0 17.4 16.8
3	1 2	9.60 099	29	9.63 865 9.63 899	34	0.36 135	9.96 234	5 6	29 28	7 21.0 20.3 19.6
3		9.60 157	29 29	9.63 934	35	0.36 066	9.96 223		27	8 24.0 23.2 22.4 9 27.0 26.1 25.2
3		9.60 186	29	9.63 968	34 35	0.36 032	9.96 218	5	26	9 27.0 20.1 25.2
3		9.60 215	29	9.64 003	34	0.35 997 0.35 963	9.96 212	5	25 24	
3	7	9.60 273	29	9.64 072	35	0.35 928	9.96 201		23	
3		9.60 302	29 29	9.64 106	34	0.35 894	9.96 196	5	22	
3 4		9.60 331	28	9.64 140	35	0.35 860	9.96 190	5	21 20	
4	1	9.60 359 9.60 388	29	9.64 175	34	0.35 825	9.96 185	6	19	
4		9.60 417	29	9.64 243	34	0.35 757	9.96 174	5	18	6 5
4	3	9.60 446	29 28	9.64 278	35 34	0.35 722	9.96 168	6	17	
4		9.60 474	29	9.64 312	34	0.35 688	9.96 162 9.96 157		16	I 0.6 0.5 2 I.2 I.0
4		9.60 532	29	9.64 381	35	0.35 619	9.96 151	5	14	3 1.8 1.5
4	7	9.60 561	29 28	9.64 415	34	0.35 585	9.96 146	5	13	4 2.4 2.0 5 3.0 2.5
4		9.60 589 9.60 618	. 29	9.64 449	34	0.35 551	9.96 140 9.96 135		I2	6 3.6 3.0
5		9.60 646	28	9.64 517	34	0.35 483	9.96 133	5	10	7 4.2 3.5 8 4.8 4.0
5	- 1	9.60 675	29	9.64 552	35	0.35 448	9.96 123	6		9 5.4 4.5
5	2	9.60 704	29 28	9.64 586	34	0.35 414	9.96 118	5	9 8	
5		9.60 732	29	9.64 620	34	0.35 380	9.96 112	5	7 6	
5		9.60 789	28	9.64 688	34	0.35 346	9.96 107 9.96 101	6	5	
5	6	9.60 818	29 28	9.64 722	34	0.35 278	9.96 095	6	4	
5	7	9.60 846 9.60 875	29	9.64 756	34	0.35 244	9.96 090	5	3	
5		9.60 875	28	9.64 790	34	0.35 210	9.96 0 84 9.96 0 79	5	2 I	
6		9.60 931	28	9.64 858	34	0.35 142	9.96 073	6	0	
		L Cos	d	L Cot	cd	L Tan	L Sin	d	,	PP
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113° (361) 66°

ı	'	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
ı	0	9.60 931	29	9.64 858	34	0.35 142	9.96 073	6	60	
ı	I	9.60 960	28	9.64 892	34	0.35 108	9.96 067	5	59	
ı	3	9.60 988	28	9.64 92 6 9.64 9 60	34	0.35 074	9.96 o62 9.96 o56	6	58 57	
ı	4	9.61 045	29	9.64 994	34	0.35 006	9.96 050	6	56	
ı	5	9.61 073	28	9.65 o 28 9.65 o 62	34	0.34 972	9.96 045	5	55	
ı		9.61 101	28	9.65 096	34	0.34 938	9.96 o39 9.96 o34	5	54 53	
ı	7	9.61 158	29	9.65 130	34	0.34 870	9.96 028	6	52	34 33
ı	9	9.61 186	28	9.65 164	33	0.34 836	9.96 022	5	51	1 3.4 3.3 2 6.8 6.6
ı	10	9.61 214	28	9.65 197	34	0.34 803	9.96 017	6	50	3 10.2 9.9
ı	12	9.61 270	28	9.65 265	34	0.34 735	9.96 005	6	49 48	4 13.6 13.2 5 17.0 16.5
ı	13	9.61 298	28	9.65 299	34	0.34 701	9.96 000	5	47	6 20.4 19.8
ı	14	9.61 326 9.61 354	28	9.65 333	33	0.34 667	9.95 994 9.95 988	6	46 45	7 23.8 23.1
ı	16	9.61 382	28	9.65 400	34	0.34 600	9.95 982	6	44	8 27.2 26.4 9 30.6 29.7
ı	17	9.61 411	27	9.65 434	34	0.34 566	9.95 977	5	43	
ł	18	9.61 438 9.61 466	28	9.65 467 9.65 501	34	0.34 533	9.95 971	6	42 41	
ı	20	9.61 494	28	9.65 535	34	0.34 465	9.95 960	5	40	
1	21	9.61 522	28 28	9.65 568	33	0.34 432	9.95 954	6	39	
ı	22	9.61 550	28	9.65 602	34 34	0.34 398	9.95 948	6	38	
ı	23	9.61 578	28	9.65 636	33	0.34 364	9.95 942	5	37 36	
ı	25	9.61 634	28 28	9.65 703	34	0.34 297	9.95 931	6	35	29 28 27
ı	26	9.61 662	27	9.65 736	33 34	0.34 264	9.95 925	6 5	34	1 2.9 2.8 2.7
ı	27 28	9.6 1 689	28	9.65 770	33	0.34 230	9.95 920	6	33	2 5.8 5.6 5.4
ı	29	9.61 745	28 28	9.65 837	34	0.34 163	9.95 908	6	31	
ı	30	9.61 773	27	9.65 870	33	0.34 130	9.95 902	5	30	5 14.5 14.0 13.5
ı	31	9.61 800	28	9.65 904	33	0.34 096	9.95 897	6	29 28	6 17.4 16.8 16.2
ı	32 33	9.61 828 9.61 856	28	9.65 937 9.65 971	34	0.34 063	9.95 891 9.95 885	6	27	7 20.3 19.6 18.9 8 23.2 22.4 21.6
ı	34	9.61 883	27 28	9.66 004	33	0.33 996	9.95 879	6	26	9 26.1 25.2 24.3
1	35 36	9.61 911	28	9.66 o38 9.66 o71	34	0.33 962	9.95 873 9.95 868	5	25 24	
ı	37	9.61 966	27	9.66 104	33	0.33 896	9.95 862	6	23	
ı	38	9.61 994	28	9.66 138	34 33	0.33 862	9.95 856	6	22	
ŀ	39 40	9.62 021	28	9.66 171	33	0.33 829	9.95 850	6	21 20	
1	41	9.62 049	27	9.66 238	34	0.33 796	9.95 839	5	19	
ı	42	9.62 104	28	9.66 271	33	0.33 729	9.95 833	6	18	
ı	43	9.62 131	27	9.66 304	33 33	0.33 696	9.95 827	6	17	6 5
١	44 45	9.62 159 9.62 186	27	9.66 337 9.66 371	34	0.33 663	9.95 821 9.95 815	6	16	1 0.6 0.5
1	46	9.62 214	28	9.66 404	33	0.33 596	9.95810	5	1.4	2 1.2 1.0 3 1.8 1.5
1	47	9.62 241	27 27	9.66 437	33	0.33 563	9.95 804 9.95 798	6	13	3 1.8 1.5 4 2.4 2.0
1	48	9.62 268 9.62 296	28	9.66 470	33	0.33 530	9.95 790	6	II	5 3.0 2.5
	50	9.62 323	27	9.66 537	34	0.33 463	9.95 786	6	10	7 4.2 3.5
	51	9.62 350	27	9.66 570	33	0.33 430	9.95 780		9	8 4.8 4.0
	52 53	9.62 377	27 28	9.66 636	33	0.33 397	9.95 775 9.95 769	5 6	8 7	9 5.4 4.5
	54	9.62 432	27	9.66 669	33	0.33 331	9.95 763	6	6	
1	55	9.62 459	27 27	9.66 702	33	0.33 298	9.95 757	6	5	
	56 57	9.62 486	27	9.66 735	33	0.33 265	9.95 751 9.95 745	6	3	
	58	9.62 541	28	9.66 801	33	0.33 199	9.95 745	6	2	
	59	9.62 568	27	9.66 834	33	0.33 166	9.95 733	6 5	1	
I	60	9.62 595		9.66 867		0.33 133	9.95 728		0	
		L Cos	d	L Cot	c d	L Tan	L Sin	d	′	PP

114° (362) **65**°

	1.0:	- 1	1.7.	1	1.0	1.0-	-1		2.0
	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.62 595	27	9.66 867	33	0.33 133	9.95 728	6	60	
I 2	9.62 622 9.62 649	27	9.66 900	33	0.33 100	9.95 722 9.95 716	6	59	
3	9.62 676	27	9.66 966	33	0.33 034	9.95 710	6	57	
4	9.62 703	27	9.66 999	33	0.33 001	9.95 704	6	56	
5 6	9.62 730	27	9.67 032	33	0.32 968	9.95 698	6	55	
	9.62 757	27	9.67 065	33	0.32 935	9.95 692 9.95 686	6	54	
8	9.62 811	27	9.67 131	33	0.32 869	9.95 680	6	52	
9	9.62 838	27	9.67 163	33	0.32 837	9.95 674	6	51	33 32
10	9.62 865	27	9.67 196	33	0.32804	9.95 668	5	50	I 3.3 3.2 2 6.6 6.4
II	9.62 892	26	9.67 229 9.67 262	33	0.32 771	9.95 663	6	49	
12	9.62 918 9.62 945	27	9.67 295	33	0.32 738	9.95 651	6	47	3 9.9 9.6 4 13.2 12.8
14	9.62 972	27	9.67 327	32	0.32 673	9.95 645	6	46	5 16.5 16.0
15	9.62 999	27 27	9.67 360	33 33	0.32 640	9.95 639	6	45	
16	9.63 026	26	9.67 393 9.67 426	33	0.32 607	9.95 633	6	44	7 23.I 22.4 8 26.4 25.6
18	9.63 052	27	9.67 458	32	0.32 542	9.95 621	6	43	9 29.7 28.8
19	9.63 106	27 27	9.67 491	33	0.32 509	9.95 615	6	41	
20	9.63 133	26	9.67 524	32	0.32 476	9.95 609	6	40	
21	9.63 159	27	9.67 556	33	0.32 444	9.95 603	6	39	
22	9.63 186	27	9.67 589	33	0.32 411	9.95 597 9.95 591	6	38	
24	9.63 239	26	9.67 654	32	0.32 346	9.95 585	6	36	
25	9.63 266	27 26	9.67 687	33 32	0.32 313	9.95 579	6	35	
26	9.63 292	27	9.67 719	33	0.32 281	9.95 573	6	34	27 26
27 28	9.63 319	26	9.67 752	33	0.32 248	9.95 567	6	33	I 2.7 2.6 2 5.4 5.2
29	9.63 372	27 26	9.67 785 9.67 817	32	0.32 183	9.95 555	6	31	2 5.4 5.2 3 8.1 7.8
30	9.63 398	27	9.67 850	33	0.32 150	9.95 549	6	30	4 10.8 10.4
31	9.63 425	26	9.67 882	33	0.32 118	9.95 543	6	29	5 13.5 13.0 6 16.2 15.6
32 33	9.63 451 9.63 478	27	9.67 915	32	0.32 085	9.95 537 9.95 531	6	28	7 18.9 18.2
34	9.63 504	26	9.67 980	33	0.32 020	9.95 525	6	26	8 21.6 20.8 9 24.3 23.4
35	9.63 531	27 26	9.68 012	32 32	0.31 988	9.95 519	6	25	9 24.3 23.4
36	9.63 557	26	9.68 044 9.68 077	33	0.31 956	9.95 513	6	24	
37 38	9.63 583	27	9.68 109	32	0.31 923	9.95 507	7	23	
39	9.63 636	26 26	9.68 142	33	0.31 858	9.95 494	6	21	
40	9.63 662	27	9.68 174	32	0.31 826	9.95 488	6	20	
41	9.63 689	26	9.68 206	33	0.31 794	9.95 482	6	19	
42 43	9.63 715	26	9.68 239	32	0.31 761	9.95 476	6	18 17	7 6 5
44	9.63 767	26	9.68 303	32	0.31 697	9.95 464	6	16	1 0.7 0.6 0.5
45 46	9.63 794 9.63 820	27 26	9.68 336	33	0.31 664	9.95 458	6	15	2 1.4 1.2 1.0
40	9.63 846	26	9.68 368	32	0.31 632	9.95 45 ² 9.95 446	6	13	3 2.I I.8 I.5 4 2.8 2.4 2.0
48	9.63 872	26	9.68 432	32	0.31 568	9.95 440	6	13	5 3.5 3.0 2.5
49	9.63 898	26 26	9.68 465	33	0.31 535	9.95 434	6 7	II	6 4.2 3.6 3.0
50	9.63 924	26	9.68 497	32	0.31 503	9.95 427	6	10	7 4.9 4.2 3.5 8 5.6 4.8 4.0
51	9.63 950	26	9.68 529	32	0.31 471	9.95 421	6	9	8 5.6 4.8 4.0 9 6.3 5.4 4.5
52 53	9.63 976	26	9.68 561	32	0.31 439	9.95 415	6	7	
54	9.64 028	26 26	9.68 626	33	0.31 374	9.95 403	6	6	
55 56	9.64 054	26	9.68 658	32 32	0.31 342	9.95 397	6	5	
50	9.64 080	26	9.68 690	32	0.31 310	9.95 391	7	3	
58	9.64 132	26	9.68 754 9.68 786	32	0.31 246	9.95 378	6	2	
59	9.64 158	26 26		32	0.31 214	9.95 372	6	I	
60	9.64 184		9.68 818		0.31 182	9.95 366		0	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	′	PP
	115°				(363)	(64°	

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Ľ	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.64 184	26	9.68818	32	0.31 182	9.95 366	6	60	
I	9.64 210	26	9.68 850	32	0.31 150	9.95 360	6	59 58	
3	9.64 236	26	9.68 882	32	0.31 118	9.95 354	6	58	
4	9.64 288	26	9.68 946	32	0.31 054	9.95 341	7	56	
5 6	9.64 313	25 26	9.68 978	32 32	0.31 022	9.95 335	6	55	
	9.64 365	26	9.69 010	32	0.30 990	9.95 329	6	54	
7 8	9.64 391	26	9.69 074	32	0.30 926	9.95 317	6	52	32 31
9	9.64417	26 25	9.69 106	32 32	0.30 894	9.95 310	7	51	I 3.2 3.I
10	9.64 442	26	9.69 138	32	0.30 862	9.95 304	6	50	2 6.4 6.2
II I2	9.64 468	26	9.69 170	32	0.30 830	9.95 298	6	49 48	3 9.6 9.3 4 12.8 12.4
13	9.64 519	25	9.69 234	32	0.30 766	9.95 286	6	47	5 16.0 15.5
14	9.64 545	26 26	9.69 266	32	0.30 734	9.95 279	7	46	6 19.2 18.6
15 16	9.64 571 9.64 596	25	9.69 298	31	0.30 702	9.95 273 9.95 267	6	45	7 22.4 21.7 8 25.6 24.8
17	9.64 622	26	9.69 361	32	0.30 639	9.95 261	6	43	9 28.8 27.9
18	9.64 647	25 26	9.69 393	32	0.30 607	9.95 254	7	42	
19 20	9.64 673	25	9.69 425	32	0.30 575	9.95 248	6	41 40	
21	9.64 724	26	9.69 488	31	0.30 543	9.95 236	6	39	
22	9.64 749	25 26	9.69 520	32	0.30 480	9.95 229	7 6	38	
23	9.64 775	25	9.69 552	32	0.30 448	9.95 223	6	37	
24 25	9.64 800	26	9.69 584	31	0.30 416	9.95 217	6	36	
26	9.64851	25 26	9.69 647	32	0.30 353	9.95 204	7	34	26 25 24
27 28	9.64 877	25	9.69 679	32 31	0.30 321	9.95 198	6	33	I 2.6 2.5 2.4 2 5.2 5.0 4.8
20	9.64 902	25	9.69 742	32	0.30 290	9.95 192 9.95 185	7	32 31	3 7.8 7.5 7.2
30	9.64 953	26	9.69 774	32	0.30 226	9.95 179	6	30	4 10.4 10.0 9.6
31	9.64 978	25	9.69 805	31	0.30 195	9.95 173	6	29	5 13.0 12.5 12.0 6 15.6 15.0 14.4
32	9.65 003	25 26	9.69 837 9.69 868	32 31	0.30 163	9.95 167	7	28	7 18.2 17.5 16.8
33 34	9.65 029	25	9.69 900	32	0.30 100	9.95 154	6	27	8 20.8 20.0 19.2 9 23.4 22.5 21.6
35	9.65 079	25 25	9.69 932	32 31	0.30 068	9.95 148	6	25	3 10 1
36	9.65 104	26	9.69 963	32	0.30 037	9.95 141	6	24	
37 38	9.65 155	25	9.70 026	31	0.29 974	9.95 129	6	23	
39	9.65 180	25 25	9.70 058	32 31	0.29 942	9.95 122	7	21	
40	9.65 205	25	9.70 089	32	0.29 911	9.95 116	6	20	
4I 42	9.65 230	25	9.70 I 2 I 9.70 I 5 2	31	0.29 879 0.29 848	9.95 110	7	19	
43	9.65 255	26	9.70 184	32	0.29 816	9.95 097	6	17	7 6
44	9.65 306	25 25	9.70 215	31	0.29 785	9.95 090	7	16	1 0.7 0.6
45 46	9.65 331 9.65 356	25	9.70 247	31 31	0.29 753	9.95 084	6	15	2 I.4 I.2 3 2.I I.8
47	9.65 381	25	9.70 309	31	0.29 691	9.95 071	7	13	4 2.8 2.4
48	9.65 406	25 25	9.70 341	32 31	0.29 659	9.95 065	6	12	5 3.5 3.0 6 4.2 3.6
49 50	9.65 431	25	9.70 372	32	0.29 628	9.95 059	7	10	7 4.9 4.2
51	9.65 481	25	9.70 404	31	0.29 565	9.95 046	6		
52	9.65 506	25	9.70 466	31	0.29 534	9.95 039	7	8	. 9 6.3 5.4
53	9.65 531	25 25	9.70 498	32 31	0.29 502	9.95 033	6	7	
54 55	9.65 556 9.65 580	24	9.70 529	31	0.29 471	9.95 027	7	6 5	
56	9.65 605	25	9.70 592	32	0.29 408	9.95 014	6	4	
57	9.65 630	25 25	9.70 623	3I 3I	0.29 377	9.95 007	7	3 2	
58 59	9.65 655 9.65 680	25	9.70 654	3 I	0.29 346	9.95 001 9.94 995	6	2 I	
60	9.65 705	25	9.70 717	32	0.29 283	9.94 988	7	0	
	L Cos	d	L Cot	c d	L. Tan	L Sin	d	,	PP

116° (364) **63**°

27° 152°

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1		L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
T		9.65 705	24	9.70 717	31	0.29 283	9.94 988	6	60	
		9.65 729	25	9.70 748	31	0.29 252	9.94 982	7	59	
		9.65 754	25	9.70779	31	0.29 221	9.94 975	6	58	
		9.65 804	25	9.70 841	31	0.29 159	9.94 962	7	56	
	5 9	9.65 828	24 25	9.70 873	32 31	0.29 127	9.94 956	6	55	
		9.65 853 9.65 878	25	9.70 904	31	0.29 096	9.94 949	7	54	
L	7 9	9.65 902	24	9.70 966	31	0.29 034	9.94 943	7 6	53 52	32 31 30
	9 9	9.65 927	25	9.70 997	31 31	0.29 003	9.94 930	7	51	1 3.2 3.1 3.0
1	0 9	9.65 952	25 24	9.71 028	31	0.28 972	9.94 923	6	50	2 6.4 6.2 6.0
I		9.65 976	25	9.71 059	31	0.28 941	9.94917	6	49	3 9.6 9.3 9.0
I		9.66 001	24	9.71 090	31	0.28 910	9.94 911	7	48	4 12.8 12.4 12.0 5 16.0 15.5 15.0
I		9.66 050	25	9.71 153	32	0.28 847	9.94 898	6	46	6 19.2 18.6 18.0
I		9.66 075	25 24	9.71 184	31 31	0.28816	9.94 891	7	45	7 22.4 21.7 21.0 8 25.6 24.8 24.0
I	- 12	9.66 099	25	9.71 215	31	0.28 785	9.94 885	7	44	9 28.8 27.9 27.0
I		9.66 148	24	9.71 240	31	0.28 723	9.94 871	7	43	
1		9.66 173	25	9.71 308	31	0.28 692	9.94 865		41	
2	12	9.66 197	24	9.71 339	31	0.28661	9.94 858	7	40	
2		9.66 221	25	9.71 370	3I 3I	0.28 630	9.94 852	7	39	
2 2		9.66 246	24	9.71 401	30	0.28 599 0.28 569	9.94 845	6	38 37	
2.	4 9	9.66 295	25	9.71 451	31	0.28 538	9.94 832	7	36	
2	5 9	9.66 319	24	9.71 493	31	0.28 507	9.94 826	6	35	
2		9.66 343	24 25	9.71 524	3I 3I	0.28 476	9.94 819	7	34	25 24 23
2		9.66 368 9.66 392	24	9.71 555 9.71 586	31	0.28 445	9.94 813 9.94 806	7	33	1 2.5 2.4 2.3 2 5.0 4.8 4.6
2		9.66 416	24	9.71 617	3 I	0.28 383	9.94 799	7	31	2 5.0 4.8 4.6 3 7.5 7.2 6.9
3	0 9	9.66 441	25	9.71 648	31	0.28 352	9.94 793	-	30	4 10.0 9.6 9.2
3	1 9	0.66 465	24	9.71 679	31	0.28 321	9.94 786	7	29	5 12.5 12.0 11.5 6 15.0 14.4 13.8
3		9.66 489 9.66 513	24 24	9.71 709	30 31	0.28 291	9.94 780 9.94 773	7	28 27	7 17.5 16.8 16.1
3.		9.66 537	24	9.71 740	31	0.28 220	9.94 773	6	26	8 20.0 19.2 18.4 9 22.5 21.6 20.7
3.	5 9	9.66 562	25	9.71 771 9.71 802	31	0.28 198	9.94 760	7	25	9 22.5 21.0 20.7
3		9.66 586	24 24	9.71 833	31 30	0.28 167	9-94 753	.7	24	
3	7 9 3 c	9.66 610 9.66 634	24	9.71 863 9.71 894	31	0.28 137	9.94 747	7	23	
31		0.66 658	24	9.71 925	31	0.28 075	9.94 734		21	
4	9	0.66 682	24	9.71 955	30	0.28 045	9.94 727	7	20	
4		0.66 706	24	9.71 986	31	0.28014	9.94 720	7	19	
4		9.66 731	25 24	9.72 017 9.72 048	31 31	0.27 983 0.27 952	9.94 714	7	18	
4.		9.66 779	24	9.72 048	30	0.27 932	9.94 707	7	16	7 6
4	5 9	9.66 803	24	9.72 109	31	0.27 891	9.94 694	6	15	I 0.7 0.6 2 I.4 I.2
4		9.66 827 9.66 851	24	9.72 140	3 I 30	0.27 860	9.94 687	7 7	14	3 2.1 1.8
4	8 6	9.66 875	24	9.72 170	31	0.27 830	9.94 680	6	I3 I2	4 2.8 2.4
4	9 9	9.66 899	24	9.72 231	30	0.27 769	9.94 667	7	II	5 3.5 3.0 6 4.2 3.6
5	9	9.66 922	23	9.72 262	31	0.27 738	9.94 660	7	10	7 4.9 4.2
5		9.66 946	24	9.72 293	31	0.27 707	9.94 654		9	
5.5		9.66 970	24 24	9.72 323	30 31	0.27 677	9.94 647	7 7	8	9 6.3 5.4
5.		0.67 018	24	9.72 354	30	0.27 616	9.94 634	7	6	
1 5	5 9	0.67 042	24	9.72 415	31	0.27 585	9.94 627	7	5	
5		9.67 066	24 24	9.72 445	30	0.27 555	9.94 620	7	4	
5		9.67 090 9.67 113	23	9.72 476	30	0.27 524 0.27 494	9.94 614	7	3	
5	9 9	9.67 137	24	9.72 537	31	0.27 463	9.94 600	7	I	
6		0.67 161	24	9.72 567	30	0.24 433	9.94 593	7	0	
	I	L Cos	d	L Cot	c d	L Tan	L Sin	d	′	PP

117° (365) 62°

28° 151°

ï	,	1 Cin	al.	1 7	A -1	1 0-4	I Cor	al .		PP
L		L Sin	<u>d</u>	L Tan	c d	L Cot	L Cos	_d		P P
ı	0	9.67 161	24	9.72 567	31	0.27 433	9.94 593	6	60	
ı	1 2	9.67 185 9.67 208	23	9.72 598 9.72 628	30	0.27 402 0.27 372	9.94 587 9.94 580	7	59 58	
ı	3	9.67 232	24	9.72 659	31	0.27 341	9.94 573	7	57	
ı	4	9.67 256	24 24	9.72 689	30 31	0.27 311	9.94 567	7	56	
ı	5	9.67 280 9.67 303	23	9.72 720 9.72 750	30	0.27 280	9.94 560 9.94 553	7	55 54	
ı	7 8	9.67 327	24	9.72 780	30	0.27 220	9.94 546	7	53	
ı		9.67 350	23 24	9.72 811	3I 30	0.27 189	9.94 540	6 7	52	31 30 29
1	9	9.67 374	24	9.72 841	31	0.27 159	9.94 533	7	51 50	1 3.1 3.0 2.9
-	II	9.67 398	23	9.72 872	30	0.27 128	9.94 526	7		2 6.2 6.0 5.8 3 9.3 9.0 8.7
	12	9.67 421 9.67 445	24	9.72 902	30	0.27 068	9.94 513	6	49 48	3 9.3 9.0 8.7 4 12.4 12.0 11.6
H	13	9.67 468	23	9.72 963	3I 30	0.27 037	9.94 506	7	47	5 15.5 15.0 14.5
	[4	9.67 492	24	9.72 993	30	0.27 007	9.94 499	7	46	
	15	9.67 515	24	9.73 O23 9.73 O54	31	0.26 977	9.94 492 9.94 485	7	45	7 21.7 21.0 20.3 8 24.8 24.0 23.2
	17	9.67 562	23	9.73 084	30	0.26 916	9.94 479	6	43	9 27.9 27.0 26.1
	81	9.67 586	24 23	9.73 114	30	0.26 886	9.94 472	7	42	
_	20	9.67 633	24	9.73 144 9.73 175	31	0.26 825	9.94 465	7	41	
- 1	21	9.67 656	23	9.73 205	30	0.26 795	9.94 451	7	39	
	22	9.67 680	24	9-73 235	30	0.26 765	9.94 445	6	38	
	23	9.67 703	23 23	9.73 265	30	0.26 735	9.94 438	7	37	
	24	9.67 726	24	9.73 295 9.73 326	31	0.26 705	9.94 431	7	36	
	26	9.67 773	23	9.73 356	30	0.26 644	9.94417	7	34	24 23 22
	27	9.67 796	23	9.73 386	30	0.26 614	9.94410	7	33	I 2.4 2.3 2.2
	28	9.67 820 9.67 843	24 23	9.73 416	30	0.26 584	9.94 404 9.94 397	7	32 31	2 4.8 4.6 4.4 3 7.2 6.9 6.6
-	30	9.67 866	23	9.73 476	30	0.26 524	9.94 390	7	30	4 9.6 9.2 8.8
	31	9.67 890	24	9.73 507	31	0.26 493	9.94 383	7	20	5 12.0 II.5 II.0 6 14.4 I3.8 I3.2
1	32	9.67 913	23	9.73 537	30	0.26 463	9.94 376	7	28	
_	33	9.67 936	23	9.73 567	30	0.26 433	9.94 369	7	27	8 19.2 18.4 17.6
	34	9.67 959	23	9.73 597 9.73 627	30	0.26 403	9.94 362	7	26	9 21.6 20.7 19.8
	36	9.68 006	24	9.73 657	30	0.26 343	9.94 349	6	24	
	37	9.68 029	23	9.73 687	30	0.26 313	9.94 342	7	23	
	38	9.68 o52 9.68 o75	23	9.73 717 9.73 747	30	0.26 283	9.94 335 9.94 328	7	22 2I	
	10	9.68 098	23	9.73 777	30	0.26 223	9.94 321	7	20	
	11	9.68 121	23	9.73 807	30	0.26 193	9.94 314	7	19	
	12	9.68 144	23	9.73 837	30	0.26 163	9.94 307	7	18	
	13 44	9.68 167	23	9.73 867 9.73 897	30	0.26 133	9.94 300	7	17	7 6
4	15	9.68 213	23	9.73 927	30	0.26 073	9.94 286	7	15	1 0.7 0.6 2 1.4 1.2
H	46	9.68 237	24	9.73 957	30	0.26 043	9.94 279	7	14	3 2.1 1.8
	47 48	9.68 260 9.68 283	23	9.73 987 9 74 017	30	0.26 013	9.94 273	7	13	4 2.8 2.4
	19	9.08 203	22	9.74 047	30	0.25 953	9.94 259	7	II	6 4.2 3.6
	50	9.68 328	23	9.74 077	30	0.25 923	9.94 252	7	10	7 4.9 4.2
	51	9.68 351	23	9.74 107	30	0.25 893	9.94 245	7	9	8 5.6 4.8 9 6.3 5.4
	52	9.68 374	23 23	9.74 137	30 29	0.25 863	9.94 238	7	8 7	315.0 3.4
	53 54	9.68 397	23	9.74 166	30	0.25 804	9.94 231	7	6	
н	55	9.68 443	23	9.74 226	30	0.25 774	9.94 217	7	5	
	56	9.68 466	23	9.74 256	30	0.25 744	9.94 210	7	4	
	57 58	9.68 489	23	9.74 286	30	0.25 714	9.94 203	7	3 2	
Ш	59	9.68 534	22	9.74 345	29	0.25 655	9.94 189	7	I	
1	60	9.68 557	23	9.74 375	30	0.25 625	9.94 182	7	0	
		L Cos	d	L Cot	c d	L Tan	L Sin	d	'	PP
									010	

118° (366) **61**°

	29							JV				
1	L Sin	d	L Tan	c d	L Cot	L Cos	d				PP	
0	9.68 557		9.74 375		0.25 625	9.94 182		60				
1	9.68 580	23	9.74 405	30	0.25 595	9.94 175	7	59				
2	9.68 603	23	9.74 435	30	0.25 565	9.94 168	7	58				
3	9.68 625	23	9.74 465	29	0.25 535	9.94 161	7	57				
4	9.68 648	23	9.74 494	30	0.25 506	9.94 154	7	56				
5	9.68 671	23	9.74 524 9.74 554	30	0.25 476	9.94 147 9.94 140	7	55				
	9.68 716	22	9.74 583	29	0.25 417	9.94 133	7	54 53				
7 8	9.68 739	23	9.74 613	30	0.25 387	9.94 135	7	52				
9	9.68 762	23	9.74 643	30	0.25 357	9.94 119	7	51				
10	9.68 784	22	9.74 673	30	0.25 327	9.94 112	7	50				
11	9.68 807	23	9.74 702	29	0.25 298	9.94 105	7	49				
12	9.68 829	22	9.74 732	30	0.25 268	9.94 098	7 8	48				
13	9.68 852	23 23	9.74 762	30 29	0.25 238	9.94 090	7	47		30	29	23
14	9.68 875	22	9.74 791	30	0.25 209	9.94 083	7	46	1	3.0	2.9	2.3
15	9.68 897	23	9.74821	30	0.25 179	9.94 076	7	45	2	6.0	5.8 8.7	4.6
17	9.68 920	22	9.74 851	29	0.25 149	9.94 069	7	44	3	9.0		6.9
18	9.68 965	23	9.74 910	30	0.25 090	9.94 055	7	43	4	12.0	11.6	9.2
19	9.68 987	22	9.74 939	29	0.25 061	9.94 048	7	4I	5 6	15.0	14.5 17.4	11.5
30	9.69 010	23	9.74 969	30	0.25 031	9.94 041	7	40	7 8	21.0	20.3	16.1
21	9,69 032	22	9.74 998	29	0.25 002	9.94 034	7	39		24.0	23.2	18.4
22	9.69 055	23	9.75 028	30	0.24 972	9.94 027	7	38	9	27.0	26.1	20.7
23	9.69 077	22	9.75 058	30 29	0.24 942	9.94 020	7	37				
24	9.69 100	22	9.75 087	30	0.24 913	9.94 012	7	36				
25 26	9.69 122	22	9.75 117	29	0.24 883	9.94 005	7	35				
27	9.69 144	23	9.75 146	30	0.24 824	9.93 991	7	33				
28	9.69 189	22	9.75 205	29	0.24 795	9.93 984	7	32				
29	9.69 212	23	9.75 235	30	0.24 765	9.93 977	7	31				
30	9.69 234	22	9.75 264	29	0.24 736	9.93 970	7	30				
31	9.69 256	22	9.75 294	30	0.24 706	9.93 963	7	29				
32	9.69 279	23	9.75 323	29	0.24 677	9.93 955	8	28				
33	9.69 301	22	9.75 353	30 29	0.24 647	9.93 948	7	27				
34	9.69 323	22	9.75 382	29	0.24618	9.93 941	7	26				
35 36	9.69 345 9.69 368	23	9.75 411	30	0.24 589	9.93 934 9.93 927	7	25				
37	9.69 390	22	9.75 441	29	0.24 539	9.93 927	7	23				
38	9.69 412	22	9.75 500	30	0.24 500	9.93 912	8	22		22	8	7
39	9.69 434	22	9.75 529	29	0.24 471	9.93 905	7	21	1	2.2	0.8	0.7
40	9.69 456		9.75 558	29	0.24 442	9.93 898	7	20	2	4.4	1.6	1.4
41	9.69 479	23	9.75 588	30	0.24 412	9.93 891	7	19	3 4	8.8	2.4 3.2	2.I 2.8
42	9.69 501	22	9.75 617	30	0.24 383	9.93 884	8	18		11.0	4.0	3.5
43	9.69 523	22	9.75 647	29	0.24 353	9.93 876	7	17	5 6	13.2	4.8	4.2
44	9.69 545	22	9.75 676	29	0.24 324 0.24 295	9.93 869	7	16	7 8	15.4	5.6	4.9
45	9.69 589	22	9.75 705	30	0.24 295	9.93 855	7 8	14	8	17.6	6.4 7.2	5.6 6.3
47	9.69 611	22	9.75 764	29	0.24 236	9.93 847		13	9	. 19.0	7.2	0.3
48	9.69 633	22	9.75 793	29	0.24 207	9.93 840	7	12				
49	9.69 655	22	9.75 822	30	0.24 178	9.93 833	7 7	II				
50	9.69 677	22	9.75 852	29	0.24 148	9.93 826	7	10				
51	9.69 699	22	9.75 881	29	0.24 119	9.93 819	8	9 8				
52 53	9.69 721	22	9.75 910	29	0.24 090	9.93 811	7	7				
54	9.69 765	22	9.75 969	30	0.24 031	9.93 797	7	6				
55	9.69 787	22	9.75 998	29	0.24 002	9.93 789	8	5				
56	9.69 809	22	9.76 027	29	0.23 973	9.93 782	7 7	4				
57	9.69831	22	9.76 056	30	0.23 944	9.93 775	7	3				
58 59	9.69 853	22	9.76 086	29	0.23 914	9.93 768	8	2 I				
60	9.69 897	22	9.76 144	29	0.23 856	9.93 753	7	6				
1	L Cos	d	L Cot	cd	L Tan	L Sin	d	1			P P	
	L 003	u	- 001	- u	Lian	L 3111	u		1			

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		30	,						49	
	1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
	0	9.69 897	20	9.76 144	-	0.23 856	9.93 753	_	60	
ı	1	9.69 919	22	9.76 173	29	0.23 827	9.93 746	8	59	
	2	9.69 941	22	9.76 202 9.76 231	29	0.23 798	9.93 738	7	58	
1	3	9.69 984	21	9.76 261	30	0.23 769	9.93 731	7	57	
1	5	9.70 006	22	9.76 290	29	0.23 710	9.93 717	7 8	55	
1		9.70 028	22	9.76 319	29	0.23 681	9.93 709	7	54	
1	7	9.70 050	22	9.76 348	29	0.23 652	9.93 702 9.93 695	7	53 52	
ı	9	9.70 093	21	9.76 406	29	0.23 594	9.93 687	8	51	30 29 28
1	10	9.70 115	22	9.76 435	29	0.23 565	9.93 680	7	50	I 3.0 2.9 2.8 2 6.0 5.8 5.6
1	II	9.70 137	22	9.76 464	29	0.23 536	9.93 673	8	49	2 6.0 5.8 5.6 3 9.0 8.7 8.4
ı	I2 I3	9.70 159	21	9.76 493	29	0.23 507	9.93 665		48	4 12.0 11.6 11.2
1	14	9.70 202	22	9.76 551	29	0.23 449	9.93 650	7 8	46	5 15.0 14.5 14.0 6 18.0 17.4 16.8
1	15	9.70 224	22	9.76 580	29	0.23 420	9.93 643	7	45	7 21.0 20.3 19.6
ł	16 17	9.70 245	22	9.76 609	30	0.23 391	9.93 636	7 8	44	8 24.0 23.2 22.4 9 27.0 26.1 25.2
1	18	9.70 288	21	9.76 668	29	0.23 361	9.93 628	7	43	9 27.0 26.1 25.2
	19	9.70 310	22	9.76 697	29	0.23 303	9.93 614	8	41	
	20	9.70 332	21	9.76 725	29	0.23 275	9.93 606	7	40	
	21	9.70 353	22	9.76 754	29	0.23 246	9.93 599	8	39	
	22	9.70 375 9.70 396	21	9.76 783	29	0.23 217	9.93 591	7	38	
	24	9.70418	22	9.76841	29	0.23 159	9.93 577	7	36	
-1	25	9.70 439	2I 22	9.76 870	29 29	0.23 130	9.93 569	8	35	22 21
-	26 27	9.70 461	21	9.76 899	29	0.23 101	9.93 562	8	34	
	28	9.70 504	22	9.76 957	29	0.23 072	9.93 554	7	33 32	I 2.2 2.I 2 4.4 4.2
_	29	9.70 525	2I 22	9.76 986	29 29	0.23 014	9.93 539	8	31	3 6.6 6.3
ı	30	9.70 547	21	9.77 015	29	0.22 985	9.93 532	7	30	4 8.8 8.4 5 11.0 10.5
	31	9.70 568	22	9.77 044	29	0.22 956	9.93 525	8	29	6 13.2 12.6
	32 33	9.70 590	21	9.77 073 9.77 IOI	28	0.22 927	9.93 517 9.93 510	7	28 27	7 15.4 14.7 8 17.6 16.8
_	34	9.70 633	22	9.77 130	29	0.22870	9.93 502	8	26	8 17.6 16.8 9 19.8 18.9
	35	9.70 654	2 I	9.77 159	29	0.22 841	9.93 495	7 8	25	
_	36 37	9.70 675	22	9.77 188	29	0.22 812	9.93 487 9.93 480	7	24	
ı	38	9.70 718	21	9.77 246	29	0.22 754	9.93 472	8	23	
1	39	9.70 739	2I 22	9.77 274	28	0.22 726	9.93 465	7	21	
-	10	9.70 761	21	9.77 303	29	0.22 697	9.93 457	7	20	
	41	9.70 782	21	9.77 332	20	0.22 668	9.93 450	8	19	
	42 43	9.70 824	21	9.77 361 9.77 390	29	0.22 639	9.93 442 9.93 435	7	18	8 7
ı	44	9.70 846	22 2I	9.77 418	28	0.22 582	9.93 427	8	16	1 0.8 0.7
	45	9.70 867 9.70 888	2 I 2 I	9.77 447	29	0.22 553	9.93 420	7 8	15	2 1.6 1.4
	46 47	9.70 909	21	9.77 476	29	0.22 524	9.93 412	7	14	3 2.4 2.I 4 3.2 2.8
н	48	9.70 931	22 2I	9.77 533	28	0.22 467	9.93 403	8	12	
Н	49	9.70 952	21	9.77 562	29	0.22 438	9.93 390	7	II	6 4.8 4.2
	50	9.70 973	21	9.77 591	28	0.22 409	9.93 382	7	10	7 5.6 4.9 8 6.4 5.6
	51 52	9.70 994	21	9.77 619	29	0.22 381	9.93 375 9.93 367	8	9	9 7.2 6.3
	53	9.71 036	2 1	9.77 677	29	0.22 332	9.93 360	7	7	
н	54	9.71 058	22	9.77 706	29 28	0.22 294	9.93 352	8	6	
1	55 56	9.71 079	21	9.77 734	20	0.22 266	9.93 344	8 7	5	
	57	9.71 121	21	9.77 763	28	0.22 237	9.93 337	8	4	
ш	58	9.71 142	2 I 2 I	9.77 820	29	0.22 180	9.93 322	7	2	
	59	9.71 163	21 2I	9.77 849	29 28	0.22 151	9.93 314	7	I	
F	60	9.71 184	 -	9.77 877		0.22 123	9.93 307		0	
Ī		L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP

(368)

	,	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP				
ı	0		<u>u</u>	l	- 4			<u>u</u>	60					
ı	7	9.71 184	21	9.77 877	29	0.22 123	9.93 307	8						
ı	2	9.71 205	21	9.77 935	29	0.22 094	9.93 299	8	59 58					
ı	3	9.71 247	21	9.77 963	28	0.22 037	9.93 284	7	57					
	4	9.71 268	2I 2I	9.77 992	29 28	0.22 008	9.93 276		56					
	5	9.71 289	21	9.78 020	29	0.21 980	9.93 269	7 8	55					
		9.71 310	21	9.78 049	28	0.21 931	9.93 261	8	54 53					
	7	9.71 352	21	9.78 106	29	0.21 894	9.93 246	7 8	52	29 28				
	9	9.71 373	21	9.78 135	29 28	0.21 865	9.93 238	8	51	I 2.9 2.8				
	10	9.71 393	21	9.78 163	29	0.21 837	9.93 230	7	50					
	II	9.71 414	21	9.78 192	28	0.21 808	9.93 223	8	49	2 5.8 5.6 3 8.7 8.4				
1	I2 I3	9.71 435 9.71 456	21	9.78 220 9.78 249	29	0.21 780	9.93 215	8	48 47	4 11.6 11.2 5 14.5 14.0				
ı	14	9.71 430	21	9.78 277	28	0.21 731	9.93 200	7	46	5 14.5 14.0 6 17.4 16.8				
	15	9.71 498	21	9.78 306	29	0.21 694	9.93 192	8	45	7 20.3 19.6				
ı	16	9.71 519	21	9.78 334	28 29	0.21 666	9.93 184	7	44	8 23.2 22.4 9 26.1 25.2				
ı	18	9.71 539 9.71 560	21	9.78 363 9.78 391	28	0.21 637	9.93 177	8	43	9 20.1 25.2				
	19	9.71 58.	21	9.78 419	28	0.21 581	9.93 161	8	42 41					
	20	9.71 602	21	9.78 448	29	0.21 552	9.93 154	7	40					
	21	9.71 622	20	9.78 476	28	0.21 524	9.93 146	8	39					
	22	9.71 643	21	9.78 505	29	0.21 495	9.93 138	8	38					
	23	9.71 664	2I 2I	9.78 533	28 29	0.21 467	9.93 131	8	37					
	24 25	9.71 685	20	9.78 562 9.78 590	28	0.21 438	9.93 123 9.93 115	8	36					
	26	9.71 726	21	9.78 618	28	0.21 382	9.93 108	7 8	35 34	21 20				
ı	27	9.71 747	21	9.78 647	29	0.21 353	9.93 100		33	I 2.I 2.0				
ı	28	9.71 767	20 2I	9.78 675	28 29	0.21 325	9.93 092	8	32	2 4.2 4.0				
	29	9.71 788	21	9.78 704	28	0.21 296	9.93 084	7	31	3 6.3 6.0 4 8.4 8.0				
ı	30	9.71 809	20	9.78 732	28	0.21 268	9.93 077	8	30					
ı	3I 32	9.71 829	21	9.78 760 9.78 789	29	0.21 240	9.93 0 69 9.93 0 61	8	29 28	5 10.5 10.0 6 12.6 12.0				
H	33	9.71 870	20	9.78 817	28	0.21 183	9.93 053	8	27	7 14.7 14.0 8 16.8 16.0				
ı	34	9.71 891	21	9.78 845	28	0.21 155	9.93 046	7	26	9 18.9 18.0				
	35	9.71 911	20 21	9.78 874	29 28	0.21 126	9.93 038	8	25					
	36	9.71 932	20	9.78 902	28	0.21 098	9.93 030	8	24					
	37 38	9.71 973	21	9.78 959	29	0.21 0/0	9.93 014	8	23					
	39	9.71 994	21	9.78 987	28 28	0.21 013	9.93 007	7 8	21					
1	40	9.72 014	20	9.79 015	28	0.20 985	9.92 999	8	20					
	41	9.72 034	21	9.79 043	20	0.20 957	9.92 991	8	19					
	42	9.72 055	20	9.79 072	28	0.20 928	9.92 983		18					
	44	9.72 096	21	9.79 100	28	0.20 872	9.92 978	8	16	8 7				
1	45	9.72 116	20	9.79 156	28	0.20 844	9.92 960	8	15	1 0.8 0.7 2 1.6 1.4				
	46	9.72 137	21	9.79 185	29 28	0.20 815	9.92 952	8	14	3 2.4 2.1				
1	47 48	9.72 I57 9.72 I77	20	9.79 213 9.79 241	28	0.20 787	9.92 944 9.92 936	8	13	4 3.2 2.8				
1	49	9.72 198	21	9.79 241	28	0.20 739	9.92 930	7	II	5 4.0 3.5 6 4.8 4.2				
	50	9.72 218	20	9.79 297	28	0.20 703	9.92 921		10					
	51	9.72 238	20	9.79 326	29	0.20 674	9.92 913	8		8 6.4 5.6				
	52	9.72 259	2I 2O	9.79 354	28	0.20 646	9.92 905	8	9 8	9 7.2 6.3				
	53	9.72 279	20	9.79 382	28	0.20 618	9.92 897	8	7					
	54 55	9.72 299 9.72 320	21	9.79 410 9.79 438	28	0.20 590	9.92 889	8	6					
	56	9.72 340	20	9.79 466	28	0.20 534	9.92 874	7 8	4					
	57	9.72 360	20	9.79 495	29	0.20 505	9.92 866	8	3					
	58	9.72 381	20	9.79 523	28	0.20 477	9.92 858	8	2					
	59 60	9.72 401	20	9.79 551	28	0.20 449	9.92 850	8	0					
	-	9.72 421		9.79 579		0.20 421		-	-					
		L Cos	d	L Cot	cd	L Tan	LSin	d	L'	PP				

_	32' 147'												
′	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP				
0	9.72 421	20	9.79 579	28	0.20 421	9.92 842	8	60					
1	9.72 441	20	9.79 607	28	0.20 393	9.92 834	8	59					
3	9.72 461	21	9.79 635	28	0.20 365	9.92 826	8	58					
4	9.72 502	20	9.79 691	28	0.20 309	9.92810	8	56					
5	9.72 522	20	9.79719	28 28	0.20 281	9.92 803	7	55					
6	9.72 542	20	9.79 747	29	0.20 253	9.92 795 9.92 787	8	54					
7 8	9.72 502	20	9.79 776	28	0.20 196	9.92 779	8	52	29 28 27				
9	9.72 602	20	9.79 832	28 28	0.20 168	9.92 771	8	51	1 2.9 2.8 2.7				
10	9.72 622	21	9.79 860	28	0.20 140	9.92 763	8	50	2 5.8 5.6 5.4				
II	9.72 643	20	9.79 888	28	0.20 112	9.92 755	8	49					
12 13	9.72 663	20	9.79 916	28	0.20 056	9.92 747 9.92 739	8	48	4 11.6 11.2 10.8 5 14.5 14.0 13.5				
14	9.72 703	20	9.79 972	28 28	0.20 028	9.92 731	8	46	6 17.4 16.8 16.2				
15	9.72 723	20 20	9.80 000	28	0.20 000	9.92 723	8	45	7 20.3 19.6 18.9 8 23.2 22.4 21.6				
16 17	9.72 743	20	9.80 028 9.80 056	28	0.19 972	9.92 715	8	44	8 23.2 22.4 21.6 9 26.1 25.2 24.3				
18	9.72 763 9.72 783	20	9.80 084	28	0.19916	9.92 707	8	43					
19	9.72 803	20 20	9.80 112	28 28	0.19888	9.92 691	8	41					
20	9.72823	20	9.80 140	28	0.19860	9.92 683	8	40					
21	9.72843	20	9.80 168	27	0.19832	9.92 675	8	39					
22 23	9.72 863	20	9.80 195 9.80 223	28	0.19805	9.92 667	8	38					
24	9.72 902	19	9.80 251	28	0.19749	9.92651	8	36					
25	9.72 922	20	9.80 279	28 28	0.19721	9.92 643	8	35	21 20 19				
26	9.72 942	20	9.80 307	28	0.19 693	9.92 635	8	34					
27 28	9.72 962 9.72 982	20	9.80 335 9.80 363	28	0.19 665	9.92 627	8	33	1 2.1 2.0 1.9 2 4.2 4.0 3.8				
29	9.73 002	20	9.80 391	28 28	0.19 609	9.92 611	8	31	3 6.3 6.0 5.7				
30	9.73 022	20	9.80 419	28	0.19 581	9.92 603	8	30	4 8.4 8.0 7.6				
31	9.73 041	19	9.80 447	27	0.19 553	9.92 595	8	29	5 10.5 10.0 9.5 6 12.6 12.0 11.4				
32	9.73 061	20	9.80 474	28	0.19 526	9.92 587	8	28	7 14.7 14.0 13.3				
33	9.73 081	20	9.80 502 9.80 530	28	0.19 498	9.92 579 9.92 571	8	27	8 16.8 16.0 15.2 9 18.9 18.0 17.1				
35	9.73 121	20	9.80 558	28 28	0.19 442	9.92 563	8	25	9 18.9 18.0 17.1				
36	9.73 140	19	9.80 586	28	0.19 414	9.92 555	9	24					
37	9.73 160 9.73 180	20	9.80 614	28	0.19386	9.92 546	8	23					
39	9.73 200	20	9.80 669	27	0.19 331	9.92 530	8	21					
40	9.73 219	19	9.80 697	28 28	0.19303	9.92 522	8	20					
41	9.73 239	20	9.80 725		0.19 275	9.92 514	8	19					
42	9.73 259	20 IQ	9.80 753	28 28	0.19 247	9.92 506	8	18					
43	9.73 278	20	9.80 781 9.80 808	27	0.19 219	9.92 498	8	17	9 8 7				
44	9.73 298	20	9.80 836	28	0.19 192	9.92 490	8	15	1 0.9 0.0 0.7				
46	9.73 337	19	9.80 864	28 28	0.19136	9.92 473	9	14	2 I.8 I.6 I.4 3 2.7 2.4 2.I				
47	9.73 357	20	9.80 892	27	0.19 108	9.92 465	8	13	4 3.6 3.2 2.8				
48	9.73 377 9.73 396	19	9.80 919	28	0.19 081	9.92 457	8	I2 II	5 4.5 4.0 3.5 6 5.4 4.8 4.2				
50	9.73 416	20	9.80 975	28	0.19 025	9.92 441	8	10					
51	9.73 435	19	9.81 003	28	0.18 997	9.92 433	8	9	8 7.2 6.4 5.6				
52	9.73 455	20 19	9.81 030	27 28	0.18970	9.92 425	8	8	9 8.1 7.2 6.3				
53	9.73 474	20	9.81 058	28	0.18 942	9.92 416	9	7					
54 55	9.73 494 9.73 513	19	9.81 086	27	0.18 914	9.92 408	8	6 5					
56	9.73 533	20	9.81 141	28	0.18 859	9.92 392	8	4					
57	9.73 552	20	9.81 169	28	0.18831	9.92 384	8	3					
58 59	9.73 572 9.73 591	19	9.81 196	28	o.18 8o4 o.18 776	9.92 376	9	2 I					
60	9.73 611	20	9.81 252	28	0.18 748	9.92 307	8	0					
-	L Cos	d	L Cot	c d	L Tan	L Sin		1	PP				
_	1000	ч	2 001	cu	Liali	1 2 3111	u	FEC					

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<u>'</u>	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP				
0	9.73 611	70	9.81 252	27	0.18 748	9.92 359	8	60					
1	9.73 630	19	9.81 279	27 28	0.18 721	9.92 351	8	59					
2	9.73 650	20 19	9.81 307	28	0.18 693	9.92 343	8	58					
3	9.73 669	20	9.81 335	27	0.18 665	9.92 335	9	57					
4	9.73 689	19	9.81 362 9.81 390	28	0.18 638	9.92 326	8	56					
5 6	9.73 708 9.73 727	19	9.81 418	28	0.18 582	9.92 318	8	55 54					
	9.73 747	20	9.81 445	27	0.18 555	9.92 302	8	53					
7 8	9.73 766	19	9.81 473	28	0.18 527	9.92 293	9	52					
9	9.73 785	19	9.81 500	27 28	0.18 500	9.92 285	8	51	28 27				
10	9.73 805	19	9.81 528	28	0.18 472	9.92 277	8	50	I 2.8 2.7				
11	9.73 824	-	9.81 556		0.18 444	9.92 269		49	2 5.6 5.4 3 8.4 8.1				
12	9.73 843	19 20	9.81 583	27 28	0.18 417	9.92 260	9	48	4 11.2 10.8				
13	9.73 863	19	9.81 611	27	0.18 389	9.92 252	8	47	5 14.0 13.5				
14	9.73 882 9.73 901	19	9.81 638 9.81 666	28	0.18 362 0.18 334	9.92 244	9	46					
15	9.73 901	20	9.81 693	27	0.18 307	9.92 235	8	45	7 19.6 18.9 8 22.4 21.6				
17	9.73 940	19	9.81 721	28	0.18 279	9.92 219	8	43	9 25.2 24.3				
18	9.73 959	19	9.81 748	27 28	0.18 252	9.92 211	8	42	71-3:7:3				
19	9.73 978	19	9.81 776	28 27	0.18 224	9.92 202	8	41					
20	9.73 997	20	9.81 803	28	0.18 197	9.92 194	8	40					
21	9.74017		9.81 831		0.18 169	9.92 186		39					
22	9.74 036	19	9.81 858	27 28	0.18 142	9.92 177	8	38					
23	9.74 055	19	9.81 886	27	0.18 114	9.92 169	8	37					
24	9.74 074	19	9.81 913 9.81 941	28	0.18 087	9.92 161	9	36					
25 26	9.74 093 9.74 II3	20	9.81 968	27	0.18 032	9.92 152 9.92 144	8	35	20 19 18				
27	9.74 132	19	9.81 996	28	0.18 004	9.92 136	8	33					
28	9.74 151	19	9.82 023	27	0.17 977	9.92 127	9	32	1 2.0 1.9 1.8 2 4.0 3.8 3.6				
29	9.74 170	19	9.82 051	28 27	0.17 949	9.92 119	8	31	3 6.0 5.7 5.4				
30	9.74 189		9.82 078	28	0.17 922	9.92 111		30	4 8.0 7.6 7.2				
31	9.74 208	19	9.82 106		0.17 894	9.92 102	9	29	5 10.0 9.5 9.0				
32	9.74 227	19	9.82 133	27 28	0.17 867	9.92 094	8	28	6 12.0 11.4 10.8 7 14.0 13.3 12.6				
33	9.74 246	19	9.82 161	27	0.17 839	9.92 0 86	9	27	7 14.0 13.3 12.0 8 16.0 15.2 14.4				
34	9.74 265	19	9.82 188	27	0.17 812	9.92 077	8	26	9 18.0 17.1 16.2				
35 36	9.74 284 9.74 303	19	9.82 243	28	0.17 785	9.92 069	9	25 24					
37	9.74 322	19	9.82 270	27	0.17 730	9.92 052	8	23					
38	9.74 341	19	9.82 298	28	0.17 702	9.92 044	8	22					
39	9.74 360	19	9.82 325	27	0.17 675	9.92 035	8	21					
40	9.74 379	-	9.82 352	28	0.17 648	9.92 027		20					
41	9.74 398	19	9.82 380		0.17 620	9.92 018	9	19					
42	9.74 417	19	9.82 407	27	0.17 593	9.92 010	8	18					
43	9.74 436	19	9.82 435	27	0.17 565	9.92 002	9	17	9 8				
44 45	9.74 455 9.74 474	19	9.82 462	27	0.17 538	9.91 993	8	16	8.0 0.0				
46	9.74 474	19	9.82 517	28	0.17 483	9.91 905	9	14	2 1.8 1.6				
47	9.74 512	19	9.82 544	27	0.17 456	9.91 968	8	13	3 2.7 2.4				
48	9.74 531	19	9.82 571	27	0.17 429	9.91 959	9	12	4 3.6 3.2				
49	9.74 549	18	9.82 599	28	0.17 401	9.91 951	9	II	5 4.5 4.0 6 5.4 4.8				
50	9.74 568	19	9.82 626	27	0.17 374	9.91 942	8	10					
51	9.74 587		9.82 653	28	0.17 347	9.91 934		9	8 7.2 6.4				
52	9.74 606	19	9.82 681	27	0.17319	9.91 925	9 8		° 9 8.1 7.2				
53	9.74 625	19	9.82 708	27	0.17 292	9.91 917	9	7					
54 55	9.74 644	18	9.82 735 9.82 762	27	0.17 265	9.91 908	8	5					
56	9.74 681	19	9.82 790	28	0.17 230	9.91 900	9	4					
57	9.74 700	19	9.82817	27	0.17 183	9.91 883	8	3					
. 58	9.74 719	19	9.82 844	27	0.17 156	9.91 874	9	2					
59	9.74 737	19	9.82 871	27	0.17 129	9.91 866	9	Ι					
60	9.74 756		9.82 899		0.17 101	9.91 857		_0					
	L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP				

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	34° 145°											
1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP			
0	9.74 756	19	9.82 899	27	0.17 101	9.91 857	8	60				
1	9.74 775	19	9.82 926	27	0.17 074	9.91 849		59				
3	9.74 794 9.74 812	18	9.82 953 9.82 980	27	0.17 047	9.91 840	9	58				
4	9.74 831	19	9.83 008	28	0.16 992	9.91 823	9	56				
5	9.74 850	19	9.83 035	27 27	0.16 965	9.91815	8	55				
6	9.74 868	19	9.83 062	27	0.16 938	9.91 806	9	54				
7 8	9.74 887 9.74 906	19	9.83 089 9.83 117	28	0.16 883	9.91 798 9.91 789	9	53 52				
9	9.74 924	18	9.83 144	27	0.16856	9.91 781	9	51	28 27 26			
10	9.74 943	18	9.83 171	27 27	0.16829	9.91 772	9	50	1 2.8 2.7 2.6 2 5.6 5.4 5.2			
II	9.74 961	19	9.83 198	27	0.16 802	9.91 763	8	49	2 5.6 5.4 5.2 3 8.4 8.1 7.8			
12 13	9.74 980 9.74 999	19	9.83 225 9.83 252	27	0.16 775	9.91 755 9.91 746	9	48	4 11.2 10.8 10.4			
14	9.75 017	18	9.83 280	28	0.16720	9.91 738		46	5 14.0 13.5 13.0 6 16.8 16.2 15.6			
15	9.75 036	18	9.83 307	27 27	0.16 693	9.91 729	9	45	7 19.6 18.9 18.2			
16	9.75 054	19	9.83 334 9.83 361	27	o.16 666 o.16 639	9.91 720	9	44				
17	9.75 073 9.75 091	18	9.83 388	27	0.16 612	9.91 712	9	43	9 25.2 24.3 23.4			
19	9.75 110	19	9.83 415	27	0.16 585	9.91 695	9	41				
20	9.75 128	19	9.83 442	27 28	0.16 558	9.91 686	9	40				
21	9.75 147	18	9.83 470	27	0.16 530	9.91 677	8	39				
22 23	9.75 165 9.75 184	19	9.83 497 9.83 524	27	0.16 503	9.91 669 9.91 660	9	38				
24	9.75 202	18	9.83 551	27	0.16 449	9.91 651	9	36				
25	9.75 221	19	9.83 578	27 27	0.16 422	9.91 643	8	35				
26 27	9.75 239	19	9.83 605	27	0.16 395	9.91 634	9	34	19 18			
28	9.75 276	18	9.83 659	27	0.16 341	9.91 617	8	33	1 1.9 1.8 2 3.8 3.6			
29	9.75 294	18	9.83 686	27	0.16 314	9.91 608	9	31	3 5.7 5.4			
30	9.75 313	18	9.83 713	27	0.16 287	9.91 599	8	30	4 7.6 7.2			
31	9.75 331	19	9.83 740	28	0.16 260	9.91 591	9	29	5 9.5 9.0 6 11.4 10.8			
32 33	9.75 350 9.75 368	18	9.83 768 9.83 795	27	0.16 232	9.91 582 9.91 573	9	27	7 13.3 12.6			
34	9.75 386	18	9.83 822	27	0.16 178	9.91 565	8	26	8 15.2 14.4 9 17.1 16.2			
35	9.75 405	19 18	9.83 849	27 27	0.16151	9.91 556	9	25	9 17.1 10.2			
36 37	9.75 423 9.75 441	18	9.83 876 9.83 903	27	0.16 124	9.91 547 9.91 538	9	24				
38	9.75 459	18	9.83 930	27	0.16 070	9.91 530	8	22				
39	9.75 478	19 18	9.83 957	27 27	0.16 043	9.91 521	9	21				
40	9.75 496	18	9.83 984	27	0.16 016	9.91 512	8	20				
41 42	9.75 514	19	9.84 011	27	0.15 989	9.91 504	9	19				
43	9.75 533 9.75 551	18	9.84 o38 9.84 o65	27	0.15 962	9.91 495 9.91 486	9	17				
44	9.75 569	18	9.84 092	27	0.15 908	9.91 477	9	16	9 8			
45 46	9.75 587 9.75 605	18	9.84 119	27 27	0.15 881	9.91 469	9	15	1 0.9 0.8 2 1.8 1.6			
47	9.75 624	19	9.84 173	27	0.15 827	9.91 451	9	13	3 2.7 2.4			
48	9.75 642	18	9.84 200	27	0.15 800	9.91 442	9	12	4 3.6 3.2			
49 50	9.75 660	18	9.84 227	27 27	0.15 773	9.91 433	8	II	5 4.5 4.0 6 5.4 4.8			
	9.75 678	18	9.84 254	26	0.15 746	9.91 425	9	10	7 6.3 5.6			
51 52	9.75 696	18	9.84 280 9.84 307	27	0.15 720	9.91 416	9	8	8 7.2 6.4 9 8.1 7.2			
53	9.75 733	19	9.84 334	27	0.15 666	9.91 398	9	7	7,0.2			
54	9.75 751	18	9.84 361	27	0.15 639	9.91 389	8	6				
55 56	9.75 769 9.75 787	18	9.84 388	27	0.15 612	9.91 381	9	5 4				
57	9.75 805	18	9.84 442	27	0.15 558	9.91 363	9	3				
58 59	9.75 823 9.75 841	18	9.84 469	27 27	0.15 531	9.91 354	9	2 I				
60	9.75 859	18	9.84 496	27	0.15 504	9.91 345	9	0				
	L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP			
_	1940	u	LOOT	l C u	Lian	(252)	u	EE.				

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1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.75 859	18	9.84 523	27	0.15 477	9.91 336	8	60	
1	9.75 877	18	9.84 550	26	0.15 450	9.91 328	9	59	
2	9.75 895	18	9.84 576	27	0.15 424	9.91 319	9	58	
3	9.75 913	18	9.84 603	27	0.15 397	9.91 310	9	57 56	
4 5	9.75 931	18	9.84 657	27	0.15 343	9.91 292	9	55	
ő	9.75 967	18	9.84 684	27	0.15 316	9.91 283	9	54	
7 8	9.75 985	18	9.84 711	27 27	0.15 289	9.91 274	9	53	
8 9	9.76 00 3 9.76 0 21	18	9.84 738 9.84 764	26	0.15 262	9.91 266 9.91 257	9	52 51	27 26
10		18	9.84 791	27	0.15 209	9.91 248	9	50	1 2.7 2.6
TT	9.76 039	18	9.84 818	27	0.15 182	9.91 239	9	49	2 5.4 5.2
12	9.76 075	18	9.84 845	27	0.15 155	9.91 239	9	48	3 8.1 7.8
13	9.76 093	18 18	9.84 872	27	0.15 128	9.91 221	9	47	4 10.8 10.4 5 13.5 13.0
14	9.76 111	18	9.84 899	27 26	0.15 101	9.91 212	9	46	6 16.2 15.6
15	9.76 129 9.76 146	17	9.84 925 9.84 952	27	0.15 075	9.91 2 0 3 9.91 194	9	45 44	7 18.9 18.2 8 21.6 20.8
17	9.76 164	18	9.84 979	27	0.15 021	9.91 185	9	43	8 21.6 20.8 9 24.3 23.4
18	9.76 182	18	9.85 006	27	0.14994	9.91 176	9	42	91 -4-3 -3-4
19	9.76 200	18	9.85 033	27 26	0.14 967	9.91 167	9	41	
20	9.76 218	18	9.85 059	27	0.14941	9.91 158	9	40	
21	9.76 236	17	9.85 086	27	0.14 914	9.91 149	8	39	
22	9.76 253	18	9.85 113	27	0.14 887 0.14 860	9.91 141 9.91 132	9	38 37	
23	9.76 271 9.76 289	18	9.85 166	26	0.14 834	9.91 132	9	36	
25	9.76 307	18	9.85 193	27	0.14 807	9.91 114	9	35	40 47
26	9.76 324	17	9.85 220	27	0.14 780	9.91 105	9	34	18 17
27	9.76 342	18	9.85 247	27 26	0.14753	9.91 096	9	33	1 1.8 1.7 2 3.6 3.4
28 29	9.76 360	18	9.85 273 9.85 300	27	0.14 727	9.91 087 9.91 078	9	32 31	3 5.4 5.1
30	9.76 378	17	9.85 327	27	0.14 673	9.91 069	9	30	4 7.2 6.8
31	9.76 413	18	9.85 354	27	0.14 646	9.91 060	9	20	5 9.0 8.5 6 10.8 10.2
32	9.76 431	18	9.85 380	26	0.14 620	9.91 051	9	28	
33	9.76 448	17	9.85 407	27	0.14 593	9.91 042	9	27	8 14.4 13.6
34	9.76 466	18	9.85 434	27 26	0.14 566	9.91 033	10	26	9 16.2 15.3
35 36	9.76 484	17	9.85 460	27	0.14 540	9.91 023 9.91 014	9	25 24	
37	9.76 501	18	9.85 487	27	0.14 513	9.91 014	9	23	
38	9.76 537	18	9.85 540	26	0.14 460	9.90 996	9	22	
39	9.76 554	17	9.85 567	27 27	0.14 433	9.90 987	9	21	
40	9.76 572	18	9.85 594	26	0.14406	9.90 978	9	20	
41	9.76 590	17	9.85 620	27	0.14 380	9.90 969	9	19	
42 43	9.76 607	18	9.85 647	27	0.14 353	9.90 960	9	18	10 9 8
43	9.76 625	17	9.85 700	26	0.14 326	9.90 931	9	16	1 1.0 0.9 0.8
45	9.76 660	18	9.85 727	27	0.14 273	9.90 933	9	15	2 2.0 1.8 1.6
46	9.76 677	17	9.85 754	27 26	0.14 246	9.90 924	9	14	3 3.0 2.7 2.4 4 4.0 3.6 3.2
47	9.76 695	17	9.85 780	27	0.14 220	9.90 915	9	13	5 5.0 4.5 4.0
48 49	9.76 712	18	9.85 807	27	0.14 193	9.90 906	10	11	6 6.0 5.4 4.8
50	9.76 747	17	9.85 860	26	0.14 140	9.90 887	9	10	7 7.0 6.3 5.6 8 8.0 7.2 6.4
51	9.76 765	18	9.85 887	27	0.14 113	9.90 878	9	9	8 8.0 7.2 6.4 9 9.0 8.1 7.2
52	9.76 782	17	9.85 913	26	0.14 087	9.90 869	9	8	
53	9.76 800	18	9.85 940	27	0.14 060	9.90 860	9	7	
54	9.76817	18	9.85 967	26	0.14 033	9.90 851	9	6	
55 56	9.76 835 9.76 852	17	9.85 993	27	0.14 007	9.90 842	10	5	
57	9.76 870	18	9.86 046	26	0.13 954	9.90 823	9	3	
58	9.76 887	17	9.86 073	27	0.13 927	9.90 814	9	2	
59	9.76 904	17	9.86 100	27 26	0.13 900	9.90 805	9	I	
60	9.76 922	-	9.86 126		0.13874	9.90 796		0	РР
	L Cos	d	L Cot	cd	L Tan	L Sin	d		I PP

F	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP					
L		<u>a</u>		C a			<u>a</u>		PP					
0	9.76 922	17	9.86 126	27	0.13874	9.90 796	9	60						
1 2	9.76 939 9.76 957	18	9.86 153	26	0.13 847	9.90 787	10	59 58						
3	9.76 974	17	9.86 206	27	0.13 794	9.90 768	9	57						
4	9.76 991	17	9.86 232	26	0.13 768	9.90 759	9	56						
5	9.77 009	17	9.86 285	27 26	0.13 741	9.90 750	9	55						
	9.77 026	17	9.86 312	27	0.13 715	9.90 741	10	54						
7 8	9.77 043 9.77 061	18	9.86 338	26	0.13 662	9.90 731 9.90 722	9	53 52						
9	9.77 078	17	9.86 365	27	0.13 635	9.90713	9	51	27 26					
10	9.77 095	17	9.86 392	27 26	0.13 608	9.90 704	9	50	I 2.7 2.6					
II	9.77 112	17 18	9.86 418		0.13 582	9.90 694	10	49	2 5.4 5.2 3 8.1 7.8					
12	9.77 130	17	9.86 445	27 26	0.13 555	9.90 685	9	48	4 10.8 10.4					
13	9.77 147	17	9.86 471 9.86 498	27	0.13 529	9.90 676	9	47	5 13.5 13.0 6 16.2 15.6					
15	9.77 181	17	9.86 524	26	0.13 476	9.90 657	IO	45						
16	9.77 199	18	9.86 551	27 26	0.13 449	9.90 648	9	44	7 18.9 18.2 8 21.6 20.8					
17	9.77 216	17 17	9.86 577	26	0.13 423	9.90 639	9	43	9 24.3 23.4					
18	9.77 233	17	9.86 603 9.86 630	27	0.13 397	9.90 630	10	42						
20	9.77 250	18	9.86 656	26	0.13 370	9.90 611	9	41 40						
21	9.77 285	17	9.86 683	27	0.13 344	9.90 602	9							
22	9.77 302	17	9.86 709	26	0.13 317	9.90 592	IO	39 38						
23	9.77 319	17	9.86 736	27	0.13 264	9.90 583	9	37						
24	9.77 336	17	9.86 762	26 27	0.13 238	9.90 574	9	36						
25	9.77 353	17 17	9.86 789	26	0.13 211	9.90 565	9	35	40 47 40					
26 27	9.77 370	17	9.86 842	27	0.13 185	9.90 555	9	34	18 17 16					
28	9.77 405	18	9.86 868	26	0.13 132	9.90 540	9	32	1 1.8 1.7 1.6					
29	9.77 422	17	9.86 894	26	0.13 106	9.90 527	10	31	2 3.6 3.4 3.2 3 5.4 5.1 4.8					
30	9.77 439	17	9.86 921	27	0.13 079	9.90 518	9	30	4 7.2 6.8 6.4					
31	9.77 456	17	9.86 947		0.13 053	9.90 509	9	29	5 9.0 8.5 8.0					
32	9-77 473	17 17	9.86 974	27 26	0.13 026	9.90 499	10	28	6 10.8 10.2 9.6 7 12.6 11.9 11.2					
33	9.77 490	17	9.87 000	27	0.13 000	9.90 490	10	27 26	8 14.4 13.6 12.8					
34 35	9.77 507 9.77 524	17	9.87 053	26	0.12 973	9.90 480	9	25	9 16.2 15.3 14.4					
36	9.77 541	17	9.87 079	26	0.12 921	9.90 462	9	24						
37	9.77 558	17	9.87 106	27 26	0.12 894	9.90 452	10	23						
38	9-77 575	17 17	9.87 132	26	0.12 868	9.90 443	9	22						
39 40	9.77 592	17	9.87 158	27	0.12 815	9.90 434	10	2I 20						
	9.77 609	17		26		9.90 424	9							
4I 42	9.77 626	17	9.87 211	27	0.12 789	9.90 415	10	19						
43	9.77 660	17	9.87 264	26	0.12 736	9.90 396	9	17	10 9					
44	9.77 677	17	9.87 290	26 27	0.12710	9.90 386	10	16	1 1.0 0.9					
45	9.77 694	17	9.87 317	26	0.12 683	9.90 377	9	15	2 2.0 1.8					
46 47	9.77 711	17	9.87 343	26	0.12 631	9.90 368	10	14	3 3.0 2.7					
48	9.77 744	16	9.87 396	27	0.12 604	9.90 330	9	12	4 4.0 3.6					
49	9.77 761	17	9.87 422	26 26	0.12 578	9.90 339	10	II	5 5.0 4.5 6 6.0 5.4					
50	9.77 778	17	9.87 448	27	0.12552	9.90 330	9	10	7 7.0 6.3					
51	9.77 795		9.87 475	26	0.12525	9.90 320	9	9						
52	9.77 812	17 17	9.87 501	26	0.12499	9.90 311	10	8	9 9.0 8.1					
53 54	9.77 829	17	9.87 554	27	0.12 473	9.90 301	9	7 6						
55	9.77 862	16	9.87 580	26	0.12 440	9.90 292	10	5						
56	9.77 879	17	9.87 606	26	0.12 394	9.90 273	9	4						
57	9.77 896	17 17	9.87 633	27 26	0.12 367	9.90 263	9	3						
58 59	9.77 913	17	9.87 659	26	0.12 341	9.90 254 9.90 244	10	2 I						
60	9.77 930	16	9.87 711	26	0.12 315	9.90 244	9	0						
1		-						-	PP					
	L Cos	d	L Cot	c d	L Tan	L Sin	a		PP					

(374)

	7	L Sin	d	L Tan	c d	L Cot	L Cos	d		РР						
H	0	9.77 946		9.87 711		0.12 289	9.90 235		60							
	ī	9.77 963	17	9.87 738	27	0.12 262	9.90 225	IO	59							
	2	9.77 980	17	9.87 764	26 26	0.12 236	9.90 216	9	58							
	3	9.77 997	17	9.87 790	27	0.12 210	9.90 206	9	57							
	4	9.78 o13 9.78 o30	17	9.87 817	26	0.12 183	9.90 197 9.90 187	10	56 55							
ı	5 6	9.78 047	17	9.87 869	26	0.12 131	9.90 178	9	54							
ш	7 8	9.78 063	16	9.87 895	26 27	0.12 105	9.90 168	10 9	53							
	8 9	9.78 o8o 9.78 o97	17	9.87 922 9.87 948	26	0.12078	9.90 159	10	52 51	27 26						
1	- 1	9.78 113	16	9.87 974	26	0.12 026	9.90 139	10	50	1 2.7 2.6						
I	- 1	9.78 130	17	9.88 000	26	0.12 000	9.90 130	9	49	2 5.4 5.2 3 8.1 7.8						
ī		9.78 147	17	9.88 027	27	0.11973	9.90 120	10	48	3 8.1 7.8 4 10.8 10.4						
1	- 1	9.78 163	16 17	9.88 053	26 26	0.11947	9.90 111	9	47	5 13.5 13.0						
I		9.78 180	17	9.88 079	26	0.11 921	9.90 101	10	46	6 16.2 15.6 7 18.9 18.2						
I		9.78 213	16	9.88 131	26	0.11 869	9.90 082	9	44	7 18.9 18.2 8 21.6 20.8						
1	7	9.78 230	17	9.88 158	27 26	0.11842	9.90 072	10	43	9 24.3 23.4						
I		9.78 246	16 17	9.88 184	26	0.11816	9.90 063	9	42							
2		9.78 263	17	9.88 236	26	0.11790	9.90 053	10	41 40							
2	1	9.78 280	16	9.88 262	26	0.11 764	9.90 043	9	39							
2		9.78 313	17	9.88 289	27	0.11 730	9.90 034	10	38							
2	3	9.78 329	16 17	9.88 315	26 26	0.11685	9.90014	10	37							
2		9.78 346	16	9.88 341	26	0.11659	9.90 005	10	36							
2 2		9.78 362	17	9.88 367 9.88 393	26	0.11 633	9.89 995	10	35	17 16						
2	- 1	9.78 395	16	9.88 420	27	0.11 580	9.89 976	9	33	1 1.7 1.6						
2		9.78 412	17 16	9.88 446	26 26	0.11 554	9.89 966	10	32	2 3.4 3.2						
3	- 1	9.78 428	17	9.88 472	26	0.11 528	9.89 956	9	31 30	3 5.1 4.8						
ш	- 1	9.78 445	16	9.88 498	26	0.11 502	9.89 947	10	29	4 6.8 6.4 5 8.5 8.0						
3	2	9.78 461 9.78 478	17	9.88 524 9.88 550	26	0.11 476	9.89 937	IO	28	6 10.2 9.6						
	3	9.78 494	16	9.88 577	27 26	0.11 423	9.89 918	9	27	7 11.9 11.2 8 13.6 12.8						
3		9.78 510	17	9.88 603	26	0.11 397	9.89 908	10	26	8 13.6 12.8 9 15.3 14.4						
3	5	9.78 527 9.78 543	16	9.88 629 9.88 655	26	0.11 371	9.89 898 9.89 888	10	25	91-3.5						
3		9.78 560	17	9.88 681	26	0.11 319	9.89 879	9	23							
3	8	9.78 576	16	9.88 707	26 26	0.11 293	9.89 869	IO IO	22							
	9.	9.78 592	17	9.88 733	26	0.11 267	9.89 859	10	21							
	0	9.78 609	16	9.88 759	27	0.11 241	9.89 849	9	1							
4	.1	9.78 625 9.78 642	17	9.88 786	26	0.11 214	9.89 830	10	19							
	3	9.78 658	16	9.88 838	26 26	0.11162	9.89 820	10	17	10 9						
4	4	9.78 674	16 17	9.88 864	26	0.11 136	9.89810	.10	16							
	5	9.78 691 9.78 707	16	9.88 890	26	0.11 110	9.89801	10	15	1 1.0 0.9 2.0 1.8						
	7	9.78 723	16	9.88 942	26	0.11 058	9.89 781	10	13	3 3.0 2.7						
4	8	9.78 739	16	9.88 968	26 26	0.11 032	9.89771	10	12	4 4.0 3.6 5 5.0 4.5						
	9	9.78 756	17	9.88 994	26	0.11 006	9.89 761	9	11	6 6.0 5.4						
	0	9.78 772	16	9.89 020	26	0.10 980	9.89 752	10	10	7 7.0 6.3						
	2	9.78 788	17	9.89 046 9.89 073	27	0.10 954	9.89 742 9.89 732	10	9 8	8 8.0 7.2 9 9.0 8.1						
	3	9.78 821	16	9.89 099	26	0.10 901	9.89 722	10	7	317.						
5	54	9.78 837	16	9.89 125	26	0.10875	9.89 712	10	6							
	55	9.78 853 9.78 869	16	9.89 151	26	0.10 849	9.89 702 9.89 693	9	5 4							
	56	9.78 886	17	9.89 203	26	0.10 797	9.89 683	10	3							
	58	9.78 902	16	9.89 229	26	0.10771	9.89 673	IO	2							
5	59	9.78 918	16	9.89 255	26	0.10 745	9.89 663	10	I							
0	30	9.78 934		9.89 281		0.10719	9.89 653		0							
L		L Cos	d	L Cot	c d	L Tan	LSin	d	1	/ PP						

Column C										
1 9.78 9.79 16 9.89 3.79 2.60 0.10 6.79 9.89 6.34 9.89 6.34 9.89 7.79 9.79	1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
1 9.78 9.56 7 9.89 9.73 7 9.89 9.73 7 9.79 9.75 7 9.89 9.73 7 9.79 9.75 7 9.89 9.73 7 9.79 9.75 7 9.89 9.7	0	9.78 934	76	9.89 281	26			70	60	
2 9,78 996 16 9,89 935 26 0.10 610 589 9,89 624 10 55 5 799 11 6 9,89 437 26 0.10 55 9,79 931 16 9,89 437 26 0.10 55 9,79 931 16 9,89 437 26 0.10 537 9,89 584 10 53 53 26 0.10 537 9,89 584 10 53 26 0.10 53 9,89 584 10 53 26 0.10 53 9,89 584 10 53 26 0.10 53 9,89 584 10 53 26 0.10 53 9,89 584 10 53 26 0.10 53 9,89 584 10 53 26 0.10 53 26 0.10 53 26 0.10 53 26 0.10 53 26 0.10 53 26 0.10 53 26 0.10 53 26 0.10 27 28 28 28 28 28 28 28		9.78 950				0.10 693				
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9 0.79 0.79 16 0.88 5.15 26 0.10 4.89 0.89 5.51 10 10 17 17 18 0.79 118 17 0.89 5.67 17 0.89 5.67 18 0.10 4.57 0.89 5.53 10 48 4 10.4 10.0 48 4 10.4 4	8									96 95
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11 0.79 111 17 0.98 567 20 0.10 31 0.89 544 10 47 10 0.10 48 4 10.4 10.0 10.0 11.5 0.79 17 16 0.98 0.10 32 0.10 381 0.80 524 10 47 10 48 4 10.4 10.0 10.0 11.5 0.79 17 16 0.98 0.10 381 0.80 524 10 47 10 48 4 10.4 10.0 10.0 11.5 0.79 17 16 0.98 0.10 381 0.80 524 10 47 48 4 10.4 10.0 10.0 11.5 13.0 12.5 13.0 13.	10	9.79 095				0.10 459	9.89 554		50	
12 9.79 144 16 9.89 903 26 0.10 381 9.89 524 10 47 16 9.89 645 26 0.10 355 9.89 534 10 47 16 9.89 647 26 0.10 355 9.89 534 10 45 7 18.2 17.5 17.							9.89 544			3 7.8 7.5
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		99.			140					
ı	1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
ı	0	9.79 887	16	9.90 837	26	0.09 163	9.89 050	10	60	
ı	I	9.79 903	15	9.90 863	26	0.09 137	9.89 040	10	59	
ı	3	9.79 918 9.79 934	16	9.90 889	25	0.09 111	9.89 030	10	58 57	
ı	4	9.79 950	16	9.90 940	26	0.09 060	9.89 009	11	56	
ı	5	9.79 965	15 16	9.90 966	26 26	0.09 034	9.88 999	10	55	
ı	6	9.79 981	15	9.90 992 9.91 018	26	0.09 008	9.88 989 9.88 978	II	54	
ı	7 8	9.79 996	16	9.91 013	25	0.08 957	9.88 968	10	53	26 25
ı	9	9.80 027	15 16	9.91 069	26 26	0.08 931	9.88 958	IO	51	1 2.6 2.5
ı	10	9.80 043	15	9.91 095	26	0.08 905	9.88 948	11	56	2 5.2 5.0
ı	II	9.80 058	16	9.91 121	26	0.08 879	9.88 937	10	49	3 7.8 7.5 4 10.4 10.0
ı	13	9.80 074 9.80 089	15	9.91 147	25	0.08 853	9.88 927 9.88 917	10	48	4 10.4 10.0 5 13.0 12.5
ı	14	9.80 105	16	9.91 198	26 26	0.08 802	9.88 906	II	46	6 15.6 15.0
ı	15	9.80 120	15 16	9.91 224	26	0.08 776	9.88 896	10	45	7 18.2 17.5 8 20.8 20.0
ı	16	9.80 136 9.80 151	15	9.91 250	26	0.08 750	9.88 886 9.88 875	11	44	9 23.4 22.5
	18	9.80 166	15	9.91 301	25	0.08 699	9.88 865	10	43	
	19	9.80 182	16 15	9.91 327	26 26	0.08 673	9.88 855	10	41	
1	20	9.80 197	16	9.91 353	26	0.08 647	9.88 844	10	40	
	2I 22	9.80 213 9.80 228	15	9.91 379	25	0.08 621	9.88 834	10	39 38	
1	23	9.80 224	16	9.91 404 9.91 430	26	0.08 570	9.88 813	II	37	
ı	24	9.80 259	15	9.91 456	26 26	0.08 544	9.88 803	10	36	
1	25	9.80 274 9.80 290	15 16	9.91 482	25	0.08 518	9.88 793 9.88 782	11	35	16 15
ı	27	9.80 305	15	9.91 507 9.91 533	26	0.08 467	9.88 772	10	34	1 1.6 1.5
ı	28	9.80 320	15	9.91 559	26	0.08 441	9.88 761	II	32	2 3.2 3.0
ı	29	9.80 336	16	9.91 585	26 25	0.08 415	9.88 751	10	31	3 4.8 4.5 4 6.4 6.0
ı	30	9.80 351	15	9.91 610	26	0.08 390	9.88 741	II	30	
ı	31 32	9.80 366 9.80 382	16	9.91 636 9.91 662	26	o.o8 364 o.o8 338	9.88 730	10	29	6 9.6 9.0
ı	33	9.80 302	15	9.91 688	26	0.08 312	9.88 709	11	27	7 II.2 IO.5 8 I2.8 I2.0
	34	9.80 412	15	9.91713	25 26	0.08 287	9.88 699	10	26	9 14.4 13.5
ı	35 36	9.80 428 9.80 443	15	9.91 739 9.91 765	26	0.08 261	9.88 688 9.88 678	10	25	
ı	37	9.80 443	15	9.91 703	26	0.08 209	9.88 668	10	23	
ı	38	9.80 473	15 16	9.91816	25 26	0.08 184	9.88 657	II	22	
ı	39	9.80 489	15	9.91 842	26	0.08 158	9.88 647	10	21	
	40	9.80 504	15	9.91 868	25	0.08 132	9.88 636	10	20	
	4I 42	9.80 519 9.80 534	15	9.91 893	26	0.08 107	9.88 626 9.88 615	11	18	
	43	9.80 550	16	9.91 945	26	0.08 055	9.88 605	10	17	11 10
	44	9.80 565	15	9.91 971	26 25	0.08 029	9.88 594	11	16	1 1.1 1.0
	45 46	9.80 580 9.80 595	15	9.91 996 9.92 022	26	0.08 004	9.88 584 9.88 573	11	15	2 2.2 2.0
	47	9.80610	15	9.92 048	26	0.07 952	9.88 563	10	13	3 3.3 3.0
	48	9.80 625	15 16	9.92 073	25 26	0.07 927	9.88 552	II	12	
	49 50	9.80 64 1 9.80 656	15	$\frac{9.92099}{9.92125}$	26	0.07 901	9.88 542	II	11 10	6 6.6 6.0
	51	9.80 671	15	9.92 125	25	0.07 850	9.88 531	10		7 7.7 7.0 8 8.8 8.0
	52	9.80 686	15	9.92 176	26	0.07 824	9.88 510	11	8	9 9.9 9.0
	53	9.80 701	15 15	9.92 202	26	0.07 798	9.88 499	II	7	
	54	9.80 716	15	9.92 227	25	0.07 773	9.88 489 9.88 478	11	6	
1	55 56	9.80 746	15	9.92 253 9.92 279	26	0.07 747	9.88 468	10	5 4	
	57	9.80 762	16	9.92 304	25	0.07 696	9.88 457	II	3	
	58 59	9.80 777 9.80 792	15	9.92 330 9.92 356	26 26	0.07 670	9.88 447	IO	2 I	
1	60	9.80 807	15	9.92 381	25	0.07 619	9.88 436	11	0	
		L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP

	40°						1	39°	
1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.80 807		9.92381	26	0.07 619	9.88 425	10	60	
1	9.80 822	15	9.92 407	26	0.07 593	9.88 415	11	59	
2	9.80 837	15	9.92 433	25	0.07 567	9.88 404	10	58	
3	9.80 852	15	9.92 458	26	0.07 542	9.88 394	II	57	
4	9.80 867 9.80 882	15	9.92 484	26	0.07 490	9.88 372	II	56 55	
5 6	9.80 897	15	9.92 535	25	0.07 465	9.88 362	10	54	
7 8	9.80 912	15	9.92 561	26	0.07 439	9.88 351	II	53	
	9.80 927	15 15	9.92 587	26 25	0.07 413	9.88 340	10	52	26 25
9	9.80 942	15	9.92612	26	0.07 388	9.88 330	II	51	
10	9.80 957	15	9.92 638	25	0.07 362	9.88 319	II	50	I 2.6 2.5 2 5.2 5.0
II	9.80 972	15	9.92 663	26	0.07 337	9.88 308	10	49	3 7.8 7.5
12	9.80 987	15	9.92 009	26	0.07 285	9.88 287	ΙI	47	4 10.4 10.0
14	9.81 017	15	9.92 740	25	0.07 260	9.88 276	II	46	5 13.0 12.5 6 15.6 15.0
15	9.81 032	15	9.92 766	26 26	0.07 234	9.88 266	10	45	
16	9.81 047	15	9.92 792	25	0.07 208	9.88 255	II	44	8 20.8 20.0
17	9.81 061	15	9.92 817	26	0.07 183	9.88 234	10	43	9 23.4 22.5
10	9.81 076	15	9.92 868	25	0.07 137	9.88 223	II	41	
20	9.81 106	15	9.92 894	26	0.07 106	9.88 212	II	40	
21	9.81 121	15	9.92 920	26	0.07 080	9.88 201	II	39	
22	9.81 136	15	9.92 925	25 25	0.07 055	9.88 191	10	38	
23	9.81 151	15	9.92 971		0.07 029	9.88 180	II	37	
24	9.81 166	15	9.92 996	25 26	0.07 004	9.88 169	II	36	
25 26	9.81 180	14	9.93 022	26	0.06 978	9.88 158	IO	35	
27	9.81 210	15	9.93 048	25	0.06 932	9.88 137	II	34	15 14
28	9.81 225	15	9.93 073	26	0.06 901	9.88 126	II	32	1 1.5 1.4
29	9.81 240	15	9.93 124	25 26	0.06 876	9.88 115	II	31	2 3.0 2.8
30	9.81 254	14	9.93 150		0.06850	9.88 105	II	30	3 4.5 4.2 4 6.0 5.6
31	9.81 269	15	9.93 175	25 26	0.06 825	9.88 094	11	29	5 7.5 7.0
32	9.81 284	15	9.93 201	26	0.06 799	9.88 083	II	28	
33	9.81 299	15	9.93 227	25	0.06 773	9.88 072	II	27	7 10.5 9.8 8 12.0 11.2
34	9.81 328	14	9.93 252 9.93 278	26	0.06 722	9.88 051	10	25	9 13.5 12.6
36	9.81 343	15	9.93 303	25	0.06 697	9.88 040	II	24	- //
37	9.81 358	15	9.93 329	26	0.06 671	9.88 029	II	23	
38	9.81 372	14	9.93 354	25 26	0.06 646	9.88 018	II	22 21	
39 40	9.81 387	15	9.93 380	26	0.06 620	9.88 007	II	20	
	9.81 402	15	9.93 406	25	0.06 594	9.87 996	11		
41	9.81 417	14	9.93 43I 9.93 457	26	0.06 569	9.87 985 9.87 975	10	18	
43	9.81 446	15	9.93 482	25	0.06 518	9.87 964	II	17	
44	9.81 461	15	9.93 508	26	0.06 492	9.87 953	II	16	11 10
45	9.81 475	14	9.93 533	25 26	0.06 467	9.87 942	II	15	1 1.1 1.0
46 47	9.81 490	15	9.93 559	25	0.06 441	9.87 931	II	14	2 2.2 2.0
48	9.81 519	14	9.93 584	26	0.00 410	9.87 909	II	13	3 3.3 3.0
49	9.81 534	15	9.93 636	26	0.06 364	9.87 898	II	II	4 4.4 4.0 5 5.5 5.0
50	9.81 549	15	9.93 661	25	0.06 339	9.87 887	II	10	5 5.5 5.0 6 6.6 6.0
51	9.81 563	14	9.93 687	26	0.06 313	9.87 877	10	9	7 7.7 7.0
52	9.81 578	15	9.93 712	25 26	0.06 288	9.87 866	II	8	
53	9.81 592	15	9.93 738	25	0.06 262	9.87 855	II	7	9 9.9 9.0
54 55	9.81 607	15	9.93 763	26	0.06 237	9.87 844 9.87 833	II	5	
56	9.81 636	14	9.93 709	25	0.00 211	9.87 822	II	4	
57 58	9.81651	15	9.93 840	26	0.06 160	9.87 811	II	3	
	9.81 665	14	9.93 865	25 26	0.06 135	9.87 800	II	2	
59	9.81 680	14	9.93 891	25	0.06 109	9.87 789	II	I	
60	9.81 694		9.93 916	_	0.06 084	9.87 778		0	PP
	L Cos	d	L Cot	cd	L Tan	L Sin	d	1.	FF

9,81 694 15 9,93 916 26 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.0	5 084 9.87 778 1 6 058 9.87 767 1 6 058 9.87 767 1 6 058 9.87 756 1 6 050 9.87 745 1 5 982 9.87 734 1 5 985 9.87 734 1 9.87 712 1 5 950 9.87 701 1 5 986 9.87 701 1 5 880 9.87 690 1 5 881 9.87 690 1	d PP
1 9.81 709 1 9.93 942 20 0.00 1 9.81 723 14 9.93 967 25 0.00 1 9.81 738 15 9.93 993 26 0.00 1 9.81 752 14 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.81 781 17 9.94 094 25 0.00 1 9.94 094 25 0.00 1 9.94 094 1	5658 9.87767 I 5633 9.87756 I 5607 9.87745 I 5982 9.87734 I 5985 9.87731 I 5905 9.87701 I 5905 9.87690 I 5854 9.87690 I	11
1 9,81 709 9,93 942 25 0.00 3 9,81 738 14 9,94 069 25 0.00 5 9,81 781 14 9,94 069 25 0.00 6 9	5 6 5 8 9.87 707 1 6 6 033 9.87 756 1 5 6 007 9.87 745 1 5 956 9.87 734 1 5 955 9.87 701 1 5 905 9.87 690 1 5 8 8 4 9.87 670 1	11 59 11 58 11 57 56 11 55 11 55
3 9.81 738 15 9.93 993 26 0.01 4 9.81 752 14 9.94 018 25 0.02 5 9.81 767 15 9.94 044 26 0.02 6 9.81 781 14 9.94 069 25 0.02	5 982 9.87 743 1 5 982 9.87 734 1 5 956 9.87 723 1 5 931 9.87 712 1 5 905 9.87 701 1 5 905 9.87 690 1 5 880 9.87 690 1	11 557 11 56 11 55 11 55
4 9.81 752 14 9.94 018 25 0.0 5 9.81 767 15 9.94 044 26 0.0 6 9.81 781 14 9.94 069 25 0.0	5 982 9.87 734 I 5 956 9.87 723 I 5 931 9.87 712 I 5 905 9.87 701 I 5 880 9.87 690 I 5 884 9.87 670 I	11 56 11 55 11 54
5 9.81 767 15 9.94 044 20 0.00 6 9.81 781 14 9.94 069 25 0.00	5 956 9.87 723 1 5 931 9.87 712 1 5 905 9.87 701 1 5 880 9.87 690 1 5 884 9.87 670 1	11 55 11 54
	5 931 9.87 712 5 905 9.87 701 1 5 880 9.87 690 1 5 854 9.87 679	TT 34
	5 880 9.87 690 I 5 854 9.87 679 I	
8 0 87 870 14 0 04 720 25 0.0	5 8 5 4 9.87 679 1	11 52 25
9 9.81 825 15 9.94 146 20 0.0		11 51
10 9.81 839 14 9.94 171 25 0.0	5 820 L 0.87 668 L	50 2 5.2 5.0
11 9.81 854 9.94 197 0.0	5 803 9.87 057 .	49 3 7.8 7.5
12 9.01 000 74 9.94 222 26 010.		40 4 10.4
13 9.51 502 15 9.94 245 25 0.0	5 727 0.87 624	11 46 6 15.6 15.0
15 9.81 911 14 9.94 299 20 0.0	5 701 9.87 613 1	11 45 7 18.2 17.5
1 74 1 20	5 070 9.07 001	TT 44 0 224 225
17 9.81 940 1 9.94 350 0.0		11 43
19 9.81 969 14 9.94 401 26 0.0	5 500 0.87 568 ¹	11 41
20 9.81 983 14 9.94 426 25 0.0	5 574 0.87 557	11 40
21 9.81 998 9.94 452 0.0	5 548 9.87 546	39
	5 5 2 5 9.0 (5 5 5) _	11 38
23 9.02 020 -+ 9.94 503 25 0.0		11 37 36
25 9.82 055 14 9.94 554 20 0.0	5 446 9.87 501 1	12 25
26 9.82 069 14 9.94 579 25 0.0	5 421 9.87 490 1	11 34 15 14
27 9.82 084 9.94 004 6 0.0	5 390 9.87 479 🦼	33 1 1 1.5 1.4
20 0 82 112 14 0.04 655 25 0.0		11 31 3 4.5 4.2
30 0.82 126 14 0.04 681 20 0.0	5 3 1 0 0 . 8 7 4 4 6	11 30 4 6.0 5.6
31 0.82 141 15 0.94 706 25 0.0	5 204 0.87 434	12 29 5 7.5 7.0 11 29 6 9.0 8.4
32 9.82 155 14 9.94 732 20 0.0	5 268 9.87 423 1	7 10.5 9.8
33 9.02 109 15 9.94 /3/ 26 0.0	5 243 9.07 412 ,	
35 0.82 108 14 0.04 808 25 0.0		11 25
36 9.82 212 14 9.94 834 20 0.0	5 166 9.87 378 1	12 24
37 9.82 226 14 9.94 859 25 0.0	5 141 9.87 307	23
30 9.02 240		11 22 11 21
40 0.82 269 14 9.94 9.35 25 0.0	5 065 0 87 334	11 20
41 9.82 283 14 9.94 961 20 0.0	5 030 0.87 322	12 10
42 9.82 297 14 9.94 986 25 0.0	5 014 9.87 311	11 18
43 9.02 311 - 9.93 012 0.0	4 900 9.07 300	12 76 12 11
45 0.82 340 14 0.05 062 25 0.0		11 15 1 1.2 1.1
46 9.82 354 14 9.95 088 20 0.0	4 912 9.87 266	11 15 2 2.4 2.2 11 3 3.6 3.3
47 9.82 368 14 9.95 113 25 0.0	4 887 9.87 255]	12 13 4 4.8 4.4
40 0 82 206 14 0 05 164 25 0.0	4 836 0.87 232 1	11 12 5 0.0 5.5
50 0.82 410 14 9.93 190 26 0.0	4 810 0.87 221	11 10 6 7.2 6.6 7 8.4 7.7
51 0 82 424 14 0.05 215 25 0.0	4 785 0.87 200	12 9 8 9.6 8.8
52 9.82 439 15 9.95 240 25 0.0	4 760 9.87 198	11 8 9 10.0 9.9
	4 734 9.07 107	12 7 6
54 9.62 407		II 5
56 9.82 495 14 9.95 342 25 0.0	4 658 9.87 153	11 3
57 9.82 509 14 9.95 368 20 0.0	4 632 9.87 141]	3
30 9.02 323 19.93 393 10.0		11 2
39 9.02 337 14 9.93 410 26 0.0	4 556 9.87 107	12 0
		d ' PP

131° (379) **48°**

	42°												
"	L Sin	d	L Tan	c d	L Cot	L Cos	d			PP			
0	9.82 551		9.95 444	25	0.04 556	9.87 107	11	60					
I	9.82 565	14	9.95 469	25 26	0.04 531	9.87 096	II	59					
2	9.82 579	14 14	9.95 495	25	0.04 505	9.87 085	12	58					
3	9.82 593	14	9.95 520	25	0.04 480	9.87 062	11	57 56					
4	9.82 607	14	9.95 545 9.95 571	26	0.04 455	9.87 050	I 2	55					
5 6	9.82 635	14	9.95 596	25	0.04 404	9.87 039	II	54					
7	9.82 649	14	9.95 622	26	0.04 378	9.87 028	11	53					
7 8	9.82 663	14	9.95 647	25 25	0.04 353	9.87 016	II	52		26	25		
9	9.82 677	14	9.95 672	26	0.04 328	9.87 005	12	51 50	11	2.6	2.5		
10	9.82 691	14	9.95 698	25	0.04 302	9.86 993	II		2	5.2	5.0		
II	9.82 705	14	9.95 723	25	0.04 277	9.86 982	12	49 48	3	7.8	7.5		
13	9.82 733	14	9.95 748 9.95 774	26	0.04 232	9.86 959	II	47	4	10.4	10.0 12.5		
14	9.82 747	14	9.95 799	25	0.04 201	9.86 947	12	46	5 6	15.6	15.0		
15	9.82 761	14	9.95 825	26	0.04 175	9.86 936	II I2	45	7 8	18.2	17.5		
16	9.82 775	14	9.95 850	25 25	0.04 150	9.86 924	II	44		20.8	20.0		
17 18	9.82 788	14	9.95 875	26	0.04 125	9.86 913	II	43	9	23.4	22.5		
19	9.82 816	14	9.95 901	25	0.04 099	9.86 890	12	42 4I					
20	9.82 830	14	9.95 952	26	0.04 048	9.86 879	II	40					
21	9.82 844	14	9.95 977	25	0.04 023	9.86 867	12	39					
22	9.82 858	14	9.95 977	25	0.03 998	9.86 855	12	38					
23	9.82872	14	9.96 028	26 25	0.03 972	9.86 844	II I2	37					
24	9.82 885	13	9.96 053	25	0.03 947	9.86 832	11	36					
25 26	9.82 899	14	9.96 078	26	0.03 922 0.03 896	9.86 821	12	35		14	13		
27	9.82 927	14	9.96 104	25	0.03 871	9.86 798	11	33	1	1.4	1.3		
28	9.82 941	14	9.96 155	26	0.03 845	9.86 786	12	32	2	2.8	2.6		
29	9.82 955	14	9.96 180	25	0.03 820	9.86 775	II I2	31	3	4.2	3.9		
30	9.82 968	13	9.96 205	25 26	0.03 795	9.86 763	11	30	4	5.6	5.2 6.5		
31	9.82 982	14	9.96 231		0.03 769	9.86 752	12	29	5 6	7.0 8.4	7.8		
32	9.82 996	14	9.96 256	25 25	0.03 744	9.86 740	12	28	7 8	9.8	9.1		
33	9.83 010	13	9.96 281	26	0.03 719 0.03 693	9.86 728	11	27		11.2	10.4		
34 35	9.83 037	14	9.96 332	25	0.03 668	9.86 705	12	25	91	12.6	11.7		
36	9.83 051	14	9.96 357	25	0.03 643	9.86 694	II	24					
37	9.83 065	14	9.96 383	26	0.03 617	9.86 682	12	23					
38	9.83 078	13	9.96 408	25 25	0.03 592	9.86 670	II	22 2I					
39 40	9.83 092	14	9.96 433	26	0.03 567	9.86 647	12	20					
	9.83 106	14	9.96 459	25	0.03 541	9.86 647	12						
4I 42	9.83 120	13	9.96 484	26	0.03 516	9.86 624	11	19					
43	9.83 147	14	9.96 535	25	0.03 465	9.86 612	12	17		12	11		
44	9.83 161	14	9.96 560	25	0.03 440	9.86 600	12	16	I	1.2	1.1		
45	9.83 174	13	9.96 586	26 25	0.03 414	9.86 589	II I2	15	2	2.4	2.2		
46	9.83 188	14	9.96 611	25	0.03 389	9.86 577	12	14	3	3.6 4.8	3·3 4·4		
47 48	9.83 202	13	9.96 662	26	0.03 364	9.86 554	11	13	4 5	6.0	5.5		
49	9.83 229	14	9.96 687	25	0.03 313	9.86 542	12	II	5 6	7.2	6.6		
50	9.83 242	13	9.96 712	25	0.03 288	9.86 530	12	10	7 8	8.4	7·7 8.8		
51	9.83 256	14	9.96 738	26	0.03 262	9.86 518	12	9	8 9	9.6	9.9		
52	9.83 270	14	9.96 763	25	0.03 237	9.86 507	11	8	91	- 0.0	3.3		
53	9.83 283	14	9.96 788	25 26	0.03 212	9.86 495	12	7					
54 55	9.83 297 9.83 310	13	9.96 814	25	0.03 186	9.86 483 9.86 472	11	6 5					
56	9.83 324	14	9.96 864	25	0.03 101	9.86 460	12	4					
57	9.83 338	14	9.96 890	26	0.03 110	9.86 448	12	3					
58	9.83 351	13	9.96 915	25	0.03 085	9.86 436	I2	2					
59	9.83 365	13	9.96 940	25	0.03 060	9.86 425	112	I					
60	9.83 378	-	9.96 966		0.03 034	9.86 413	-	0					
	L Cos	d	L Cot	c d	L Tan	L Sin	d	/ PP					

_	45												
Г	1	L Sin	d	L Tan	c d	L Cot	L Cos	d			PF		
	0	9.83 378	14	9.96 966	25	0.03 034	9.86 413	12	60				
	1 2	9.83 392	13	9.96 991	25	0.03 009	9.86 401	12	59 58				
	3	9.83 405	14	9.97 016	26	0.02 958	9.86 377	12	57				
	4	9.83 432	13	9.97 067	25	0.02 933	9.86 366	11	56				
ш	5	9.83 446	14	9.97 092 9.97 118	25 26	0.02 908	9.86 354 9.86 342	12	55				
	- 1	9.83 473	14	9.97 143	25	0.02 857	9.86 330	12	53				
	7 8	9.83 486	13	9.97 168	25 25	0.02 832	9.86 318	12	52		26	25	
	9	9.83 500	13	9.97 193	26	0.02 807	9.86 306	11	51 50	I	2.6	2.5	
1	1	9.83 513	14	9.97 219	25	0.02 781	9.86 283	12	49	2	5.2	5.0	
-	2	9.83 527 9.83 540	13	9.97 244	25	0.02 731	9.86 271	12	48	3 4	7.8	7·5 10.0	
1		9.83 554	14	9.97 295	26	0.02 705	9.86 259	12	47	5	13.0	12.5	
I	4 5	9.83 567 9.83 581	14	9.97 320 9.97 345	25	0.02 680	9.86 247 9.86 235	12	46		15.6	15.0 17.5	
I		9.83 594	13	9.97 371	26	0.02 629	9.86 223	12	44	7 8	20.8	20.0	
1		9.83 608	14	9.97 396	25 25	0.02 604	9.86 211	II	43	9	23.4	22.5	
	8 9	9.83 621	13	9.97 421 9.97 447	26	0.02 579 0.02 553	9.86 200	12	42 41				
2		9.83 648	14	9.97 472	25	0.02 528	9.86 176	12	40				
	ī	9.83 661	13	9.97 497	25	0.02 503	9.86 164	12	39				
2	2	9.83 674	13	9.97 523	26 25	0.02 477	9.86 152	12	38				
	3 4	9.83 688	13	9.97 548 9.97 573	25	0.02 452	9.86 140 9.86 128	12	37 36				
	5	9.83 715	14	9.97 598	25	0.02 402	9.86 116	12	35			40	
	6	9.83 728	13	9.97 624	25	0.02 376	9.86 104	12	34		14	13	
	7 8	9.83 741	14	9.97 649	25	0.02 351	9.86 o92 9.86 o8o	12	33	1 2	2.8	1.3 2.6	
	9	9.83 768	13	9.97 700	26	0.02 300	9.86 068	12	31	3	4.2	3.9	
3	0	9.83 781	13	9.97 725	25 25	0.02 275	9.86 056	12	30	4 5	5.6 7.0	5.2 6.5	
3	I	9.83 795	14	9.97 750	26	0.02 250	9.86 044 9.86 032	12	29 28	5 6	8.4	7.8	
	3	9.83 808 9.83 821	13	9.97 776 9.97 801	25	0.02 224	9.86 032	12	27	7 8	9.8	9.1 10.4	
	4	9.83 834	13	9.97 826	25	0.02 174	9.86 008	12	26	9	12.6	11.7	
	5	9.83 848 9.83 861	14	9.97851	25	0.02 149	9.85 996	12	25				
	7	9.83 874	13	9.97 902	25	0.02 098	9.85 972	12	23				
3	8	9.83 887	13	9.97 927	25 26	0.02 073	9.85 960	12	22				
	9	9.83 901	14	9.97 953	25	0.02 047	9.85 948	12	21 20				
	0	9.83 914	13	9.97 978	25	0.02 022	9.85 936	12	19				
	ļI ļ2	9.83 927 9.83 940	13	9.98 003	26	0.01 997	9.85 912	12	18				
4	13	9.83 954	14	9.98 054	25 25	0.01 946	9.85 900	12	17		12	11	
	14 15	9.83 967	13	9.98 079	25	0.01 921	9.85 888	12	16 15	1 2	1.2 2.4	I.I 2.2	
	16	9.83 993	13	9.98 130	26	0.01 870	9.85 864	12	14	3	3.6	3.3	
4	17	9.84 006	13	9.98 155	25	0.01 845	9.85 851	13	13	4	4.8 6.0	4.4	
	18 19	9.84 020	13	9.98 180	26	0.01 820	9.85 839 9.85 827	12	12	5 6	7.2	5·5 6.6	
_	50	9.84 046	13	9.98 231	25	0.01 769	9.85815	12	10	7 8	8.4	7.7 8.8	
	51	9.84 059	13	9.98 256	25	0.01 744	9.85 803	12	9	8	9.6	9.9	
	52	9.84 072	13	9.98 281	25	0.01 719	9.85 791	12	8				
	53 54	9.84 085	13	9.98 307	25	0.01 693	9.85 779 9.85 766	13	7 6				
-	55	9.84 112	14	9.98 357	25	0.01 643	9.85 754	12	5				
1	56	9.84 125	13	9.98 383	26	0.01 617	9.85 742	12	4				
1	57 58	9.84 138	13	9.98 408	25	0.01 592	9.85 730 9.85 718	12	3 2				
ı	59	9.84 164	13	9.98 458	25	0.01 542	9.85 706	12	1				
	60	9.84 177	13	9.98 484	20	0.01 516	9.85 693	13	0				
1		L Cos	d	L Cot	cd	L Tan	L Sin	d	1	}	Р	P	

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	44° 135°								
1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.84 177	13	9.98 484	25	0.01 516	9.85 693	12	60	
Ι	9.84 190	13	9.98 509	25	0.01 491	9.85 681	12	59	
2	9.84 203	13	9.98 534 9.98 560	26	0.01 466	9.85 669 9.85 657	12	58 57	
3 4	9.84 229	13	9.98 585	25	0.01 415	9.85 645	12	56	
5 6	9.84 242	13	9.98 610	25	0.01 390	9.85 632	13	55	
	9.84 255	13	9.98 635	25 26	0.01 365	9.85 620	I 2 I 2	54	
7 8	9.84 269	13	9.98 661 9.98 686	25	0.01 339	9.85 608 9.85 596	12	53 52	
9	9.84 295	13	9.98 711	25	0.01 289	9.85 583	13	51	
10	9.84 308	13	9.98 737	26	0.01 263	9.85 571	12	50	
II	9.84321	13	9.98 762	25	0.01 238	9.85 559	12	49	
12	9.84 334	13	9.98 787	25 25	0.01 213	9.85 547	12	48	
13	9.84 347	13	9.98 812	26	0.01 162	9.85 534	12	47	26 25 14
15	9.84 373	13	9.98 863	25	0.01 137	9.85 510	12	45	1 2.6 2.5 1.4
ıő	9.84 385	12	9.98 888	25 25	0.01 112	9.85 497	13	44	2 5.2 5.0 2.8
17	9.84 398	13	9.98 913	26	0.01 087	9.85 485	12	43	3 7.8 7.5 4.2
18	9.84 411	13	9.98 939 9.98 964	25	0.01 061	9.85 473	13	42 41	4 10.4 10.0 5.6 5 13.0 12.5 7.0
20	9.84 437	13	9.98 989	25	0.01011	9.85 448	12	40	5 13.0 12.5 7.0 6 15.6 15.0 8.4
21	9.84 450	13	9.99 015	26	0.00 985	9.85 436	12	39	7 18.2 17.5 9.8
22	9.84 463	13	9.99 040	25	0.00 960	9.85 423	13	38	
23	9.84 476	13	9.99 065	25 25	0.00 935	9.85 411	12	37	9 23.4 22.5 12.6
24 25	9.84 489 9.84 502	13	9.99 090	26	0.00 910	9.85 386	13	36	
26	9.84 515	13	9.99 141	25	0.00 859	9.85 374	12	34	
27	9.84 528	13	9.99 166	25	0.00 834	9.85 361	13	33	
28	9.84 540	12	9.99 191	25 26	0.00 809	9.85 349	12	32	
29	9.84 553	13	9.99 217	25	0.00 783	9.85 337	13	31 30	
30	9.84 566	13	9.99 242	25	0.00 758	9.85 324	12		
31 32	9.84 579 9.84 592	13	9.99 267	26	0.00 733	9.85 299	13	29 28	
33	9.84 605	13	9.99 318	25	0.00 682	9.85 287	12	27	
34	9.84 618	13	9.99 343	25 25	0.00 657	9.85 274	13	26	
35 36	9.84 630 9.84 643	13	9.99 368 9.99 394	26	0.00 632	9.85 262 9.85 250	12	25 24	
37	9.84 656	13	9.99 394	25	0.00 581	9.85 237	13	23	40 40
38	9.84 669	13	9.99 444	25	0.00 556	9.85 225	12	22	13 12
39	9.84 682	13	9.99 469	25 26	0.00 531	9.85 212	13	21	I I.3 I.2 2 2.6 2.4
40	9.84 694	13	9.99 495	25	0.00 505	9.85 200	13	20	3 3.9 3.6
4I	9.84 707	13	9.99 520	25	0.00 480	9.85 187	12	18	4 5.2 4.8
42 43	9.84 733	13	9.99 545	25	0.00 455	9.85 175 9.85 162	13	17	5 6.5 6.0 6.0 7.8 7.2
44	9.84 745	12	9.99 596	26	0.00 404	9.85 150	12	16	7 9.1 8.4
45	9.84 758	13	9.99 621	25 25	0.00 379	9.85 137	13	15	
46 47	9.84 771	13	9.99 646	26	0.00 354	9.85 125	13	14	9 11.7 10.8
48	9.84 796	12	9.99 697	25	0.00 328	9.85 100	12	12	
49	9.84 809	13	9.99 722	25 25	0.00 278	9.85 087	13	II	
50	9.84 822	13	9.99 747	26	0.00 253	9.85 074	13	10	
51	9.84835	12	9.99 773	25	0.00 227	9.85 062	13	9	
52 53	9.84 847 9.84 860	13	9.99 798	25	0.00 202 0.00 177	9.85 049 9.85 037	12	8 7	
54	9.84 873	13	9.99 848	25	0.00 177	9.85 024	13	6	
55	9.84 885	12	9.99874	26	0.00 126	9.85 012	12	5	
56	9.84 898	13	9.99 899	25 25	0.00 101	9.84 999	13	4	
57 58	9.84 911	12	9.99 924 9.99 949	25	0.00 076	9.84 986	12	3 2	
59	9.84 936	13	9.99 975	26	0.00 025	9.84 961	13	ī	
60	9.84 949	13	0.00 000	25	9.00 000	9.84 949	12	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP

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